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Description and User's Manual of the Inelastic Dynamic Analysis Program. Optimum Seismic Protection for New Building Construction in Eastern Metropolitan Areas

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The end Buschie Inelastic Dynamic Analysis F Manual (Optimum Seismic Prot In Eastern Metropolitan Area Author(s) S. Anagnostopoulos, J. M. Ro Performing Organization Name and Address	Program, Descript tection for New E as, Internal Stud pesset	ion and User's Building Construct Ly Report 16)	S. Report Date Septembe ion 4 8. Parlorming (No. 16	r 1972 Drgenization Rept. No
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Abstract (Limit: 200 words) A computer program, develope in FORTRAN IV and using 3501	ed for the non-li of primary memo	near dynamic anal Pry on an IBM 370/	ysis of buil 165 computer	dings, written , is described.
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DESCRIPTION AND USER'S MANUAL OF THE TINELASTIC DYNAMIC ANALYSIS PROGRAM

1. General Considerations

A computer program has been developed for the non-linear dynamic analysis of buildings, written in FORTRAN IV and using 350k of primary memory on an I.B.M. 370/165 computer. No secondary storage is required. The program is designed for buildings having a maximum of 30 stories, 30 different structural components (in plan) and 3000 points of ground acceleration in each of the two principal directions. Detailed information about the mathematical model and the underlying assumptions can be found in the Sc.D. thesis of S. Anagnostopoulos.

Since it was intended primarily for research, no special effort was put into adding special features, desirable in a program for commercial use (such as free input, problem-oriented language, unit conversion, etc.). The geometry of the building is specified through the number of stories, the heights, the number of structural components, and a plan. The information given for a plan is the coordinates of some point along the centerline of each component and the orientation of this centerline with respect to the x axis. The masses are given for each floor level separately, together with the coordinates of the centroid and the corresponding moments of inertia. For bending springs (shear walls) the required properties are given floor by floor. For shear springs there is the option of either specifying the spring characteristics (and spring type) floor by floor directly or in the case of frames to specify its geometry and the member

properties at each level, and then the program will compute the spring properties by using the approximate formulas presented in the thesis by Anagnostopoulos. Information for identical elements or floors need not be repeated. A single number is required for the viscous damping, the percentage of critical to be used in each mode. The user has the option to specify the number of modes he wants for the elastic part of the analysis, together with the coordinates of a "geometrical center" with respect to which the modal shapes will be computed. The next set of information needed by the program is about the earthquake ground motions. It can read and store two different earthquake records (up to 3000 points each), one for the x and the other for the y direction, and it can combine them with appropriate direction cosines, so that directions of the motion other than x and y can be considered. The user can also specify a number of scales by which the originally read accelerograms will be multiplied and new analyses will be performed. The information given with each earthquake record is a scale factor, a time interval Δt and the values of the acceleration. Finally, the last piece of information required concerns plotting of various timehistories for relative displacements, absolute accelerations, interstory displacements and force versus deformation, at any level and for any direction. If the required number of plots exceeds the capacity of the program, the analysis will automatically be repeated until all the requested plots have been produced. This particular feature was a product of trade-off between increasing core requirements, possibility of using secondary storage and computational costs, arising from the fact that at each step of the numerical analysis previous information is lost, unless stored.

2. Program Description

MAIN

The main program is the spine of the computer module and most of the operations and tasks needed for the analysis are performed in there. It starts with initialization of various variables and arrays and proceeds with the reading of the input. There are only two other routines, SHART and READR that read input information. SMART is called only in the cases of frames to read data for geometry and member properties and then to compute the equivalent springs with the formulas described in Chapter 2 of the earlier mentioned thesis. The user, however, has the option to input directly the properties of the equivalent springs when he chooses not to use the approximate formulas employed in SMART. READR reads the earthquake record from punched cards. The stiffness and mass matrices are assembled in the main program and then subroutine EIGEN determines the natural frequencies and modal shapes. The damping matrix is subsequently formed and READR is called to read the earthquake record. Information about the required plots is then read in the MAIN and the necessary initializations are performed for the numerical analysis. Subroutine RUNGE that uses a 4th order Runge-Kutta numerical procedure is called to perform the first step of the numerical analysis while for all the subsequent steps subroutine BIGGS is used. The forces in the various springs are computed by calling appropriate routines, depending on the type of non-linearities that each spring represents. Maximum, cumulative and root-mean-square effects are calculated in the MAIN, to be printed after the analysis has been completed. After all the output has been printed, the MAIN will set-up the headers to be printed on the plots requested earlier and will call subroutine GRFIVC which will

