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EARTHQUAKE RESPONSE OF SEA-BASED  
STORAGE TANKS BY A  
HYBRID ELEMENT METHOD-  
THEORY AND COMPUTER ANALYSIS

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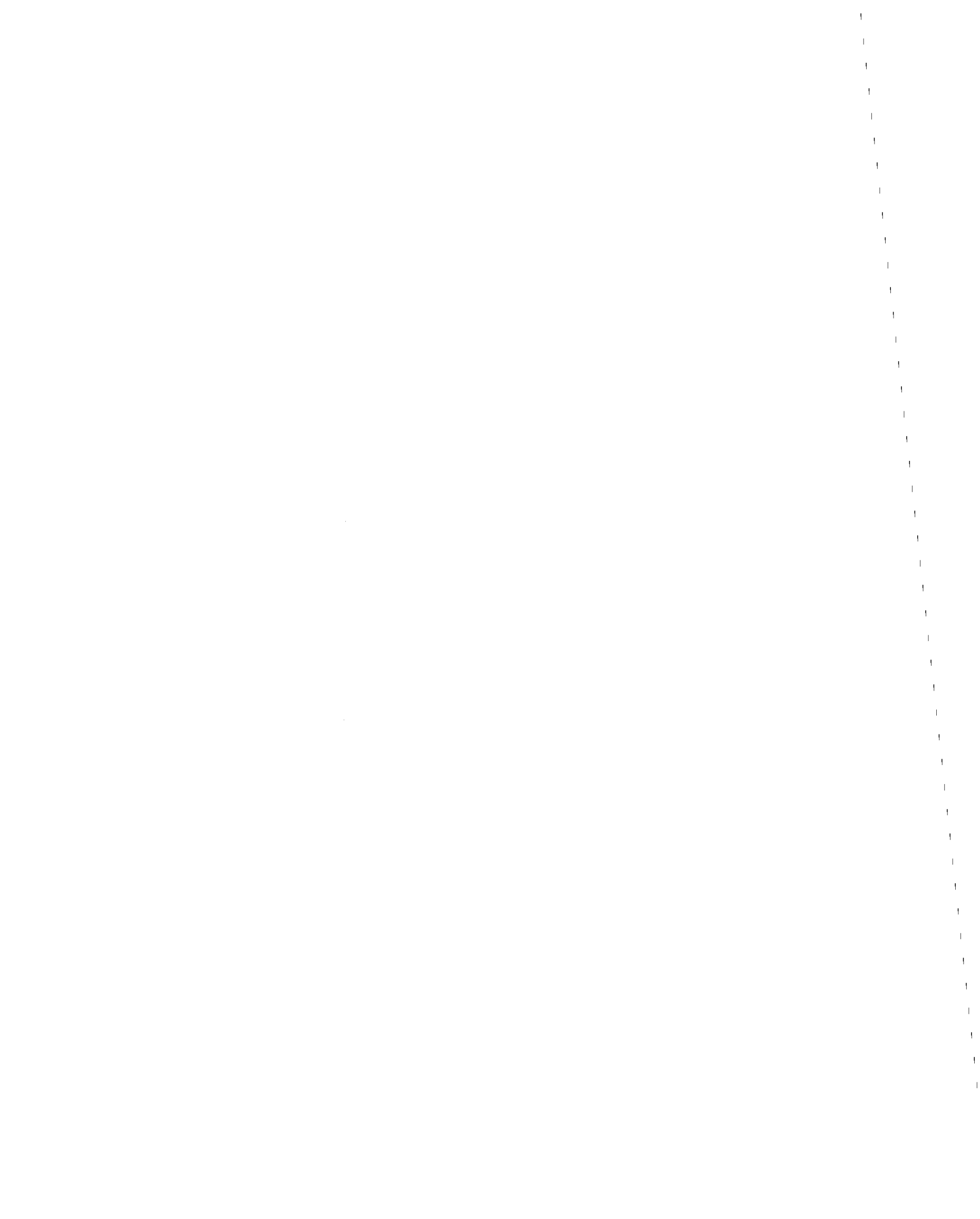
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## FOREWORD

This work was supported by the Earthquake Hazard Mitigation Program of the National Science Foundation, Washington, D.C. under grant PFR 79-19949, which is a continuation of PFR 78-09866.

This study addresses the problem of dynamic response of submerged storage tanks subject to earthquake excitations, in an attempt to formulate a general evaluation procedure using the hybrid-finite element method and to synthesize a comprehensive and predictive computer code for engineering applications. This technical report presents the formulation and encoding of the research findings.

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## ABSTRACT

An effective method for the linear analysis of dynamic response of submerged underwater oil storage tanks to loadings of earthquake excitations is presented. The tank is axisymmetric in shape, has a flexible wall/roof. A general hybrid-finite element solution procedure has been formulated, wherein the tank structure, the interior fluids, as well as the near field of the exterior water region are discretized into a toroidal mesh network. The tank displacement is expressed as a superposition of the first few modes of the structure's free vibration. Contribution from the hydrodynamic interaction to the coupled motion is obtained by solving the Laplace equation with the appropriate boundary conditions, which includes a matching to the exterior far-field pressure (analytic) representation to simplify the computational process. The effects of fluids surrounding and inside the tank are studied. It is demonstrated that these effects are, in general, significant on the tank earthquake response analysis.

A comprehensive and predictive computer program for use in such tank response analysis is developed for design engineering applications.

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## INTRODUCTION

In recent years, exploration and production of oil offshore have increased tremendously. Many of the new fields are far into the ocean and the adjacent land area is often desolate and uninhabited, rendering the conventional method of using pipelines and onshore terminals more and more costly. For countries in scarcity of land space (such as Japan), utilization of the sea may become necessary for the purpose of long-term petroleum storage. The alternative of storing crude at the producing sites to be shipped via tankers to harbors is thus becoming more and more economical, both in terms of capital investment and in operating cost.

The first submerged underwater oil storage tank was placed in service in December of 1969. Referred to as the Khazzan Dubai #1, the tank is located in 150 feet of water, 60 miles off the shore of the Trucial Coast in the Arabian Gulf (Chamberin, 1970). It weighs 15,000 ton and holds 500,000 barrels of oil. It has the appearance (Figures 1 and 2) of an inverted funnel with a 270-foot-diameter base and a roof which is a portion of a 180-foot-radius hemisphere. A conical transition connects the roof to a 30-foot-diameter shaft that extends above the ocean surface. The "bottomless" tank rests on the ocean floor and operates on the water displacement principle; it is always filled with either water or oil or a combination of the two. Filling is accomplished by placing oil through the shaft, the additional weight of the oil on the water creates a pressure imbalance which forces the water out of the tank through openings in the wall. Deep-well pumps are used for discharging oil. As oil is withdrawn, inflow of water takes place, replacing the removed oil.

New concepts and designs of oil storage tanks have since been developed for all areas of the world. Some of the tanks rest on ocean floors and are either completely submerged or partially submerged with part of the tank protruding above water; other designs take the form of floating, bottomless tanks, moored to the ocean floors.

The primary forcing function these storage tanks must be designed to resist is that due to waves in the heaviest storm; and for bottom-supported tanks located in earthquake-prone areas, seismic-induced hydrodynamic forces must, of course, also be considered. Because of the exorbitant cost incurred in the construction of these huge structures, and the environmental hazards associated with the failure of such structures, an accurate evaluation of the hydrodynamic forces is vital. In order to predict the response of an underwater tank to waves and earthquakes, the development of a reliable computation method is a pressing need for the construction of storage tanks in seismic areas. This present study is specifically aimed at the earthquake-induced response for a completely submerged tank filled with oil and water.

Earthquake analysis of such cantilever structures requires special considerations which do not arise in land-based structures; any procedure for analysis must recognize the additional dynamic forces and modifications in the dynamic properties caused by the surrounding water and the fluids inside. If the tank is perfectly rigid, the motions of the fluids inside and outside the structure may be treated independently. However, to accommodate for the more stable structures made of flexible resilient materials, extra care needs to be exercised in studying their dynamic behavior, by virtue of the fact that the structure and fluid motions are coupled. The effect of the tank structural deformation on the dynamic response is the emphasis of this investigation.

## 2. RELATED PAST WORK

There have been few works that directly address the problem intended in the present study. The ones bearing the closest relationship appear to be that of Takayama (1976) and Helou (1981). Takayama treated transient waves inside a vibrated oil storage; the tank is a rigid rectangular or cylindrical structure, submerged undersea. However, no attention was given to the effect of surrounding water, and no numerical results are furnished. Helou extended the problem wherein the tank wall is flexible. However, he was only concerned with cylindrical tanks where analytic solution can be found; no numerical scheme was developed for general applications.

A wealth of research papers do exist which provide valuable sources of pertinent information, most having to do with the hydrodynamic pressure distribution of structures under earthquake excitations. For land-based tanks of simple geometries under the assumption of inviscid, compressible or incompressible fluid, and irrotational motion of small amplitudes, many solution procedures have been formulated. First, Jacobsen (1949) evaluated the dynamic mass effect of fluid inside a cylindrical tank and outside a cylindrical pier, when the base experiences an impulsive seismic load. Then, Housner (1956) set the foundation of general earthquake-proof design analysis by introducing a simple approximation method which avoids partial differential equations and infinite series. Thereafter, many works appear which deal with the deformation of tank structure. Notable among them are Baron and Skalak (1962), Arya, Thakkar and Goyal (1972), and Yang (1976), who use the Rayleigh-Ritz method; and Edwards (1969) and Shaaban and Nash (1975), who employ the finite-element method. In all cases, fluid is treated as a continuum and appropriate shell theories are selected for the development (Sanders, 1959; Flugge, 1960; Basu and Gould, 1975; Ghosh and Wilson, 1975). In Yang's work, the nature of the impulsive and convective effects is carefully identified, and he based his dynamic analysis on

assumed mode shapes of the tanks free vibration. Wu *et al.* (1975) developed a computer program to calculate the natural frequencies of the fluid-tank system. Earthquake analysis of the resonant oscillation (sloshing) phenomena in elastic shells can be found in Chester (1968), Faltinsen (1974), Aslam, Godden and Scalise (1979) and Mei, Foda and Tong (1979).

So far we have been quoting only works concerning ground tanks. The problem associated with motion of water surrounding submerged tanks is more difficult to solve. For objects of simple geometries, attempts were made using the Schwinger variational technique (Black and Mei, 1970), the Galerkin method (Garrett, 1971), and the integral equation method (Garrison and Seetharama Rao, 1971). Tung (1979) also pursued the problem of submerged bodies subject to harmonic ground excitation, using a semi-analytical method to obtain the hydrodynamic forces and confirmed the insignificance of the gravity effect, as long as the excitation frequencies are moderately high. For objects of more complicated shapes, numerical methods must be employed. The finite-element method, known for its versatility, was used by Chakrabarti and Chopra (1972) and Liaw and Chopra (1973) in studies of seismic response of gravity dams and intake towers. This approach is further enhanced by the adoption of an analytic super-element, thereby reducing the mesh requirement in the far field (ordinarily it is required that the outer truncation boundary must be far enough away from the longest waves). The so-called "hybrid" finite-element method, which combines judiciously finite-element solution for fluid motion near the object and an analytic representation for the far field, has been proven to be highly efficient. Among the pioneers are Berkhoff (1972), Bai and Yeung (1974), Chen and Mei (1974) and Yue, Chen and Mei (1976).

### 3. FORMULATION

Although the subject of seismic response of submerged storage tanks is relatively new and unexplored, as we have pointed out in the previous chapter, much of the pertinent analysis tools have been developed. It is the purpose of this research to utilize these tools in formulating a general hybrid-finite element solution procedure, for the hydrodynamic response of flexible underwater storage tanks subject to earthquake motions; and to synthesize this procedure into a comprehensive predictive computer code which can be used for engineering applications.

The tank structure in question is of general axisymmetric shape, has a flexible wall and/or roof, and is rigidly attached to the ocean floor. This assumption that the support foundation does not move relative to the ground reduces the scope somewhat, since the effect of marine soil-structure interaction can have significant consequence on the hydrodynamic analysis. However, it is expected that this variation can be accommodated by our hybrid-finite element procedure, and will be dealt with in a future study. The tank will be completely filled with oil and/or water and sealed (this last restriction can be lifted by simply changing the input format). Finally, in the following presentation, we simplify matters by ignoring irregular bottom topography and depletion of interior compartments. Their presence can be handled straightforwardly by carefully discretizing these components into finite elements.

The equation of motion of the tank structure can be written in terms of the structure discretization as

$$[M]\{\ddot{x}\} + [C]\{\dot{x}\} + [K]\{x\} = -\{F\} \quad , \quad (3.0)$$

where  $[M]$ ,  $[C]$  and  $[K]$  are the mass, damping and stiffness matrices of the system, respectively.  $\{\ddot{x}\}$ ,  $\{\dot{x}\}$  and  $\{x\}$  are the acceleration, velocity and displacement vector of the structure relative to its base,

$\{F\}^*$  is the load vector of the external forces, which includes the hydrodynamic pressure  $\{P_S\}$  due to the presence of fluids inside and outside of the system. For nodal circles on the inner shell interfacing with the interior oil and water,  $\{P_S\}$  is sought from the equation of motion governing the dynamic interaction between the shell and the interior fluids; the same goes for  $\{P_S\}$  at nodal circles on the outer tank surface. Thus, before attacking (3.0), we need to solve two boundary value problem suitably formulated based on the two appropriate Laplace equations. The flexibility of the tank shell is entered into both radial boundary conditions influenced by the ground acceleration, consequently  $\{P_S\}$  intertwines with  $\{\ddot{x}\}$ .

Both boundary value problem are solved using the variational principle of finite element theory. In the "far away" exterior region, a matching of analytic representation of  $\{P_S\}$  is invoked (this region is to have been rid of all geometrical irregularities). Once  $\{P_S\}$  is obtained (in terms of  $\{\ddot{x}\}$  and the earthquake ground acceleration  $\{\ddot{f}_h\}$ ), (3.0) can be solved by transformation into modal coordinates wherein the displacement is expressed in terms of the first few modes of the tank force vibration. The resultant linear second-order differential equation in the generalized displacement amplitude can be solved by the ordinary step-by-step integration schemes.

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\* Vectors enclosed in braces { } are associated with the appropriate (interior fluids domain, structure, or exterior water region discretizations) nodal coordinates. Thus, if  $N_0$  is the number of nodal-circles in the oil domain,  $\{P_0\}$  is the column vector of nodal pressure distribution of dimension  $N_0$ , ordered in the global nodal number sequence. However, in the case of structure discretization, the vector is represented by the  $(r, z, \theta)$  coordinates at each nodal-circle, making  $\{P\}$  a vector of dimension  $3N$ , if  $N$  is the number of nodal-circles in the structure assemblage. The symbol " $\rightarrow$ " will be reserved for the ordinary three-dimensional continuum vectors.

### 3.1 Dynamic Behavior of Fluids

#### 3.1.1 Interior Fluids

##### A. Problem Formulation

Consider a axisymmetric tank submerged underwater which is filled with oil on top of water (more generally, two fluids of densities  $\rho_0$  and  $\rho_w$ , where  $\rho_w > \rho_0$ ) with respective heights of  $h_0$  and  $h_w$  as shown in Figure 3 ( $h_0$  depends on the radial distance from the axis). Choose the coordinate system as depicted in Figure 3 with the axis of tank symmetry being the z-axis and the direction of earthquake ground motion being the (positive) x-axis, and the origin at the center of oil-water interface. We will also need the usual  $(r, z, \theta)$  cylindrical coordinate system.

Let  $\vec{v}(x, y, z; t)$  denote the velocity vector of the fluid particle at  $(x, y, z; t)$ . Then, based on the usual assumptions of inviscid and incompressible fluids, irrotational motion and small amplitude waves, the linearized momentum equations of fluid motion read

$$\begin{aligned} \frac{\partial \vec{v}_0}{\partial t} &= -\frac{1}{\rho_0} \nabla p_0, \\ \frac{\partial \vec{v}_w}{\partial t} &= -\frac{1}{\rho_w} \nabla p_w. \end{aligned} \tag{3.1}$$

We use the suffixes o and w to represent quantities pertaining to oil and water, respectively.

Take the curl of (3.1) and apply the continuity equations

$$\begin{aligned}\nabla \cdot \vec{v}_0 &= 0, \\ \nabla \cdot \vec{v}_w &= 0,\end{aligned}\tag{3.2}$$

we obtain

$$\begin{aligned}\nabla^2 p_0 &= 0 && \text{in } V_0, \\ \nabla^2 p_w &= 0 && \text{in } V_w.\end{aligned}\tag{3.3}$$

Let  $\vec{f}_h(t)$  denote the horizontal ground acceleration induced by an earthquake, then since the translatory velocity in the x-direction should be equal to  $\dot{\vec{f}}_h$ , we have

$$\begin{aligned}\frac{\partial p_0}{\partial n} &= -\rho_0 [(\vec{f}_h + \ddot{x}) \cdot \vec{n}] && \text{across } \partial V_{0w}, \\ \frac{\partial p_w}{\partial n} &= -\rho_w [(\vec{f}_h + \ddot{x}) \cdot \vec{n}] && \text{across } \partial V_{ww}.\end{aligned}\tag{3.4}$$

In (3.4),  $\frac{\partial}{\partial n} = \vec{n} \cdot \nabla$ , and  $\vec{n}$  is the unit outward normal to the tank boundary.  $\ddot{x}$  is the acceleration of the tank structure relative to the ground. The presence of the  $\ddot{x}$  term is dictated by the flexibility of the tank shell. Now if the tank had a roof which is rigid, we would have

$$\frac{\partial p_0}{\partial z} = 0 \quad \text{along } \partial V_{ot}.$$

However, to allow for the general case where the "roof" is also flexible (and more likely, inseparable from the wall as in the case of a half-dome tank), we will use the same boundary condition as in (3.4). Consequently, we include  $\partial V_{ot}$  as part of  $\partial V_{0w}$ . The assumption of a rigid floor support implies that



$$\frac{\partial P_w}{\partial z} = 0 \quad (3.5)$$

along  $\partial V_{wb}$  ( $z = -h_w$ ).

Now, if we let  $\zeta(x,y,z;t)$  stand for the displacement of the oil-water interface from its equilibrium position, the (linearized) dynamic interfacial condition affirms the continuity of the total pressure such that

$$P_{T0} - P_{Tw} = (\rho_0 - \rho_w) g \zeta \quad \text{along } z = 0. \quad (3.6)$$

And the (linearized) kinematic condition maintains fluid particles on interface to stay on the interface (continuity of vertical velocity) so that

$$\frac{\partial^2 \zeta}{\partial t^2} = - \frac{1}{\rho_0} \frac{\partial P_0}{\partial z} = - \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} \quad \text{along } z = \zeta. \quad (3.7)$$

Under the small amplitude assumption, only minor error is incurred by evaluating equation (3.7) along  $z = 0$ . If we assume that the gravitational effects are small compared to the forced oscillation so that

$$g \frac{(\rho_w - \rho_0)}{\rho_0} \frac{T^2}{L} \ll 1, \quad (3.8)$$

Equation (3.6) is then reduced to

$$P_0 = P_w \quad \text{along } z = 0, \quad (3.9)$$

so that sloshing waves at the oil and water interface are ignored. Here,  $L$  and  $T$  are the characteristic scales of length and time, respectively. This assumption can be justified because earthquake excitations are generally of high frequencies. In our validation of the computer results (§ 4), we included such surface wave effects and found that the calculated response was practically frequency independent for moderately high frequency values.

B. Solution via Variational Principle

Since the tanks under consideration are of general shape except for axisymmetry, no closed form analytic solution is readily available. We now present as a prelude to the finite element solution scheme, a variational functional in  $P_o$  and  $P_w$  whose stationarity is equivalent to the system of equations of SA being satisfied. It is well-known that in general, the less restrictive Galerkin method produces results identical to those one would obtain from any variational principle. We choose to use the variational method to illuminate the process, demonstrating the matrix assembly along the way. The Galerkin method will be employed in the exterior problem to simplify our presentation.

Consider the functional

$$\begin{aligned}
 F(P_o, P_w) = & \int_{V_o} \frac{1}{2\rho_o} (\nabla P_o)^2 dV_o + \int_{\partial V_{ow}} P_o [(\vec{f}_n + \vec{x}) \cdot \vec{n}] dA_{ow} \\
 & - \int_{\partial V_i} \frac{1}{2\rho_w} (P_w - P_o) \frac{\partial P_w}{\partial z} dA_i \\
 & + \int_{V_w} \frac{1}{2\rho_w} (\nabla P_w)^2 dV_w + \int_{\partial V_{ww}} P_w [(\vec{f}_n + \vec{x}) \cdot \vec{n}] dA_{ww} \\
 & - \int_{\partial V_i} \frac{1}{2\rho_o} (P_w - P_o) \frac{\partial P_o}{\partial z} dA_i
 \end{aligned} \tag{3.10}$$

where we have used  $(\nabla P)^2$  to denote  $\nabla P \cdot \nabla P$ . Clearly if  $P_0$  and  $P_w$  satisfy the system of equations of §A, then  $\delta F(P_0, P_w) = 0$ . We now show that, conversely, if  $\delta F(P_0, P_w) = 0$  then the system of §A is solved. For simplicity, we will drop all the differential symbol in the integrals provided that there is no chance of confusion.

Now,

$$\begin{aligned}
 \delta F(P_0, P_w) = & \int_{V_0} \frac{1}{\rho_0} \nabla P_0 \cdot \nabla \delta P_0 + \int_{\partial V_{0w}} [(\vec{f}_n + \vec{x}) \cdot \vec{n}] \delta P_0 \\
 & - \frac{1}{2\rho_w} \int_{\partial V_i} (P_w - P_0) \frac{\partial \delta P_w}{\partial z} - \frac{1}{2\rho_w} \int_{\partial V_i} \frac{\partial P_w}{\partial z} \delta P_w \\
 & + \frac{1}{2\rho_w} \int_{\partial V_i} \frac{\partial P_w}{\partial z} \delta P_0 \\
 & + \int_{V_w} \frac{1}{\rho_w} \nabla P_w \cdot \nabla \delta P_w + \int_{\partial V_{ww}} [(\vec{f}_n + \vec{x}) \cdot \vec{n}] \delta P_w \\
 & - \frac{1}{2\rho_0} \int_{\partial V_i} (P_w - P_0) \frac{\partial \delta P_0}{\partial z} - \frac{1}{2\rho_0} \int_{\partial V_i} \frac{\partial P_0}{\partial z} \delta P_w \\
 & + \frac{1}{2\rho_0} \int_{\partial V_i} \frac{\partial P_0}{\partial z} \delta P_0 \quad . \tag{3.11}
 \end{aligned}$$

From Green's identity, we have

$$\int_{V_0} \frac{1}{\rho_0} \nabla P_0 \cdot \nabla \delta P_0 = - \int_{V_0} \frac{1}{\rho_0} \nabla^2 P_0 \delta P_0 - \int_{\partial V_i} \frac{1}{\rho_0} \frac{\partial P_0}{\partial z} \delta P_0 + \int_{\partial V_{ow}} \frac{1}{\rho_0} \frac{\partial P_0}{\partial n} \delta P_0 \quad (3.12)$$

Note that along  $\partial V_i$  we have  $\frac{\partial P_0}{\partial n} = - \frac{\partial P_0}{\partial z}$  since  $\vec{n}$  is pointing downward. And from  $\frac{\partial P_w}{\partial n} = \frac{\partial P_w}{\partial z}$  we deduce

$$\int_{V_w} \frac{1}{\rho_w} \nabla P_w \cdot \nabla \delta P_w = - \int_{V_w} \frac{1}{\rho_w} \nabla^2 P_w \delta P_w - \int_{\partial V_{wb}} \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} \delta P_w + \int_{\partial V_i} \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} \delta P_w + \int_{\partial V_{ww}} \frac{1}{\rho_w} \frac{\partial P_w}{\partial n} \delta P_w \quad (3.13)$$

Substituting (3.12) and (3.13) into (3.14) we obtain

$$\begin{aligned}
\delta F(P_o, P_w) = & - \int_{V_o} \frac{1}{\rho_o} \nabla^2 P_o \delta P_o \\
& + \int_{\partial V_{ow}} \frac{1}{\rho_o} \left( \frac{\partial P_o}{\partial n} + \rho_o [(\vec{f}_n + \vec{x}) \cdot \vec{n}] \right) \delta P_o \\
& + \int_{\partial V_i} \frac{1}{2} \left( \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} - \frac{1}{\rho_o} \frac{\partial P_o}{\partial z} \right) \delta P_o \\
& + \int_{\partial V_i} \frac{1}{2} \left( \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} - \frac{1}{\rho_o} \frac{\partial P_o}{\partial z} \right) \delta P_w \\
& - \int_{\partial V_i} \frac{1}{2\rho_w} (P_w - P_o) \frac{\partial \delta P_w}{\partial z} - \int_{\partial V_i} \frac{1}{2\rho_o} (P_w - P_o) \frac{\partial \delta P_o}{\partial z} \\
& - \int_{V_w} \frac{1}{\rho_w} \nabla^2 P_w \delta P_w + \int_{\partial V_{wb}} \frac{1}{\rho_w} \frac{\partial P_w}{\partial z} \delta P_w \\
& + \int_{\partial V_{ww}} \frac{1}{\rho_w} \left( \frac{\partial P_w}{\partial n} + \rho_w [(\vec{f}_n + \vec{x}) \cdot \vec{n}] \right) \delta P_w . \quad (3.14)
\end{aligned}$$

If we observe now that each  $\delta$ -differential quantity can be varied independently, for  $\delta F(P_o, P_w)$  to be zero, each of the integrals in (3.14) must be identically zero. We thus have the system of equations of §A, and our statement is verified.

C. Finite-Element Approximation

By utilizing the axisymmetry of the tank, the interior fluid domain composed of  $V_0$  and  $V_w$  may be discretized into a finite-element system comprising of toroidal elements with quadrilateral (vertical) cross-section (cylindrical elements at the axis of symmetry). If we use the cylindrical coordinates  $(r, z, \theta)$  to define the global coordinate system, and the natural coordinates  $(s, t, \theta)$  within each element as the local coordinate system (see Figure 4,  $-1 \leq s \leq 1$ ,  $-1 \leq t \leq 1$ ) we can write the coordinate transformation on element  $e$  as

$$r = \sum_{k=1}^4 N_k^e(s, t) r_k^e = \{N^e\}^T \{r^e\},$$

$$z = \sum_{k=1}^4 N_k^e(s, t) z_k^e = \{N^e\}^T \{z^e\},$$
(3.15)

where

$$N_1^e = (1-s)(1-t)/4, \quad N_2^e = (1+s)(1-t)/4,$$

$$N_3^e = (1+s)(1+t)/4, \quad N_4^e = (1-s)(1+t)/4.$$
(3.16)

are the bilinear interpolation functions, and  $(r_k^e, z_k^e, \theta)$ ,  $k = 1, \dots, 4$  are the global coordinates for the four nodes of the quadrilateral cross-section. Within each element  $e$ , the hydrodynamic pressure is then expressed as

$$p^e = \sum_{k=1}^4 N_k^e \cos \theta \cdot p_k^e = \{N^e\}^T \{p^e\} \cos \theta.$$
(3.17)

From §B, the system of equations of §A can be solved by imposing  $\delta F(P_o, P_w) = 0$ . We now do this at the element level, assembling the element stiffness matrices and solve the unknowns  $\{p^e\}$ .

We first rewrite (3.10) as

$$F(P_o, P_w) = \int_{V_o} \frac{1}{2\rho_o} (\nabla P_o)^2 dV_o \quad I_1$$

$$+ \int_{V_w} \frac{1}{2\rho_w} (\nabla P_w)^2 dV_w \quad I'_1$$

$$+ \int_{\partial V_{ow}} P_o [(\vec{f}_n + \vec{x}) \cdot \vec{n}] dA_{ow} \quad I_2$$

$$+ \int_{\partial V_{ww}} P_w [(\vec{f}_n + \vec{x}) \cdot \vec{n}] dA_{ww} \quad I'_2$$

$$+ \int_{\partial V_i} \frac{1}{2\rho_o} P_o \frac{\partial P_o}{\partial z} dA_i \quad I_3$$

$$- \int_{\partial V_i} \frac{1}{2\rho_w} P_w \frac{\partial P_w}{\partial z} dA_i \quad I'_3$$

$$+ \int_{\partial V_i} \frac{1}{2\rho_w} P_o \frac{\partial P_w}{\partial z} dA_i \quad I_4$$

$$- \int_{\partial V_i} \frac{1}{2\rho_o} P_w \frac{\partial P_o}{\partial z} dA_i \quad I'_4$$

and then evaluate each of these integrals numerically based on the finite-element scheme in the following sections. Due to the similarity between each  $I_k$  and  $I'_k$ , only the details of  $I_k$  will be presented.

### C1. Integral $I_1$

If we assume that the domain  $V_0$  is divided into  $E_0$  number of elements, we can approximate  $I_1$  by

$$\begin{aligned} I_1 &= \sum_{e=1}^{E_0} \int_{V_0^e} \frac{1}{2\rho_0} (\nabla p_0^e)^2 dV_0^e \\ &= \sum_{e=1}^{E_0} \int_{V_0^e} \frac{1}{2\rho_0} \left[ \nabla \left( \{N^e\}^T \{p_0^e\} \cos\theta \right) \right]^2 dV_0^e \\ &= \sum_{e=1}^{E_0} \{p_0^e\}^T \int_{V_0^e} \frac{1}{2\rho_0} \left( \nabla \{N^e\} \cos\theta \right) \left( \nabla \{N^e\}^T \cos\theta \right) dV_0^e \{p_0^e\} . \end{aligned}$$

Denote the integral in the above formula by  $[K_{V_0^e}]$ , then since

$$\int_{V_0^e} dV_0^e = \int_0^{2\pi} \int_{A_0^e} r dr dz d\theta ,$$

$A_0^e$  being the area of the finite-element (vertical) cross-section, and since



$$\frac{\partial}{\partial x} = -\cos\theta \frac{\partial}{\partial r} - \frac{\sin\theta}{r} \frac{\partial}{\partial \theta}, \quad (3.18)$$

$$\frac{\partial}{\partial y} = -\sin\theta \frac{\partial}{\partial r} + \frac{\cos\theta}{r} \frac{\partial}{\partial \theta},$$

We can rewrite  $[K_{V_0}^e]$  as

$$\int_0^{2\pi} \int_{A_0^e} \frac{1}{2\rho_0} \left( \left\{ \frac{\partial N^e}{\partial r} \right\}^T \left\{ \frac{\partial N^e}{\partial r} \right\} \cos^2\theta + \left\{ \frac{\partial N^e}{\partial z} \right\}^T \left\{ \frac{\partial N^e}{\partial z} \right\} \cos^2\theta + \left\{ N^e \right\}^T \left\{ N^e \right\} \frac{\sin^2\theta}{r^2} \right) r dr dz d\theta.$$

Thus the  $(i,j)$ -th entry of  $[K_{V_0}^e]$  is

$$[K_{V_0}^e]_{ij} = \frac{\pi}{2\rho_0} \int_{A_0^e} \left( \frac{\partial N_i^e}{\partial r} \frac{\partial N_j^e}{\partial r} + \frac{\partial N_i^e}{\partial z} \frac{\partial N_j^e}{\partial z} + \frac{N_i^e N_j^e}{r^2} \right) r dr dz, \quad i,j=1,2,3,4.$$

To facilitate the evaluation of  $[K_{V_0}^e]_{ij}$ , it is convenient to transform the integral into the local coordinates of  $e$ . Thus,

$$\int_{A_0^e} dr dz = \int_{-1}^1 \int_{-1}^1 |J| ds dt,$$

where  $|J|$  is the determinant of the Jacobian

$$[J] = \begin{pmatrix} \frac{\partial r}{\partial s} & \frac{\partial z}{\partial s} \\ \frac{\partial r}{\partial t} & \frac{\partial z}{\partial t} \end{pmatrix} = \begin{pmatrix} \frac{\partial}{\partial s} \\ \frac{\partial}{\partial t} \end{pmatrix} \{N^e\}^T \begin{pmatrix} r_1^e & z_1^e \\ r_2^e & z_2^e \\ r_3^e & z_3^e \\ r_4^e & z_4^e \end{pmatrix}$$

The last relation is obtained from (3.16). Now  $[K_{V_0}^e]_{ij}$  can be evaluated over element  $e$  using the natural coordinates.

We can write  $I_1$  in terms of matrices and vectors relating to all nodes if we extend the  $\{P_0^e\}$ 's to  $\{P_0\}$  by placing zeros at the appropriate components. Recall that the components of  $\{P_0\}$  is ordered according to the global nodal-circle number sequencing. Then

$$I_1 = \{P_0\}^T [K_{V_0}] \{P_0\}, \quad (3.19)$$

where  $[K_{V_0}]$  is the global matrix whose  $(i,j)$ -th entry is

$$\sum [K_{V_0}^e]_{e(i)e(j)}$$

The sum is taken over all elements  $e$  where nodes  $i$  and  $j$  belong to simultaneously ( $e(i)$  denotes the local node number of  $i$ ). Since each  $[K_{V_0}^e]$  is symmetric, so is  $[K_{V_0}]$ .

## C2. Integral $I_2$

Assuming that  $V_0$  has  $E_{ow}$  elements in contact with  $\partial V_{ow}$ , we can approximate  $I_2$  by

$$I_2 = \sum_{e=1}^{E_{ow}} \int_{\partial V_{ow}} P_0^e [(\vec{f}_n + \vec{x}) \cdot \vec{n}] dA_{ow}^e \quad (3.20)$$

Under the structural finite-element discretization, we introduce the nodal acceleration vector  $\{\ddot{\Delta}\}$  (cf. Figure 5):

$$\{\ddot{\Delta}\}^T = (\ddot{\Delta}_{1r}, \ddot{\Delta}_{1z}, \ddot{\Delta}_{1\theta}, \ddot{\Delta}_{2r}, \ddot{\Delta}_{2z}, \ddot{\Delta}_{2\theta}, \dots, \ddot{\Delta}_{Nr}, \ddot{\Delta}_{Nz}, \ddot{\Delta}_{N\theta}). \quad (3.21)$$

And if for each  $\beta$ , the local angle between the normal  $\vec{n}$  and the XY-plane, we define the Nx3N transformation matrix [G] by

$$[G](\beta) = \begin{bmatrix} \cos\beta, & \sin\beta, & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & \cos\beta, & \sin\beta, & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \cos\beta, & \sin\beta, & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & \cos\beta, & \sin\beta, & 0 \end{bmatrix} \quad (3.22)$$

We can then write

$$(\vec{f}_h + \vec{x}) \cdot \vec{n} = \{N^e\}^T [G] (\{\ddot{f}_h^e\} + \{\ddot{x}^e\}) \cos\theta. \quad (3.23)$$

along the  $A_{ow}^e$  surface. Where we have used the same bilinear interpolation functions of (3.16), now acting on the inner fluid-structure interfacial nodes.