plot, using the SC4020 plotter, the time histories that were requested by input codes and stored permanently during the analysis. At the end it will check whether the number of scales (which are used to multiply the accelerogram) has been exhausted and if not, it will read the next scale and it will branch to the toint at which it reads the information about the plots and the analysis will be repeated for the new record. The program will stop when all the earthquake scales have been exhausted.

READR (TITLE, SCALE, DT, ACCG, NACCG, VO)

lt reads the digitized record in the following format: lst rard: Title of the record in FORMAT 20A4 2nd card: Scale, Dt in FORMAT 2F10.5 Set of cards: Ground accelerations in FORMAT 8F9.6 Last card: Any real number greater than 900. in F9.6 to indicate the end of the record.

READR will also print the title, the scale by which the values of the ground accelerations are multiplied inside READR, the time step Dt and the number of acceleration values it has read.

Input arguments: none

Recurn arguments:

- TITLE: Array containing the title of the record.
- SCALE: Factor by which all the values of the ground acceleration read have been multiplied
- DT : Time step
- ACCG : Array containing the ground accelerations (multiplied already by SCALE)

NACCG: Number of acceleration points

VO : Is not used here

SMART (I)

It reads the required information and computes the properties of the non-linear springs in the case of unbraced, braced, infilled and partially infilled frames. Depending on the particular type of spring, it will assign values for the initial stiffness and strength as well as values for the degradation factors. Partially infilled frames must be read as type 6 springs and will remain as such in case their shear capacity is inadequate, otherwise SHART will make them of type 2.

Input arguments:

I : Integer identifier of the frame Output arguments: none

The rest of the information is transmitted through the COHMON.

DEFLT (JCOD, DLIM, AA, BB, CC)

It assigns default values to the degrading factors and maximum ductility factors in the case that they are not specified by the user.

Input arguments:

JCOD : Code indicating the spring type

Return arguments:

DLIM : Maximum ductility factor which if exceeded, failure is assumed AA, BB, CC: Degrading factors for the various models

EIGEN (A, R, N, NT, MV)

I.B.M. routine that computes eigenvalues and eigenvectors of a real symmetric matrix

Input arguments:

- A : Original matrix (symmetric) destroyed in computation. Resultant eigenvalues are developed in diagonal of matrix A in descending order.
- N : Order of matrices A and R
- NT : Value of first dimension of R in calling program
- MV : Input code
 - O computes eigenvalues and eigenvectors
 - 1 computes eigenvalues only

Return arguments:

- A : Contains the eigenvalues in its diagonal in descending order
- R : Resultant matrix of eigenvectors (stored column-wise in same sequence as eigenvalues)

<u>RUNGE</u> (STK, AMASS, DAMP, RI, R, F, UI, UP1, U, UP, NDIM, N, DT, A1, A2, A3, A4, B1, B2, B3, B4)

Routine that performs a 4th order Runge-Kutta numerical analysis. In this particular program it is used only once, at the beginning of the numerical integration in order to provide the necessary starting points for the Constant Velocity method.

Input arguments:

STK : Stiffness matrix (dimension NDIM × NDIM, Size N × N) AMASS: Mass vector DAMP : Damping matrix (dimension NDIM × NDIM, Size N × N) Ri : Excitation vector at time step 1 R : Excitation vector at time step 2 F : Force vector at time step 1 U1 : Displacement vector at time step 1 UP1 : Velocity vector at time step 1 NDIM : Dimension of matrices STK and DAMP in MAIN N : Size of matrices STK and DAMP in MAIN N : Size of matrices STK and DAMP in MAIN A1, A2, A3, A4 } Auxiliary vectors for intermediate computations

Return arguments:

- U : Displacement vector at time step 2
- UP : Velocity vector at time step 2

BIGGS (AMASS, STF, DAMP, R, F, A, U1, U2, U, NDIM, N, DT)

Routine that uses the Constant Velocity (or Impulse Acceleration) method for the numerical integration of the equations of motion.