Now we can write

$$I_2 = \sum_{e=1}^{E_{ow}} \int_{z_\lambda^e}^{z_u^e} \int_0^{2\pi} \{P_o^e\}^T \{N^e\} \{N^e\}^T [G] (\{\ddot{f}_h^e\} + \{\ddot{x}^e\}) \cos^2\theta \, r d\theta dz$$

$$= \{P_o\}^T [O] (\{\ddot{f}_h\} + \{\ddot{x}\}), \quad (3.24)$$

where  $z_\lambda^e$  and  $z_u^e$  delimit the vertical extent of element e on  $V_{ow}$ , and the global matrix [O] is assembled from the element matrices

$$\int_{z_\lambda^e}^{z_u^e} \pi r \{N^e\} \{N^e\}^T [G] \, dz, \quad e=1, \dots, E_{ow} \quad (3.25)$$

and

$$\{\ddot{f}_h\}^T = \{L\} \ddot{f}_h = (1, 0, -1, 1, 0, -1, \dots, 1, 0, -1) \ddot{f}_h, \quad (3.26)$$

$\{L\}$  is the vector which translates ground motion to loads on the nodal-circles.

C3. Integral  $I_3$

$$I_3 = \sum_{e=1}^{E_i} \int_{\partial V_i^e} \frac{1}{2\rho_0} (\{N^e\}^T \{P_0^e\} \left\{ \frac{\partial N^e}{\partial z} \right\}^T \{P_0^e\}) \cos^2 \theta \, dA_i^e$$

$$= \sum_{e=1}^{E_i} \{P_0^e\}^T \int_{r_\lambda^e}^{r_u^e} \frac{\pi}{2\rho_0} \{N^e\} \left\{ \frac{\partial N^e}{\partial z} \right\}^T r \, dr \{P_0^e\},$$

where  $r_\lambda^e$  and  $r_u^e$  delimit the radial extent of element  $e$ . Also note that  $N^e$  and its derivatives are to be evaluated at  $z = 0$ .

Again, we can write  $I_3$  in global form as

$$I_3 = \{P_0\}^T [K_{i0}] \{P_0\}. \quad (3.27)$$

C4. Integral  $I_4$

$$I_4 = \sum_{e=1}^{E_j} \int_{\partial V_i^e} \frac{1}{2\rho_w} (\{N_o^e\}^T \{P_o^e\} \left\{ \frac{\partial N_w^e}{\partial z} \right\}^T \{P_w^e\}) \cos^2 \theta \, dA_i^e$$

$$= \sum_{e=1}^{E_j} \{P_o^e\}^T \int_{r_l^e}^{r_u^e} \frac{\pi}{2\rho_w} \{N_o^e\} \left\{ \frac{\partial N_w^e}{\partial z} \right\}^T r \, dr \{P_w^e\}$$

Note that we have added subscripts o and w to  $N^e$  here because this integral involves both the upper and the lower layers. In terms of the local coordinates, it is remarked that for  $\{N_o^e\}$ , we have  $t = -1$  and for  $\left\{ \frac{\partial N_w^e}{\partial z} \right\}^T$  we have  $t = 1$ .

In the global form we have

$$I_4 = \{P_o\}^T [K_{ow}] \{P_w\}. \quad (3.28)$$

D. Total Global Matrix

Summarizing and treating  $\{P_o\}$  and  $\{P_w\}$  as unknowns, the functional (3.10) becomes

$$F(\{P_o\}, \{P_w\}) = \{P_o\}^T [K_{V_o}] \{P_o\} + \{P_w\}^T [K_{V_w}] \{P_w\}$$

$$+ \{P_o\}^T [O] (\{\ddot{f}_h\} + \{\ddot{x}\}) + \{P_w\}^T [W] (\{\ddot{f}_h\} + \{\ddot{x}\})$$

$$+ \{P_o\}^T [K_{i_o}] \{P_o\} + \{P_w\}^T [K_{i_w}] \{P_w\}$$

$$+ \{P_o\}^T [K_{ow}] \{P_w\} + \{P_w\}^T [K_{wo}] \{P_o\}. \quad (3.29)$$

For F to be stationary, we require

$$\begin{aligned} \frac{\partial F}{\partial P_{ok}} &= 0, & k &= 1, \dots, NO \\ \frac{\partial F}{\partial P_{wk}} &= 0, & k &= 1, \dots, NW. \end{aligned} \quad (3.30)$$

Since  $P_o = P_w$  at the interface, we have a set of  $NO + NW -$  (number of interfacial nodes) equations, which gives

$$\begin{aligned} 2[K_{V_o}] \{P_o\} + 2[K_{i_o}] \{P_o\} + [K_{ow}] \{P_w\} + [K_{wo}]^T \{P_w\} \\ = - [O] (\{\ddot{f}_h\} + \{\ddot{x}\}), \end{aligned}$$

and

$$\begin{aligned} 2[K_{V_w}] \{P_w\} + 2[K_{i_w}] \{P_w\} + [K_{ow}]^T \{P_o\} + [K_{wo}] \{P_o\} \\ = - [W] (\{\ddot{f}_h\} + \{\ddot{x}\}). \end{aligned} \quad (3.31)$$

If we define  $\{P_{ow}\}$  to be the vector of interior nodal pressure distributions, ordered according to the global nodal number sequence (thus no repetition on interface), we can combine the matrix equations of (3.31) to assemble

$$[K_{INT}] \{P_{ow}\} = - [OW] (\{\ddot{f}_h\} + \{\ddot{x}\}). \quad (3.32)$$

To solve for the inner pressure distribution (at least in the case of a rigid tank, when  $\{\ddot{x}\} = 0$ ), we can solve (3.32) by Gaussian elimination routines serving this purpose are readily available. However, as  $\{\ddot{x}\}$  is still unknown in the general flexible case, (3.32) will be used as input to the general structural equation of motion to solve for the earthquake response later.

### 3.1.2 Exterior Water Region

#### A. Problem Formulation

Consider the same axisymmetric tank of §3.1.1 now submerged in water of depth H as depicted in Figure 3. We use the same coordinate system as before, extended to the exterior water region, introducing only the additional boundary surfaces.

Again, under the assumptions of water being inviscid and incompressible, undergoing motion which is irrotational, and that wave amplitudes are small, the governing field equation is

$$\nabla^2 p_w = 0 \quad \text{in } V \quad (3.33)$$

where  $P_w$  is the water hydrodynamic pressure. Since water is the only fluid of concern here, we will henceforth omit the subscript w.

The rigid floor support implies the homogeneous boundary condition at the sea bottom since we only consider horizontal ground motion:

$$\frac{\partial P}{\partial z} = 0 \quad z = -h_w \quad (3.34)$$

Along the lateral surface of the tank, we have as before

$$\frac{\partial P}{\partial n} = -\rho_w [(f_h + x) \cdot \vec{n}] \quad \text{across } S_1, \quad (3.35)$$

$x$  enters because of the flexibility of the tank shell.

For the free surface boundary condition, generally one combines the dynamic condition  $P = \rho_w g(\eta - z)$  with the kinematic condition

$$\frac{\partial^2 \eta}{\partial t^2} = -\frac{1}{\rho_w} \frac{\partial P}{\partial z} \quad \text{to obtain} \quad \frac{\partial^2 P}{\partial t^2} = -g \frac{\partial P}{\partial z} \quad \text{at } z = 0.$$

However, as demonstrated by Liaw and Chopra (1973), the surface waves have negligible effects on the hydrodynamic response of the fluid-tank system except at very low frequencies. Since most of the earthquake excitation energy is contained in higher frequency components, we can safely assume that the gravity effects are of little consequence. Consequently, we use

$$P = 0 \quad \text{at } z = H - h_w, \quad (3.36)$$

as the free surface boundary condition.

Finally, since we are dealing with an infinite domain, in order to have a bounded solution, we further require that

$$P \rightarrow 0 \quad \text{as } r \rightarrow \infty. \quad (3.37)$$

These conditions are duly adjusted, if necessary, to account for any bottom irregularities.

#### B. Solution via Galerkin's Method/Hybrid Element Approximation

Since the exterior water region is an infinite domain, the size of the finite-element discretization is an important issue. A straightforward application of the finite-element method, even with a domain truncation adjusted to the convergence rate, may be potentially cumbersome and costly, due to the conflicting requirements that the size of the elements be a fraction of the shortest wavelength, and that the outer truncation boundary be far enough away from the longest waves. Instead, we adopt the hybrid approach of using the available analytic solution for  $P$  at a few wavelengths away from the tank, as soon as most of the



significant geometrical irregularities are passed. We introduce a fictitious (cylindrical) surface  $S_f$  here and use the analytic  $P$  to go backward to match the finite-element solution.

Again using a finite-element discretization of the exterior region between  $S_i$  and  $S_f$  composing of ring-shaped elements having quadrilateral (vertical) cross-sections, we have, as in (3.17) of §3.1.1

$$p^e = \sum_{k=1}^4 N_k^e \cos\theta \cdot p_k^e ,$$

$\{N_e\}$  is as defined in (3.16), but note that it now acts on the exterior nodal-circles. Let us denote  $N_k^e \cos\theta$ , the finite-element interpolation functions, by  $T_k^e$ . The Galerkin criterion requires that

$$\int_V T_k (\nabla^2 p) dV = 0 \quad k = 1, 2, 3, 4. \quad (3.38)$$

From Green's theorem we have

$$-\int_V (\nabla T_k \cdot \nabla p) dV + \int_S T_k \frac{\partial p}{\partial n} dS = 0 \quad k = 1, 2, 3, 4, \quad (3.39)$$

where  $S$  is the union of all the surface of the discretized domain.

Now

$$\begin{aligned} & \int_V (\nabla T_k \cdot \nabla p) dV \\ &= \sum_{V^e} \sum_{\ell=1}^4 \int_{V_e} \left( \frac{\partial T_k^e}{\partial r} \frac{\partial T_\ell^e}{\partial r} + \frac{\partial T_k^e}{\partial z} \frac{\partial T_\ell^e}{\partial z} + \frac{1}{r^2} \frac{\partial T_k^e}{\partial \theta} \frac{\partial T_\ell^e}{\partial \theta} \right) p_\ell^e dV^e \\ &= \sum_{V^e} \sum_{\ell=1}^4 \int_0^{2\pi} \int_{A^e} \left( \frac{\partial N_k^e}{\partial r} \frac{\partial N_\ell^e}{\partial r} \cos^2\theta + \frac{\partial N_k^e}{\partial z} \frac{\partial N_\ell^e}{\partial z} \cos^2\theta + \frac{N_k^e N_\ell^e}{r^2} \sin^2\theta \right) r dr dz d\theta p_\ell^e \end{aligned} \quad (3.40)$$

The similarity between the last expression under the intergral signs and that of  $[K_{V_0}^e]$  in Section C1 of §3.1.1 is quite apparent. By letting  $k$  run from 1 through 4, we can assemble the element matrix  $[H_V]$ , and it is then a trivial matter to assemble this into the global form of

$$[H_V]\{P\}. \quad (3.41)$$

Recall that  $\{P\}$  is a vector of dimension NE, NE being the number of exterior water nodal-circles.

The second term of (3.39) can be expressed as

$$\int_S T_k \frac{\partial P}{\partial n} dS = \int_{S_s} T_k \frac{\partial P}{\partial z} dS_s + \int_{S_i} T_k \frac{\partial P}{\partial n} dS_i - \int_{S_b} T_k \frac{\partial P}{\partial z} dS_b + \int_{S_f} T_k \frac{\partial P}{\partial r} dS_f. \quad (3.42)$$

By (3.34) and (3.36), the first and third terms on the right-hand-side of (3.42) vanish. Since  $P = 0$  on  $S_s$ , the corresponding rows and columns in the matrix  $[H_V]$  also vanish. The solution procedure is therefore simplified by removing all equations associated with nodes at the surface. From (3.35) we have

$$\int_{S_i} T_k \frac{\partial P}{\partial n} dS_i = \int_{S_i} -\rho_w T_k [(\ddot{f}_h + \ddot{x}) \cdot \vec{n}] dS_i.$$

If we use the same  $\{N_S^e\}$  as defined in (3.16) of §3.1.1 C, acting now on the exterior water-tank interfacial nodes, based on (3.23), we can rewrite

$$\begin{aligned} \int_{S_i} T_k \frac{\partial P}{\partial n} dS_i &= \sum_{S^e} \int_0^{2\pi} \int_{z_\ell^e}^{z_u^e} -\rho_w T_k^e \{N_S^e\}^T [G] (\{\ddot{f}_h\} + \{\ddot{x}\}) \cos\theta r dz d\theta \\ &= \int_{S^e} \int_{z_\ell^e}^{z_u^e} -\rho_w \pi r N_k^e \{N_S^e\}^T [G] (\{\ddot{f}_h\} + \{\ddot{x}\}) dz \end{aligned} \quad (3.43)$$

If we let  $k$  run from 1 through 4, we can then assemble the following global form

$$- [B] (\{\ddot{f}_h\} + \{\ddot{x}\}). \quad (3.44)$$

To evaluate the last term of (3.42) we need to know the pressure distribution on  $S_f$ , which is obtained from the analytic representation for  $P$  outside of  $S_f$ ,

$$P_E = \sum_{m=1}^{\infty} \alpha_m K_{\lambda}(k_m r) \cos k_m(z+h_w) \cos \theta. \quad (3.45)$$

where  $k_m = \frac{(2m-1)\pi}{2H}$ , and  $K_{\lambda}$  is the modified Bessel function of the second kind of order  $\lambda$ .  $\alpha_m$  is to be determined. Consequently, along  $S_f$  we have

$$\frac{\partial P}{\partial n} = \frac{\partial P_E}{\partial r} = - \sum_{m=1}^{\infty} \frac{\alpha_m k_m}{2} [K_0(k_m r_f) + K_2(k_m r_f)] \cos k_m(z+h_w) \cos \theta \quad (3.46)$$

where  $r_f$  is the radial coordinate of  $S_f$ . If we truncate the series to leave with  $M$  terms, we can write (3.45) as

$$\frac{\partial P}{\partial n} = - \sum_{m=1}^M d_m \alpha_m, \quad (3.47)$$

with

$$d_m = \frac{k_m}{2} [K_0(k_m r_f) + K_2(k_m r_f)] \cos k_m(z+h_w) \cos \theta.$$

Therefore,

$$\begin{aligned}
 \int_{S_f} T_k \frac{\partial P}{\partial n} dS_f &= - \int_0^{2\pi} \int_{-h_w}^{H-h_w} T_k \sum_{m=1}^M d_m \alpha_m r_f dz d\theta \\
 &= - \sum_{m=1}^M \sum_{S_f^e} \int_0^{2\pi} \int_{z_l^e}^{z_u^e} T_k^e d_m^e r_f dz d\theta \alpha_m \\
 &= - \sum_{m=1}^M \sum_{S_f^e} q_{mk}^e \alpha_m .
 \end{aligned} \tag{3.48}$$

Now the  $\alpha_m$ 's are determined (in terms of P) from the continuity requirement of pressure across the fictitious surface  $S_f$ :

$$P = P_E \quad \text{at } S_f . \tag{3.49}$$

Using  $d_m$  as the weighting function, we get

$$\int_{S_f} d_m P dS_f = \int_{S_f} d_m P_E dS_f \tag{3.50}$$

Substituting the expression  $P^e = \sum_{k=1}^4 T_k^e P_k^e$  and the expression (3.45) for  $P_E$  at  $S_f$  (truncated to M terms) into (3.50), we have

$$\sum_{k=1}^4 \sum_{S_f^e} q_{mk}^e P_k^e = \sum_{j=1}^M \alpha_j a_{mj} . \tag{3.51}$$

where

$$\begin{aligned}
 a_{mj} &= \int_0^{2\pi} \int_{-h_w}^{H-h_w} d_m K_1(k_j r_f) \cos k_j(z+h_w) \cos \theta r_f dz d\theta \\
 &= \int_0^{2\pi} \int_{-h_w}^{H-h_w} \frac{r_f k_m}{2} K_1(k_j r_f) [K_0(k_m r_f) + K_2(k_m r_f)] \cos k_m(z+h_w) \cos k_j(z+h_w) \cos^2 \theta dz d\theta \\
 &= \begin{cases} 0 & \text{if } m \neq j \\ \frac{\pi}{4} k_m r_f^H K_1(k_m r_f) [K_0(k_m r_f) + K_2(k_m r_f)] & \text{if } m = j. \end{cases} \quad (3.52)
 \end{aligned}$$

Substituting (3.51) into (3.48) we get

$$\int_{S_f} T_k \frac{\partial p}{\partial n} dS_f = \sum_{m=1}^M \frac{1}{a_{mm}} \left( \sum_{S_f^e} q_{mk}^e \right) \sum_{\ell=1}^4 \left( \sum_{S_f^e} q_{m\ell}^e p_{\ell}^e \right). \quad (3.53)$$

Define the  $M \times 4$  element matrix  $[Q^e]$  as having  $q_{mk}^e$  as the  $(m,k)$ -th entry, and the  $M \times M$  diagonal matrix  $[A]^{-1}$  of entries  $1/a_{mm}$ , we can form the global equivalent

$$[Q]^T [A]^{-1} [Q] \{P\}. \quad (3.54)$$

Consequently, we can write (3.39) in the equivalent global form

$$- [H_V] \{P\} - [Q]^T [A]^{-1} [Q] \{P\} = [B] (\{\ddot{f}_h\} + \{\ddot{x}\}). \quad (3.55)$$

As in §3.1.1 D, (3.55) will be input to the equation of motion to solve for the earth quake response in the following section.

### 3.2 Dynamic Behavior of Fluid-Structure System

The equation of motion of the tank structure under consideration can be written in terms of our finite-element discretization as

$$[M]\{\ddot{x}\} + [C]\{\dot{x}\} + [K]\{x\} = -\{E\} - \{P_S\}, \quad (3.56)$$

with  $\{x\}$  the vector of nodal displacements relative to the tank support, expressed in the nodal  $r$ ,  $z$  and  $\theta$  components.  $[M]$  is the mass matrix

$$[M] = \text{diag } \frac{1}{2} \{M_1, M_1, M_1, M_2, M_2, M_2, \dots, M_N, M_N, M_N\}, \quad (3.57)$$

with  $M_k$  the mass of the tank material between neighboring nodal-circles, which is lumped at the  $k$ -th node.  $[C]$  and  $[K]$  are the damping and stiffness matrices.

$$\{E\} = [M]\{\ddot{f}_h\}. \quad (3.58)$$

Finally,  $\{P_S\}$  is the vector of nodal loads associated with the hydrodynamic pressures. As these pressures act only on the inner and outer surfaces of the tank, the elements in  $\{P_S\}$  corresponding to non-interfacial nodes are zero. Indeed,  $\{P_S\}$  has many zero entries, since the pressures act in the direction of the surface normal, thus all  $\theta$ -components (circumferential) vanish, and if a section of the interface (inner or outer) is cylindrical, the corresponding  $z$ -components also vanish.

Since the materials used in the construction of the tank is assumed to be flexible, the structural deformation entails the coupling of the free vibration with the hydrodynamic interaction. Generally based on the algorithm selected, the coupling of this sort can be categorized into a weak and a strong one. In weak coupling, the fluid pressure is first used to "drive" the structure into a new shape, and a new pressure field

in turn is evaluated using this new configuration. Strong coupling avoids these cycles, forces acting on the structural nodes and on the fluids are determined simultaneously. We use the latter.

If we now strip off all non-interfacial nodal components from  $\{P_{ow}\}$  ((3.32) of §3.1.1) and  $\{P\}$  ((3.55) of §3.1.2), rewrite them in terms of the  $r, z, \theta$  components, and extend them to  $\{P_S\}$ ; at the same time picking out the accompanying terms from  $[K_{INT}]$  and  $[H_V] + [Q]^T[Q]$  to reassemble the coefficient matrix for  $\{P_S\}$ , we can combine (3.32) and (3.55) into

$$[H]\{P_S\} = - [F] (\{\ddot{f}_h\} + \{\ddot{x}\}) \quad (3.59)$$

Here  $[F]$  also incorporates the contributions from  $[OW]$  and  $[B]$ .

Assuming that inversion of  $[H]$  can be done efficiently, we can then substitute (3.59) into (3.56) to get

$$([M] - [H]^{-1}[F])\{\ddot{x}\} + [c]\{\dot{x}\} + [K]\{x\} = - ([M] - [H]^{-1}[F])\{\ddot{f}_h\} \quad (3.60)$$

This equation has the standard form of a second-order linear ordinary differential equation, which can be solved straightforwardly by a number of conventional time-integration schemes. However, it is quite obvious that inverting  $[H]$  should not be recommended. The alternative is to utilize the nodal superposition method commonly used in structural analysis. Therein the structural response  $\ddot{x}, \dot{x}$  and  $x$  are expressed by the eigenvectors (mode shapes  $\{\phi\}$ ) of the undamped structural vibrations (without fluids). The  $\{\phi\}$ 's are obtained from the following eigenvalue problem

$$[K]\{\phi_j\} = \omega_j^2 [M]\{\phi_j\}, \quad (3.61)$$

where  $\omega_j$  denotes the  $j$ -th eigenvalue (natural vibration frequency) of the structure. It should be pointed out here that, in general, the mode shapes and natural frequencies of our entire coupled fluid-tank system are different from the  $\{\phi_j\}$  and  $\omega_j$  here. For the entire system, no precise physical meanings can be imparted to  $\{\phi_j\}$  and  $\omega_j$ , except that  $\{\phi_j\}$  is a set of linearly independent vectors out of which structural response can be composed of. For that matter, just about any set of linear independent vectors can be used in this approach, were it not for the advantage of our particular set  $\{\phi\}$  that it diagonalizes the matrices  $[M]$ ,  $[C]$  and  $[K]$ :

$$\begin{aligned} \{\phi_j\}^T [M] \{\phi_j\} &= [M_j^*] \\ \{\phi_j\}^T [C] \{\phi_j\} &= [C_j^*] = 2\zeta_j \omega_j [M_j^*] \\ \{\phi_j\}^T [K] \{\phi_j\} &= [K_j^*] = \omega_j^2 [M_j^*] \end{aligned} \quad (3.62)$$

$[M_j^*]$ ,  $[C_j^*]$  and  $[K_j^*]$  are diagonal matrices referred to as the generalized mass, generalized damping and generalized stiffness matrices.  $\zeta_j$  is the  $j$ -th mode damping ratio (assumed to be small).

Using  $\{\phi_j\}$ , any arbitrary displacement  $\{x\}$  can be expressed as a linear combination of them:

$$\{x\} = \sum_{j=1}^J \{\phi_j\} Y_j. \quad (3.63)$$

The above expansion is exact if  $J$  is equal to the total number of degrees of freedom,  $3N$ , of the structure finite-element system because the  $\{\phi_j\}$ 's form a basis of a space of dimension  $3N$ . Usually, for earthquake type of excitations, the responses can be approximated by the first few modes fairly well.



Now (3.59) can be written as

$$[H]\{P_S\} = - [F]\{\ddot{f}_h\} - \sum_{j=1}^J [F]\{\phi_j\} \ddot{Y}_j . \quad (3.64)$$

If we rewrite  $\{P_S\}$  as

$$\{P_S\} = \sum_{j=1}^J \{P_{Sj}\} \ddot{Y}_j + \{P_{S0}\} \ddot{f}_h , \quad (3.65)$$

where  $\{P_{Sj}\}$  is the solution of

$$[H]\{P_{Sj}\} = - [F]\{\phi_j\} , \quad (3.66)$$

and  $\{P_{S0}\}$  the solution of

$$[H]\{P_{S0}\} = - [F]\{L\} . \quad (3.67)$$

Note that (3.66) and (3.67) can be solved without inverting  $[H]$ . And since in the numerical process, the solution is gotten in a piecemeal fashion, one need not worry about the possible singular behavior of  $[H]$  during its construction.

$\{P_{S0}\}$  can be viewed as the pressure response due to the rigid body motion of the tank, and  $\{P_{Sj}\}$  is the pressure response due to the  $j$ -th mode of tank free vibration. Substituting the expressions for  $\{x\}$  and  $\{P_S\}$  into (3.56), multiplying on the left by  $\{\phi_j\}^T$  and using the orthogonality property of the mode shapes, we obtain

$$\begin{aligned} & ([M_j^*] + \{\phi_j\}^T \{P_{Sj}\}) \ddot{Y}_j + [C_j^*] \dot{Y}_j + [K_j^*] Y_j \\ & = - (\{\phi_j\}^T [M] \{L\} + \{\phi_j\}^T \{P_{S0}\}) \ddot{f}_h . \quad j = 1, \dots, J \end{aligned} \quad (3.68)$$

The term  $\{\phi_j\}^T \{P_{Sj}\}$  can be interpreted as the modal added mass matrix, and  $\{\phi_j\}^T \{P_{S0}\}$  the generalized hydrodynamic force due to tank rigid-body motion. To solve (3.68), commonly used time-integration can be applied.

It should be pointed out that the added-mass matrix in (3.68) is not diagonal. Consequently, the system is coupled. This system could, of course, be transformed into an uncoupled set by using the mode shapes of the coupled fluid-tank system, which are eigenvectors of

$$[K^*] \{\psi_j\} = \lambda_j^2 ([M^*] + [\phi]^T [P_S]) \{\psi_j\} .$$

We choose to solve (3.68) more straightforwardly.

The use of normal modes of the structural free vibration to reduce the number of unknown coordinates may be viewed as an application of the Ritz method.

#### 4. NUMERICAL RESULTS/VALIDATION

A computer program named ERST, for Earthquake Response of Sea-Based Storage Tanks, has been developed to implement the formulation of §3 to evaluate the elasto-hydrodynamic response of axisymmetric storage tanks submerged underwater induced by earthquake ground motions. A detailed discussion of ERST is given in Appendix A and the full program listing is furnished in Appendix B. In this section, we document some results obtained from the computer codes which were used to validate the program.

The simplest test is to see whether we can reproduce the well-known series solutions for cases where the tank structure is a rigid circular cylinder submerged underwater. Due to rigidity, the inner fluid motion and the outer water motion are uncoupled from the tank vibration. Consequently, we can test the interior response and the exterior response separately.

Since many of the available results are obtained with gravity effect included, we modified our program accordingly (we used the variational principle in the new coding to aid in our validation; the results were compared to be within 2% of ERST which uses the Galerkin scheme). We first compared the work of Tung (1979) studying (exterior) hydrodynamic forces on submerged cylindrical tanks under ground excitation. Considering a tank of relative dimensions  $H: (H-h_w) = 2$  and  $R: H = 1$ , under the assumed earthquake ground acceleration of  $e^{-i\omega t}$  with  $\omega = 10$  rad/sec, we found excellent agreement with the (analytic) data presented in Figure 4 of Tung's paper. We reproduced the relevant portion of the curves in our Figure 6. The pressures are evaluated on the tank wall at  $\theta = 0^\circ$ .

For the pressure response due to the interior fluid motion, we compared with the results of Takayama (1976) and Helou (1981). Again, the tank is a hollow circular cylinder with a flat top. Here,  $R=10$  ft,  $h_0=h_w=5$  ft,  $\rho_0=0.86$  and  $\rho_w=1$  in  $g/cm^3$ . We selected a finite-element idealization of 20 elements distributed symmetrically relative to the oil-water interface. In Figure 7, the x-z plane section of the assemblage is presented. From the sources quoted above, we have, for the analytic representation hydrodynamic pressure of oil and water,

$$P_o = -\rho_o R \cos\theta e^{-i\omega t} - \rho_o \sum_{m=1}^{\infty} \frac{1}{k_m} G_m'' \cosh k_m(z-h_o) \cos\theta e^{-i\omega t}, \quad (4.1)$$

$$- \leq z \leq h_o ,$$

$$P_w = -\rho_w R \cos\theta e^{-i\omega t} + \rho_w \sum_{m=1}^{\infty} \frac{1}{k_m} G_m'' \frac{\sinh k_m h_o}{\sinh k_m h_w} \cosh k_m(z+h_w) \cos\theta e^{-i\omega t} \quad (4.2)$$

$$-h_w < z < 0 ,$$

if the system undergoes a ground velocity (n.B., not acceleration)  $e^{-i\omega t}$ ;

In the above formula,

$$G_m'' = \omega^2 \bar{G}_m \frac{\sinh k_m h_w}{\sinh k_m h_o}, \quad \bar{G}_m = \frac{k_m C_m J_1(k_m R)}{K_m - M_m \omega^2},$$

and

$$M_m = k_m \left( 1 + \frac{\rho_o \tanh k_m h_w}{\rho_w \tanh k_m h_o} \right) \quad (4.3)$$

$$C_m = \left( \frac{\rho_o}{\rho_w} - 1 \right) \frac{2k_m R}{J_1(k_m R)(k_m^2 R^2 - 1) \cosh k_m h_w} \quad (4.4)$$

$$K_m = \left( 1 - \frac{\rho_o}{\rho_w} \right) g k_m^2 \tanh k_m h_w, \quad (4.5)$$

$k_m$  for  $m = 1, 2, \dots$  are the roots of  $J_1'(k_m R) = 0$ .

Pressures for a range of frequencies are calculated using the above formulae and our computer program. As can be seen from the results presented in Figures 8 through 11, the comparisons are quite satisfactory. Pressure distribution normalized by the excitation frequency are plotted against the nodes at the inner tank wall ( $\theta=0^\circ$ ). The figures are for  $\omega = 0.5$  rad/sec, 1.1 rad/sec, 6 rad/sec and 10 rad/sec. Notice that since gravity effects are considered here,  $P_o$  does not equal to  $P_w$  exactly. Also, note that the curves are for hydrodynamic pressures only, one would need to add on the hydrostatic pressures to extrapolate the location of equal pressures (where  $z = \zeta$ ).

Close examination of Figures 8 through 11 reveals that, while there is little change of the pressure curves from  $\omega = 0.5$  rad/sec to  $\omega = 1.1$  rad/sec, there is significant (trend-reversal) difference from there on to  $\omega = 6$  rad/sec. Eventually, the curves "stabilized" and become practically frequency independent (this is confirmed from calculation of a number of frequencies ranging from 3.7 rad/sec, 4.8 rad/sec to 60 rad/sec). Now, with the gravitational effects included, one could expect the fluid-structure system to exhibit sloshing phenomena at the natural frequencies  $\omega_m$  where

$$K_m = \omega_m^2 M_m. \quad (4.6)$$

For the data used in our test, these frequencies are

$$\omega_1 \approx 1.97, \quad \omega_2 \approx 3.92, \quad \omega_3 \approx 4.98, \quad \omega_4 \approx 5.83, \quad \omega_5 \approx 6.57, \dots$$

Since the density difference between oil and water is small (0.14 g/cm<sup>3</sup>) the sloshing amplitudes will be small. Within the frequency spectrum of importance due to earthquake excitations, only high modes of sloshing waves are expected. These are short-length waves of minor importance. Since the pressure distribution is independent of frequencies in this spectrum, this reinforces our belief that as far as our system configuration is concerned, the gravitational effects can be safely ignored, as we did in our analysis.

To ascertain that our 20-element finite-element scheme has converged enough to be believed, we increased the assemblage to 100 elements, whose layout is basically the same as that of the 20-element case, except that 10 columns are used. We present the results in Tables 1 and 2 (for  $\omega = 1.1$  rad/sec and 10 rad/sec). As one can see, although the results are certainly more accurate for the finer mesh, the results of the 20-element discretization is very respectable, and from the computational stand-point, by far more cost-efficient.

Although we know of no analytical results for the response problem of an axisymmetric tank with inclined wall, we made several calculations using a 20-element discretization on a slant tank similar to the one we used above, except that an inclination (from vertical axis of 0°, 15° and 30°) is imposed on the side wall.  $R = 10$  feet at the tank base. Figures 12 and 13 show that pressure distribution along the side wall ( $\theta = 0^\circ$ ) for  $\omega = 1$  rad/sec and  $\omega = 6$  rad/sec, respectively. For  $\beta = 15^\circ$ , it is calculated that resonance occurs at  $\omega \approx 2.5, 4.5, \dots$  (see Figure 14). Again, for earthquake bound frequencies, the sloshing phenomena will be negligible.

ERST has been implemented on the CDC Cyber 176 Computer of the United Computing Systems at Dallas, Texas, under the NOS/BE operating system. For the simple rigid circular cylindrical structure with a 20-element symmetric finite-element discretization as described above, undergoing harmonic ground acceleration, a typical run requires less than 2 seconds CPU time.

Our last series of tests involve a simple flexible (circular) cylindrical tank under a ground acceleration of  $\sin\omega t$ , for various values of  $\omega$ . The results are presented in Figures 15 through 17. Here  $R = 10$  m,  $h_o = h_w = 5$  m and  $H = 20$  m. A uniformly positioned 20-element finite-element system is selected for the interior fluid domain, which is then extended naturally to form a 45-element mesh for the exterior water and a 12-element one for the tank structure. In Figure 15,  $\omega = 1$  Hz, the hydrodynamic pressure distribution for the first two modes of response is plotted for  $t = .25$  sec and  $.75$  sec ( $1/4$  and  $3/4$  cycles after the initial excitation). In Figures 16 and 17,  $\omega = 10$  Hz, and we show response of the first mode as well as the first two modes for  $t = .025$  sec and  $.075$  sec. Notice that the interior pressure forces are approximately 1.5 to 2 times in value to that of the exterior pressure. Also notice that in Figure 15,  $\frac{\partial p^o}{\partial z}$  is close to zero even though the "roof" is not assumed to be rigid; but in Figures 16 and 17, larger displacements step in and change the pressure distribution now that frequency is bigger. The tank's natural vibration frequencies are  $\omega_1 = 16.7$  Hz,  $\omega_2 = 33.7$  Hz.

We were unable to make a comparison of our results to that of Helou's (1981) presented in his Figure 4.3 for, unfortunately, his results are incorrect as evidenced by the fact that  $\frac{\partial p^w}{\partial z} \neq 0$  at the ocean floor, violating the rigid boundary condition there.

Table 1. Pressure distribution at wall ( $\theta = 0^\circ$ )  
under different finite element discretizations.

z	P/ $\omega$ at Wall		
	20-element	100-element	Analytical
5.0	-8.438	-8.432	-8.431
2.0	-8.410	-8.404	-8.403
1.0	-8.386	-8.381	-8.381
0.66	-8.376	-8.372	-8.372
0.33	-8.366	-8.361	-8.361
0	-8.354	-8.349	-8.349
0	-10.286	-10.292	-10.292
-0.33	-10.272	-10.278	-10.276
-0.66	-10.260	-10.265	-10.266
-1.0	-10.248	-10.254	-10.255
-2.0	-10.221	-10.228	-10.228
-5.0	-10.188	-10.195	-10.196

$\omega = 1.1$  rad/sec

Table 2. Pressure distribution at wall ( $\theta = 0^\circ$ )  
under different finite element discretizations.

z	P/ $\omega$ at Wall		
	20-element	100-element	Analytical
5.0	-8.999	-8.996	-8.996
2.0	-9.088	-9.078	-9.075
1.0	-9.168	-9.159	-9.153
0.66	-9.203	-9.198	-9.201
0.33	-9.244	-9.247	-9.250
0	-9.293	-9.322	-9.342
0	-9.194	-9.162	-9.137
-0.33	-9.251	-9.247	-9.241
-0.66	-9.298	-9.304	-9.309
-1.0	-9.339	-9.350	-9.357
-2.0	-9.432	-9.444	-9.446
-5.0	-9.536	-9.539	-9.539

$\omega = 10$  rad/sec



## 5. SUMMARY AND FUTURES WORK

A rational and effective method to assess the effects of fluid-structure interaction, on the dynamic response of submerged underwater oil storage tanks under earthquake excitations, has been developed. Our approach is the hybrid-finite element method, discretizing the tank structure, the interior fluids, as well as the near field of the exterior water region into a ring-shaped mesh network. Solution for the hydrodynamic pressure distribution is substituted into the structural equation of motion in modal coordinates to obtain the system displacement information. A comprehensive and predictive computer code is developed for design engineering applications. The program is described in the Appendices. Our program has been validated against known analytical solutions and shown to be effective and accurate with the added flexibility for arbitrary axisymmetric tank shapes.

During this investigation, we also reconfirmed the fact that gravity effects can be safely neglected in evaluating the hydrodynamic pressure induced at the wall of a submerged tank, such as the one under study. It is also observed that due to the unappreciable difference of  $\rho_0$  and  $\rho_w$ , changes in the ratio  $h_0/h_w$  above do not significantly influence the fluid-structure response.

From (3.68), it can be seen that the hydrodynamic interaction caused by the fluids inside and outside the tank contributes to the structural equation of motion in the forms of additional terms which can be viewed as added mass and added excitations. The added inertia of water increases the natural period of the tank free oscillation, and decreases (depends on the deflected shape) the modal damping ratios. However, the presence of water does not influence the stiffness matrix [K].

Finally, the incorporation of analytic representation of  $P_w$  in the hybrid approach proves to be a useful cost-saver especially for tanks of odd shape and with irregular bottom topography. It is anticipated that this super-element should play an even bigger role in the treatment of soil-structure interactions.

The computer program developed in this study can be used, with appropriate modifications, for the following studies:

1. Tanks of open bottoms.
2. Tanks which are floating or moored.
3. Tanks which are non-axisymmetric.
4. Effects of non-rigid tank support and marine soil-structure interaction.

Understanding the nonlinear behavior of the kind of systems we have been investigating should, of course, be the ultimate study goal, but the numerical details it involves are very complicated. An in-depth analysis may also be needed to relax our assumptions that vertical ground motion and fluid incompressibility can be neglected. For the former, other modes of shell vibration, such as the breathing mode may need to be considered. Compressibility may become important for high values of excitation frequencies (for large-scale earthquakes). Indeed, with sound speed in water in the vicinity of 4720 ft/sec such high frequency excitations give rise to sound waves of lengths comparable to the tank dimension and the water depth. For squatty tanks, the compressibility effect may not be ignored.

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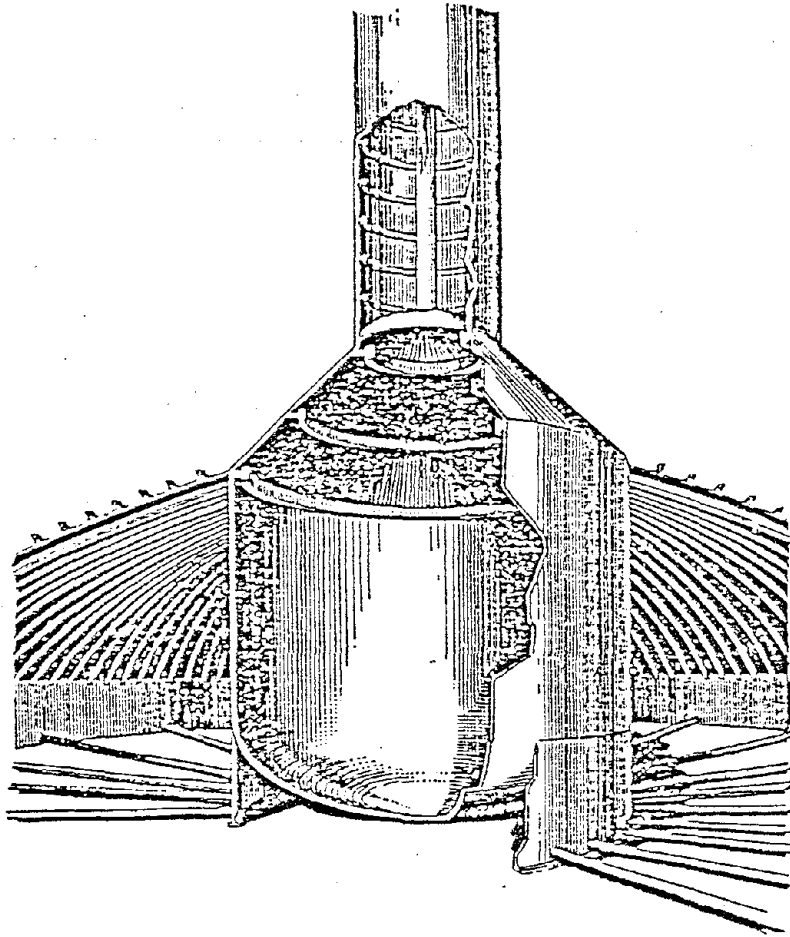


Figure 1. Section Through Khazzan Dubai 1

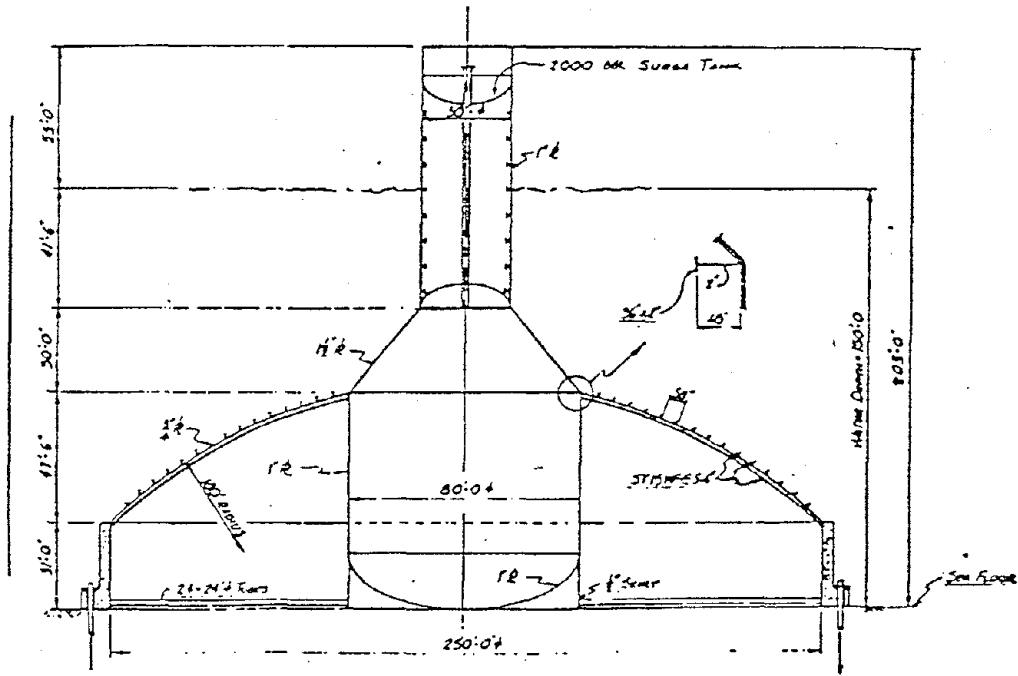


Figure 2. Major Dimensions of Khazzan Dubai 1

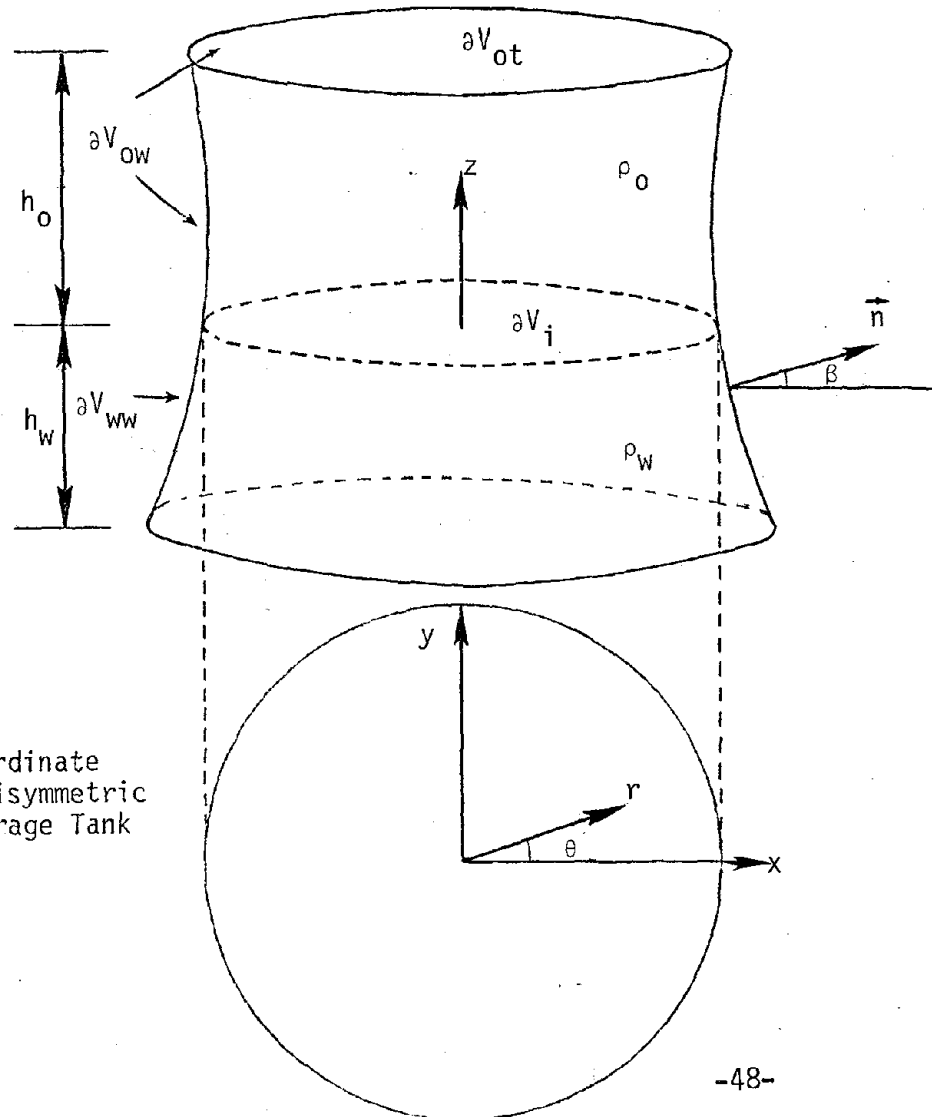
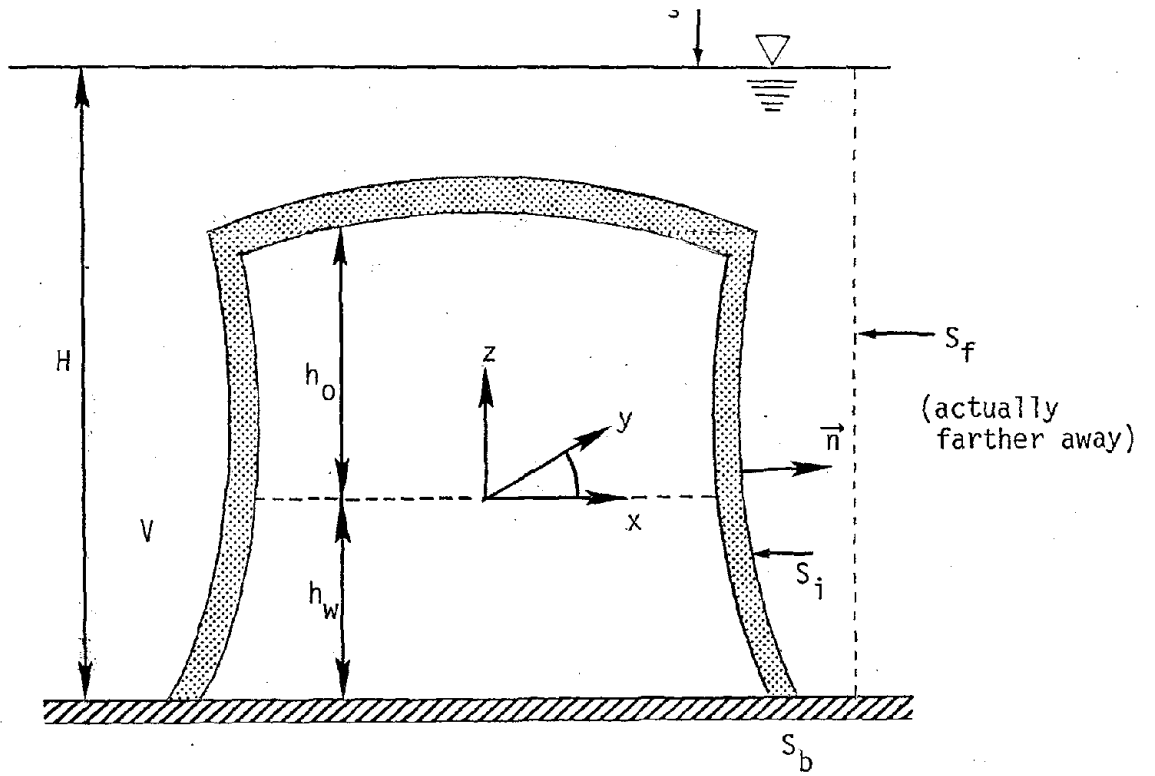
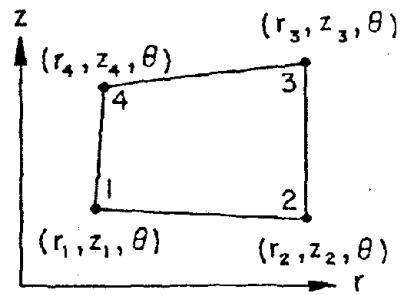
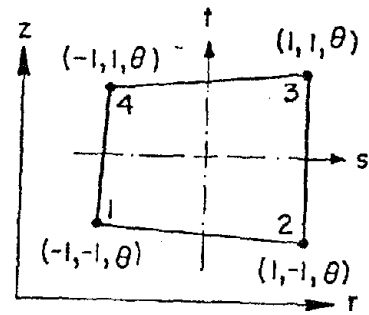


Figure 3. Coordinate System for Axisymmetric Submerged Storage Tank





Global Coordinate System



Local Coordinate System

Figure 4. Finite Element Coordinate System

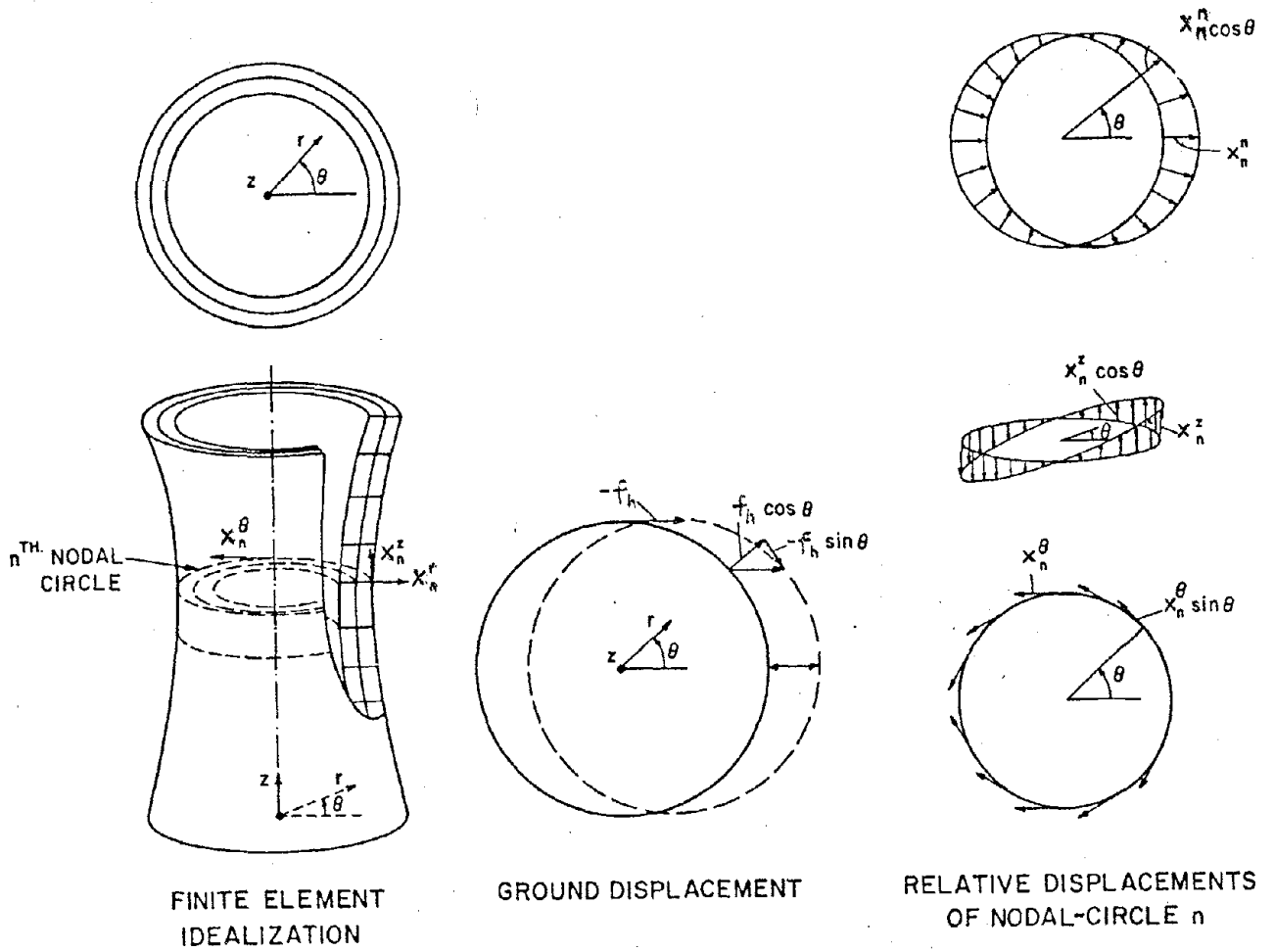


Figure 5. Axisymmetric Structure Subjected to Horizontal Ground Motion

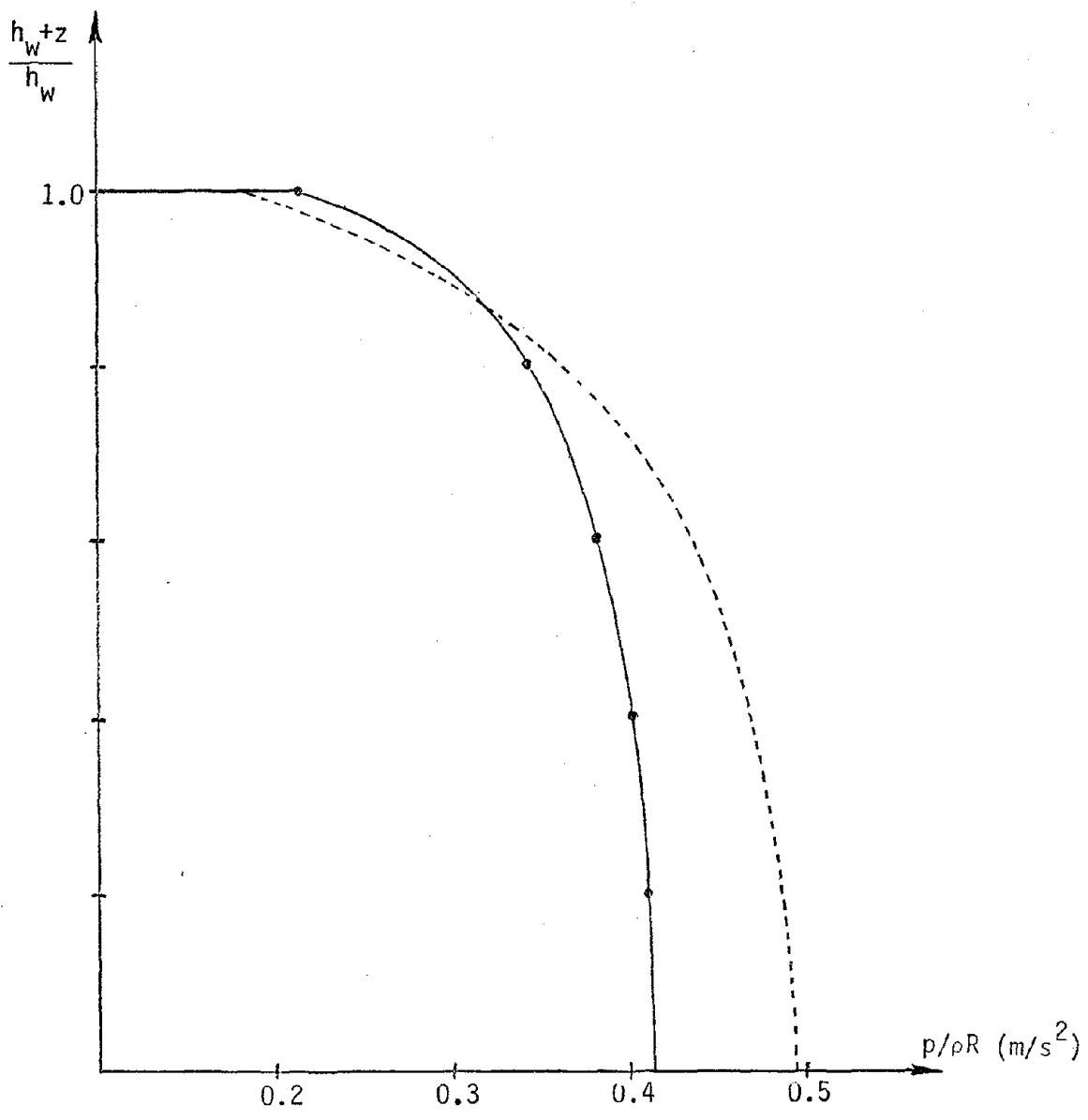
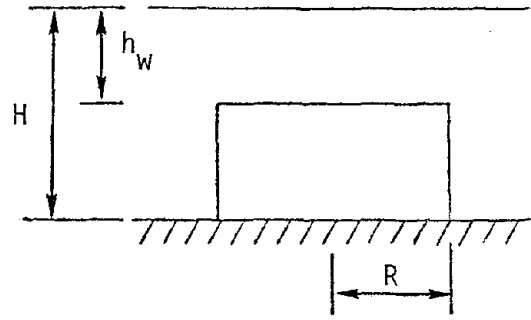


Figure 6. Pressures on wall of cylindrical tank  $\theta = 0^\circ$ .  
 —  $H/(H-h_w) = 2$ ; - - -  $H/(H-h_w) = 5$ ,  $R/H = 1$

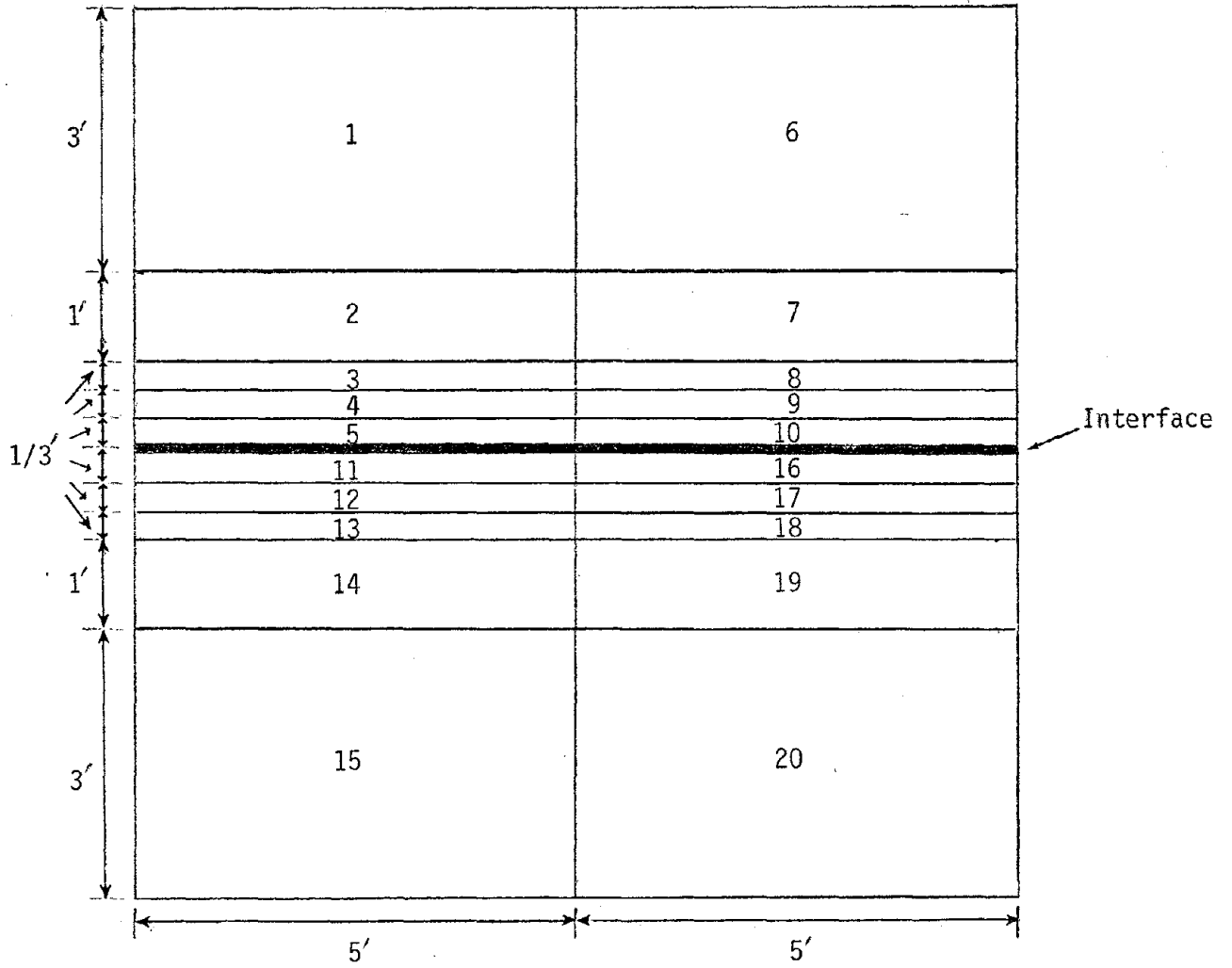
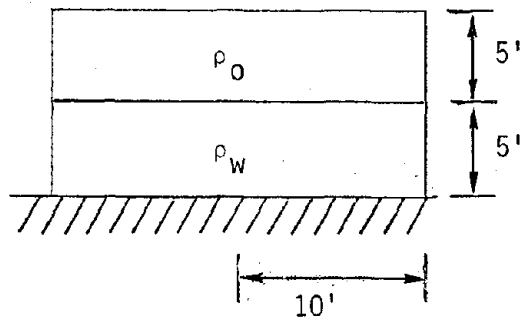


Figure 7. Interior Fluid Domain Finite Element Discretization



Z	FEM	Analytical
5.0	-16.639	-16.637
2.0	-16.631	-16.629
1.0	-16.623	-16.623
0.66	-16.619	-16.619
0.33	-16.616	-16.616
0	-16.612	-16.612

Z	FEM	Analytical
0	-19.491	-19.491
-0.33	-19.485	-19.485
-0.66	-19.481	-19.481
-1.0	-19.478	-19.478
-2.0	-19.470	-19.470
-5.0	-19.460	-19.460

$\omega = 0.5 \text{ rad/sec.}$

■ FEM

— Analytical

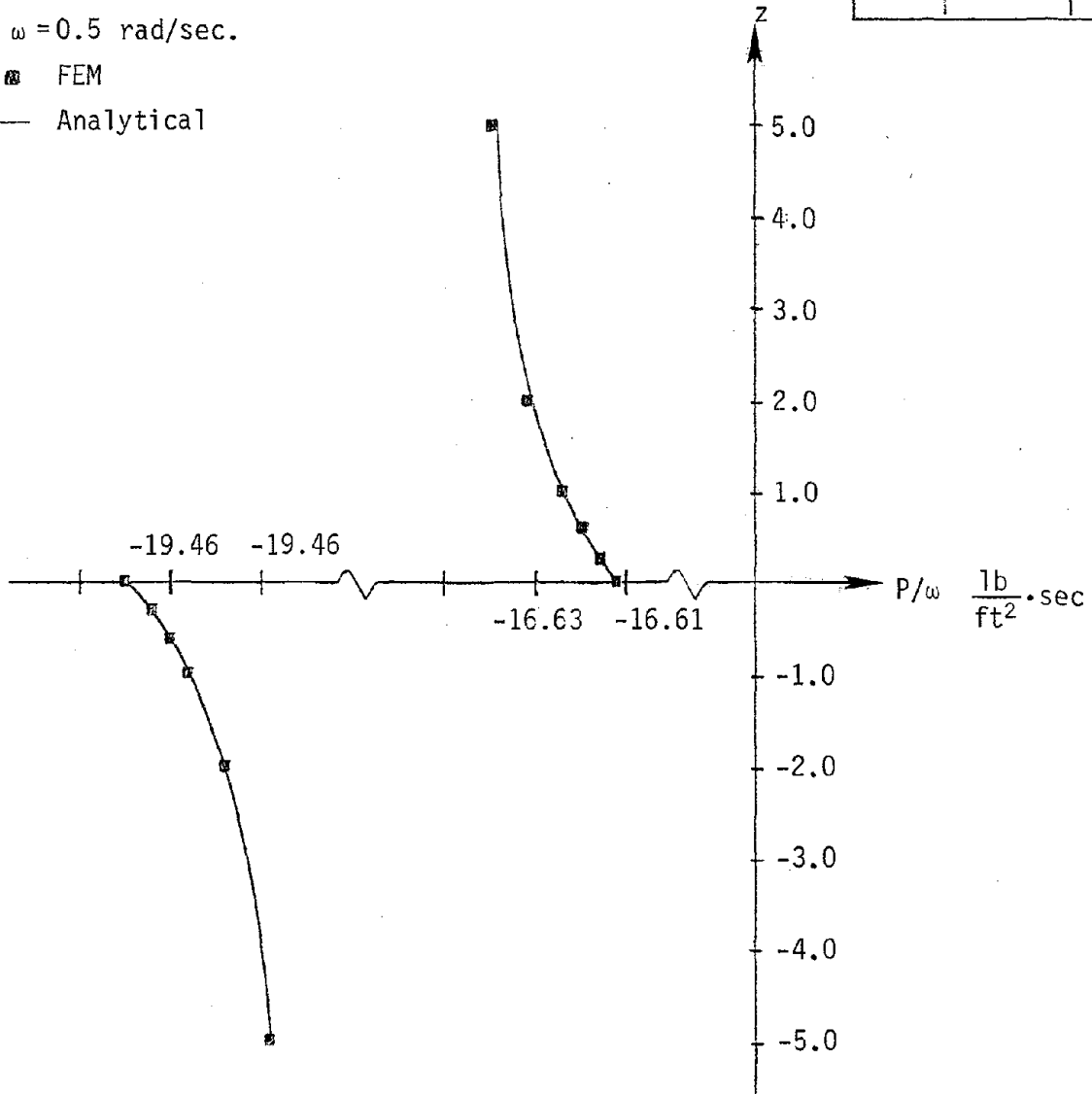
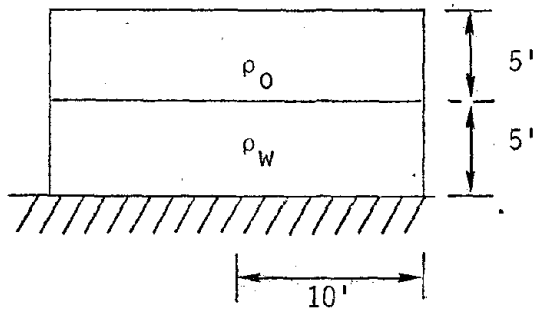


Figure 8. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Cylindrical Tank



Z	FEM	Analytical
5.0	-16.373	-16.359
2.0	-16.319	-16.305
1.0	-16.272	-16.262
0.66	-16.253	16.245
0.33	-16.233	16.224
0	-16.210	-16.200

Z	FEM	Analytical
0	-19.959	-19.970
-0.33	-19.932	19.939
-0.66	-19.903	19.920
-1.0	-19.885	-19.899
-2.0	-19.833	-19.846
-5.0	-19.769	-19.784

$\omega = 1.1$  rad/sec.

■ FEM  
 — Analytical

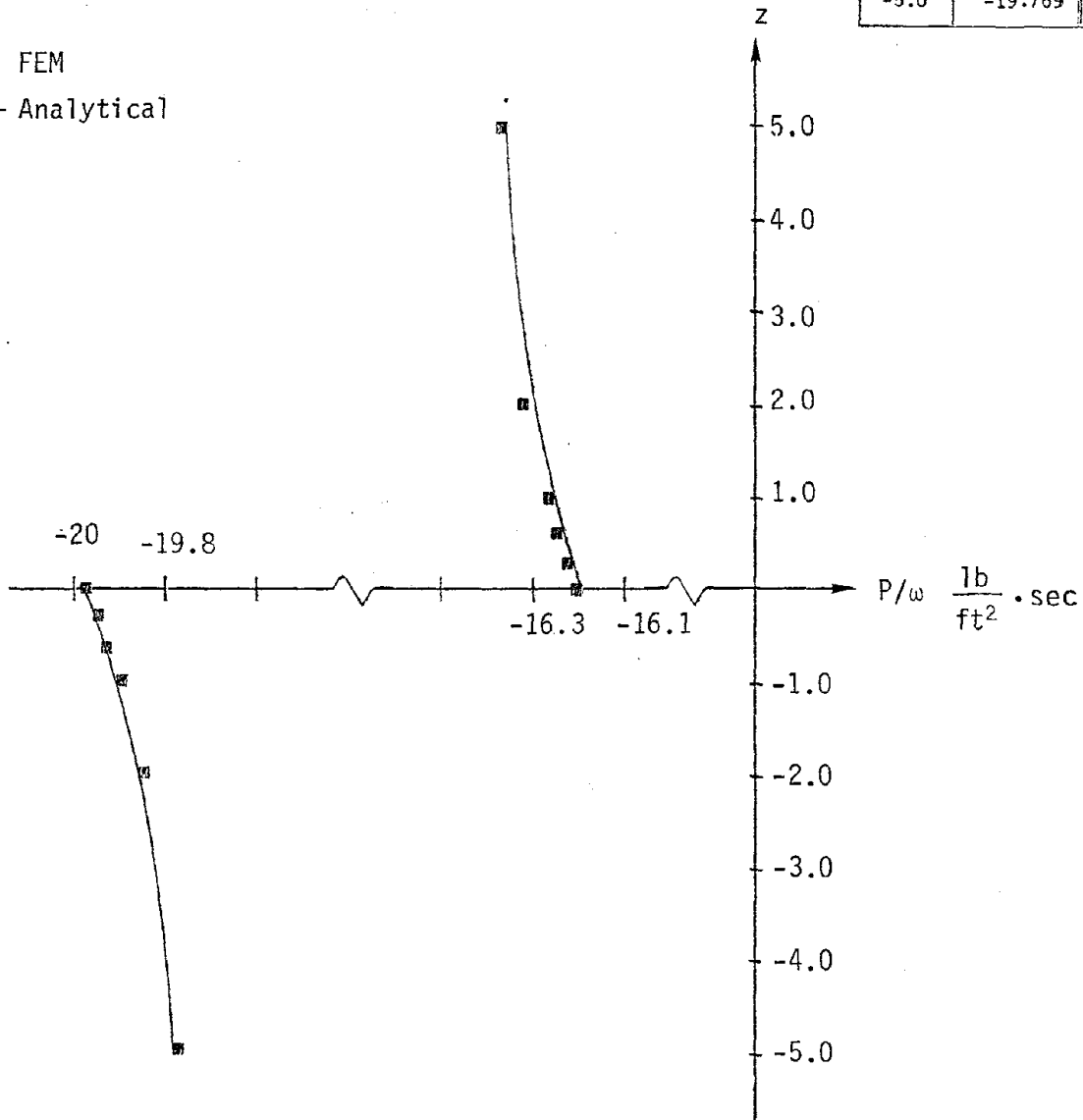
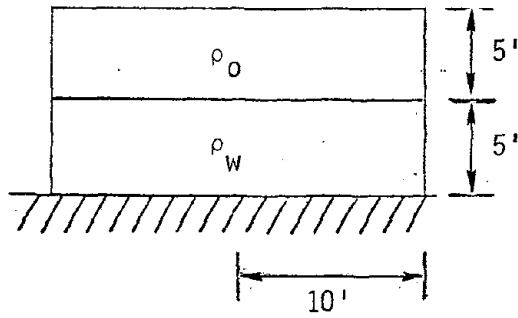


Figure 9. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Cylindrical Tank



Z	FEM	Analytical
5.0	-17.531	-17.526
2.0	-17.743	-17.731
1.0	-17.943	-17.956
0.66	-18.030	
0.33	-18.133	
0	-18.261	-19.374

Z	FEM	Analytical
0	-17.574	-17.440
-0.33	-17.723	
-0.66	-17.842	
-1.0	-17.945	-17.927
-2.0	-18.176	-18.191
-5.0	-18.422	-18.430

$\omega = 6.0$  rad/sec.