Input arguments:

AMASS: Mass vector
STF : Contains pseudo-inverse of: 1/Dt² M + 1/2Dt C
 (derived from CROUT in MAIN)
DAMP : Contains damping matrix C
R : Excitation vector at time step n
F : Force vector at time step n (= -KU_n)
U1 : Displacement vector at step n (= U_n)
U2 : Displacement vector at step n-1 (= U_{n-1})

NDIM : Dimension of matrices STF, DAMP in MAIN N : Size of matrices STF, DAMP in MAIN DT : Time step of integration

Return arguments:

- A : Acceleration vector at time step n (* U_n)
- U : Displacement vector at time step n+1 (= U_{n+1})

CROUT (A, N, NDIM)

It performs the forward pass of the Gauss elimination procedure on a general matrix A.

Input arguments:

A : Original square matrix

N : Size of matrix A

NDIM : Dimension of A in MAIN

Return arguments:

A : Contains the pseudo-inverse of the original matrix

MATMP (A, N, B, NDIM, M)

Routine that performs the forward pass of the Gauss elimination on the right hand side vectors and the backsweep.

Input arguments:

- A : Pseudo-inverse of a matrix as obtained by CROUT
- N : Size of matrix A
- B : Right hand side vector (or vectors, then B is a matrix with M columns)

NDIM : Dimension of A in MAIN

M : Number of right hand side vectors

Return arguments:

B : Contains for each vector (or column) A⁻¹B if A was the original matrix entering CROUT

MAX (A, NA, ALOW, ATOP, ISK, IAO, DA, IGG)

Routine that determines the maximum and minimum values to be placed on a scale, on which the elements of an array A will be plotted.

Input arguments:

A	:	Vector	whose	elements	are	to	be	plotte	d
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NA : Number of elements in array A

ALOW, ATOP: Minimum and maximum limits in the case that IGG > 0

ISK : Number of elements to be skipped when searching in A

- IAO : Location of starting element in A
- IGG ≤ 0 MAX will search to determine ALOW and ATOP
- IGG > 0 ALOW, ATOP are input arguments

Return arguments:

```
ALOW, ATUP: Minimum and maximum limits of the scale on which A will be
plotted. (It is ALOW \leq A_{ii}: in , ATOP \geq A_{ii} and \geq A_{ii})
```

DA : Step that is used for the grid on the plot

<u>GRFIVC</u> (KO, LT, MRIGHT, MBOT, MTOP, NIVC, MIVC, IIVC, JIVC, NX, NY, NSPEC, NDASH, NPTS, IPOIN, ISXO, ISKX, ISYO, ISKY, LINE, IAVX, IAVY, NT, NTX, NTY, TIT, TITX, TITY, X, Y, SETXL, SETXR, SETYB, SETYT)

Routine that plots a set of values Y versus a set of values X using the SC4020 plotter.

Input arguments:

- KO : Determines the nature of scale
 - = 1 x, y both linear
 - = 2 x linear, y logarithmic
 - = 3 x logerithmic, y linear
 - = 4 x, y both logarithmic

LT, MRIGHT, MBOT, MTOP: Left, right, bottom and top margins in raster units

- NIVC, MIVC: Every nth vertical and every mth horizontal line to be reemphasized. If N₁VC and/or MIVC = 0 no lines are printed.
- IIVC, JIVC: Every ith vertical and every jth horizontal line to be ^aabeled.
 If IIVC and/or JIVC = 0 no lines labeled.
 - NX, NY: Indicate number of characters to be displayed in labels including decimal point and must be $|NX \text{ or } NY| \le 7$ If NX and/or NY are negative, labels are in scientific notation.
 - NSPEC: = 1 Film will not be advanced, for multiple plots
 - ≠ 1 Standard procedure
 - NDASH: = 1 Dashed lines

≠ 1 Solid

NPTS : Number of points to be plotted

- **IPOIN:** = 0 Points will not be plotted
 - ≠ 0 Points will be plotted

The value of IPOIN will be the code of the plotted character

- ISXO : Location of the first element of vector X to be plotted
- ISYO : Location of the first element of vector Y to be plotted
- ISKX : Number of elements to be skipped in vector X
- ISKY : Number of elements to be skipped in vector Y