■ FEM

— Analytical

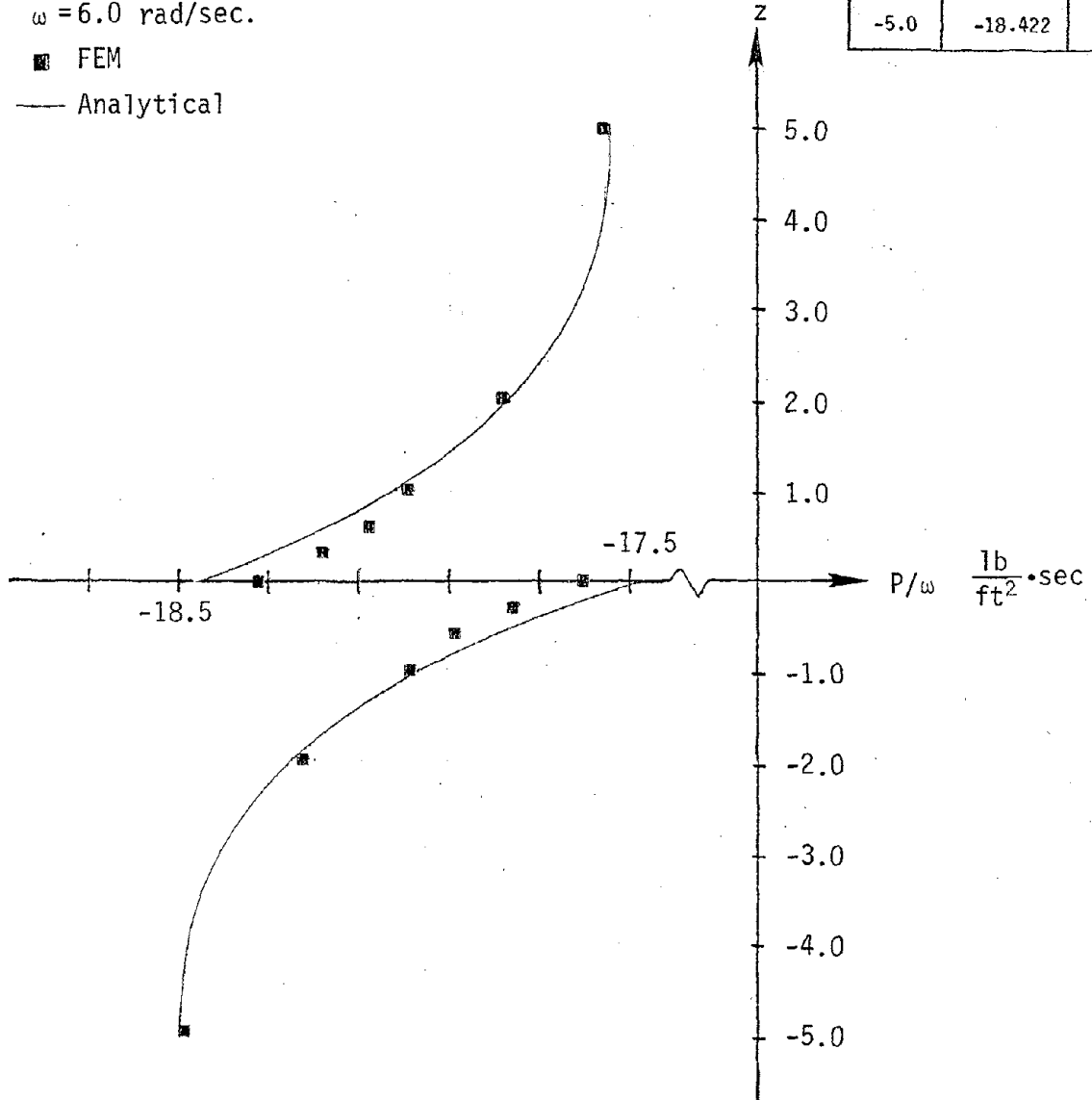
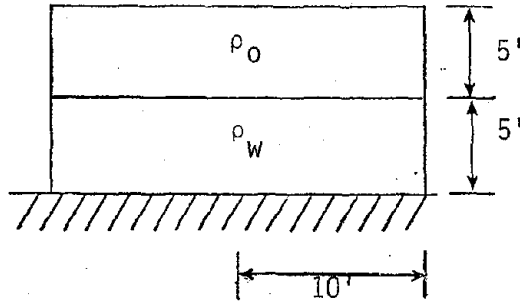


Figure 10. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Cylindrical Tank



Z	FEM	Analytical
5.0	-17.462	-17.456
2.0	-17.634	-17.609
1.0	-17.789	-17.760
0.66	-17.857	-17.853
0.33	-17.937	-17.949
0	-18.032	-18.127

Z	FEM	Analytical
0	-17.753	-17.729
-0.33	-17.951	-17.931
-0.66	-18.042	-18.063
-1.0	-18.121	-18.156
-2.0	-18.302	-18.333
-5.0	-18.504	-18.509

$\omega = 10.0$  rad/sec

■ FEM

— Analytical

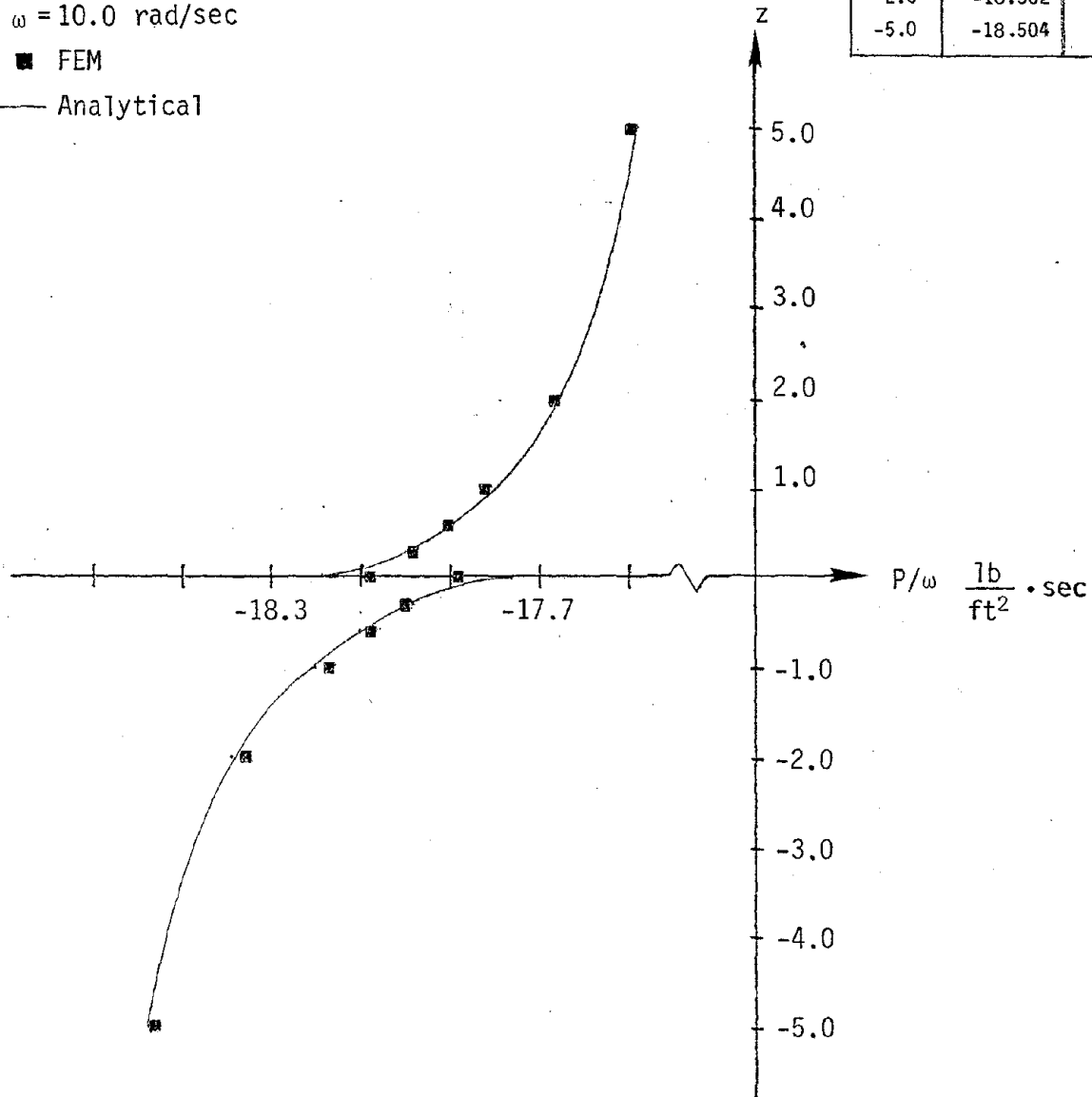


Figure 11. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Cylindrical Tank



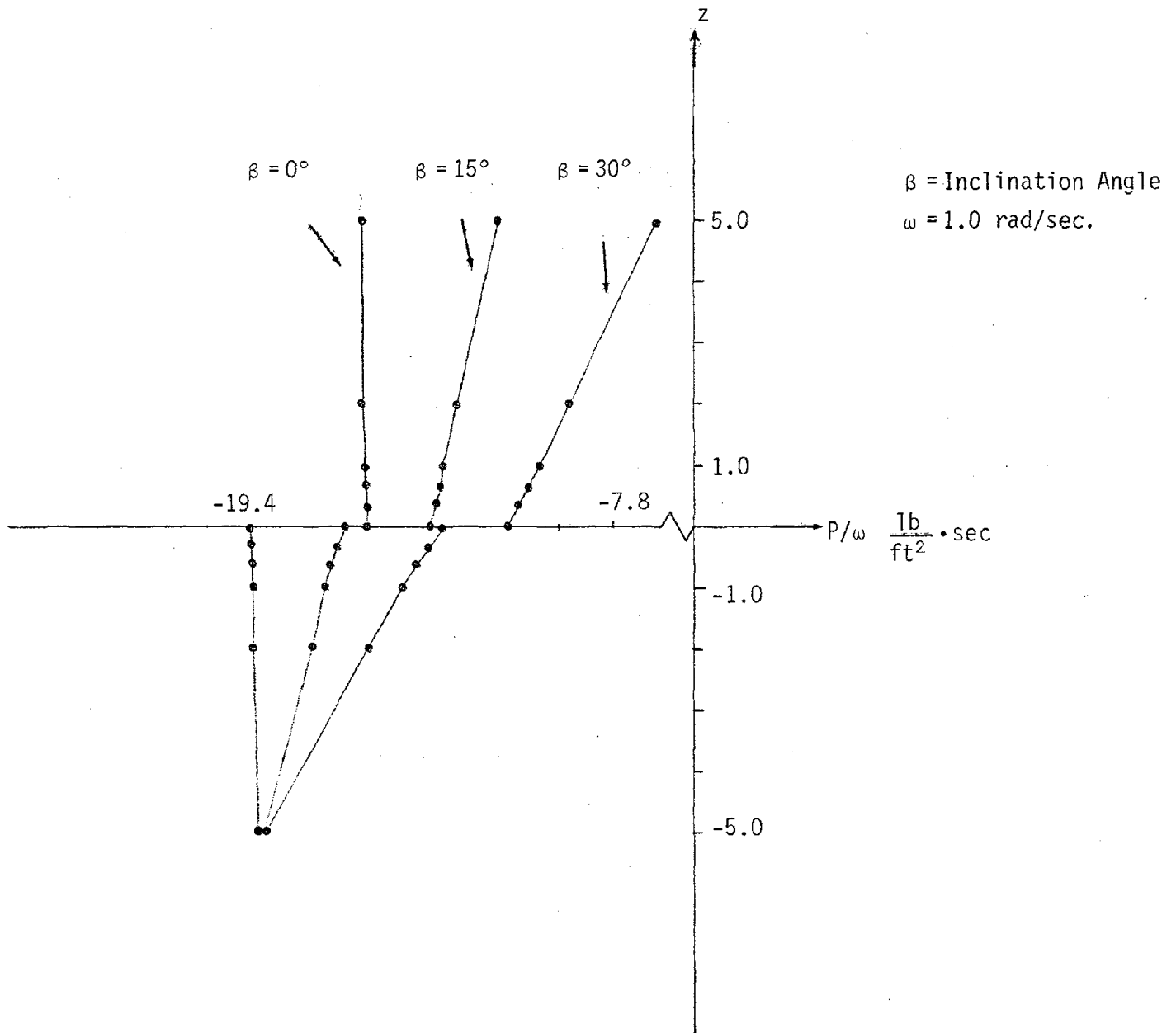


Figure 12. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Inclined Tank

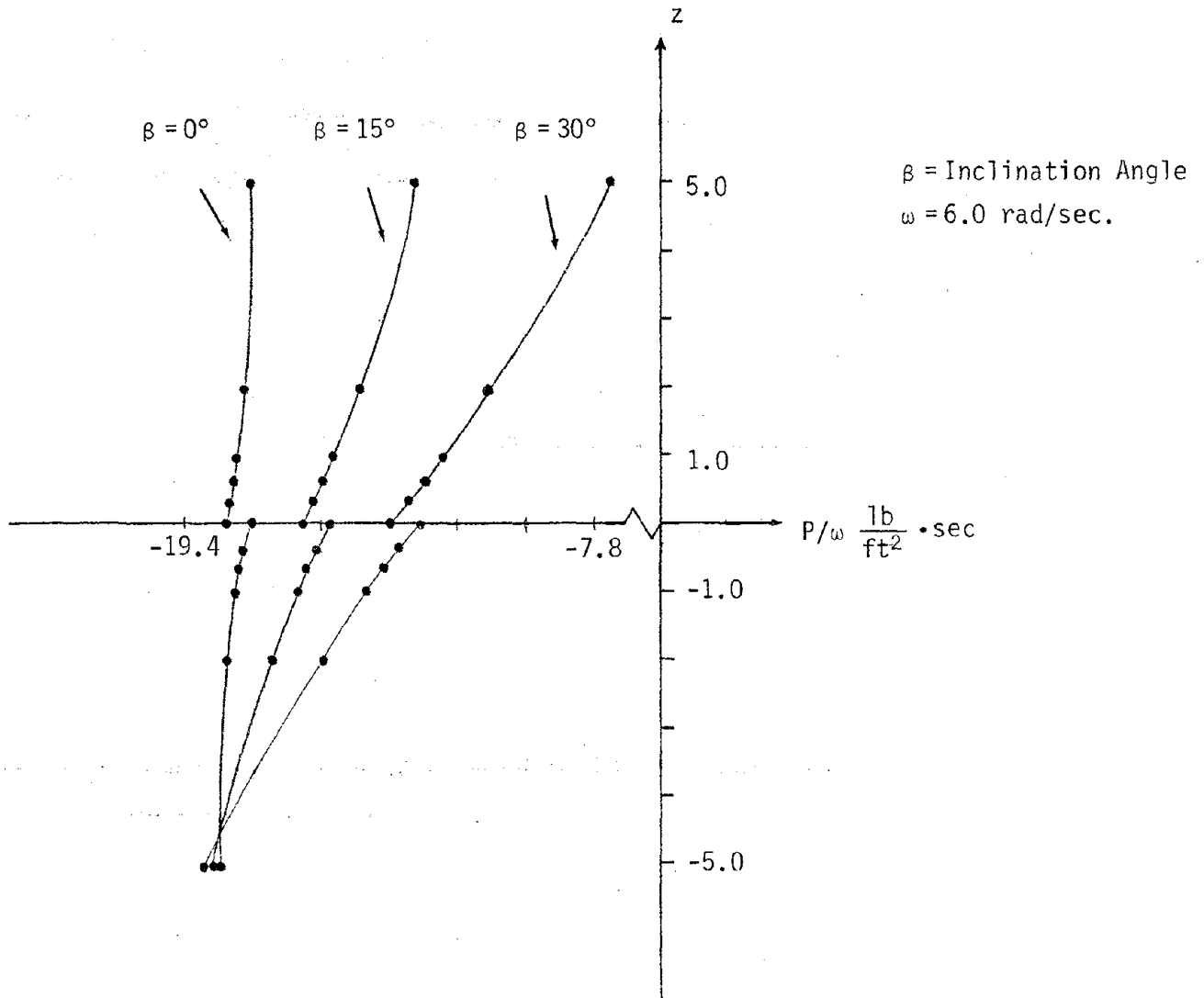


Figure 13. Pressure Distribution at Inner Wall ( $\theta = 0^\circ$ ) of a Submerged Inclined Tank

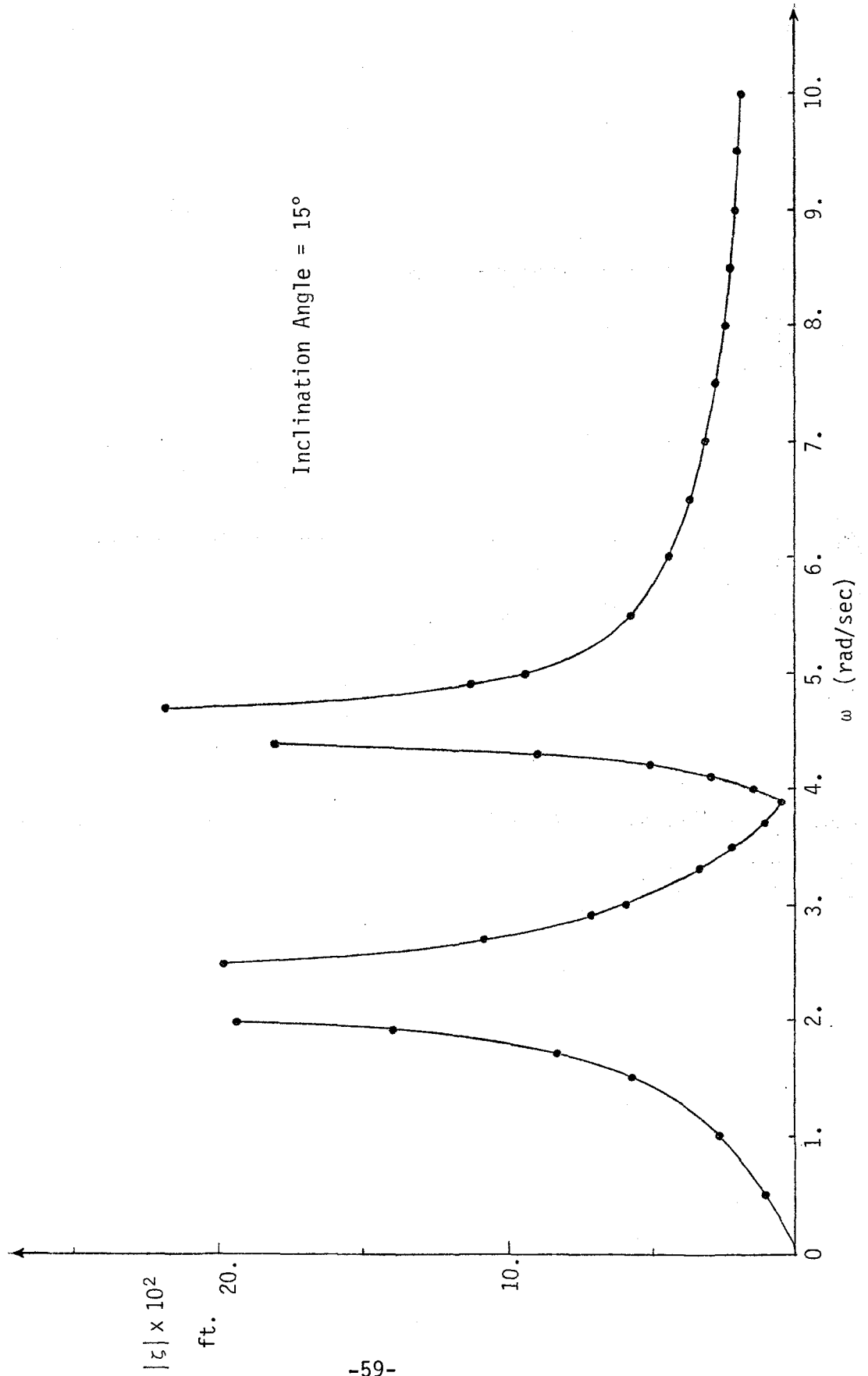


Figure 14. Oil-Water Interface Displacement-Frequency Curve of a Submerged Inclined Tank

$\omega = 2\pi$  rad/sec  
 Modes through 2

— Pressure on Inner Wall  
 - - - Pressure on Exterior Wall

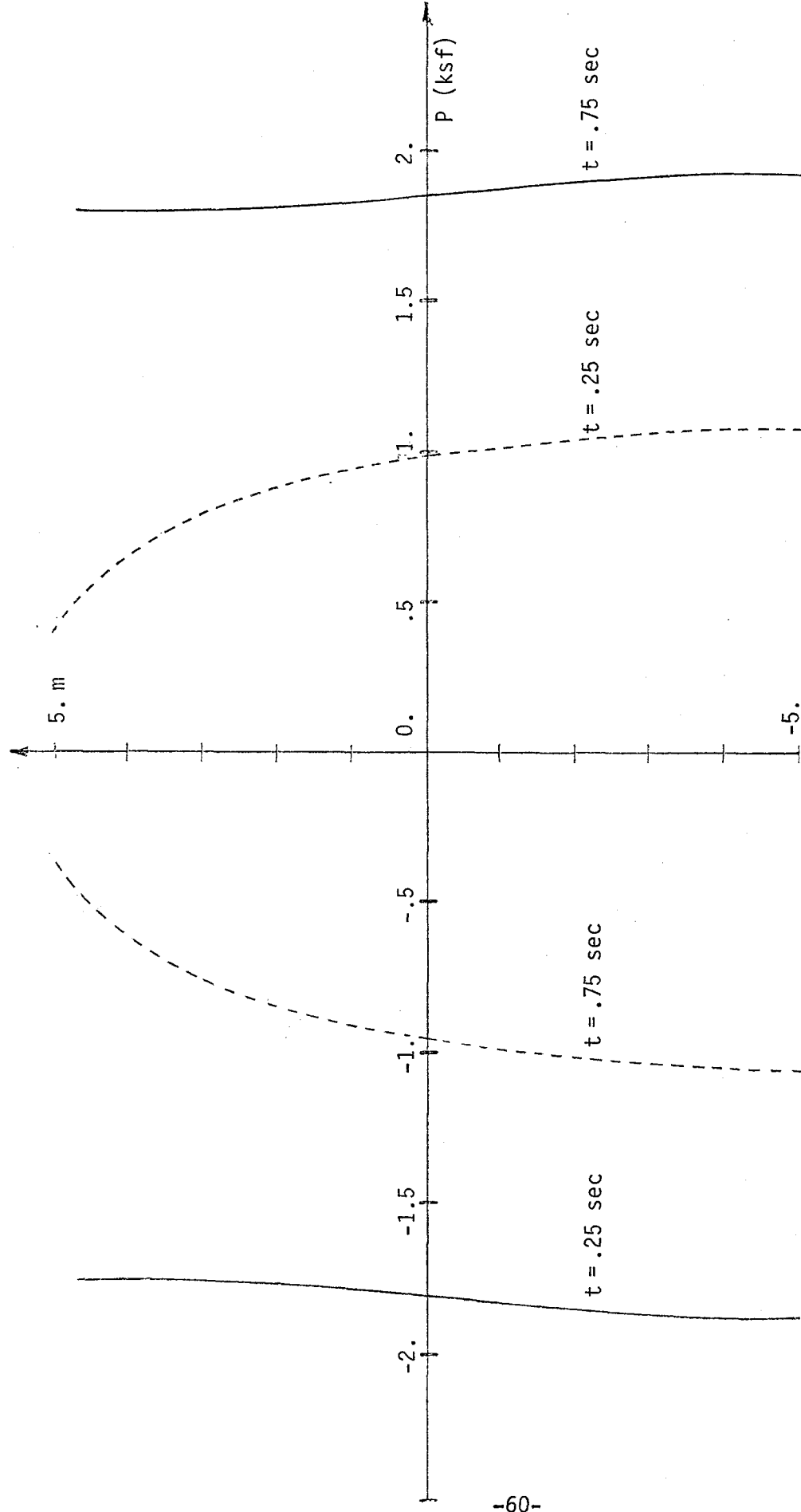


Figure 15. Pressure Distribution at Tank Wall ( $\theta = 0^\circ$ ) of a Submerged Flexible Tank

$\omega = 20\pi$  rad/sec  
Modes through 1

— Pressure on Inner Wall  
- - - Pressure on Exterior Wall

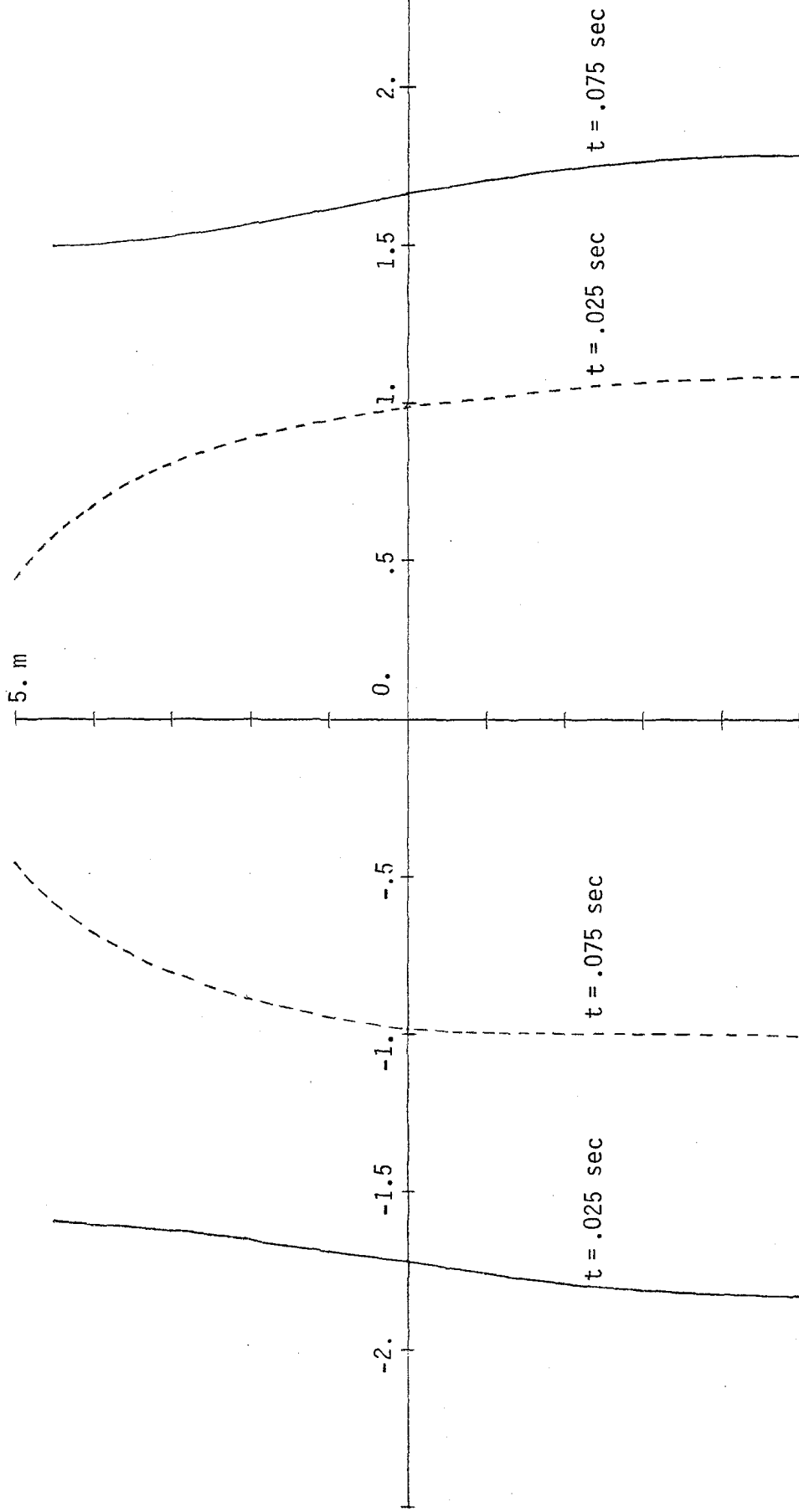


Figure 16. Pressure Distribution at Tank Wall 1 ( $\theta = 0^\circ$ ) of a Submerged Flexible Tank

$\omega = 20\pi$  rad/sec  
Modes through 2

— Pressure on Inner Wall  
- - - Pressure on Exterior Wall

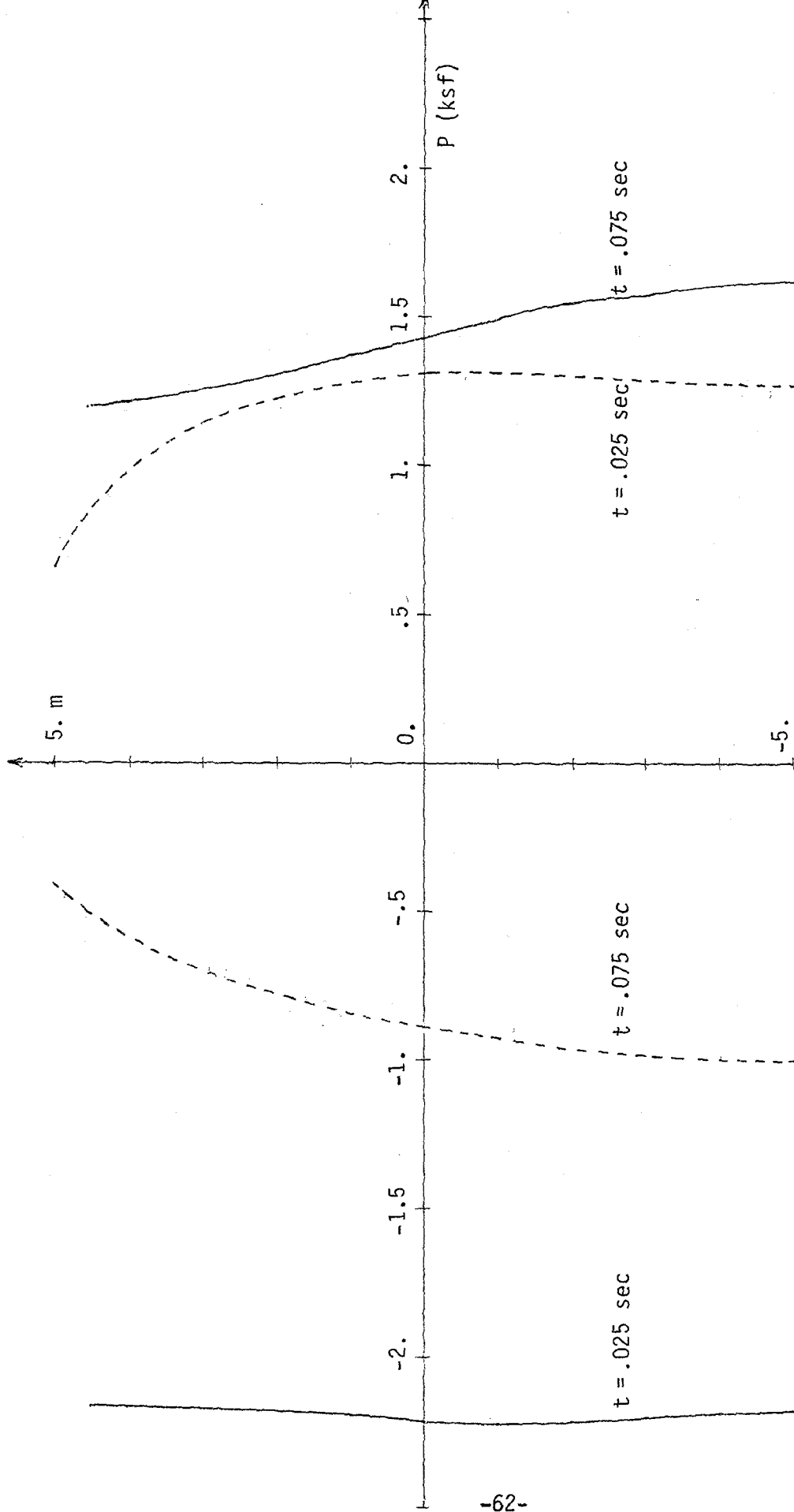


Figure 17. Pressure Distribution at Tank Wall ( $\theta = 0^\circ$ ) of a Submerged Flexible Tank

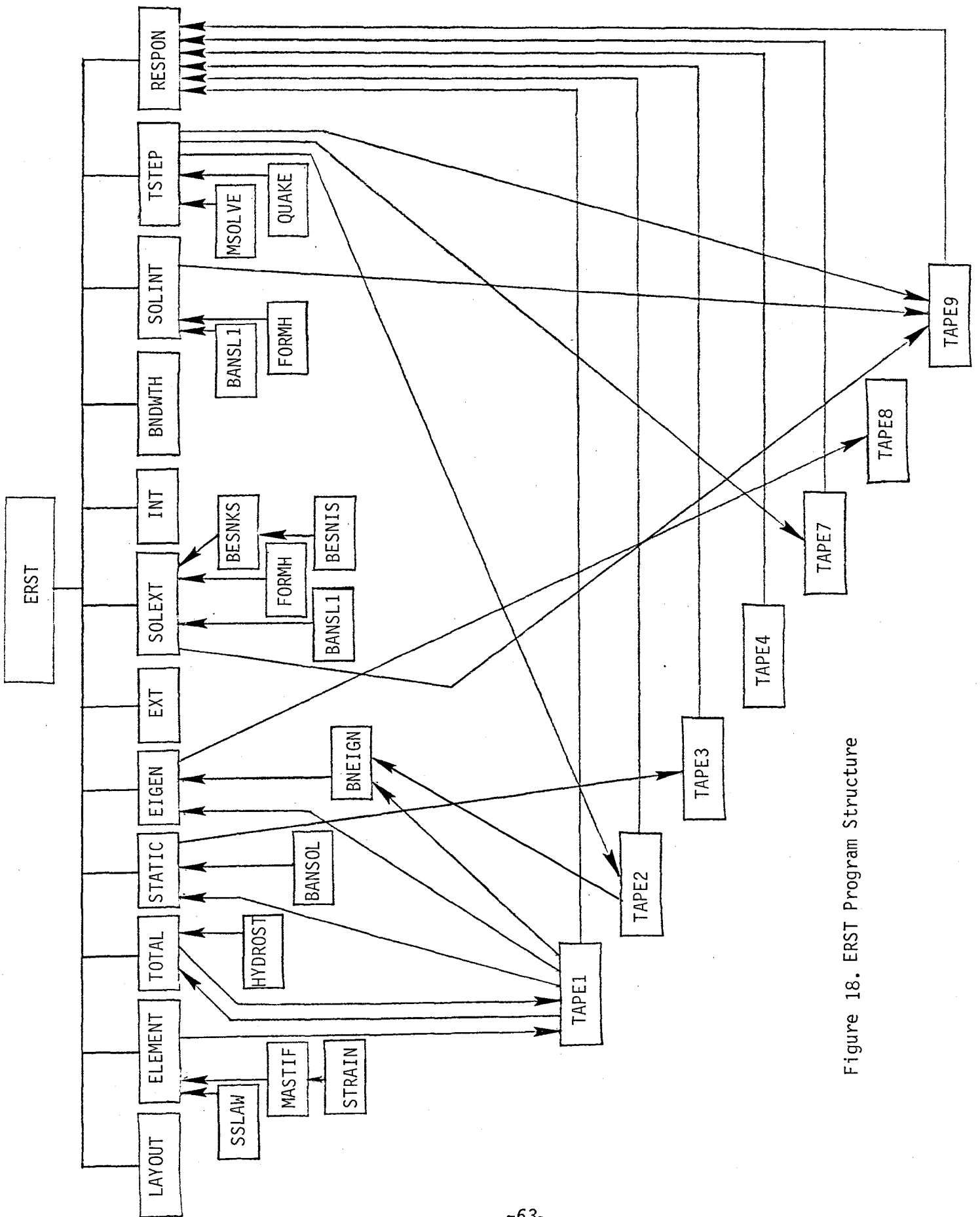


Figure 18. ERST Program Structure

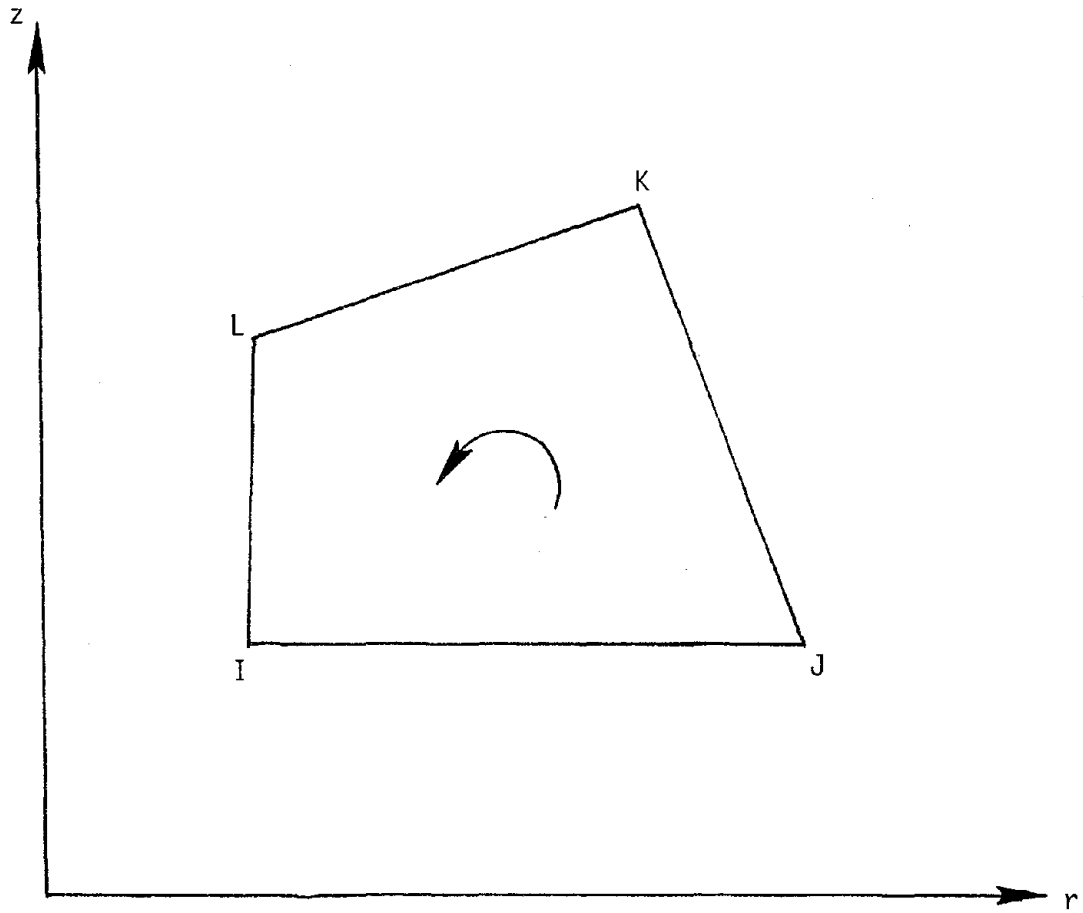


Figure 19. Finite Element Nodal Points Ordering Scheme



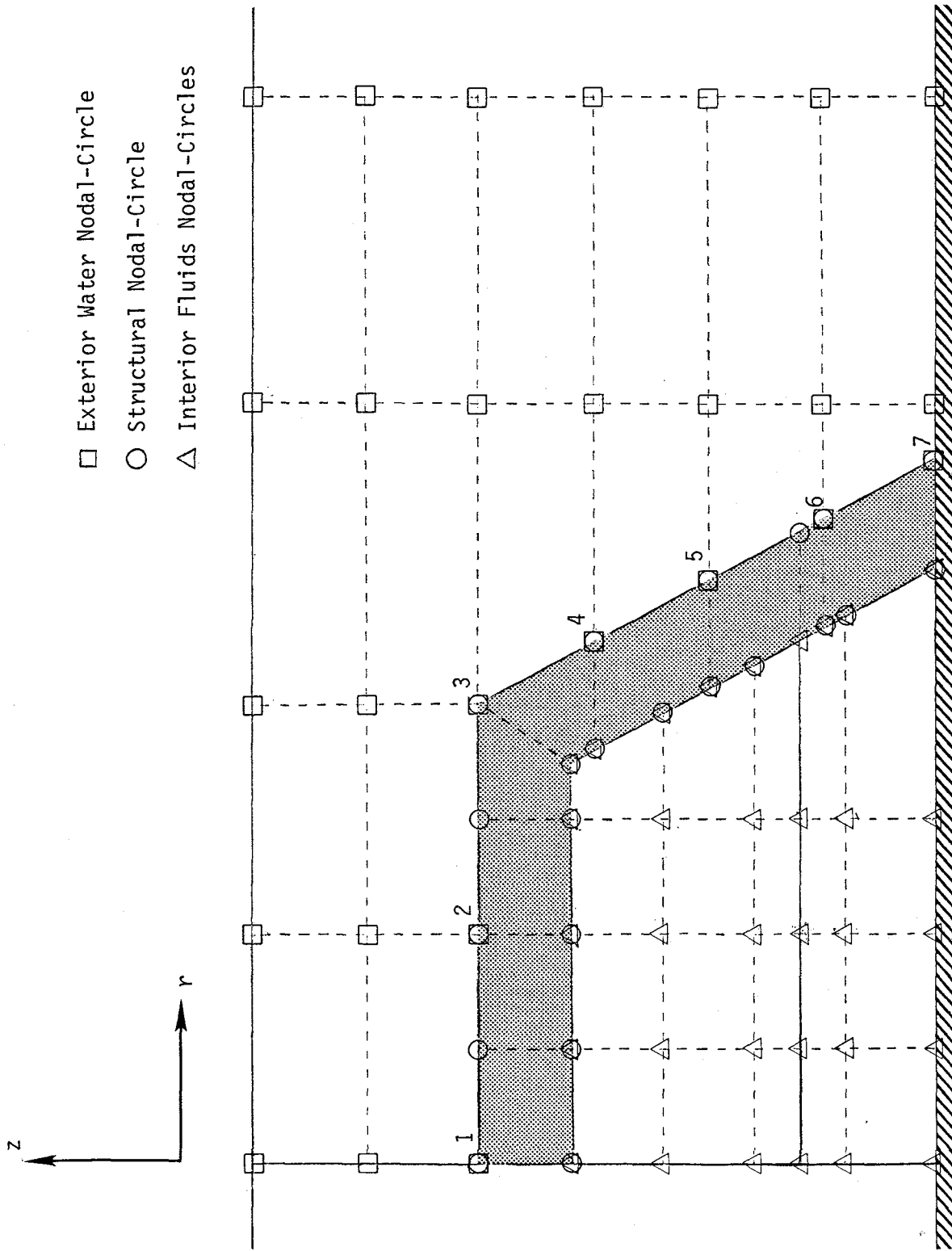


Figure 20. Finite Element Assemblages Shown at Cross-Section  $\theta = 0^\circ$ .  
 (Note that exterior water node sequence starts at structure interface.)

Appendix A. USER'S GUIDE TO COMPUTER PROGRAM "ERST"

The computer program named ERST, for Earthquake Response of Sea-Based Storage Tanks, is developed and synthesized to evaluate the elasto-hydrodynamic response of axisymmetric storage tanks submerged underwater induced by earthquake ground motions.

The tank structure is rigidly attached to the ocean floor, has a flexible wall. The tank has a vertical axis of symmetry, is submerged underwater (structures protruding out of ocean surface can also be handled with minimum modifications) and filled with two different layers of fluids. The whole system is discretized into three assemblages of toroidal finite elements for: the interior fluids domain, the tank shell, and the near field exterior water region.

Nodal displacements, stresses, as well as hydrodynamic pressures are output as the response to the input (horizontal) ground acceleration. Both the dynamic and the static responses are evaluated. A significant portion of the code pertaining to the dynamic behavior of exterior water-structure interaction is based on the EATSW program written by Dr. C. Y. Liaw for earthquake analysis of axisymmetric intake tower structures surrounded by water, purchased through the NISEE/Computer Applications Program, and modified to interface with the developed interior fluids-structure interaction program through the kind assistance of Dr. Liaw.

Figure 18 gives the general code structure with accompanying descriptions of the functions of the subroutines and the tape files employed. Note that a plotting scheme is built in based on the available subroutines GRAF11, PLOT, OPLT, MULPLT (in subroutines LAYOUT, EIGEN and TSTEP) interfaced to a Calcomp plotter. Users are advised to modify this portion to suit one's own environment.

- ERST - Driver program
  - LAYOUT - Determines structure characteristics and finite-element configurations
  - ELEMENT - Determines element stress strain, mass and stiffness matrices
  - TOTAL - Assembles global mass and stiffness matrices; also evaluates hydrostatic contribution for static analysis
  - STATIC - Computes static displacements and stress for static analysis
  - EIGEN - Determines structural free vibration modes and frequencies
  - EXT - Prepares for exterior water finite-element system set-up
  - SOLEXT - Computes generalized force vector and mass matrix contributed from exterior water and superelement
  - INT - Prepares for interior fluids finite-element system set-up
  - BNDWTH - Determines interior fluid element matrix bandwidth
  - SOLINT - Computes generalized forces vector and mass matrix contributed from interior fluids
  - TSTEP - Solves for modal equation of motion by time-step integration
  - RESPON - Calculates dynamic response by modal superpositions
- 
- TAPE1 - Stores element mass and stiffness matrices information
  - TAPE2 - Stores compacted mass matrix as well as x-displacement response information
  - TAPE3 - Stores element static response information
  - TAPE4 - Stores total stress information
  - TAPE6 - Stores plot information
  - TAPE7 - Stores Y-displacmeent response information
  - TAPE8 - Stores eigenmodes and eigenvalues information
  - TAPE9 - Stores hydrodynamic pressure as well as interpolated earthquake data information

In the following, we describe the data deck structure to be used for executing the program.

I. TITLE CARD (8A1Ø)

II. STRUCTURE INFORMATION (NAMELIST:TANK)

NUMNP: number of structural nodal-circles

NUMEL: number of structural elements

NUMMAT: number of different structural materials

NMODE: number of modes of vibration included. If NMODE=Ø and IGRAV=Ø, only static responses are evaluated.

WLO: level of water surrounding the structure (in feet)

WLI: level of water in the interior of a hollow structure (in feet)

NPO: number of structural nodal-circles on the exterior surface affected by the surrounding water

NPI: number of structural nodal-circles on the interior surface affected by interior fluids

IGRAV=Ø, perform static analysis only

    =1, perform dynamic analysis only

    =2, perform static as well as dynamic analysis

READFRQ=.FALSE., compute and write to TAPE8 frequencies and mode shapes of the structure without the surrounding water

READFRQ=.TRUE., skip calculation of frequencies and mode shapes; instead read from TAPE8

PLOTANK=.TRUE., plot structure elements

PLOTMOD=.TRUE., plot mode shapes

### III. MATERIAL PROPERTY INFORMATION

One set of cards must be supplied for each different material used in structure.

Card 1 (I5,5X,A11)

Columns 1 - 5: Material sequence number

11 - 21: Either 'ISOTROPIC' or 'ORTHOTROPIC' to indicate material property

Card 2I (3F10.0): Properties of Isotropic Material

Columns 1 - 10: Modulus of elasticity (in ksf - kips per square foot)

11 - 20: Poisson's ratio

21 - 30: Mass density (in kip-sec<sup>2</sup>/ft<sup>4</sup>)

Card 20 (6F10.0): Properties of Orthotropic Material

Columns 1 - 10:  $E_n$ , modulus of elasticity (in ksf)

11 - 20:  $E_s$ , modulus of elasticity (in ksf)

21 - 30:  $E_t$ , modulus of elasticity (in ksf)

31 - 40:  $\nu_{ns}$ , Poisson's ratio

41 - 50:  $\nu_{nt}$ , Poisson's ratio

51 - 60:  $\nu_{st}$ , Poisson's ratio

Card 3 (5F10.0): Properties of Orthotropic Material  
(continued from Card 20)

Columns 1 - 10:  $G_{ns}$ , shear modulus (in ksf)

11 - 20:  $G_{nt}$ , shear modulus (in ksf)

21 - 30:  $G_{st}$ , shear modulus (in ksf)

31 - 40: Mass density (in kip-sec<sup>2</sup>/ft<sup>4</sup>)

41 - 50: Angle  $\beta$  in degrees measured counter-clockwise from the r-axis to the n-axis

The n-s axes are the principal axes for the orthotropic material, and t is the tangential direction of the axisymmetric coordinates.

IV. STRUCTURAL NODAL-CIRCLE CARDS (I5,F5.0,2F10.0,2I5,2F10.0)

- Columns 1 - 5: Nodal-circle number
- 8 - 10: Boundary condition code  
"1" in column 8 if r-displacement is restrained  
"1" in column 9 if z-displacement is restrained  
"1" in column 10 if  $\theta$ -displacement is restrained
- 11 - 20: r-ordinate (in feet)
- 21 - 30: z-ordinate (in feet)
- 31 - 40: Used for layer generation, otherwise leave blank.

Nodal-circle cards must be in numerical sequence. If cards are omitted and Columns 31 - 60 are left blank, the omitted nodal-points are generated along a straight line between the defined nodal-points. (See Note 1); or if Columns 31 - 60 are not blank, they are generated in layers (see Note 2).

Note 1: Straight line generation

If the (L-1) cards for nodal-circles N+1, N+2, ..., N+L-1 are omitted and Columns 31 - 60 of the card for nodal-circle N are left blank, the omitted nodal-circles are generated at equal intervals on the straight line joining nodes N and (N+L).

Note 2: Layer generation

Layer generation may be used after two rows of nodal-circles are completely defined. If, on the card for node N, the following data is specified:

- Columns 31 - 35: MOD: module, m ( $> 0$ )
- 36 - 40: NLIM: limit of generation ( $> N$ )
- 41 - 50: FACX: amplification factor  $f_r$  (default  $f_r=1$ )
- 51 - 60: FACZ: amplification factor  $f_z$  (default  $f_z=1$ )

the r-z coordinates of points N+1, N+2, ..., NLIM are generated by the formulas:

$$r_k = r_{k-m} + f_r \cdot (r_{k-m} - r_{k-2m})$$

$$z_k = z_{k-m} + f_z \cdot (z_{k-m} - z_{k-2m})$$

for  $k = N+1, \dots, NLIM$ . If  $NLIM = NUMNP$ , no more nodal-cards are needed. If  $NLIM < NUMNP$ , the card for circle  $(NLIM+1)$  must follow.

The boundary condition code for generated nodal-circles is set equal to zero, i.e., these nodal-circles are unrestrained in all  $r$ ,  $z$  and  $\theta$  coordinates.

#### V. STRUCTURAL ELEMENT CARDS (6I5)

Columns 1 - 5: Element number

6 - 10:	Nodal-Point I	The maximum difference "b" between these numbers is an indication of the bandwidth of the Stiffness Matrix. "b" may be minimized by a judicious numbering of nodal points.
11 - 15:	Nodal-Point J	
16 - 20:	Nodal-Point K	
21 - 25:	Nodal-Point L	
26 - 30:	Material identification	

Nodal-point numbers I, J, K and L must be in sequence in a counter-clockwise direction around the element (cf. Figure 19). Element cards must be in element number sequence. If element cards are omitted, the program automatically generates the omitted information by incrementing by one the preceding I, J, K and L. The material identification for the generated card is set equal to the corresponding value on the last card. The last element card must always be supplied. Triangular elements are also permissible; they are identified by repeating the last nodal number (i.e., I, J, K, K).

## VI. WATER PRESSURE CARDS

Card Set 1 (16I5): This set of cards are to be omitted, if  $NPO = \emptyset$ .

Columns 1 - 5: Nodal-circles of the structure affected by the  
6 - 10: surrounding water;  $n_1, n_2, \dots, n_k = NPO$ , starting  
etc. from roof center.

Card Set 2 (16I5): This set of cards are to be omitted, if  $NPI = 0$ .

Columns 1 - 5: Nodal-circles of the structure affected by the  
6 - 10: interior fluids;  $m_1, m_2, \dots, m_L, L = NPI$ , starting  
etc. from inner roof center.

## VII. EXTERIOR FLUID CARDS

Card 1. FLUID DOMAIN DISCRETIZATION (NAMELIST: EXTFLD)

NUMPEX: number of fluid nodal-circles

NUELEX: number of fluid elements

NUINTEX: number of nodal-circles on the fluid-structure inter-  
face in the finite element idealization of the fluid

NUFSF: number of nodal circles on the free surface in the  
finite element idealization of the fluid and at the  
z-axis.

NUCOF: number of coefficients of super-element pressure  
representation.



Card 2. FLUID NODAL-CIRCLES (2I5,2F10.0,2I5,2F10.0)

Nodal-circles in the finite element idealization of the fluid domain must be numbered in such a way, that the first NUINTEX nodal-circles are located on the structure-fluid interface (cf. Figure 20). The numbering must start at the top as shown there. In the finite element idealization for the fluid domain, nodal-circles on the interface must be provided to coincide with the nodal-circle in the structural idealization. Additional nodal-circles can be included in the idealization of the fluid domain, as shown in Figure 20.

One card for each nodal-circle containing the following information must be provided.

Columns 1 - 5: Fluid nodal-circle number

6 - 10: ICODE: Boundary condition code for fluid nodal-circle. If the fluid nodal-circle is on the interface and coincides with a structural nodal-circle, ICODE = the number of the coincident structural nodal circle.

If the fluid nodal-circle is on the interface but does not coincide with a structural nodal-circle, then ICODE = -1.

If the fluid nodal-circle is on the free surface of the fluid domain, ICODE = -2.

For all other nodal-circles, leave Columns 26-30 blank. Special attention must be given to fluid nodal-circle number 1; it must coincide with the roof center of the tank.

11 - 20: r-ordinate (in feet)

21 - 30: z-ordinate (in feet)

31 - 60: Used for layer generation; otherwise leave blank.

Nodal-circle cards must be in numerical sequence starting from one. If cards are omitted and Columns 31-60 are left blank, the omitted nodal-points are generated along a straight line between the defined nodal-circles (see IV, Note 1); or if columns 31-60 are used, they are generated in layers (see IV, Note 2). The boundary condition code (ICODE) of a generated nodal circle is set equal to the value of ICODE on the last card.

Card 3. FLUID ELEMENTS (9I5)

Columns 1 - 5 Element number  
6 - 10: Nodal-Circle I  
11 - 15: Nodal-Circle J  
16 - 20: Nodal-Circle K  
21 - 25: Nodal-Circle L

Fluid Element Surface Code (=2, hybrid surface)

26 - 30: surface IJ  
31 - 35: surface JK  
36 - 40: surface KL  
41 - 45: surface LI

Nodal-circle numbers I, J, K and L must be in sequence in a counter-clockwise direction around the element (cf. Figure 19). Element cards must be in element number sequence. If element cards are omitted, the program automatically generates the omitted information by incrementing by one the preceding I, J, K and L. The last element card must always be supplied. Triangular elements are also permissible; they are identified by repeating the last nodal number (i.e., I, J, K, K)

## VIII. INTERIOR FLUID CARDS

### Card 1. FLUID DOMAIN DISCRETIZATION (NAMELIST: INTFLD)

NUNPIN: number of fluid nodal-circles  
NUELIN: number of fluid elements  
ROIL: specific gravity of oil  
NUINTIN: number of elements at oil/water interface  
NUELOIL: number of oil elements; the oil elements must be numbered from 1 to NUELOIL

### 2. FLUID NODAL-CIRCLES (2I5,2F10.0,2I5,2F10.0)

One card for each nodal-circle containing the following information must be provided.

Columns 1 - 5: Fluid nodal-circle number

6 - 10: ICODE: Boundary condition code for fluid nodal-circle. If the fluid nodal-circle is on the wall and coincides with a structural nodal-circle, ICODE = the number of the coincident structural nodal-circle.

If the fluid nodal-circle is both on the wall and on the interface and coincides with a structural nodal-circle, then ICODE = - (the number of the coincident structural nodal-circle).

11 - 20: r-ordinate (in feet)

21 - 30: z-ordinate (in feet)

31 - 60: Used for layer generation; otherwise leave blank.

Nodal-circle cards must be in numerical sequence starting from one. If cards are omitted and Columns 31-60 are left blank, the omitted nodal-points are generated along a straight line between the defined nodal-circles (see IV, Note 1), or if Columns 31-60 are used, they are generated in layers (see IV, Note 2). The boundary condition code (ICODE) of a generated nodal-circle is set equal to zero.

Card 3. FLUID ELEMENTS (5I5)

Columns 1 - 5: Element number  
6 - 10: Nodal-circle I  
11 - 15: Nodal-circle J  
16 - 20: Nodal-circle K  
21 - 25: Nodal-circle L

Nodal-circle numbers I, J, K and L must be in sequence in a counter-clockwise direction around the element (cf. Figure 19). Element cards must be in element number sequence. If element cards are omitted, the program automatically generates the omitted information by incrementing by one the preceding I, J, K and L. The last element card must always be supplied. Triangular elements are also permissible; they are identified by repeating the last number (i.e., I, J, K, K).

Card 4. OIL/WATER INTERFACIAL ELEMENT (16I5)

List of NUINTIN element numbers on the oil-water interface.

IX. RESPONSE CONTROL CARDS (NAMELIST: RESPONS)

NGRD:=1, if only one component of ground motion, along  $\theta = 0^\circ$ , is to be considered

=2, if two components of ground motion, along  $\theta = 0^\circ$  and  $\theta = 90^\circ$ , are to be included.

NT: number of integration steps in time

DT: time interval in step-by-step integration

NXFH: number of ordinates describing time history of ground motion component 1 along  $\theta = 0^\circ$ .

NYFH: number of ordinates describing time history of ground motion component 2 along  $\theta = 90^\circ$ .

PLOTALL=.FALSE., ground motion not plotted.

=.TRUE., plot ground motion.

X. DAMPING RATIO CARDS (7F10.0)

Columns 1 - 10: Damping ratio for first mode of vibration of the tank.

11 - 20: Damping ratio for second mode of vibration of the tank.

21 - 30: Damping ratio for third mode of vibration of the tank.

etc.

XI. GROUND ACCELERATION CARDS

(i) FIRST COMPONENT - Along  $\theta = 0^\circ$

Card 1 TITLE (8A10)

Card 2 ACCELERATION (6(F6.3,F6.4),8X)

NXFH time-acceleration pairs describing the time-history of the component of ground acceleration along  $\theta = 0^\circ$  are to be specified on these cards, with six pairs per card. Time must be expressed in seconds and accelerations as multiples of g, the acceleration due to gravity.

(ii) SECOND COMPONENT - Along  $\theta = 90^\circ$

Card 1 TITLE (8A10)

Card 2 ACCELERATION (6(F6.3,F6.4),8X)

NYFH time-acceleration pairs describing the time-history of the component of ground acceleration along  $\theta = 90^\circ$  are to be specified on these cards, with six pairs per card. Time must be expressed in seconds and accelerations in multiples of g.

## XII. OUTPUT INFORMATION CARDS

### Card 1. OUTPUT CONTROL (NAMELIST: PRINTIT)

- NPRINT: Print interval. Nodal-circle displacement amplitudes and element stress amplitudes are written on TAPE3 every NPRINT time-intervals. If printed output of time history response is required (i.e., NNODE  $\neq$   $\emptyset$  and/or NNEL  $\neq$   $\emptyset$ ), nodal-circle displacements and/or element stresses are also printed every NPRINT time-intervals.
- NNODE: Total number of nodal-circles at which time-history of displacements is to be printed.
- NNEL: Total number of elements at which time-history of stresses is to be printed.
- NANGLE: Total number of different directions around the circumference of a nodal-circle or axisymmetric element at which displacement and stresses are to be printed.

### Card 2. ANGLE SELECTION (8F1 $\emptyset$ . $\emptyset$ )

List of NANGLE values of angles (in degrees) describing directions along the circumference at which displacements and stresses are to be printed. These cards are to be omitted in NANGLE =  $\emptyset^\circ$ .

### Card 3. NODAL CIRCLE SELECTION (16I5)

List of NNODE nodal circle numbers at which displacements are to be printed. These cards are to be omitted if NNODE =  $\emptyset$ .

### Card 4. ELEMENT SELECTION (16I5)

List of NNEL element numbers for which stresses are to be printed. These cards are to be omitted if NNEL =  $\emptyset$ .

## OUTPUT

The following is printed by the program (note that some of these may be suppressed according to the options provided in Cards II and XII).

1. First set of input data: structural and material properties, options, etc.
2. Hydrostatic loads: i.e., equivalent nodal-circle loads due to hydrostatic pressure of the surrounding water and fluids inside the tank. Nodal-circle displacements and element stresses for static loads. Added-mass due to fluids inside the tank.
3. Frequencies and mode shapes of the structure, including the effect of interior fluids but not the effect of water surrounding the structure.
4. Second set of input data: geometric data for the surrounding and interior fluids, structural nodal-points affected by hydrodynamic interaction.
5. The generalized mass matrix and the generalized force vector, including hydrodynamic effects.
6. Third set of input data: response data including number of time steps, time increment, and modal damping ratios, earthquake acceleration data, control data for output of time history of response.
7. Displacements of selected nodal circles (see card group XII), stresses in selected elements along selected angles at instants of time, determined by the print interval NPRINT. The displacements and stresses printed include the static values at the beginning of the earthquake motion.
8. The peak values of displacement amplitudes of each nodal-circle and amplitudes of stress in each element and with time at which they occur during the earthquake. These peak values exclude the static values.

## 9. The following quantities are written on TAPE3:

Logical Record 1: NUMNP, NUMEL, NMODE, DT, NT, NPRINT, IGRAV, NGRD

Starting with Record 2, two records are written for every NPRINT time-intervals for each ground motion component using the following two statements:

```
WRITE (3) X
```

```
WRITE (3) STRESS
```

X and STRESS are one-dimensional arrays, dimensioned properly so that X(3\*I-2), X(3\*I-1) and X(3\*I) are the r, z and  $\theta$ -components, respectively, of the displacement amplitude at nodal-circle I, I=1,...,NUMNP. Similarly, STRESS(6\*N-5), STRESS(6\*N-4), STRESS(6\*N-3), STRESS(6\*N-2), STRESS(6\*N-1) and STRESS(6\*N) are the amplitudes of the six components,  $\sigma^{rr}$ ,  $\sigma^{zz}$ ,  $\sigma^{\theta\theta}$ ,  $\sigma^{rz}$ ,  $\sigma^{r\theta}$  and  $\sigma^{z\theta}$  in the element number N, N=1,2,...,NUMEL.

If IGRAV = 1, the dynamic responses start with the first set of X and STRESS. However, if IGRAV = 2, the first set of X and STRESS is the static response; the dynamic response starts with the second set.

STORAGE REQUIREMENTS

The card storage requirements of the program are separated into fixed and variable parts with the fixed part consisting of instructions, non-subscripted variables, and those arrays which do not depend on the size of the individual problem. The variable part is stored in Array A, which appears in the blank COMMON statement.

The blank COMMON storage requirements of the program can be changed depending on the size of the problem to be solved. This is done by using the RFL job control statement to increase the program size:

```
RFL(MMAX)
```

MMAX (in octal) is the total memory words requested. N=MMAX-45000 is the available memory size for blank COMMON storage.



The value for N must exceed each of the following:

- (1)  $3 \cdot \text{NUMNP} \cdot (4 + \text{MBAND}) + 11 \cdot \text{NUMEL} + 11 \cdot \text{NUMMAT} + \text{NBC} + \text{NPO} + \text{NPI}$
- (2)  $3 \cdot \text{NUMNP} \cdot (8 + \text{MBAND}) + 5 \cdot \text{NUMEL} + 11 \cdot \text{NUMMAT} + \text{NBC} + \text{NMODE} \cdot (\text{NMODE} + 1)$
- (3)  $5 \cdot \text{NUMNP} + (2 + 3 \cdot \text{NUMNP} + \text{NMODE} + 3 \cdot \text{NUINTEX}) \cdot \text{NMODE} + (3 + \text{NEBAND} + \text{NMODE}) \cdot \text{NUMPEX} + 8 \cdot \text{NUELEX} + \text{NUINTEX} + \text{NUFSF} + (1 + \text{NEBAND} + \text{NMODE}) \cdot \text{NUCOF}$
- (4)  $5 \cdot \text{NUMNP} + (2 + 3 \cdot \text{NUMNP} + \text{NMODE}) \cdot \text{NMODE} + 7 \cdot \text{NUELIN} + (4 + 2 \cdot \text{NMODE} + \text{NIBAND}) \cdot \text{NUNPIN}$
- (5)  $5 \cdot \text{NUMNP} + (408 + 3 \cdot \text{NUMNP} + 2 \cdot \text{NMODE}) \cdot \text{NMODE} + 2 \cdot \text{NXFH} + 2 \cdot \text{NYFH} + \text{NT}$
- (6)  $852 + (22 + 4 \cdot \text{NMODE}) \cdot \text{NUMNP} + 805 \cdot \text{NMODE} + 42 \cdot \text{NUMEL} + \text{NMODE} + \text{NNEL} + \text{NANGLE} + 2 \cdot \text{NT}$

where:

- NUMNP: number of nodal circles in the structural idealization
- NUMEL: number of elements in the structural idealization
- NUMMAT: number of different structural materials
- NBC: number of structural displacement constraints in the structural idealization
- NPO: number of nodal circles on the exterior surface of the structure affected by the surrounding water
- NPI: number of nodal circles on the interior surface of the structure affected by the fluids in the tank interior
- $\text{MBAND} = 3 \cdot (\text{MB} + 1)$
- $\text{MB} = \max_i \text{MB}_i, i = 1, \text{NUMEL}$
- $\text{MB}_i$ : difference between the largest and smallest structural nodal-circle numbers for structural element i
- NMODE: number of modes of vibration included
- NUMPEX: number of nodal circles in the exterior water idealization
- NUELEX: number of elements in the exterior water idealization

NUINTEX: number of fluid nodal-circles on the exterior structure-fluid interface  
 NUFSP: number of exterior fluid nodal-circles on the free surface of the fluid  
 NEBAND = NEB + 1  
 $NEB = \max_i NEB_i, i = 1, N U E L E X$   
 $NEB_i$ : difference between the largest and smallest nodal circle numbers for exterior fluid element  $i$   
 NUNPIN: number of nodal circles in the interior fluid idealization  
 NUELIN: number of elements in the interior fluid idealization  
 NIBAND = NIB + 1  
 $NIB = \max_i NIB_i, i = 1, N U E L I N$   
 $NIB_i$ : difference between the largest and smallest nodal circle numbers for interior fluid element  
 NXFH: number of ordinates describing time-history of first ground motion component, along  $\theta = 0^\circ$   
 NYFH: number of ordinates describing time-history of second ground motion component, along  $\theta = 90^\circ$   
 NT: number of integration time steps  
 NNODE: total number of structural nodal-circles at which time-history of displacements is to be printed  
 NNEL: total number of structural elements for which time-history of stresses is to be printed  
 NANGLE: total number of different locations around the circumference at which displacements and stresses are to be printed

If only frequencies and mode shapes are desired along with static analysis, it suffices to check (1) and (2) above.

The computer time required for solution depends on a number of factors. The more important ones are the number of integration time steps (NT), the number of structural nodal circles (NUMNP), the bandwidth (MBAND) of the structural stiffness matrix (the nodal circles should be numbered in a manner which minimizes the bandwidth), the number of structural elements (NUMEL), the number of modes of vibration to be included (NMODE), interval for printing and writing (NPRINT), and the number of nodal-circles (NUNPEX, NUNPIN) and elements (NUELEX, NUELIN) in the idealization of the fluid domain.

APPENDIX B. PROGRAM "ERST" LISTINGS

```

1 PROGRAM ERST(INPUT, OUTPUT, TAPE1, TAPE2, TAPE3, TAPE4, TAPE6=OUTPUT,
1 TAPE7, TAPE8, TAPE9)

```

```

C *****
C EARTHQUAKE RESPONSE OF SEA-BASED STORAGE TANKS
C *****

```

```

C THIS PROGRAM SHOULD BE COMPILED USING THE FTN "STATIC" OPTION
C WHEREBY MTOP CAN BE ADJUSTED DYNAMICALLY AT RUN TIME VIA THE CM
C OR RFL PARAMETER ON THE JOB CARD.