LINE : = 1 Graph wanted

- = 0 Graph not wanted (only points)
- IAVX : = 0 Subroutine MAX will search for ALOW, ATOP
 - = 1 Subroutine MAX will not search for ALOW, ATOP but it will use earlier values
 - = 2 It will -nput as limits to MAX SETXL, SETXR and MAX will only determine DA.
- IAVY : Same as IAVX but for the Y vector
- NT : Number of header characters
- NTX : Number of characters of the X title
- NTY : Number of characters of the Y title
- TIT : Header
- TITX : X title
- TITY : Y title
- SETXL, SETXR, SETYB, SETYT: arguments to be transmitted to subroutine MAX in the case that IAVX and/or IAVY = 2, to be used as ALOW and ATOP

Return arguments: none

BILIN (FY, RK1, RK2, FO, YO, FN, YN, JFLAG, JNDEX)

Routine that computes forces for a bilinear spring. Input arguments:

- FY : Force at yield
- RK1 : Initial stiffness (slope of the first branch)
- RK2 : Slope of the second branch
- FO : Force at the last step (step n)

YO : Displacement at the last step (step n) YN : New value of the displacement (step n+1) JFLAG: Code to identify load reversal JNDEX: Code to identify the loading or unloading branch <u>Return arguments</u>:

FN : New value of the force (step n)JNDEX: Code to identify the loading or unloading branch

STDG1 (. . . .)

Old version of STDG2. Less accurate and less efficient. It should be eliminated.

STDG2 (FY, RK, FO, YO, FN, YN, IDUM1, IDUM2, DUM1, CYP1, CYP2, DUM3, DUM4)

Routine that computes the force in a stiffness degrading spring, whose unloading is parallel to the initial branch.

Input arguments:

FY	:	Force at yield
RK	:	Initial stiffness
FO	:	Force at the last step (step n)
YO	:	Displacement at the last step (step n)
YN	:	New value of the displacement (step n+1)
IDUMI	,	IDUM2, DUM1, DUM3, DUM4: Dummy arguments
CYPI	:	Maximum positive displacement attained up to step n
CYP2	:	Minimum negative displacement attained up to step n

Return arguments:

FN : New value of the force (step n+1) CYP1, CYP2: as above

STRDGI (FY, RK, FO, YO, FN, YN, JFLAG, JNDEX, A, B, C, DIAX, MCYCL, JPOS, JNEG)

Routine that computes the force in a stiffness and strength degrading spring that corresponds to an infilled concrete frame.

Input arguments:

FY, RK, FO, YO, YN: as in STDG2
JFLAG, JNDEX : as in BILIN
A, B, C : Degrading factors
DMAX : Absolute value of the maximum attained displacement
MCYCL : Number of complete cycles
JPOS : Number of yieldings that occurred on the positive side
JNEG : Number of yieldings that occurred on the negative side
Return arguments:

FN : New value of the force (at step n+1)
JNDEX, DMAX, MCYCL, JPOS, JNEG: as above

STRDG2 (FY, RK, FO, YO, FN, YN, JFLAG, JNDEX, A, B, C, DMAX, MCYCL, JPOS, JNEG, RMI, FMI)

Routine that computes the force in a stiffness and strength degrading spring that corresponds to an infilled concrete frame.

Input arguments:

All but RMI, FMI: as in STRDG1

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- RMI : Minimum value of stiffness corresponding to that of the frame alone
- Fi4I : Minimum value of strength corresponding to that of the frame alone

Return arguments:

Same as in STRDG1

TRILIN (FY1, FY2, R1, R2, F0, Y0, FN, YN, FA1, FA2)

Routine that computes the force in a trilinear spring

Input arguments:

- FY1 : Value of the force at the end of the first branch
- FY2 : Ultimate value of the yield force
- R1 : Initial stiffness (slope of the first branch)
- R2 : Stiffness after formation of plastic hinges (slope of the second branch)
- F0 : Force at the last step (step n)
- YO : Displacement at the last step (step n)
- YN : New value of displacement (step n+1)
- FA1, FA2: Auxiliary variables

Return arguments:

FN : New value of the force (step n+1)

3. Output

The program prints the data about the building, the characteristics of the earthquake motion and the data about the plots requested right after it reads the appropriate information, so that the user can check his input. In the case of shear walls it prints the stiffness coefficients rather than the wall dimensions but it may be desirable to change that part and print the information as it is read.