```

```

C COMMON/FCNST/PI, ROW, WLD
C COMMON/CNTRL/NUMNP, NANGLE, MBAND, NBC, NF, NPO, NPI, TRACE, READFRQ
C DIMENSION HED(8)
C COMMON A(20000)
C LOGICAL READFRG, PLOTANK, PLOTMOD
C LOGICAL PLOTACC
C 1 NAMELIST /TANK/ NUMNP, NUMEL, NUMMAT, NMODE, WLD, WLI, NPO, NPI, IGRAV,
1 READFRG, PLOTANK, PLOTMOD
C NAMELIST /EXTFLD/ NUMPEX, NUELEX, NUNTEX, NUFSEF, NUCCOF
C NAMELIST /INTFLD/ NUMPIN, NUELIN, NUNLIN, NUVELOIL, ROIL
C NAMELIST /RESPNS/ NGRD, NT, DT, NXFH, NYFH, PLOTACC
C NAMELIST /PRINTIT/ NPRINT, NNODE, NNEL, NANGLE
C DATA PLOTANK/ F. /, PLOTMOD/ F. /, PLOTACC/ F. /, READFRG/ F. /
C PI=3.14159265
C ROW=0.0625/32.2

```

```

C GET THE AVAILABLE BLANK COMMON MEMORY SIZE

```

```

C CALL PFL(MTOP)
C MSTOP = MTOP - LOGF(A(1)) + 1

```

```

C READ AND PRINT OF CONTROL INFORMATION

```

```

C READ 1000, HED
C READ TANK
C PRINT TANK
C PRINT 2000, HED, NUMNP, NUMEL, NUMMAT, NMODE, WLD, WLI, NPO, NPI

```

```

C READ DATA AND DETERMINE ELEMENT PROPERTIES

```

```

C N2=1+NUMNP
C N3=N2+NUMNP
C N4=N3+5*NUMEL
C N5=N4+NUMMAT*9
C N6=N5+NUMMAT
C N8=N6+NUMMAT
C NEG=3*NUMNP
C N9=N8+NEG
C CALL MSCHECK(MSTOP, N9+NUMNP, "LAYOUT")
C CALL LAYOUT(A(1), A(N2), A(N3), A(N4), A(N5), A(N6), A(NB), A(N9),
1 NUMMAT, NUMEL, PLOTANK)
C NF=0
C IF(IGRAV.EQ.1) NF=1

```

```

120 CALL ELEMENT(A(1), A(N2), A(N3), A(N4), A(N5), A(N6), A(NB), NF, NUMEL)

```

```

C FORM TOTAL MASS AND STIFFNESS MATRICES

```

85

```
60 C
    N9=NB+NBC
    N10=N9+NEG
    N11=N10+NEG
    N12=N11+(NEG*MBAND)
    N13=N12+NPO
    CALL MSCHECK(MSTOR,N13+NPI,"TOTAL")
    CALL TOTAL(A(1),A(N2),A(NB),A(N9),A(N10),A(N11),A(N12),A(N13),WLO
    1 ,WLI,NPO,NEG,MBAND,NUMEL,IGRAV)
    C
    C SOLVE FOR STATIC LOADS
    C
    C NUM=6*NUMEL
    IF(NF.NE.O) GO TO 150
    N14=N13+NPI
    CALL MSCHECK(MSTOR,N14+NUM,"STATIC")
    CALL STATIC(A(NB),A(N9),A(N10),A(N11),A(N14),NEG,MBAND
    1,NUM,NUMEL)
    150 IF(NF.EQ.O) GO TO 200
    C
    C MODE SHAPES AND NATURAL FREQUENCIES
    C
    N12=N11+NMODE
    N13=N12+(NEG*MBAND)
    N14=N13+NEG
    N15=N14+NEG
    N16=N15+NEG
    N17=N16+NEG
    CALL MSCHECK(MSTOR,N17+NMODE*#2,"EIGEN")
    CALL EIGEN(A(NB),A(N9),A(N10),A(N11),A(N12),A(N13),A(N1
    14),A(N15),A(N16),A(N17),NEG,NMODE,MBAND,A(1),A(N2),PLOTMOD)
    C
    C SOLVE FOR HYDRODYNAMIC RESPONSE (INCOMPRESSIBLE FLUID)
    C
    N13=N12+(NEG*NMODE)
    NTEMP=N10-1
    WRITE (1) (A(I),I=N9,NTEMP)
    NTEMP=N13-1
    WRITE (1) (A(I),I=N11,NTEMP)
    BACKSPACE 1
    BACKSPACE 1
    N4=N3+NEG
    N5=N4+NMODE
    N6=N5+(NEG*NMODE)
    N7=N6+NMODE
    N8=N7+(NMODE*NMODE)
    NTEMP=N4-1
    READ(1) (A(I),I=N3,NTEMP)
    NTEMP=N6-1
    READ(1) (A(I),I=N4,NTEMP)
    BACKSPACE 1
    BACKSPACE 1
    C
    C WATER TREATED AS A FINITE-ELEMENT SYSTEM
    C
    C READ EXTFLD
    C PRINT EXTFLD
```

86

```

115      PRINT 2040
      C
      C
      C
120      READ AND PRINT WATER ELEMENT PROPERTIES
      PRINT 2050, NUNPEX, NUELEX, NUINTEX, NUFSE, NUCOF
      N9=NB+NMODE*NUINTEX*3
      N10=N9+NUINTEX
      N11=N10+NUNPEX
      N12=N11+NUNPEX
      N13=N12+8*NUELEX
      CALL MSCHECK(MSTOR, N13+NUFSF, "EXT")
      CALL EXT(A(N9), A(N10), A(N11), A(N12), A(N13),
1      NUNPEX, NUELEX, NEBAND, NUINTEX, NUCOF, WLO)
      C
130      SOLVE FOR RESPONSES OF WATER FINITE-ELEMENT SYSTEM
      C
      C
      NEGF=NUNPEX+NUCOF
      N14=N13+NUFSF
      N15=N14+NEGF
      N16=N15+NEGF*NMODE
      N17=N16+NEGF*NEBAND
      CALL MSCHECK(MSTOR, N17, "SOLEXT")
      CALL SOLEXT(A(N3), A(N4), A(N5), A(N6), A(N7), A(N8), A(N9),
1      A(N10), A(N11), A(N12), A(N13), A(N14), A(N15), A(N16),
2      NMODE, NEG, NUNPEX, NUELEX, NUINTEX, NUFSE, NEBAND, NEGF)
      C
140      INTERIOR FLUIDS TREATED AS A FINITE-ELEMENT SYSTEM
      C
      C
      READ INTFLD
      PRINT INTFLD
      N9=NB+NUNPIN
      N10=N9+NUNPIN
      N11=N10+NUNPIN
      N12=N11+4*NUELIN
      N13=N12+NUELIN
      N14=N13+NUELIN
      N15=N14+NUELIN
      CALL MSCHECK(MSTOR, N15, "INT")
      CALL INT(A(N8), A(N9), A(N10), A(N11), A(N12), A(N13), A(N14),
1      ROIL, NUJINTIN, NUELIN, NUNPIN, NUELOIL)
      CALL BNDWTH(A(N8), A(N9), A(N11), A(N12), A(N14), NUELIN, NUNPIN,
1      NIBAND)
      N13=N12+NMODE*NUNPIN
      N14=N13+NUNPIN*NIBAND
      N15=N14+NUNPIN
      N16=N15+NUNPIN*NMODE
      CALL MSCHECK(MSTOR, N16, "SOLINT")
      CALL SOLINT(A(N5), A(N6), A(N7), A(N8), A(N9), A(N10), A(N11), A(N12),
1      A(N13), A(N14), A(N15), ROIL, NUELIN, NIBAND, NUNPIN, NEG, NMODE,
2      NUELOIL)
      C
165      TIME RESPONSE OF MODAL DISPLACEMENTS
      C
      C
      READ RESPNS
      PRINT RESPNS
      IF (NGRD.EQ.1) PRINT 2020, NT, DT
      IF (NGRD.EQ.2) PRINT 2021, NT, DT
170

```

87

```
175 NG=NGRD
    NBUF=200*NMODE
    N10=NB
    N11=N10+NMODE
    NTAPE=2
179 N12=N11+NXFH
    N13=N12+NXFH
    N14=N13+NMODE
    N15=N14+NMODE
    N16=N15+NMODE
    N17=N16+NMODE
    N18=N17+NMODE
    N19=N18+NBUF
    N20=N19+NT
    N21=N20+NBUF
    N22=N21+NMODE*NMODE
    CALL MSCHECK(MSTOR,N22,"TSTEP")
    CALL TSTEP(A(N4),A(N6),A(N7),A(N10),A(N11),A(N12),A(N13),A(N14),
1 A(N15),A(N16),A(N17),A(N18),A(N19),A(N20),A(N21),
2 NMODE,NT,DT,NXFH,NBUF,NBLOCK,NGRD,NTAPE,NG,PLOTACC)
    IF (NG.EQ.1) GO TO 185
    NG=1
    NTAPE=7
    NXFH=NYFH
    GO TO 179
C
C
C SUPERPOSITION OF MODES AND EVALUATION OF STRESSES
C
185 CONTINUE
    READ PRIN1IT
    PRINT PRIN1IT
    IF (NANGLE.EQ.0) NANGLE=1
    N2=N1+NANGLE
    N3=N2+NMODE
    N4=N3+(NEG*NMODE)
    READ (1)
    NTEMP=N4-1
    READ(1) (A(I),I=N2,NTEMP)
    N5=N4+NUM
    N7=N6+NNEL
    N8=N7+NBUF
    N9=N8+NBUF
    N10=N9+NMODE
    N11=N10+NMODE
    N12=N11+NEQ
    N13=N12+NEQ
    N14=N13+6
    N15=N14+6
    N16=N15+12*10
    N17=N16+6*12*10
    N18=N17+NUM
    N19=N18+NEQ
    N20=N19+NEQ
    N21=N20+NUM
    N22=N21+NEQ
    N23=N22+NUM
```



```

230 N24=N23+NEQ
    N25=N24+NUM
    N26=N25+NEQ
    N27=N26+NUM
    N28=N27+NUM
    N29=N28+NUMNP
    N30=N29+NUMNP*NMODE
    N31=N30+NT
    N32=N31+NT
    N33=N32+NBUF
    N34=N33+NBUF
    N35=N34+NMODE
    N36=N35+NMODE
    CALL MSCHECK(MSTOR,N36,"RESPON")
    CALL RESPON(A(1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(N8),
    1 A(N9),A(N10),A(N11),A(N12),A(N13),A(N14),A(N15),A(N16),A(N17),
    2 A(N18),A(N19),A(N20),A(N21),A(N22),A(N23),A(N24),A(N25),A(N26),
    3 A(N27),A(N28),A(N29),A(N30),A(N31),A(N32),A(N33),A(N34),A(N35),
    3 NMODE,NEQ,NANGLE,NPRINT,NNODE,NNEL,NUMNP,NUMEL,NUM,
    4 NBLOCK,NBUF,NBUF,IGRAV,DT,NT,NGRD)
240 200 IF(IGRAV.NE.2) GO TO 250
    IF(NF.GE.1) GO TO 250
    NF=1
    GO TO 120
245 250 PRINT 3000
    1000 FORMAT (8A10)
    2000 FORMAT (1H1,8A10//
    1 35H NUMBER OF NODAL POINTS----- I4 /
    2 35H NUMBER OF ELEMENTS----- I4 /
    3 35H NUMBER OF DIFF. MATERIALS----- I4 /
    4 35H NUMBER OF EIGENMODES----- I4 /
    5 35H WAER LEVEL OUTSIDE TANK----- F10.3,3HFT. /
    6 35H WAER LEVEL INSIDE TANK----- F10.3,3HFT. /
    7 35H NUMBER OF PRESSURE POINTS OUTSIDE- I4 /
    8 35H NUMBER OF PRESSURE POINTS INSIDE-- I4 /
    2020 FORMAT (1H1/46H ONLY ONE COMPONENT OF GROUND MOTION INCLUDED /
    1 * NO. OF TIME STEPS SELECTED =*,I7/* DT IN SECONDS =*,F10.4/)
    2021 FORMAT (1H1/42H TWO COMPONENTS OF GROUND MOTION INCLUDED /
    1 * NO. OF TIME STEPS SELECTED =*,I7/* DT IN SECONDS =*,F10.4/)
    2040 FORMAT (1H1/41H INTERACTION PROBLEM IS SOLVED BY F.E.M. /)
    2050 FORMAT (//35H NUMBER OF NODAL POINTS OF FLUID = ,I10,
    1 /35H NUMBER OF ELEMENT OF FLUID = ,I10,
    2 /35H NUMBER OF N.P. ON THE INTERFACE = ,I10,
    3 /38H NUMBER OF N.P. ON THE FREE SURFACE = ,I7,
    4 /49H NUMBER OF POWER SERIES TERMS FOR SUPERELEMENT = ,I2)
270 3000 FORMAT (///17H END OF PROBLEM )
    STOP
    END

```

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ENTRY POINTS DEF LINE REFERENCES  
22633 ERST 1

VARIABLES	SN	TYPE	RELOCATION	ARRAY	REFS	15	31	8*51	7*55	8*65	5*74	12*87
O A		REAL	/ /		94	96	5*126	14*137	7*153	5*155	11*162	15*189
24642 DT		REAL			35*243	DEFINED	105	107	209			
24731 HED		REAL			REFS	22	170	171	189	243		
24674 I		INTEGER		ARRAY	REFS	14	38	DEFINED	35			
					REFS	94	96	105	107	209		
24625 IGRAV		INTEGER			DEFINED	94	54	65	243	81	87	
2		INTEGER	CNTRL		REFS	18	62	65	74			
24711 MBAND		INTEGER			REFS	13	243	73	86	125	136	152
24711 MBUF		INTEGER			REFS	189	243	DEFINED	31			
24651 MSTOR		INTEGER			REFS	50	64					
					161	188	242					
24650 MTOP		INTEGER			REFS	30	31					
1		INTEGER	CNTRL		REFS	13	23	203	204	243		
					DEFINED	203						
3		INTEGER	CNTRL		REFS	13	59					
24712 NBLOCK		INTEGER			REFS	189	243	189	213	214	238	239
24702 NBUF		INTEGER			REFS	184	186					
					243	DEFINED	173					
24676 NEBAND		INTEGER			REFS	126	135	137	62	65	74	81
24660 NEG		INTEGER			REFS	49	60	61	87	92	99	101
					82	83	84	85	218	224	225	227
					137	162	206	217	48			
24677 NEGF		INTEGER			229	231	243	DEFINED	137	DEFINED	131	
4		INTEGER	CNTRL		REFS	133	134	135	76	250		
					REFS	13	53	71				
					DEFINED	53	54	251				
24701 NG		INTEGER			REFS	189	192	DEFINED	172	193	243	
24640 NGRD		INTEGER			REFS	22	170	171	172	189		
24700 NIBAND		INTEGER			REFS	155	158	162				
24623 NMODE		INTEGER			REFS	18	38	80	86	87	92	100
					101	102	2*103	120	134	137	157	160
					162	173	175	179	180	181	182	183
					2*187	189	205	206	215	216	235	240
					241	243						
24647 NNEL		INTEGER			REFS	23	212	243				
24646 NNODE		INTEGER			REFS	23	211	243				
6		INTEGER			REFS	13	18	38	64	72		
5		INTEGER	CNTRL		REFS	13	18	38	63	65		
24645 NPRINT		INTEGER			REFS	23	243					
24641 NT		INTEGER			REFS	22	170	171	185	189	236	237
					243							
24703 NTAPE		INTEGER			REFS	189	DEFINED	176	194			
24673 NTEMP		INTEGER			REFS	94	96	105	107	209		
					DEFINED	93	95	104	106	208		
24632 NUCOF		INTEGER			REFS	20	119	126	131	137		
24627 NUILEX		INTEGER			REFS	20	119	124	126	151		
24634 NUIELIN		INTEGER			REFS	21	148	149	150	151	153	155
					162							
24636 NUIELOIL		INTEGER			REFS	21	153	162	193			
24631 NUIFSF		INTEGER			REFS	20	119	125	132	137		
24630 NUIINTEX		INTEGER			REFS	20	119	120	121	126		
24635 NUIINTIN		INTEGER			REFS	21	153	162	193			

VARIABLES	SN	TYPE	RELOCATION	REFS	73	74	210	223	226	228	230
24666	NUM	INTEGER		232	243	243	DEFINED	70	226	228	230
24621	NUMEL	INTEGER		18	38	38	44	51	55	65	70
24622	NUMMAT	INTEGER		74							
0	NUMNP	INTEGER	CNTRL	18	38	38	45	46	47	51	50
24626	NUMPEX	INTEGER		13	18	18	38	42	43	48	50
24633	NUMPIN	INTEGER		234	243	243					
24643	NXFH	INTEGER		20	119	119	122	123	126	131	137
24644	NYFH	INTEGER		21	145	145	146	147	153	155	157
24662	N10	INTEGER		158	160	160	162				
				REFS	177	177	178	189	DEFINED	195	
				REFS	195	195					
				REFS	61	65	74	87	93	122	126
				REFS	147	153	162	175	189	216	243
				REFS	60	121	146	174	215		
				DEFINED							
24663	N11	INTEGER		REFS	62	65	74	80	87	96	123
				REFS	126	148	153	155	162	177	189
				REFS	217	243	61	122	147	175	216
				REFS	63	81	81	87	92	124	126
24664	N12	INTEGER		REFS	137	153	155	157	162	178	189
				REFS	218	243	62	80	123	148	177
				REFS	217						
24665	N13	INTEGER		REFS	64	65	72	82	87	95	125
				REFS	132	137	150	153	158	162	179
				REFS	189	243	DEFINED	63	81	92	124
				REFS	149	178	218				
24667	N14	INTEGER		REFS	73	74	83	87	133	137	151
				REFS	153	159	162	180	189	220	243
				REFS	72	82	132	150	158	179	219
				DEFINED							
24670	N15	INTEGER		REFS	84	87	134	137	152	160	162
				REFS	181	221	243	DEFINED	83	133	151
				REFS	159	220					
24671	N16	INTEGER		REFS	85	87	135	137	161	182	189
				REFS	222	243	84	134	160	181	221
				REFS	86	87	136	183	189	223	243
24672	N17	INTEGER		DEFINED							
				REFS	85	135	182	222	DEFINED	183	223
24704	N18	INTEGER		REFS	184	189	224	243	DEFINED	184	224
24705	N19	INTEGER		REFS	185	189	225	243	DEFINED	184	224
24652	N2	INTEGER		REFS	43	51	55	65	87	205	209
				REFS	243	42	204				
				DEFINED							
24706	N20	INTEGER		REFS	186	189	226	243	DEFINED	185	225
24707	N21	INTEGER		REFS	187	189	227	243	DEFINED	186	226
24710	N22	INTEGER		REFS	188	228	243	DEFINED	187	227	
24713	N23	INTEGER		REFS	229	243	DEFINED	228			
24714	N24	INTEGER		REFS	230	243	DEFINED	229			
24715	N25	INTEGER		REFS	231	243	DEFINED	230			
24716	N26	INTEGER		REFS	232	243	DEFINED	231			
24717	N27	INTEGER		REFS	233	243	DEFINED	232			
24720	N28	INTEGER		REFS	234	243	DEFINED	233			
24721	N29	INTEGER		REFS	235	243	DEFINED	234			
24653	N3	INTEGER		REFS	44	51	55	99	105	137	206
				REFS	243	43	205				
				DEFINED							
24722	N30	INTEGER		REFS	236	243	DEFINED	235			
24723	N31	INTEGER		REFS	237	243	DEFINED	236			
24724	N32	INTEGER		REFS	238	243	DEFINED	237			
24725	N33	INTEGER		REFS	239	243	DEFINED	238			
24726	N34	INTEGER		REFS	240	243	DEFINED	239			

VARIABLES	SN	TYPE	RELOCATION	REFS	241	243	DEFINED	240	104	107	137
24727 N35		INTEGER		REFS	242	DEFINED	241	240	100	107	137
24730 N36		INTEGER		REFS	45	51	55	100	44	99	206
24654 N4		INTEGER		REFS	189	210	243	DEFINED	137	162	211
24655 N5		INTEGER		REFS	46	51	55	101			
24656 N6		INTEGER		REFS	243	45	100	210			
24675 N7		INTEGER		REFS	47	51	55	102	106	137	162
24657 N8		INTEGER		REFS	189	212	243	46	101	211	
				DEFINED	102	189	162	213	213	243	
24661 N9		INTEGER		REFS	49	51	55	59	65	74	87
				REFS	120	145	153	155	162	174	214
				REFS	137	47	103	213			
				DEFINED	50	51	60	65	74	87	94
				REFS	121	137	146	153	155	162	215
				REFS	243	49	59	120	145	214	
				DEFINED	12	DEFINED	25				
0 PI		REAL	FCONST	REFS	17	22	189	DEFINED	24		
24301 PLOTACC		LOGICAL		REFS	16	18	51	DEFINED	24		
24277 PLOTANK		LOGICAL		REFS	16	18	87	DEFINED	24		
24300 PLOTMOD		LOGICAL		REFS	13	16	18	DEFINED	24		
10 READFRG		LOGICAL		REFS	21	153	162	DEFINED	24		
24637 ROIL		REAL		REFS	12	DEFINED	26				
1 ROW		REAL		REFS	13						
7 TRACE		REAL		REFS	18	38	65	65	126		
24624 WLI		REAL		REFS	18	18	38				
2 WLO		REAL		REFS	12	18	38				
				REFS	12	18	38				
FILE NAMES		MODE									
0 INPUT		MIXED									
2054 OUTPUT		MIXED									
				READS	36	113	143	168	201	169	170
				WRITES	37	114	115	119	144		
					171						
4130 TAPE1		UNFMT		WRITES	253	READS	105	107	207	209	
				MOTION	94	108	109				
					97						
6204 TAPE2											
10260 TAPE3											
12334 TAPE4											
2054 TAPE6											
14410 TAPE7											
16464 TAPE8											
20540 TAPE9											
EXTERNALS		TYPE	ARGS	REFERENCES							
BNDWTH			8	155							
EIGEN			16	87							
ELEMENT			9	55							
EXT			11	126							
INT			12	153							
LAYOUT			11	51							
MSCHECK			3	50							
				242							
PFL			1	30							
RESPON			51	243							
SOLEXT			22	137							
SOLINT			18	162							
STATIC			9	74							
TOTAL			15	65							
TSTEP			26	189							

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
LOC	INTEGER	1	INTRIN	31

NAMELISTS	DEF LINE	REFERENCES
EXTFLD	20	113
INTFLD	21	143
PRINTIT	23	201
RESPONS	22	168
TANK	18	36

STATEMENT LABELS	DEF LINE	REFERENCES
22706	120	55
22767	150	76
23316	179	177
23370	185	200
23546	200	249
23553	250	253
24447	1000	254
24451	2000	255
24516	2020	264
24533	2021	266
24550	2040	268
24557	2050	269
24610	3000	274

COMMON BLOCKS	LENGTH
FCNST	3
CNTRL	9
/ /	20000

STATISTICS	PROGRAM LENGTH	REFERENCES
PROGRAM LENGTH	3003B	1539
BUFFER LENGTH	21762B	9202
SCM LABELED COMMON LENGTH	14B	12
SCM BLANK COMMON LENGTH	47040B	20000
52000B SCM USED		

```

1      *DECK MSCHECK
      SUBROUTINE MSCHECK(MMAX,MNEED,MESSAGE)
      IF (MMAX.GE.MNEED) RETURN
      PRINT 5, MESSAGE, MNEED-MMAX
      5 FORMAT (// * --- NOT ENOUGH MEMORY FOR SUBROUTINE - *,A10,
1         /* --- NEED*,I9,* MORE WORDS*
2         /* --- PROGRAM STOPPED*//)
      STOP "NOT ENOUGH MEMORY"
      END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES				
3 MSCHECK	2	3				
VARIABLES	SN	TYPE	RELOCATION	REFS	DEFINED	DEFINED
0 MESSAGE		INTEGER	F.P.	4	4	2
0 MMAX		INTEGER	F.P.	3	4	2
0 MNEED		INTEGER	F.P.	3	4	2

94

FILE NAMES	MODE	WRITES	
OUTPUT	FMT	4	
STATEMENT LABELS	DEF LINE	REFERENCES	
21 5	5	4	
FMT			
STATISTICS			
PROGRAM LENGTH	41B	33	
52000B	SCM USED		

```

1      SUBROUTINE LAYOUT(R,Z,IX,E,RO,WANG,NEBC,CODE,NUMMAT,NUMEL,PLOTT)
C*****
C      GEOMETRY AND MATERIAL PROPERTIES OF STRUCTURE ARE READ IN.
C      NODAL POINTS CAN BE GENERATED AT EQUAL INTERVAL DR IN LAYERS.
C*****
C
C      LOGICAL PLOTT
DIMENSION R(1),Z(1),NEBC(1),CODE(1),IX(NUMEL,1),E(9,1),RO(1),WANG(
1  1),NPTS(100),IFIG(100),RPL0T(5,100),ZPLOT(5,100)
COMMON/CNTRL/NUMNP,ANGLE,MBAND,NBC
DATA XMAT/6HISOTRO/

C      READ AND PRINT OF MATERIAL PROPERTIES
C
C      DO 110 M=1,NUMMAT
READ 1001, MTYPE,XXMA
IF (XXMA.NE.XMAT) GO TO 109
READ 1010, EE,EEU,RO(MTYPE)
PRINT 2006, MTYPE,EE,EEU,RO(MTYPE)
WANG(MTYPE)=0.
DO 102 I=1,9
IF (I.LE.3) E(I,MTYPE)=EE
IF (I.GT.3.AND.I.LE.6) E(I,MTYPE)=EEU
IF (I.GT.6) E(I,MTYPE)=EE/(2.*(1.+EEU))
102 CONTINUE
GO TO 110
109 READ 1011, (E(I,MTYPE),I=1,9),RO(MTYPE),WANG(MTYPE)
PRINT 2007, MTYPE,(E(I,MTYPE),I=1,9),RO(MTYPE),WANG(MTYPE)
110 CONTINUE

C      READ AND PRINT NODAL POINT DATA
C
C      PRINT 2004
L=0
NBC=0
120 READ 1002, N,CODE(N),R(N),Z(N),MOD,NLIM,FACR,FACZ
L1=L+1
IF (N-L1) 190,170,130
130 IF (L.LE.0) GO TO 180
DIV=N-L
DR=(R(N)-R(L))/DIV
DZ=(Z(N)-Z(L))/DIV
M=N-1
DO 140 K=L1,M
CODE(K)=0.0
R(K)=R(K-1)+DR
140 Z(K)=Z(K-1)+DZ
GO TO 170
150 L1=N+1
IF (FACR.LE.0.0) FACR=1.0
IF (FACZ.LE.0.0) FACZ=1.0
PRINT 2100, MOD,NLIM,FACR,FACZ
160 N=N+1
N1=N-MOD
N2=N1-MOD
IF (N1.LE.0.OR.N2.LE.0) GO TO 200

```

```

60      CODE(N)=0.0
        R(N)=R(N1)+FACR*(R(N1)-R(N2))
        Z(N)=Z(N1)+FACZ*(Z(N1)-Z(N2))
        IF (N.LT.NLIM) GO TO 160
        MOD=0
170     L=N
        PRINT 2002, (K, CODE(K), R(K), Z(K), K=L1, N)
        COD=CODE(N)
        IF (COD.EQ.0.0) GO TO 175
        D=100
        DO 172 J=1,3
        IF (COD.LT.D) GO TO 172
        NBC=NBC+1
        NEBC(NBC)=3*N-3+J
        COD=COD-D
172     D=D/10.
175     IF (MOD.GT.0) GO TO 150
        IF (N-NUMNP) 120,220,210
180     PRINT 2130
        STOP
190     PRINT 2140, N
        STOP
200     PRINT 2150
        STOP
210     PRINT 2160, N, NUMNP
        STOP
220     CONTINUE
85     C
        C READ AND PRINT OF ELEMENT PROPERTIES
        C
        PRINT 2001
        N=0
        MBAND=0
90     230 READ 1003, M, (IX(M,I), I=1,5)
        240 N=N+1
        IF (M.EQ.N) GO TO 260
        DO 250 I=1,4
        IX(N,I)=IX(N-1,I)+1
        IX(N,5)=IX(N-1,5)
95     260 PRINT 2003, N, (IX(N,I), I=1,5)
        IF (N.EQ.NUMEL) GO TO 270
        IF (N.EQ.M) GO TO 230
        GO TO 240
100    270 IF (.NOT.PLOTT) GO TO 280
        DO 278 N=1, NUMEL
        NPTS(N)=5
        IFIG(N)=2
        DO 275 I=1,4
        RPLOT(I,N)=R(IX(N,I))
105    275 ZPLOT(I,N)=Z(IX(N,I))
        RPLOT(5,N)=RPLOT(1,N)
        ZPLOT(5,N)=ZPLOT(1,N)
        CALL GPLT
        CALL MULTPLT(RPLOT,ZPLOT,NPTS,NUMEL,1,5,100,"R-AXIS",6,
110    1 "Z-AXIS",6,9,IFIG)
        CALL PLOT(0.,0.,999)
        C DETERMINE BAND WIDTH
        C

```



```

115      280 MB=0
          DO 290 N=1,NUMEL
            DO 290 I=1,4
            DO 290 J=1,4
            MM=IABS(IX(N,I)-IX(N,J))
            IF (MM.GT.MB) MB=MM
          290 CONTINUE
          MBAND=3*MB+3
          1001 FORMAT (I5,5X,A6)
          1002 FORMAT (I5,F5.0,2F10.0,2I5,2F10.0)
          1003 FORMAT (6I5)
          1010 FORMAT (3F10.0)
          1011 FORMAT (6F10.0/5F10.0)
          2001 FORMAT (1H1,*ELEMENT NO.
          2002 FORMAT (17,F10.2,2F10.3)
          2003 FORMAT (11I3,4I6,1I2)
          2004 FORMAT (3BHIND,PT,RESTRAINT R-ORD Z-ORD //)
          2006 FORMAT (///16H MATERIAL NUMBER ,I3,15H ISOTROPIC //,
          1 6H E =,F16.6,6HK/SFT./6H NU =,F16.6/6H RHO =,F16.6,
          2 16H K-SEC**2/FT.**4//)
          2007 FORMAT (///16H MATERIAL NUMBER I1, 17H ORTHOTROPIC//
          1 6H EN =,F16.6,4X,6H ES =,F16.6,4X,6H ET =,F16.6,6HK/SFT.//
          2 6H NUNTS=,F16.6,4X,6H NUNT=,F16.6,4X,6H NUST=,F16.6/
          3 6H GNS=,F16.6,4X,6H GNT=,F16.6,4X,6H GST=,F16.6/
          4 4HORO= F16.6,16H K-SEC**2/FT.**4//
          5 12H ANGLE BELT=,F16.6)
          2100 FORMAT (21H GENERATION WITH MOD=I3,3X,6H MLIM=I4,3X,6H FACR=F10.5,
          1 3X,6H FACZ=F10.5)
          2130 FORMAT (28H FIRST JOINT CARD IS MISSING)
          2140 FORMAT (31H COORDINATE CARD FOR JOINT NO. I5,16H NOT IN SEQUENCE)
          2150 FORMAT (42H INSUFFICIENT INFORMATION TO GENERATE MESH)
          2160 FORMAT (14H JOINT NUMBER I5,21H EXCEEDS GIVEN NUMNP=I5)
          RETURN
          END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION		REFERENCES	
3 LAYOUT	1	147	ARRAY	F. P.	ARRAY	F. P.
VARIABLES	SN	TYPE	ARRAY	F. P.	ARRAY	F. P.
1043 COD	REAL	REAL	66	69	66	69
0 CODE	REAL	REAL	9	42	9	42
1044 D	REAL	REAL	69	47	69	47
1035 DIV	REAL	REAL	42	48	42	48
1036 DR	REAL	REAL	47	REFS	47	REFS
1037 DZ	REAL	REAL	48	REFS	48	REFS
0 E	REAL	REAL	9	REFS	9	REFS
1023 EE	REAL	REAL	20	REFS	20	REFS
1024 EEU	REAL	REAL	20	REFS	20	REFS
1032 FACR	REAL	REAL	51	REFS	51	REFS
			72	REFS	72	REFS
			65	REFS	65	REFS
			64	REFS	64	REFS
			72	REFS	72	REFS
			65	REFS	65	REFS
			73	REFS	73	REFS
			41	REFS	41	REFS
			67	REFS	67	REFS
			23	REFS	23	REFS
			19	REFS	19	REFS
			19	REFS	19	REFS
			37	REFS	37	REFS
			24	REFS	24	REFS
			51	REFS	51	REFS
			53	REFS	53	REFS
			25	REFS	25	REFS
			25	REFS	25	REFS
			59	REFS	59	REFS
			25	REFS	25	REFS
			19	REFS	19	REFS
			37	REFS	37	REFS
			46	REFS	46	REFS

VARIABLES	SN	TYPE	RELOCATION	REFS	52	53	60	DEFINED	37	52
1033	FACZ	REAL		REFS	2*23	3*24	2*25	28	29	91
1025	I	INTEGER		REFS	2*106	2*107	119	DEFINED	22	28
				REFS	94	97	105	117		
1214	IFIG	INTEGER	ARRAY	REFS	9	111	DEFINED	104	106	107
0	IX	INTEGER	ARRAY	REFS	9	95	96	97		
				REFS	1	91	95	96		
1045	J	INTEGER		DEFINED	71	119	DEFINED	68	118	
1040	K	INTEGER		REFS	46	2*47	2*48	4*64	DEFINED	45
1026	L	INTEGER		REFS	38	40	41	42	43	64
				REFS	35	63				
1034	L1	INTEGER		REFS	39	45	64	DEFINED	38	50
1020	M	INTEGER		REFS	45	91	93	99	DEFINED	16
				REFS	91					44
1046	MB	INTEGER		REFS	120	122	DEFINED	115	120	
2	MBAND	INTEGER		REFS	11	DEFINED	90	122		
1047	MM	INTEGER	CNTRL	REFS	2*120	DEFINED	119			
1030	MDD	INTEGER		REFS	53	55	56	74	DEFINED	37
1021	MTYPE	INTEGER		REFS	19	2*20	21	23	24	25
				REFS	4*29	17				62
				REFS	3*37	39	41	42	43	3*28
1027	N	INTEGER		REFS	54	58	59	60	61	50
				REFS	65	71	75	82	92	64
				REFS	2*96	98	99	103	104	2*95
				REFS	2*108	2*119	DEFINED	37	54	2*106
				REFS	102	116				89
1	NANGLE	INTEGER	CNTRL	REFS	11			DEFINED	36	70
3	NBC	INTEGER	CNTRL	REFS	11	70	71	DEFINED		
0	NEBC	INTEGER	ARRAY	REFS	9	DEFINED	1	71		
1031	NLIM	INTEGER		REFS	53	61	DEFINED	37		
1050	NPTS	INTEGER	ARRAY	REFS	9	111	DEFINED	103		
0	NUHEL	INTEGER		REFS	9	98	102	111	116	
				REFS	1					
0	NUMMAT	INTEGER	F.P.	DEFINED	16	DEFINED	1			
0	NUMNP	INTEGER	F.P.	REFS	11	75	82			
1041	N1	INTEGER	CNTRL	REFS	56	57	2*59	2*60	DEFINED	55
1042	N2	INTEGER		REFS	57	59	60	DEFINED	56	
0	PLOTT	LOGICAL	F.P.	REFS	8	101	DEFINED	1		
0	R	REAL	F.P.	REFS	9	2*42	47	3*59	64	106
				REFS	1	37	47	59		
0	RO	REAL	ARRAY	DEFINED	9	20	29	DEFINED	1	19
1360	RPLOT	REAL	ARRAY	REFS	9	108	111	DEFINED	106	108
0	WANG	REAL	ARRAY	REFS	9	29	DEFINED	1	21	28
472	XMAT	REAL		REFS	18	DEFINED	12			
1022	XX1A	REAL		REFS	18	DEFINED	17			
0	Z	REAL	ARRAY	REFS	9	2*43	48	3*60	64	107
				REFS	1	37	48	60		
2344	ZPLOT	REAL	ARRAY	DEFINED	1	109	111	DEFINED	107	109
				REFS	9					
FILE NAMES	MODE									
INPUT	FMT		READS	17	19	28	37	91		
OUTPUT	FMT		WRITES	20	29	34	53	64	76	78
			82	88	97					80

EXTERNALS      TYPE      ARGS      REFERENCES  
 MULTPLT      13      0      111  
 OPLT      0      0      110

EXTERNALS PLOT TYPE ARGS REFERENCES

INLINE FUNCTIONS TYPE ARGS DEF LINE REFERENCES

IABS INTEGER 1 INTRIN 119

STATEMENT LABELS DEF LINE REFERENCES

0	102		26	22	
56	109		28	18	
100	110		30	16	27
106	120		37	75	
0	130	INACTIVE	40	39	
0	140		48	45	
152	150		50	74	
164	160		54	61	
207	170		63	39	49
250	172		73	68	69
254	175		74	66	
261	180		76	40	
264	190		78	39	
267	200		80	57	
272	210		82	75	
275	220		84	75	
301	230		91	99	
316	240		92	100	
0	250		95	94	
336	260		97	93	
357	270		101	98	
0	275		107	105	
0	278		109	102	
415	280		115	101	
0	290		121	116	117
636	1001	FMT	123	17	118
640	1002	FMT	124	37	
644	1003	FMT	125	91	
646	1010	FMT	126	19	
650	1011	FMT	127	28	
653	2001	FMT	128	88	
662	2002	FMT	129	64	
665	2003	FMT	130	97	
670	2004	FMT	131	34	
676	2005	FMT	132	20	
713	2007	FMT	135	29	
745	2100	FMT	141	53	
756	2130	FMT	143	76	
763	2140	FMT	144	78	
772	2150	FMT	145	80	
1000	2160	FMT	146	82	

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS	NOT INNER
11	110	M	16 30	72B			
37	102	I	22 26	15B	OPT		
144	140	K	45 48	5B	INSTACK		
214		K	64 64	12B		EXT REFS	
243	172	J	68 73	10B	INSTACK		
304		I	91 91	11B		EXT REFS	
327	250	I	94 95	2B	INSTACK		
341		I	97 97	11B		EXT REFS	

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
362 278	N	102 109	25B	NOT INNER
374 275	I	105 107	4B	INSTACK
417 290	N	116 121	25B	NOT INNER
420 290	I	117 121	21B	NOT INNER
430 290	J	118 121	6B	INSTACK

COMMON BLOCKS LENGTH  
CNTRL 4

STATISTICS  
PROGRAM LENGTH 1780  
SCM LABELED COMMON LENGTH 4B 4  
52000B SCM USED 3364B

```

1      SUBROUTINE ELEMENT(R,Z,IX,E,RO,WANG,NEBC,NF,NUMEL)
C*****
C      STRUCTURAL ELEMENT MASS AND STIFFNESS MATRICES ARE FORMED AND
C      WRITTEN ONTO TAPE1 ELEMENTWISE
C*****
C      DIMENSION R(1),Z(1),NEBC(1),IX(NUMEL,1),E(9,1),RO(1),
10     COMMON/LS4ARG/LM(12),SS(6,12),XC,YC,ELMASS(4),S(12,12),MTYPE,Q(12)
11     ,C(6,6)
C      DIMENSION RR(4),ZZ(4),EE(9)
C      MC=0
C      DO 400 N=1,NUMEL
C      MTYPE=IX(N,5)
C      IF(MTYPE.EQ.MC) GO TO 307
C      DO 305 MM=1,9
305     EE(MM)=E(MM,MTYPE)
C      BETA=WANG(MTYPE)
C      RHO=RO(MTYPE)
C      CALL SSLAW(EE,BETA,C,NF)
307     DO 310 I=1,4
C      II=IX(N,I)
C      RR(I)=R(II)
310     ZZ(I)=Z(II)
C      CALL MASTIF(RR,ZZ,XC,YC,ELMASS,C,S,SS,Q,RHO,NF)
C      DO 320 I=1,4
C      IK=3*IX(N,I)-3
C      DO 320 J=1,3
C      JK=4*J-4+I
C      LM(JK)=IK+J
320     CONTINUE
C      MC=MTYPE
C      DO 400 CALL WRITE1(LM,283,N,NUMEL)
C      RETURN
C      END

```

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SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	DEFINED	REFS	DEFINED
3 ELEMENT	1	35					
VARIABLES	SN	TYPE	RELOCATION	REFS	DEFINED	REFS	DEFINED
136 BETA		REAL		21	21	19	26
367 C		REAL	LS4ARG	10	18	26	18
0 E		REAL	F.P.	8	21	18	1
155 EE		REAL		12	26	25	28
126 ELMASS		REAL	LS4ARG	10	27	23	30
140 I		INTEGER		23	24	25	
				DEFINED			
141 II		INTEGER		22	25	23	23
142 IK		INTEGER		24	28	28	28
0 IX		INTEGER	F.P.	31	15	28	28
				REFS		REFS	DEFINED
		ARRAY		8	8	1	1

VARIABLES	SN	TYPE	RELOCATION	REFS	30	31	34	29
143 J		INTEGER		REFS	30	DEFINED		
144 JK		INTEGER		REFS	31	DEFINED		
0 LM		INTEGER	LS4ARG	REFS	10	DEFINED		31
133 MC		INTEGER		REFS	16	DEFINED		33
135 MM		INTEGER		REFS	2*18	DEFINED		
352 MTYPE		INTEGER	LS4ARG	REFS	10	DEFINED		19
				DEFINED	15			20
134 N		INTEGER		REFS	15	DEFINED		34
0 NEBC		INTEGER	F.P.	REFS	8	DEFINED		28
0 NF		INTEGER	F.P.	REFS	21	DEFINED		1
0 NUMEL		INTEGER	F.P.	REFS	8	DEFINED		34
353 Q		REAL	LS4ARG	REFS	10	DEFINED		1
0 R		REAL	F.P.	REFS	8	DEFINED		
137 RHO		REAL		REFS	26	DEFINED		
0 RO		REAL	F.P.	REFS	8	DEFINED		20
145 RR		REAL		REFS	12	DEFINED		24
132 S		REAL	LS4ARG	REFS	10	DEFINED		
14 SS		REAL	LS4ARG	REFS	10	DEFINED		
0 WANG		REAL	F.P.	REFS	8	DEFINED		1
124 XC		REAL		REFS	10	DEFINED		
125 YC		REAL	LS4ARG	REFS	10	DEFINED		
0 Z		REAL	F.P.	REFS	8	DEFINED		1
151 ZZ		REAL		REFS	12	DEFINED		25

EXTERNALS

NAME	TYPE	ARGS	REFERENCES
MASTIF		11	26
SSLAW		4	21
WRITE1		4	34

STATEMENT LABELS

DEF LINE	REFERENCES
18	17
22	16
25	22
32	27
34	14

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
12	400	N	14 34	71B	EXT REFS NOT INNER
23	305	MM	17 18	3B	INSTACK
42	310	I	22 25	5B	INSTACK
53	320	I	27 32	21B	NOT INNER
64	320	J	29 32	4B	INSTACK

COMMON BLOCKS

NAME	LENGTH
LS4ARG	283

STATISTICS

PROGRAM LENGTH	203B	131
SCM LABELED COMMON LENGTH	433B	283
52000B SCM USED		

```

1      C
      C SUBROUTINE SSLAW(EE, BETA, C, NF)
      C *****
      C STRESS STRAIN LAW IN N-S-T SYSTEM
      C *****
      C DIMENSION EE(9), C(6, 6), D(6, 6), CC(6, 6)
      DO 65 II=1, 6
      DO 65 KK=1, 6
      C(II, KK)=0.
      65 D(II, KK)=0.
      C(1, 1)=1.0/EE(1)
      C(1, 2)=-EE(4)*C(1, 1)
      C(1, 3)=-EE(5)*C(1, 1)
      C(2, 1)=C(1, 2)
      C(2, 2)=1.0/EE(2)
      C(2, 3)=-EE(6)*C(2, 2)
      C(3, 1)=C(1, 3)
      C(3, 2)=C(2, 3)
      C(3, 3)=1.0/EE(3)
      C(4, 4)=EE(7)
      IF (NF.EQ.0) GO TO 70
      C(5, 5)=EE(8)
      C(6, 6)=EE(9)
      70 CONTINUE
      DO 200 N=1, 3
      DD=C(N, N)
      DO 100 J=1, 3
      DD 100 J)=C(N, J)/DD
      DO 150 I=1, 3
      IF (N-I) 110, 150, 110
      110 DO 140 J=1, 3
      IF (N-J) 120, 140, 120
      120 C(I, J)=C(I, J)+C(I, N)*C(N, J)
      140 CONTINUE
      150 C(I, N)=C(I, N)/DD
      C(N, N)=1.0/DD
      200 CONTINUE
      C
      C ROTATE MATERIAL PROPERTIES TO R-Z-TH SYSTEM
      C
      IF (BETA.EQ.0.0) GO TO 500
      ANG=BETA/57.2957795
      SS=SIN(ANG)
      CS=COS(ANG)
      S2=SS*SS
      C2=CS*CS
      SC=SS*CS
      D(1, 1)=C2
      D(1, 2)=S2
      D(1, 4)=SC
      D(2, 1)=S2
      D(2, 2)=C2
      D(2, 4)=-SC
      D(3, 3)=1.0
      D(4, 1)=-2.*SC
      D(4, 2)=-D(4, 1)

```

```

D(4,4)=C2-S2
D(5,5)=1.0
D(6,6)=1.0
DO 287 JJ=1,6
D1=C(1,1)*D(1, JJ)+C(1,2)*D(2, JJ)+C(1,3)*D(3, JJ)
D2=C(2,1)*D(1, JJ)+C(2,2)*D(2, JJ)+C(2,3)*D(3, JJ)
D3=C(3,1)*D(1, JJ)+C(3,2)*D(2, JJ)+C(3,3)*D(3, JJ)
D4=C(4,4)*D(4, JJ)
D5=C(5,5)*D(5, JJ)
D6=C(6,6)*D(6, JJ)
DO 287 II=JJ,6
CC(II, JJ)=D(1, II)*D1+D(2, II)*D2+D(3, II)*D3+D(4, II)*D4+D(5, II)*D5+D
1(6, II)*D6
287 CC(JJ, II)=CC(II, JJ)
DO 300 I=1,6
DO 300 J=1,6
300 C(I, J)=CC(I, J)
500 RETURN
END

```

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SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS 3 SSLAW  
DEF LINE 1  
REFERENCES 75

VARIABLES SN TYPE RELOCATION

ENTRY POINTS	DEF LINE	REFERENCES	SN	TYPE	RELOCATION	REFS	DEFINITION	REFS	DEFINITION
245	ANG		44	REAL		45	DEFINED	43	DEFINED
0	BETA		42	REAL	F.P.	43	DEFINED	1	DEFINED
0	C		7	REAL	F.P.	13	14	15	17
326	CC		29	ARRAY		3*34	36	3*62	3*63
247	CS		67	REAL		DEFINED	1	10	12
251	C2		16	REAL		17	18	19	20
262	D		29	ARRAY		34	36	37	74
242	DD		7	REAL		71	74	DEFINED	69
254	D1		2*47	REAL		48	45	45	71
255	D2		49	REAL		53	58	DEFINED	47
256	D3		7	REAL		57	3*62	3*63	3*64
257	D4		6*69	REAL		DEFINED	11	49	50
260	D5		54	REAL		55	56	57	59
261	D6		29	REAL		36	37	DEFINED	27
0	EE		69	REAL		DEFINED	62	63	64
244	I		69	REAL		DEFINED	64	65	66
237	II		69	REAL		DEFINED	66	67	68
243	J		69	REAL		DEFINED	67	67	68
253	JJ		7	REAL	F.P.	12	13	14	17
			21	INTEGER		24	DEFINED	1	16
			31	INTEGER		3*34	2*36	2*74	DEFINED
			10	INTEGER		11	7*69	2*71	DEFINED
			2*29	INTEGER		33	3*34	2*74	DEFINED
			73	INTEGER		3*63	3*64	65	66



VARIABLES	SN	TYPE	RELOCATION	69	2*71	DEFINED	61	9	2*34	2*36	2*37
240 KK		INTEGER		REFS	10	11	DEFINED	9			
241 N		INTEGER		REFS	2*27	2*29	31	33			
				DEFINED	26						
0 NF		INTEGER	F. P.	REFS	22	DEFINED	1				
252 SC		REAL		REFS	51	54	56	DEFINED	48		
246 SS		REAL		REFS	2*46	48	DEFINED	44			
250 S2		REAL		REFS	50	52	58	DEFINED	46		

EXTERNALS	TYPE	ARGS	REFERENCES
COS	REAL	1 LIBRARY	45
SIN	REAL	1 LIBRARY	44

STATEMENT LABELS	DEF LINE	REFERENCES	9
0 65	11	8	
44 70	25	22	
0 100	29	28	
0 110	32	2*31	
0 120	34	2*33	
101 140	35	32	33
104 150	36	30	31
0 200	38	26	
0 287	71	61	68
0 300	74	72	73
233 500	75	42	

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
7	65	II	8 11	14B	NOT INNER
15	65	KK	9 11	3B	INSTACK
45	200	N	26 38	52B	NOT INNER
54	100	J	28 29	4B	INSTACK
62	150	I	30 36	30B	NOT INNER
75	140	J	32 35	6B	INSTACK
142	287	JJ	61 71	54B	NOT INNER
177	287	II	68 71	13B	OPT
217	300	I	72 74	14B	NOT INNER
225	300	J	73 74	3B	INSTACK

STATISTICS	PROGRAM LENGTH	406B	262
	52000B	SCM USED	

```

1      SUBROUTINE STRAIN(S,T,RR,ZZ,H,B,FAC,N)
C*****
C      FORM STRAIN DISPLACEMENT MATRIX
C*****
C
10     DIMENSION B(6,18),HS(6),HT(6),HR(6),HZ(6)
        DIMENSION RR(4),ZZ(4),H(6)
        DIMENSION II(6),JJ(6),LL(6)
        DATA II/1,2,3,4,13,14/JJ/5,6,7,8,15,16/LL/9,10,11,12,17,18/
        DO 50 I=1,108
50      B(I)=0.0
        SM=1.0-S
        SP=1.0+S
        TM=1.0-T
        TP=1.0+T
        H(1)=SM*TM/4.
        H(2)=SP*TM/4.
        H(3)=SP*TP/4.
        H(4)=SM*TP/4.
        H(5)=(1.0-S*S)
        H(6)=(1.0-T*T)
        HS(1)=-TM/4.
        HS(2)=-HS(1)
        HS(3)=TP/4.
        HS(4)=-HS(3)
        HS(5)=-2.0*S
        HS(6)=0.
        HT(1)=-SM/4.
        HT(2)=-SP/4.
        HT(3)=-HT(2)
        HT(4)=-HT(1)
        HT(5)=0.
        HT(6)=-2.0*T
        PZT=HT(1)*ZZ(1)+HT(2)*ZZ(2)+HT(3)*ZZ(3)+HT(4)*ZZ(4)
        PZS=HS(1)*ZZ(1)+HS(2)*ZZ(2)+HS(3)*ZZ(3)+HS(4)*ZZ(4)
        PRS=HS(1)*RR(1)+HS(2)*RR(2)+HS(3)*RR(3)+HS(4)*RR(4)
        PRT=HT(1)*RR(1)+HT(2)*RR(2)+HT(3)*RR(3)+HT(4)*RR(4)
        XJ=PRS*PZT-PRT*PZS
        PSR=PZT/XJ
        PTR=-PZS/XJ
        PSZ=-PRT/XJ
        PTZ=PRS/XJ
        DO 100 I=1,6
100      HR(I)=PSR*HS(I)+PTR*HT(I)
        HZ(I)=PSZ*HS(I)+PTZ*HT(I)
        R=H(1)*RR(1)+H(2)*RR(2)+H(3)*RR(3)+H(4)*RR(4)
        DO 200 K=1,6
200      I=II(K)
        J=JJ(K)
        L=LL(K)
        B(1,I)=HR(K)
        B(2,J)=HZ(K)
        B(3,I)=H(K)/R
        B(3,L)=N*B(3,I)
        B(4,I)=HZ(K)
        B(4,J)=HR(K)
    
```

```

60      B(5,I)=-B(3,L)
        B(5,L)=B(1,I)-B(3,I)
        B(6,J)=B(5,I)
        200 B(6,L)=B(2,J)
        FAC=XJ*R
        RETURN
        END
    
```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	SN	TYPE	ARRAY	F.P.	REFS	55	58	2*59	60	61	56
3 STRAIN	1	63	F.P.					DEFINED						
0 B	REAL							57	55	58	2*59	60	61	56
0 FAC	REAL							57	55	58	2*59	60	61	56
0 H	REAL							57	55	58	2*59	60	61	56
242 HR	REAL							19	21	22	DEFINED	1	17	18
226 HS	REAL							19	21	22	DEFINED	1	17	18
234 HT	REAL							19	21	22	DEFINED	1	17	18
250 HZ	REAL							19	21	22	DEFINED	1	17	18
204 I	INTEGER							19	21	22	DEFINED	1	17	18
256 II	INTEGER							19	21	22	DEFINED	1	17	18
224 J	INTEGER							19	21	22	DEFINED	1	17	18
264 JJ	INTEGER							19	21	22	DEFINED	1	17	18
223 K	INTEGER							19	21	22	DEFINED	1	17	18
225 L	INTEGER							19	21	22	DEFINED	1	17	18
272 LL	INTEGER							19	21	22	DEFINED	1	17	18
0 N	INTEGER							19	21	22	DEFINED	1	17	18
213 PRS	REAL							19	21	22	DEFINED	1	17	18
214 PRT	REAL							19	21	22	DEFINED	1	17	18
216 PSR	REAL							19	21	22	DEFINED	1	17	18
220 PSZ	REAL							19	21	22	DEFINED	1	17	18
217 PTR	REAL							19	21	22	DEFINED	1	17	18
221 PTZ	REAL							19	21	22	DEFINED	1	17	18
212 PZS	REAL							19	21	22	DEFINED	1	17	18
211 PZT	REAL							19	21	22	DEFINED	1	17	18
222 R	REAL							19	21	22	DEFINED	1	17	18
0 RR	REAL							19	21	22	DEFINED	1	17	18
0 S	REAL							19	21	22	DEFINED	1	17	18
205 SM	REAL							19	21	22	DEFINED	1	17	18
206 SP	REAL							19	21	22	DEFINED	1	17	18
0 T	REAL							19	21	22	DEFINED	1	17	18
207 TM	REAL							19	21	22	DEFINED	1	17	18
210 TP	REAL							19	21	22	DEFINED	1	17	18
215 XJ	REAL							19	21	22	DEFINED	1	17	18

VARIABLES	SN	TYPE	REAL	ARRAY	RELOCATION	F.P.	REFERENCES	DEFINED	REFS	39	8	4*35	4*36	DEFINED	1
0	ZZ														

STATEMENT LABELS	DEF LINE	REFERENCES
0 50	12	11
0 100	46	44
0 200	61	48

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
12	50	I	11 12	28	INSTACK
114	100	I	44 46	108	INSTACK
144	200	K	48 61	258	OPT

STATISTICS  
PROGRAM LENGTH 303B 195  
52000B SCM USED

```

1      SUBROUTINE MASTIF(RR, ZZ, RM, ZM, ELMASS, D, GK, GC, G, RHO, N)
C*****
C      FORM ELEMENT MASS MATRIX M AND ELEMENT STIFFNESS MATRIX K
C*****
C      DIMENSION SS(2), RR(4), ZZ(4), ELMASS(4), GK(12, 12), GC(6, 12), Q(12)
DATA SS/-0.57735026918963, 0.57735026918963/
FZ=-RHO*32.2
DO 150 I=1, 4
150 ELMASS(I)=0.0
DO 170 J=1, 18
P(J)=0.0
DO 160 I=1, 6
BB(I, J)=0.0
160 B(I, J)=0.0
DO 170 I=1, 18
170 S(I, J)=0.0
RM=(RR(1)+RR(2)+RR(3)+RR(4))/4.0
ZM=(ZZ(1)+ZZ(2)+ZZ(3)+ZZ(4))/4.0
DO 500 II=1, 2
DO 500 JJ=1, 2
CALL STRAIN(SS(II), SS(JJ), RR, ZZ, H, B, FAC, N)
IF(N.EQ.0) FAC=2.*FAC
DO 400 J=1, 18
D1=(D(1, 1)*B(1, J)+D(1, 2)*B(2, J)+D(1, 3)*B(3, J)+D(1, 4)*B(4, J)+D(1, 5)
1 *B(5, J)+D(1, 6)*B(6, J))*FAC
D2=(D(2, 1)*B(1, J)+D(2, 2)*B(2, J)+D(2, 3)*B(3, J)+D(2, 4)*B(4, J)+D(2, 5)
1 *B(5, J)+D(2, 6)*B(6, J))*FAC
D3=(D(3, 1)*B(1, J)+D(3, 2)*B(2, J)+D(3, 3)*B(3, J)+D(3, 4)*B(4, J)+D(3, 5)
1 *B(5, J)+D(3, 6)*B(6, J))*FAC
D4=(D(4, 1)*B(1, J)+D(4, 2)*B(2, J)+D(4, 3)*B(3, J)+D(4, 4)*B(4, J)+D(4, 5)
1 *B(5, J)+D(4, 6)*B(6, J))*FAC
D5=(D(5, 1)*B(1, J)+D(5, 2)*B(2, J)+D(5, 3)*B(3, J)+D(5, 4)*B(4, J)+D(5, 5)
1 *B(5, J)+D(5, 6)*B(6, J))*FAC
D6=(D(6, 1)*B(1, J)+D(6, 2)*B(2, J)+D(6, 3)*B(3, J)+D(6, 4)*B(4, J)+D(6, 5)
1 *B(5, J)+D(6, 6)*B(6, J))*FAC
DO 400 I=J, 18
S(I, J)=S(I, J)+B(1, I)*D1+B(2, I)*D2+B(3, I)*D3+B(4, I)*D4+B(5, I)*D5+B(
1 6, I)*D6
400 S(J, I)=S(I, J)
IF(N.EQ.0) GO TO 470
DO 450 I=1, 4
450 ELMASS(I)=ELMASS(I)+FAC*H(I)*RHO
470 IF(N.NE.0) GO TO 500
BZ=FZ*FAC
P(5)=P(5)+BZ*H(1)
P(6)=P(6)+BZ*H(2)
P(7)=P(7)+BZ*H(3)
P(8)=P(8)+BZ*H(4)
500 CONTINUE
IF(N.NE.0) GO TO 510
DO 505 I=1, 18
505 IF(S(I, I).EQ.0.0) S(I, I)=1.0
C
C      FORM STRESS DISPLACEMENT MATRIX

```

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```

60      C 510 CALL STRAIN(O,O,O,O,RR,ZZ,H,BB,FAC,N)
        DO 530 I=1,6
        DO 530 J=1,18
        B(I,J)=O.O
        DO 530 K=1,6
        530 B(I,J)=B(I,J)+D(I,K)*BB(K,J)
        C
        C ELIMINATE EXTRA DEGREES OF FREEDOM
        C
        DO 550 NN=1,6
        L=18-NN
        K=L+1
        DO 550 I=1,L
        C=S(I,K)/S(K,K)
        DO 540 J=1,6
        540 B(J,I)=B(J,I)-C*B(K,J)
        DO 550 J=1,L
        S(I,J)=S(I,J)-C*S(K,J)
        IF(N.NE.O) GO TO 570
        DO 560 I=9,12
        560 S(I,I)=O.
        C
        C RELOCATE STIFFNESS MATRIX AND LOAD VECTOR
        C
        570 DO 580 I=1,12
        G(I)=P(I)
        DO 580 J=1,12
        580 GK(I,J)=S(I,J)
        DO 590 J=1,6
        DO 590 K=1,12
        590 GC(J,K)=B(J,K)
        RETURN
        END
    
```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	6*37	6*27	6*29	6*31	6*33	6*35
3 MASTIF	1	90	ARRAY	6*37	64	2*74	89	DEFINED	17	62
VARIABLES	SN	TYPE	ARRAY	REFS	64	64	DEFINED	16	47	6*35
520 B		REAL	ARRAY	64	64	64	89	DEFINED	17	62
674 BB		REAL		REFS	59	64	DEFINED	16	47	
511 BZ		REAL	ARRAY	REFS	49	50	51	DEFINED		
515 C		REAL		REFS	74	72	72	DEFINED		
O D		REAL	ARRAY	REFS	6*27	6*29	6*31	6*33	6*35	6*37
503 D1		REAL		64	DEFINED	1				
504 D2		REAL		REFS	40	27				
505 D3		REAL		REFS	40	29				
506 D4		REAL		REFS	40	31				
		REAL		REFS	40	33				

VARIABLES	SN	TYPE	RELOCATION	REFS	DEF	REFS	DEF	REFS	DEF	REFS	DEF	REFS	DEF
507 D5		REAL		REFS	40	REFS	35	REFS	35				
510 D6		REAL		REFS	40	REFS	37	REFS	37				
0 ELMASS		REAL	ARRAY	REFS	7	REFS	45	REFS	45				
502 FAC		REAL	F. P.	REFS	24	REFS	25	REFS	25				
475 FZ		REAL		REFS	37	REFS	47	REFS	47				
1576 H		REAL	ARRAY	REFS	47	REFS	10	REFS	10				
476 I		INTEGER		REFS	8	REFS	24	REFS	24				
500 II		INTEGER		REFS	12	REFS	16	REFS	16				
477 J		INTEGER		REFS	62	REFS	3*64	REFS	19				
501 JJ		INTEGER		REFS	24	REFS	83	REFS	22				
512 K		INTEGER		REFS	2*86	REFS	11	REFS	15				
514 L		INTEGER		REFS	60	REFS	78	REFS	83				
0 N		INTEGER	F. P.	REFS	24	REFS	16	REFS	17				
513 NN		INTEGER		REFS	6*33	REFS	6*37	REFS	39				
1554 P		REAL	ARRAY	REFS	3*74	REFS	2*86	REFS	2*89				
0 Q		REAL		REFS	73	REFS	85	REFS	87				
0 OC		REAL		REFS	24	REFS	23	REFS	23				
0 GK		REAL		REFS	2*64	REFS	3*72	REFS	74				
0 RHO		REAL		REFS	63	REFS	70	REFS	88				
0 RM		REAL		REFS	70	REFS	71	REFS	75				
0 RR		REAL		REFS	24	REFS	25	REFS	43				
1050 S		REAL	ARRAY	REFS	1	REFS	85	REFS	87				
516 SS		REAL	ARRAY	REFS	69	REFS	68	REFS	68				
0 ZM		REAL		REFS	8	REFS	48	REFS	49				
0 ZZ		REAL		REFS	14	REFS	48	REFS	49				
EXTERNALS		TYPE	ARGS	REFERENCES		REFERENCES		REFERENCES					
STRAIN			B	24		59							

STATEMENT LABELS	DEF LINE	REFERENCES
0 150	12	11
0 160	17	15
0 170	19	13
0 400	42	26
0 450	45	44
235 470	46	43
251 500	52	22
0 505	55	54
270 510	59	53
0 530	64	60
0 540	74	73
0 550	76	68
0 560	79	78
405 570	83	77
0 580	86	83

STATEMENT LABELS	DEF LINE	REFERENCES
0 150	12	11
0 160	17	15
0 170	19	13
0 400	42	26
0 450	45	44
235 470	46	43
251 500	52	22
0 505	55	54
270 510	59	53
0 530	64	60
0 540	74	73
0 550	76	68
0 560	79	78
405 570	83	77
0 580	86	83

///

STATEMENT LABELS	DEF LINE	REFERENCES	PROPERTIES
0 590	89	87	88
LOOPS LABEL	FROM-TO	LENGTH	PROPERTIES
14 150	11 12	28	INSTACK
20 170	13 19	25B	NOT INNER
27 160	15 17	3B	INSTACK
40 170	18 19	2B	INSTACK
61 500	22 52	175B	EXT REFS NOT INNER
62 500	23 52	172B	EXT REFS NOT INNER
75 400	26 42	127B	NOT INNER
204 400	39 42	15B	OPT
230 450	44 45	4B	INSTACK
263 505	54 55	4B	INSTACK
277 530	60 64	27B	NOT INNER
300 530	61 64	23B	NOT INNER
314 530	63 64	4B	INSTACK
327 550	68 76	46B	NOT INNER
333 550	71 76	37B	NOT INNER
350 540	73 74	3B	INSTACK
363 550	75 76	4B	INSTACK
402 560	78 79	2B	INSTACK
406 580	83 86	20B	NOT INNER
417 580	85 86	3B	INSTACK
427 590	87 89	14B	NOT INNER
435 590	88 89	3B	INSTACK

STATISTICS  
 PROGRAM LENGTH 52000B SCM USED 1627B 919



```

1      SUBROUTINE WRITE1(A,LA,N,NUMEL)
C*****
C      WRITE MATRIX A ON TAPE1 AS AN ARRAY
C*****
C      DIMENSION A(LA)
COMMON/BUF/B(2830)
LB=2830
IF (N.NE.1) GO TO 100
REWIND 1
M=0
100 MM=M+LA
DO 200 I=1,LA
II=I+M
200 B(II)=A(I)
M=MM
IF (N.EQ.NUMEL) GO TO 300
IF ((M+LA).LE. LB) GO TO 400
300 WRITE (1) B
M=0
400 RETURN
END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	DEFINED
3 WRITE1	1	22	ARRAY	7	16
			ARRAY	8	20
			ARRAY	15	16
			F. P.	7	15
			F. P.	19	14
			F. P.	13	19
			F. P.	17	13
			F. P.	10	18
			F. P.	18	DEFINED
				1	1

FILE NAMES	MODE	WRITES	REFERENCES	MOTION
TAPE1	UNFMT	20	11	11

STATEMENT LABELS	DEF LINE	REFERENCES
13 100	13	10
0 200	16	14
37 300	20	18
42 400	22	19

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
23 200	I	14 16	48	INSTACK

SUBROUTINE WRITE1

COMMON BLOCKS    LENGTH  
BUF                2830

STATISTICS

PROGRAM LENGTH        548        44  
SCM LABELED COMMON LENGTH    54168    2830  
520008 SCM USED

```

1  SUBROUTINE TOTAL(R,Z,NEBC,MASS,XS,A,IJBEO,IJBCI,WLO,WLI,
    1  NPPD,NEG,MBAND,NUMEL,IGRAV)
C *****
C TOTAL STIFFNESS AND MASS MATRICES AND LOAD VECTOR ARE FORMED BY
C READING ELEMENTAL INFORMATIN FROM TAPE1.
C NODAL LOADS DUE TO WATER PRESSURE ARE CALCULATED.
C *****
10  COMMON/CNTRL/NUMNP, NANGLE, MBAN ,NBC, NF, NPP , NPPI, TRACE
    1, C(6,6)
    DIMENSION R(1), Z(1), NEBC(1), MASS(1), XS(1), A(NEG, MBAND), IJBEO(NPPO)
    1, IJBCI(1)
    REAL MASS
C
C FORM MASS AND STIFFNESS MATRICES
C
    DO 100 I=1, NEG
    MASS(I)=0.0
    XS(I)=0.0
    DO 100 J=1, MBAND
    100 A(I, J)=0.0
    DO 140 N=1, NUMEL
    CALL READI(LM, 283, N, NUMEL)
    DO 120 I=1, 12
    II=LM(I)
    XS(II)=XS(II)+Q(I)
    DO 110 J=1, 12
    JJ=LM(J)-II+1
    IF(JJ.LT.1) GO TO 110
    A(II, JJ)=A(II, JJ)+S(I, J)
    110 CONTINUE
    120 CONTINUE
    IF(NF.EQ.0) GO TO 140
    DO 130 I=1, 4
    II=LM(I)
    MASS(II)=MASS(II)+ELMASS(I)
    MASS(II+1)=MASS(II)
    130 MASS(II+2)=MASS(II)
    140 CONTINUE
C
C STATIC PRESSURE
C
    IF (NPPD.EQ.0.AND.NPPI.EQ.0) GO TO 160
    IF (NPPD.EQ.0) GO TO 145
    IF (IGRAV.EQ.2.AND.NF.NE.0) GO TO 145
    READ 1010, (IJBEO(K), K=1, NPPO)
    PRINT 2010
    CALL HYDROST(R, Z, IJBEO, NPPO, XS, WLO, -1.0)
    145 IF (NPPI.EQ.0) GO TO 160
    IF (IGRAV.EQ.2.AND.NF.NE.0) GO TO 165
    READ 1010, (IJBCI(K), K=1, NPPI)
    PRINT 2011
    CALL HYDROST(R, Z, IJBEO, NPPI, XS, WLI, 1.0)
    160 CONTINUE
C

```

C DISPLACEMENT BOUNDARY CONDITION

```

60 C 165 TRACE=0.
    DO 170 I=1,NEG
    170 TRACE=TRACE+ABS(A(I,1))
    IF (NF.NE.O) GO TO 187
    DO 185 I=3,NEG,3
    IF (A(I,1).EQ.O.O) A(I,1)=1.0
    185 CONTINUE
    187 IF (NBC.LE.O) GO TO 190
    DO 189 K=1,NBC
    I=NEBC(K)
    A(I,1)=O.O
    XS(I)=O.
    DO 189 J=2,MBAND
    A(I,J)=O.
    L=I-J+1
    IF (L.LE.O) GO TO 189
    A(L,J)=O.
    189 CONTINUE
    190 WRITE (1) A
    BACKSPACE 1
    REWIND 4
    WRITE (4) IJBCO
    BACKSPACE 4
    1010 FORMAT (16I5)
    2010 FORMAT ( 1H1/26H WATER OUTSIDE THE TANK /)
    2011 FORMAT (///26H FLUIDS INSIDE THE TANK /)
    RETURN
    END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	VARIABLES	SN	TYPE	RELOCATION	REFS
3	1	86				F.P.	
0	A		0		REAL	ARRAY	13
367	C		0		REAL	LS4ARG	1
126	ELMASS		0		REAL	ARRAY	11
346	I		0		INTEGER	ARRAY	11
			0		INTEGER	ARRAY	20
			351	II	INTEGER	ARRAY	-21
			0	IGRAV	INTEGER	F.P.	2*65
			352	JJ	INTEGER	F.P.	26
			353	K	INTEGER	F.P.	38
							19
							47
							2*28
							27
							13
							55
							13
							50
							23
							22
							31
							48
							62
							32
							27
							70
							28
							73
							64
							69
							2*38
							2*39
							2*40
							78
							70
							73
							32
							74
							64
							76
							37
							48
							76
							48
							53
							68

VARIABLES	SN	TYPE	RELOCATION	REFS	75	76	74	77
354 L		INTEGER		REFS		DEFINED		
0 LM		INTEGER	ARRAY LS4ARG	REFS	11	25	30	37
0 MASS		REAL	ARRAY F.P.	REFS	13	15	38	40
				DEFINED	1	20	39	40
2 MBAN		INTEGER	CNTRL	REFS	10			
0 MBAND		INTEGER	F.P.	REFS	13	22	72	1
352 MTYPE		INTEGER	LS4ARG	REFS	11			
350 N		INTEGER		REFS	25	DEFINED	24	
1 NANGLE		INTEGER	CNTRL	REFS	10			
3 NBC		INTEGER	CNTRL	REFS	10	67	68	
0 NEBC		INTEGER	F.P.	REFS	13	69	DEFINED	1
0 NEG		INTEGER	F.P.	REFS	13	19	61	64
4 NF		INTEGER	CNTRL	REFS	10	35	47	52
5 NPP		INTEGER	CNTRL	REFS	10			
6 NPPI		INTEGER	CNTRL	REFS	10	45	51	55
0 NPPD		INTEGER	F.P.	REFS	13	45	46	50
				DEFINED	1			
0 NUMEL		INTEGER	F.P.	REFS	24	25	DEFINED	1
0 NUMNP		INTEGER	CNTRL	REFS	10			
353 Q		REAL	LS4ARG	REFS	11	28		
0 R		REAL	ARRAY	REFS	13	50	DEFINED	1
132 S		REAL	ARRAY F.P.	REFS	11	32		
14 SS		REAL	ARRAY LS4ARG	REFS	11			
7 TRACE		REAL	ARRAY LS4ARG	REFS	10	62	DEFINED	60
0 WLI		REAL	CNTRL	REFS	10			
0 WLD		REAL	F.P.	REFS	55	DEFINED	1	62
124 XC		REAL	F.P.	REFS	50	DEFINED	1	
0 XS		REAL	LS4ARG	REFS	11			
			ARRAY F.P.	REFS	13	28	50	55
125 YC		REAL	LS4ARG	REFS	11			DEFINED
0 Z		REAL	ARRAY F.P.	REFS	13	50	DEFINED	1

FILE NAMES	MODE	REFS	79	80
INPUT	FMT	48		
OUTPUT	FMT	49		
TAPE1	UNFMT	78	MOTION	
TAPE4	UNFMT	81	MOTION	

EXTERNALS	TYPE	ARGS	REFERENCES
HYDROST		7	55
READ1		4	50
			25

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
ABS	REAL	1	INTRIN	62

STATEMENT LABELS	DEF LINE	REFERENCES
0 100	23	19
51 110	33	29
0 120	34	26
0 130	40	36
71 140	41	24
124 145	51	46
150 160	56	45
150 165	60	52
0 170	62	61
0 185	66	64
174 187	67	63

STATEMENT LABELS	DEF LINE	REFERENCES	72	75
216 189	77	68		
224 190	78	67		
327 1010 FMT	83	48	53	
331 2010 FMT	84	49		
336 2011 FMT	85	54		

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	NOT INNER	EXT REFS	NOT INNER
11 100	I	19 23	14B				
20 100	J	22 23	2B	INSTACK			
26 140	N	24 41	46B				
32 120	I	26 34	24B				
43 110	J	29 33	10B	INSTACK			
63 130	I	36 40	5B	INSTACK			
156 170	I	61 62	4B	INSTACK			
170 185	I	64 66	3B	INSTACK			
177 189	K	68 77	25B				
213 189	J	72 77	5B	INSTACK			

COMMON BLOCKS LENGTH  
 CNTRL 8  
 LS4ARG 283

STATISTICS  
 PROGRAM LENGTH 400B 256  
 SCM LABELED COMMON LENGTH 443B 291  
 52000B SCM USED