Results of the analysis will then be printed in the following order:

- 1. Natural periods and modal shapes (two for x and y and one for torsion).
- 2. For each shear spring (frame) and for each floor it will print maximum interstory displacements, maximum ductility factors and permanent sets. In the case of shear walls it will print maximum interstory displacements, maximum ductility factors, maximum shears and maximum over-turning moments.
- 3. For each floor level:
 - a) Maximum floor acceleration, direction and time of occurrence.
 - b) Maximum floor displacement (with respect to the ground) direction and time of occurrence.
 - c) Maximum interstory displacement (of the centroids), direction and time of occurrence.
 - d) Maximum x acceleration, displacement and interstory displacement, corresponding y and rotational values and times of occurrence.
 - e) Maximum y acceleration, displacement and interstory displacement, corresponding x and rotational values and times of occurrence.
 - f) Maximum torsional acceleration, rotation and interstory rotation, corresponding x and y values and times of occurrence.

4. For each floor level:

Root mean square of the maximum accelerations and interstory displacements of all the elements for the x and y directions.

5. For each floor level:

Root mean square of the time histories of the global accelerations and interstory displacements for the x and y directions and for the torsion.

6. For each floor level:

Average root mean square of accelerations and interstory displacements for the x and y directions computed from time histories of each of the elements.

7. Maximum base shears and overturning moments in the x and y directions.

Output 4, 5, 6 is intended for later use of the program to estimate economic damage to the building due to earthquakes of different intensities. The program has also the capability of producing plots on an SC4020 plotter. The user can request and obtain any number of plots for the following:

- 1. For any floor level and for any of the three directions:
 - a) Time histories of absolute accelerations.
 - b) Time histories of displacements (and rotation) relative to ground.
 - c) Time histories of interstory displacements (and rotations).
 - d) Plot of total floor shear (torsional moment) vs. corresponding displacement (rotation) for all the duration of the earthquake.
- 2. For any element and for any floor:
 - a) Time histories of accelerations.
 - b) Time histories of displacements relative to ground.
 - c) Time histories of interstory displacements.

d) Plot of spring force vs. deformation for all the duration of the earthquake.

The user can specify the starting and finishing time for the time history plots.

The maximum number of points that can be plotted in one analysis is 4500. If the user specifies plots that need N points in total where N > 4500, the program will repeat the analysis $(\frac{N}{4500} + 1)$ times until it produces all the requested plots. For each earthquake scale that the user requests, he must specify what plots he wants. These plots can be different from one scale to another.

4. User's Manual

		FORMAT
<u>One Card</u> :	Title	20 A 4
<u>One Card</u> :	NST = Number of stories	110
<u>Set of Cards</u> :	Heights (NST numbers)	8F10.3
<u>Ong Card</u> :	NEL = Number of elements	110
One Card :	ICOD, NSIM	2110
	ICOD = 1 Read springs directly	
	ICOD = 2 Read through SI1ART	
	NSIM = Additional number of elements for which following information applies	
	a) <u>ICOD = 1</u>	

	P	One Card :	N1, N2, JCOD		3110
	Different Flo		N1, N2 = Identifiers of floor numbers with same properties (N2-N1+1 floors); N2 = O if information refers to a single floor.		
	ach		JCOD = 1 ÷ 8 = Spring type		
	or	<u>One Card</u> :	AR1, AR2, AF1, AF2, AA, BB, CC, DLIM		8F10.3
	۴L		If JCOD = 4 read a card in 2F10.3 with RKMIN, FYMIN		
			AR1 = Initial stiffness, AR2 = second stiffn	ess	
			AF1 = Force at 1 St yield, AF2 = Ultimate forc	e	
Ę			AA, BB, CC = Degradation factors		
EME			DLIM = Maximum ductility factor		
E F			For Shear Walls: (JCOD = 7)		
CTUR			ARl = Modulus of elasticity		
STRU			AR2 = Moment of inertia		
ACH			AF1 = Shear area		
OR E			AF2 = Plastic moment capacity		
Ē			AA = Ultimate shear capacity		
			BB = Torsional rigidity		
			b) $1000 = 2$		
		<u>One Card</u> :	NSP, E, G y	110,	2F10.3
			NSP ≖ Number of spans		
			E = Modulus of elasticity		
			бу = Yield stress for bracing		
		Set of Cards:	Spans (NSP numbers)		8F10.3
	Г	<u>One Card</u> :	N1, N2, JCOD, SCOL, UL, A, B, C (3	110,	5F10.3)
l	1		N1, N2, JCOD as before		

/1

			SCOL = Maximum shear capacity
			UL = Maximum ductility factor
			A, B, C = Degradation factors
			If JCOD = 6 read a card with average clear height in Fl0.3
		Set of Cards:	IC_1 , MPC_1 , IC_2 , MPC_2 , 8F10.3
			IC = Column moment of inertia
			MPC = Plastic moment of a column
1		Set of Cards:	IG ₁ , MPG ₁ , IG ₂ , MPG ₂ , 8F10.3
EMEN	oor		IG = Girder moment of inertia
	nt F		MPG = Plastic moment of a girder
NCTURA	i ffere		<u>Columns and girders are numbered</u> sequentially from left to right
I STR	ц С		If <u>JCOD = 3</u> : <u>One Card</u> : Number of struts I10
EACH	r Ea		Set of Cards: IDSPAN, ABR (I10, F10.3)
FOR	Ĕ		ABR = Area of bracing
			If <u>JCOD = 4,5</u> : <u>One Card</u> : Number of infilled spans IlO
			<u>Set of Cards</u> : E,G,h,t,ℓ,τ (6F10.3, 1)
			E = Modulus of elasticity
			G = Shear modulus
			$h,t,\ell = Infill dimensions$
			τ = Shear strength of infill
		Set of Cards:	N1, x, y, ALF (one card per element) (I10, 3F10.3
			N1 = Element ID
			x,y = Coordinates of a point on the element
			ALF = Angle (in degrees) of the element's centerline with the x axis

	Set of Cards:	AMX, AMY, AIN, XCM, YCM (one card per floor)	5F10.3
		AMX,AMY = Masses x, y	
		AIN = Slab moment of inertia about centroid	
		XCM,YCM = Coordinates of centroid	
	<u>One Card</u> :	Damping ratio β	F10.3
	One Card :	NMOD, XCR, YCR (110,	2F10.3)
		NMOD = Number of modes to be printed	
		XCR,YCR = Coordinates of geometrical center (modal shapes are computed with respect to that point)	
	<u>One Card</u> :	NSCAL	I 10
		NSCAL = Total number of motions for which the analysis will be performed	
	<u>One Card</u> :	NEAR	110
		NEAR = Number of earthquake records to be read	
	<u>One Card</u> :	Direction cosines for the motions	2F10.3
ßſ	<u>One Card</u> :	Earthquake title	20 A4
REC	One Card :	SCALE, DT	2F10.5
DARD	Set of Cards:	Ground accelerations	8 F9 .6
STAND	<u>One Card</u> :	999.	F9.6
	One Card :	NPLOT, NPTSM	2110
		NFLOT = Number of plots	
		NPTSM = Average number of points per plot	
	Set of Cards:	IPFL, IPCOD, IPDIR, NPL1, NPTS, IPEL (NPLOT # of cards)	6110
		IPFL = Floor ID	
		IPCOD = Plotting code	



CODES

ICOD = 1 + Read spring properties directly
2 + Read properties of frames through SMART
JCOD = 1 + Bilinear spring
2 + Stiffness degradation (Concrete frame)
3 + Stiffness degradation (Braced frame)
4 + Stiffness and strength degradation (Infilled steel frame)
5 + Stiffness and strength degradation (Infilled concrete frame)
6 + Limited shear capacity
7 + Shear wall
8 + Trilinear spring
24

IPCOD = 1 + Absolute accelerations vs. time

- 2 + Displacements relative to ground vs. time
- 3 + Interstory displacement vs. time
- 4 + Force vs. distortion
- IPDIR = 1 + x direction
 - 2 + y direction
 - $3 \rightarrow Rotation$