```

1      SUBROUTINE READ1(A,LA,N,NUMEL)
C*****
C      READ MATRIX A (IN ARRAY FORM) FROM TAPE1.
C*****
C      DIMENSION A(LA)
COMMON/BUF/B(2830)
LB=2830
IF (N.NE.1) GO TO 100
REWIND 1
M=0
READ (1) B
100 MM=M+LA
DO 200 I=1,LA
II=I+M
200 A(I)=B(II)
M=MM
IF (N.EQ.NUMEL) GO TO 400
IF ((M+LA).LE.LB) GO TO 400
READ (1) B
M=0
400 RETURN
END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
3 READ1	1	23

VARIABLES	SN	TYPE	RELOCATION	REFS	DEF	REFS	DEF	REFS	DEF	REFS	DEF	REFS
0 A		REAL	ARRAY	7	DEFINED	1	DEFINED	17	DEFINED	1	DEFINED	17
0 B		REAL	ARRAY	8	DEFINED	17	DEFINED	13	DEFINED	17	DEFINED	13
57 I		INTEGER	BUF	16	DEFINED	17	DEFINED	15	DEFINED	17	DEFINED	15
60 II		INTEGER		17	DEFINED	16	DEFINED	16	DEFINED	16	DEFINED	16
0 LA		INTEGER	F.P.	7	DEFINED	14	DEFINED	20	DEFINED	15	DEFINED	20
54 LB		INTEGER		20	DEFINED	9	DEFINED	9	DEFINED	9	DEFINED	9
55 M		INTEGER		14	DEFINED	16	DEFINED	20	DEFINED	14	DEFINED	20
56 MM		INTEGER		18	DEFINED	19	DEFINED	14	DEFINED	14	DEFINED	14
0 N		INTEGER	F.P.	10	DEFINED	19	DEFINED	1	DEFINED	1	DEFINED	1
0 NUMEL		INTEGER	F.P.	19	DEFINED	1	DEFINED	1	DEFINED	1	DEFINED	1

FILE NAMES	MODE	READS	REFS	DEF	REFS	DEF	REFS	DEF	REFS	DEF	REFS	DEF	REFS
TAPE1	UNFMT	13	21	21	MOTION	11							

STATEMENT LABELS	DEF LINE	REFERENCES
15 100	14	10
0 200	17	15
42 400	23	19

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
25 200	1	15 17	3B	INSTACK

COMMON BLOCKS    LENGTH  
BUF                    2830

STATISTICS

PROGRAM LENGTH                    61B        49  
SCM LABELED COMMON LENGTH        5416B     2830  
52000B SCM USED



```

1      SUBROUTINE HYDROST(R,Z,IJBC,NPP,XS,WL,SGN)
C*****
C      CALCULATE HYDROSTATIC PRESSURE
C*****
C      DIMENSION IJBC(1),XS(1),R(1),Z(1)
      PRINT 2020
      I=IJBC(1)
      J=IJBC(2)
      R1=0.
      R2=0.
      LI=1.
      IF (WL.LT.Z(I)) GO TO 50
      PJ=.0625*(WL-Z(I))*SGN*(I)
      NN=NPP-1
      GO TO 100
50      II=3*I-2
      JJ=3*J-2
      X=WL-Z(J)
      PJ=0.0625*X*SGN*(J)
      DZ=Z(I)-Z(J)
      DR=R(I)-R(J)
      F=X/DZ
      RI1=PJ*F**2*DZ/6.
      RI2=-PJ*F**2*DR/6.
      RJ1=PJ*F*(1.-F/3.)*DZ/2.
      RJ2=-PJ*F*(1.-F/3.)*DR/2.
      XS(II)=XS(II)+RI1
      XS(II+1)=XS(II+1)+RI2
      XS(JJ)=XS(JJ)+RJ1
      XS(JJ+1)=XS(JJ+1)+RJ2
      RI=RJ1
      R2=RJ2
      PRINT 2030, I,RI1,RI2
      NN=NPP-1
      LI=2.
100     DO 150 L=L1,NN
          PI=PJ
          I=IJBC(L)
          J=IJBC(L+1)
          II=3*I-3
          JJ=3*J-3
          DR=R(I)-R(J)
          DZ=Z(I)-Z(J)
          PJ=0.0625*(WL-Z(J))*SGN*(J)
          RI1=(2.*PI+PJ)*DZ/6.
          RI2=- (2.*PI+PJ)*DR/6.
          RJ1=(2.*PJ+PI)*DZ/6.
          RJ2=- (2.*PJ+PI)*DR/6.
          XS(II+1)=XS(II+1)+RI1
          XS(II+2)=XS(II+2)+RI2
          XS(JJ+1)=XS(JJ+1)+RJ1
          XS(JJ+2)=XS(JJ+2)+RJ2
          RI1=RI1+RI
          RI2=RI2+R2
          RI=RJ1

```

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```

R2=RJ2
PRINT 2030, I, RI1, RI2
150 CONTINUE
PRINT 2030, J, R1, R2
2020 FORMAT (1X,4HEQUIVALENT NODAL FORCES DUE TO FLUID PRESSURE //
1 32H NO. PT. R-LOAD Z-LOAD/)
2030 FORMAT (112,2F10.3)
RETURN
END
60
65

```

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM  
10 I IJBC ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

SYMBOLIC REFERENCE MAP (R=2)

ENTRY	POINTS	DEF	LINE	REFERENCES	RELOCATION
3	HYDROST	1		65	
VARIABLES	SN	TYPE			RELOCATION
246	DR	REAL			
245	DZ	REAL			
247	F	REAL			
233	I	INTEGER			
242	II	INTEGER			
0	IJBC	INTEGER			F.P.
		ARRAY			
234	J	INTEGER			
243	JJ	INTEGER			
254	L	INTEGER			
237	L1	INTEGER			
241	NN	INTEGER			
0	NPP	INTEGER			F.P.
255	PI	REAL			
240	PJ	REAL			
0	R	REAL			F.P.
		ARRAY			
250	RI1	REAL			
251	RI2	REAL			
252	RJ1	REAL			
253	RJ2	REAL			
235	R1	REAL			
236	R2	REAL			
0	SGN	REAL			F.P.

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REFS	26	28	48	50	50	23	44
REFS	24	25	27	47	47		
DEFINED	22	45			49		
REFS	25	26	2*27	2*28	2*28	24	42
REFS	14	2*15	18	22	23	35	
44	45	59	DEFINED	9	40		
REFS	2*29	2*30	2*51	2*52	DEFINED	18	42
REFS	7	9	10	40	41		
DEFINED	1						
REFS	19	20	21	22	23	43	44
45	61		DEFINED	10	41		
REFS	2*46	2*32	2*53	2*54	DEFINED	19	43
REFS	2*31	41	DEFINED	38			
REFS	40	DEFINED	13	37			
REFS	38	DEFINED	16	36			
REFS	38	DEFINED	1	1			
REFS	16	36	DEFINED	50	DEFINED	39	48
REFS	47	48	49	28	39	47	
REFS	25	26	27	28	46		
49	50	DEFINED	15	21	2*44	46	
REFS	7	15	21	2*23			
DEFINED	1						
REFS	29	35	51	55	59		
DEFINED	25	47	55				
REFS	30	35	52	56			
DEFINED	26	48	56				
REFS	31	33	53	57	DEFINED	27	49
REFS	32	34	54	58	DEFINED	28	50
REFS	55	61	DEFINED	11	33	57	
REFS	56	61	DEFINED	12	34	58	
REFS	15	21	46	DEFINED	1	58	

VARIABLES	SN	TYPE	RELOCATION	REFS	14	15	20	46	DEFINED	1
O WL		REAL	F.P.	REFS	21	24	20	20	DEFINED	1
244 X		REAL		REFS	7	29	30	20		51
O XS		REAL	ARRAY F.P.	REFS	54	53	1	31	32	31
					52	53	54	29	30	32
O Z		REAL	ARRAY F.P.	REFS	7	14	15	20	2*22	2*45
				DEFINED	1					46

FILE NAMES	OUTPUT	MODE	WRITES	8	35	59	61
		FMT					

STATEMENT LABELS	DEF LINE	REFERENCES
30 50	18	14
106 100	38	17
0 150	60	38
207 2020	62	8
222 2030	64	35

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
110 150	L	38 60	47B		

STATISTICS	PROGRAM LENGTH	271B	185
	52000B	SCM USED	

```

1      SUBROUTINE STATIC(NEBC,SMASS,XS,A,STRES,NEG,MBAND,NUM,NUMEL)
C*****
C      DISPLACEMENTS DUE TO STATIC LOADS ARE CALCULATED. ELEMENT STRESSES
C      ARE COMPUTED. STATIC DISPLACEMENTS AND STRESSES ARE WRITTEN
C      ONTO TAPES.
C*****
10     COMMON/CNTRL/NUMNP, NANGLE, MBAN, NBC, NF, NPPD, NPPI, TRACE
COMMON/LS4ARG/LM(12), SS(6, 12), XC, YC, ELMASS(4), S(12, 12), MTYPE, Q(12)
1, C(6, 6)
DIMENSION NEBC(1), SMASS(1), XS(1), A(NEG, MBAND), STRES(NUM), SIG(6)
REWIND 3
READ (1) A
BACKSPACE 1
DO 50 K=1, NBC
I=NEBC(K)
50   A(I, 1)=1.0
CALL BANSOL(NEG, MBAND, NEG, A, XS, 0)
CALL BANSOL(NEG, MBAND, NEG, A, XS, 1)
MPRINT=0
REWIND 1
DO 300 N=1, NUMEL
CALL READ1(LM, 283, N, NUMEL)
IY=6
IF (NF.EQ.0) IY=4
DO 180 I=1, 6
SIG(I)=0.0
DO 180 J=1, 12
JJ=LM(J)
180  SIG(I)=SIG(I)+SS(I, J)*XS(JJ)
DO 190 J=1, IY
190  SIG(J)=6.94444*SIG(J)
NN=6*N
DO 195 I=1, 6
STRES(NN-6+I)=SIG(I)
195  CONTINUE
IF (MPRINT) 280, 270, 280
270  CONTINUE
PRINT 2000
MPRINT=50
280  MPRINT=MPRINT-1
PRINT 2001, N, XC, YC, (SIG(I), I=1, IY)
300  CONTINUE
PRINT 2009
DO 360 I=1, NEG
360  XS(I)=XS(I)*12.
PRINT 2010, (M, XS(3*N-2), XS(3*N-1), XS(3*N), N=1, NUMNP)
WRITE (3) (XS(I), I=1, NEG)
WRITE (3) STRES
2000  FORMAT (1H1, 23HELEMENT STRESSES IN PSI//
1 6H EL, NO 7X 1HR 7X 1HZ 7X 5HSIG R 7X 5HSIG Z 7X 5HSIG T
2 6X 6HTAU RZ 6X 6HTAU RT 6X 6HTAU ZT /)
2001  FORMAT (15, 1X, 2F8.2, 6E12.4)
2009  FORMAT (1H1, 44HDISPLACEMENTS DUE TO STATIC LOADS--IN INCHES //
1 41H NODAL PT R-DISPLACEMENT Z-DISPLACEMENT
2 16H T DISPLACEMENT )

```

2010 FORMAT (19,3E16.4)  
RETURN  
END

60

SYMBOLIC REFERENCE MAP (R=2)

VARIABLES	SN	TYPE	DEF LINE	REFERENCES	RELOCATION	REFS	12	19	20	DEFINED	1	14	18
3	STATIC		1	59									
0 A		REAL	ARRAY		F.P.	REFS	12						
367 C		REAL	ARRAY		LS4ARG	REFS	10						
126 ELMASS		REAL	ARRAY		LS4ARG	REFS	10						
340 I		INTEGER				DEFINED	17						
343 IY		INTEGER				REFS	18	28	3*31	2*36			
344 J		INTEGER				REFS	17	27	35	43	43	2*47	49
345 JJ		INTEGER				REFS	32	43	DEFINED	25	46	49	
337 K		INTEGER				REFS	30	31	2*33	DEFINED	29	32	
0 LM		INTEGER	ARRAY			REFS	31	DEFINED	30				
2 MBAN		INTEGER			LS4ARG	REFS	17	DEFINED	16				
0 MBAND		INTEGER			CNTRL	REFS	10	24	30				
341 MPRINT		INTEGER			F.P.	REFS	9						
352 MTYPE		INTEGER				REFS	12	19	20	DEFINED	1		
342 N		INTEGER			LS4ARG	REFS	38	42	DEFINED	21	41	42	
1 NANGLE		INTEGER				REFS	10						
3 NBC		INTEGER				REFS	24	34	43	4*48	DEFINED	23	48
0 NEBC		INTEGER			CNTRL	REFS	9						
0 NEG		INTEGER	ARRAY		CNTRL	REFS	9	16					
4 NF		INTEGER			F.P.	REFS	12	17	DEFINED	1			
346 NN		INTEGER			F.P.	REFS	12	2*19	2*20	46	49		
6 NPPI		INTEGER				DEFINED	1						
5 NPPO		INTEGER			CNTRL	REFS	9	26					
0 NUM		INTEGER				REFS	36	DEFINED	34				
0 NUMEL		INTEGER			CNTRL	REFS	9						
0 NUMNP		INTEGER			CNTRL	REFS	9						
353 Q		REAL	ARRAY		F.P.	REFS	12	DEFINED	1				
132 S		REAL	ARRAY		F.P.	REFS	23	24	DEFINED				
347 SIG		REAL	ARRAY			REFS	9	48	DEFINED				
0 SMASS		REAL			CNTRL	REFS	10						
14 SS		REAL	ARRAY		LS4ARG	REFS	10	31	33	36	43		
0 STRES		REAL	ARRAY			DEFINED	28	31	33				
7 TRACE		REAL			F.P.	REFS	12	DEFINED	1				
124 XC		REAL			LS4ARG	REFS	10	50	DEFINED		36		
0 XS		REAL	ARRAY		CNTRL	REFS	9						
125 YC		REAL			LS4ARG	REFS	10	43	20	31	47	3*48	49

FILE NAMES	MODE
OUTPUT	FMT
TAPE1	UNFMT
	WRITES
	READS
	MOTION
	40
	43
	45
	14
	15
	48
	22

125

FILE NAMES	MODE	WRITES	50	MOTION	13
TAPES	UNFMT	REFERENCES	20		
EXTERNALS	TYPE	ARGS			
BANSOL	6				
READ1	4				

STATEMENT LABELS	DEF LINE	REFERENCES
0 50	18	16
0 180	31	27
0 190	33	32
0 195	37	35
0 270	39	38
127 280	42	2*38
0 300	44	23
0 360	47	46
272 2000	51	40
306 2001	54	43
311 2009	55	45
326 2010	58	48

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
26 50	K	16 18	4B	INSTACK
55 300	N	23 44	64B	EXT REFS NOT INNER
64 180	I	27 31	17B	NOT INNER
73 180	J	29 31	5B	INSTACK
106 190	J	32 33	3B	INSTACK
120 195	I	35 37	2B	INSTACK
146 360	I	46 47	3B	INSTACK
154	N	48 48	12B	EXT REFS

COMMON BLOCKS	LENGTH
CNTRL	8
LS4ARG	283

STATISTICS	
PROGRAM LENGTH	365B
SCM LABELED COMMON LENGTH	443B
52000B SCM USED	291

```

1      C      SUBROUTINE BANSOL(NN,MM,NDIM,A,B,KK)
2      C      *****
3      C      LINEAR EQUATION SOLVER FOR SYMMETRIC BANDED MATRICES
4      C      KK = 0 TRIANGULARIZES BAND MATRIX A
5      C      KK = 1 REDUCES AND BACKSUBSTITUTES VECTOR B
6      C      KK = 2 BACKSUBSTITUTES VECTOR B
7      C      *****
8      C      DIMENSION A(NDIM,1), B(1)
9      C
10     C      NR = NN - 1
11     C      IF (KK-1) 100,300,400
12     C      100 DO 200 N = 1,NR
13     C      M = N - 1
14     C      IF (A(N,1).EQ.0.) A(N,1) = 1.0E-16
15     C      PIVOT = A(N,1)
16     C      MR = MINO (MM,NN-M)
17     C      DO 200 L = 2,MR
18     C      C = A(N,L)/PIVOT
19     C      IF (C.EQ.0.) GO TO 200
20     C      I = M + L
21     C      J = 0
22     C      DO 180 K = L,MR
23     C      J = J + 1
24     C      180 A(I,J) = A(I,J) - C*A(N,K)
25     C      A(N,L) = C
26     C      200 CONTINUE
27     C      IF (A(NN,1).EQ.0.) A(NN,1) = 1.0E-16
28     C      GO TO 500
29     C      300 DO 350 N = 1,NR
30     C      M = N - 1
31     C      MR = MINO (MM,NN-M)
32     C      C = B(N)
33     C      B(N) = C/A(N,1)
34     C      DO 350 L = 2,MR
35     C      I = M + L
36     C      350 B(I) = B(I) - A(N,L)*C
37     C      400 B(NN) = B(NN)/A(NN,1)
38     C      DO 450 K = 2,NN
39     C      M = NN - K
40     C      N = M + 1
41     C      MR = MINO (MM,K)
42     C      DO 450 L = 2,MR
43     C      I = M + L
44     C      450 B(N) = B(N) - A(N,L)*B(I)
45     C      500 RETURN
46     C      END

```

ENTRY POINTS DEF LINE RELOCATIONS  
 3 BANSOL 1 47

VARIABLES SN TYPE RELOCATION  
 O A REAL ARRAY F.P.

O B REAL ARRAY F.P.

167 C REAL

170 I INTEGER

171 J INTEGER

172 K INTEGER

O KK INTEGER F.P.

166 L INTEGER

163 M INTEGER

O MM INTEGER

165 MR INTEGER F.P.

162 N INTEGER

O NDIM INTEGER F.P.

O NN INTEGER F.P.

161 NR INTEGER

164 PIVOT REAL

INLINE FUNCTIONS TYPE ARGS DEF LINE REFERENCES  
 MINO INTEGER 0 INTRIN 18 33

STATEMENT LABELS DEF LINE REFERENCES  
 O 100 INACTIVE 14 13

O 180 26 24

61 200 28 14 19 21

73 300 31 13 36

O 350 38 31 44

123 400 39 13

O 450 46 40

156 500 47 30

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES  
 15 200 N 14 28 51B NOT INNER  
 31 200 L 19 28 33B NOT INNER  
 50 180 K 24 26 5B INSTACK  
 74 350 N 31 38 27B NOT INNER  
 113 350 L 36 38 5B INSTACK  
 131 450 K 40 46 25B NOT INNER  
 146 450 L 44 46 5B INSTACK

STATISTICS PROGRAM LENGTH 221B 145  
 52000B SCM USED

LINE	TEXT	REFS	DEF LINE	REFERENCES
10	39	10	17	20
16	46	16	DEFINED	1
17	38	38	DEFINED	2*26
29	29	29	DEFINED	16
34	34	34	38	2*46
35	35	35	38	46
21	21	21	27	38
20	20	20	DEFINED	22
2*26	2*26	2*26	DEFINED	25
25	25	25	23	24
26	26	26	43	40
41	41	41	DEFINED	37
13	13	13	1	45
20	20	20	24	37
22	22	22	36	44
19	19	19	33	37
22	22	22	41	42
32	32	32	43	45
33	33	33	43	1
24	24	24	36	DEFINED
15	15	15	17	20
2*35	2*35	2*35	38	DEFINED
10	10	10	DEFINED	14
12	12	12	18	31
1	1	1	2*29	33
14	14	14	31	3*39
20	20	20	DEFINED	12
17	17	17	DEFINED	17
33	33	33	43	18
33	33	33	DEFINED	44
26	26	26	20	27
14	14	14	DEFINED	26
1	1	1	1	14
33	33	33	2*29	31
17	17	17	DEFINED	33
31	31	31	DEFINED	40
20	20	20	DEFINED	40
43	43	43	DEFINED	41

28



```

1      C
      SUBROUTINE BNEIGN(NN,MM,NMO,NBC,EV,NEBC,SMASS,A,B,V,R,CN,SN,TRACE)
      DIMENSION EV(1),NEBC(1),SMASS(1),A(NN,1),B(1),R(1),SN(1),CN(1),
1      V(1)
5      C
      INITIALIZE
      C
      TOL=1.0E-12
      IFLAG = 0
      NLOOP = 5
      NSMAX = 50
      PSHIFT = 0.
      MM1 = MM + 1
      NW = NN*MM
      NEIG = 0
      NR = NN
      NNR = NN - 1
      REWIND 2
      C
20     C
      REDUCE TO CLASSICAL EIGENVALUE PROBLEM A*X = E*X
      C
      DO 120 I = 1,NN
      X = SMASS(I)
      IF (X.GT.0.) GO TO 110
      PRINT 12, I
12     FORMAT (30HNEG. OR ZERO MASS, EQUATION = I5)
      IFLAG = 1
      GO TO 120
110    SMASS(I) = 1./SQRT(X)
120    CONTINUE
      IF (IFLAG.NE.0) STOP
      DO 130 I = 1,NN
      L = I - 1
      MR = MINO (MM,NN-I+1)
      DO 130 J = 1,MR
      K = L + J
130    A(I,J) = A(I,J)*SMASS(I)*SMASS(K)
      C
40     C
      IMPOSE BOUNDARY CONDITIONS ON A
      C
      IF (NBC.LE.0) GO TO 150
      DO 140 N = 1,NBC
      I = NEBC(N)
      A(I,1) = 100.*TRACE
140    CONTINUE
      C
      COMPACT MATRIX A INTO A 1-D ARRAY V
      C
150    DO 160 J = 2,MM
      L = NN*(J-1)
      M = NN - J + 1
      DO 160 I = 1,M
      K = L + I
160    V(K) = A(I,J)
      WRITE (2) (V(I),I=1,NW)
      C
55     C
      COMPUTE SMALLEST EIGENVALUE AND ASSOCIATE EIGENVECTOR OF A

```

129

```

C
C BY INVERSE ITERATION
60 165 NEIG = NEIG + 1
    E1 = 0.
    SHIFT = 0.
    NS = 0
    KKT = 2
    CALL BANSOL(NR,MM,NN,V,B,O)
    DO 170 I = NR,NN
170 B(I) = 0.
    DO 180 I = 1,NR
180 B(I) = 1.
    IF (NBC.LE.O) GO TO 200
    DO 190 N = 1,NBC
    I = NEBC(N)
190 B(I) = 0.
200 NS = NS + 1
    CALL BANSOL(NR,MM,NN,V,B,KKT)
    KKT = 1
    E = 0.
    DO 220 I = 1,NR
    IF (ABS(B(I)).GT.ABS(E)) E = B(I)
220 CONTINUE
    E = 1./E
    EPS = (E-E1)/E*100.
    DO 230 I = 1,NR
230 B(I) = B(I)*E
    E1 = E
    IF (ABS(EPS).GT.1..AND.NS.LT.15) GO TO 200
    NL = NLOOP - 3
250 DO 260 I = 1,NR
260 R(I) = B(I)
    NS = NS + 1
    CALL BANSOL(NR,MM,NN,V,B,1)
    E = 0.
    DO 300 I = 1,NR
    IF (ABS(B(I)).GT.ABS(E)) E = B(I)
300 CONTINUE
    SUMD = 0.
    DO 320 I = 1,NR
    B(I) = B(I)/E
    D = ABS(B(I)-R(I))
    SUMD = SUMD + D**2
    IF (D.GT.DMAX) DMAX = D
320 CONTINUE
    IF (DMAX.LE.TOL.OR.NS.GE.NSMAX) GO TO 400
    NL = NL + 1
    IF (NL.LT.NLOOP) GO TO 250
    REWIND 2
    READ (2) (V(I),I=1,NW)
    NL = 0
    X = 0.
    Y = 0.
    DO 340 I = 1,NR
    X = X + B(I)*R(I)
    Y = Y + B(I)*B(I)
340

```

```

115 SHIFT = SHIFT + AMAX1(1., -4. *SUMD. O. 9) * X / (Y * E)
DO 350 I = 1, NR
350 V(I) = V(I) - SHIFT
CALL BANSOL(NR, MM, NN, V, B, O)
GO TO 250
400 X = 0.
Y = 0.
DO 420 I = 1, NR
X = X + B(I) * R(I)
420 Y = Y + B(I) * B(I)
SHIFT = SHIFT + X / (Y * E)
EV(NEIG) = SHIFT + PSHIFT
SHIFT = SHIFT - TOL
PSHIFT = EV(NEIG) - TOL
Y = SQRT(Y)
DO 430 I = 1, NN
430 R(I) = B(I) / Y
IF (NEIG. GE. NMO) GO TO 650
C
C
C
135 DEFLATE BAND MATRIX
REWIND 2
READ (2) (V(I), I=1, NW)
DO 450 NX = 1, NR
FB = R(NX)
IF (FB. NE. O.) GO TO 480
450 CONTINUE
480 DO 500 I = 1, NR
L = NW + I
V(I) = V(I) - SHIFT
500 V(L) = 0.
NRS = NR - 1
NR1 = NR + 1
Q1 = R(1) ** 2
S2 = 0.
C = 1.
DO 600 I = 1, NRS
K = I + 1
Q = Q1 + R(K) ** 2
IF (I. LT. NX) GO TO 550
S2 = Q1 / Q
C = R(K) / SQRT(Q)
IF (FB. LT. O.) C = -C
550 S = SQRT(S2)
C2 = C * C
SN(I) = S
CN(I) = C
Q1 = Q
L = NW + I
A11 = V(I)
A22 = V(K)
A12 = V(L)
X = 2. * A12 * S * C
V(I) = A11 * C2 + A22 * S2 - X
V(K) = A22 * C2 + A11 * S2 + X
V(L) = A12 * (C2 - S2) + (A11 - A22) * S * C
MR = MINO (I, MM)

```

```

175 IF (MR.LE.1) GO TO 570
    L1 = I
    DO 560 J = 2,MR
      L1 = L1 + NNR
      L2 = L1 + NN
      A1 = V(L1)
      A2 = V(L2)
      V(L1) = A1*C - A2*S
      V(L2) = A2*C + A1*S
560 MR = MINO (MM1,NR1-I)
570 IF (MR.LT.3) GO TO 600
      L2 = K
      DO 580 J = 3,MR
        L2 = L2 + NN
        L1 = L2 + NNR
        A1 = V(L1)
        A2 = V(L2)
        V(L1) = A1*C - A2*S
        V(L2) = A2*C + A1*S
      600 CONTINUE
    C
    C STORE DEFLATED MATRIX, EIGENVECTOR, SINES AND COSINES OF
    C JACOBI ROTATION MATRICES
    C
195 REWIND 2
    WRITE (2) (V(I), I=1,NN)
    WRITE (1) (R(I),SN(I),CN(I), I=1,NN)
    NR = NR - 1
    IF (NBC.LE.0) GO TO 165
    DO 620 N = 1,NBC
      I = NEBC(N)
      IF (I.GE.NX) NEBC(N) = I - 1
    620 CONTINUE
    GO TO 165
    C
    C RECOVER EIGENVECTORS OF ORIGINAL MATRIX
    C AND CHECK EIGENVALUE ARRANGEMENT
    C
205 DO 700 I = 1,NN
    700 A(I,NMD) = R(I)
    IF (NMD.LE.1) GO TO 900
    LL = NMD - 1
    DO 800 N = 1,LL
      M = NMD - N
      NRS = NN - M
      NR = NRS + 1
      BACKSPACE 1
      READ (1) (A(I,M),SN(I),CN(I), I=1,NN)
      BACKSPACE 1
      KK = M + 1
      DO 800 L = 1,NRS
        I = NR - L
        K = I + 1
        DO 800 J = KK,NMD
          A1 = A(I,J)
          A2 = A(K,J)
          A(I,J) = A1*CN(I) + A2*SN(I)

```

SUBROUTINE BNEIGN 76/176 OPT=1 STATIC

```

230      800 A(K,J) = A2*CN(I) - A1*SN(I)
        DO 830 K = 1,LL
          M = LL - K + 1
          DO 830 J = 1,M
            E1 = EV(J)
            E2 = EV(J+1)
            IF (E1.LT.E2) GO TO 830
            EV(J+1) = E1
            EV(J) = E2
          DO 820 I = 1,NN
            TEMP = A(I,J)
            A(I,J) = A(I,J+1)
            A(I,J+1) = TEMP
          830 CONTINUE
          900 DO 920 I = 1,NN
            X = SMASS(I)
            SMASS(I) = 1./X**2
          DO 920 J = 1,NM0
            920 A(I,J) = A(I,J)*X
          RETURN
          END
245

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	
3 BNEIGN	1	248	ARRAY	F.P.
VARIABLES	SN	TYPE	ARRAY	F.P.
O A	REAL	REAL		
1237 A1	REAL	REAL		
1232 A11	REAL	REAL		
1234 A12	REAL	REAL		
1240 A2	REAL	REAL		
1233 A22	REAL	REAL		
O B	REAL	REAL	ARRAY	F.P.
1226 C	REAL	REAL		
O CN	REAL	REAL	ARRAY	F.P.
1231 C2	REAL	REAL		
1216 D	REAL	REAL		
1214 DMAX	REAL	REAL		
1211 E	REAL	REAL		
1212 EPS	REAL	REAL		
O EV	REAL	REAL	ARRAY	F.P.

REFS	3	37	54	226	227	239	240
247	DEFINED	1	37	44	211	219	228
229	240	241	247				
REFS	179	180	189	190	228	229	
DEFINED	177	187	226				
REFS	168	169	170	DEFINED	164		
REFS	167	170	166	166			
REFS	179	180	189	190	228	229	
DEFINED	178	188	227				
REFS	168	169	170	DEFINED	165		
REFS	3	65	75	2*79	84	89	91
2*94	99	100	113	2*114	118	123	2*124
131	DEFINED	1	67	69	73	84	99
REFS	157	2*159	161	167	170	179	180
189	190	DEFINED	150	156	157		
REFS	3	198	228	229	DEFINED	1	161
219	168	169	170	DEFINED	159		
REFS	101	2*102	DEFINED	100			
REFS	102	104	DEFINED	96	102	94	99
REFS	79	81	2*82	84	85	92	94
115	125	DEFINED	77	79	81		
REFS	86	DEFINED	82	234	DEFINED	1	126
REFS	3	128	233				
236	237						

VARIABLES	SN	TYPE	RELOCATION	REFS	235	236	DEFINED	61	85	233
1205 E1		REAL		REFS	235	236	DEFINED			
1243 E2		REAL		REFS	237	DEFINED	234			
1221 F8		REAL		REFS	157	DEFINED	139			
1175 I		INTEGER		REFS	23	29	33	34	3*37	44
				53	55	67	69	73	2*79	2*84
				2*89	2*99	2*100	108	2*113	2*114	2*117
				2*123	2*131	137	143	2*144	152	154
				160	163	164	168	171	173	181
				197	2*203	2*211	3*219	224	226	3*228
				2*229	2*240	241	244	245	2*247	
				DEFINED	32	43	52	55	66	68
				72	83	88	93	98	108	112
				116	130	137	142	151	177	198
				202	219	223	238	243		
1164 IFLAG		INTEGER		REFS	31	DEFINED	9	27		
1201 J		INTEGER		REFS	36	2*37	50	54	226	227
				228	233	234	236	237	239	2*240
				241	DEFINED	35	49	174	184	225
				232						
1202 K		INTEGER		REFS	37	54	153	165	167	183
				227	231	DEFINED	36	53	152	224
				230						
1242 KK		INTEGER		REFS	225	DEFINED	221			
1210 KKT		INTEGER		REFS	75	DEFINED	64	76		
1177 L		INTEGER		REFS	36	53	145	166	223	
				REFS	33	50	143	163		
				DEFINED	214	230	231	213		
1241 LL		INTEGER		REFS	175	176	177	187	189	
1235 L1		INTEGER		REFS	173	175	186			
1236 L2		INTEGER		DEFINED	178	175	186	186	190	
				REFS	178	180	185			
				REFS	176	183	185			
1204 M		INTEGER		DEFINED	176	216	219	221	232	
				REFS	52	216	219			
				DEFINED	51	215	231			
				REFS	13	14	34	49	65	91
			F. P.	118	171	DEFINED	1			
				REFS	181	DEFINED	13	184		
1170 MM1		INTEGER		REFS	35	172	174	182		
1200 MR		INTEGER		REFS	34	171	181			
				DEFINED	43	72	202	203	215	
1203 N		INTEGER		REFS	42	71	201	214		
				DEFINED	41	42	70	71	201	
			F. P.	REFS	41	42	70	200		
				DEFINED	1					
				REFS	3	43	72	202	1	203
			F. P.	REFS	60	126	128	132	15	60
1172 NEIG		INTEGER	ARRAY	REFS	105	106	DEFINED	105	109	
1213 NL		INTEGER		REFS	87	106	DEFINED	10		
1165 NLOOP		INTEGER		REFS	132	211	212	213	225	246
			F. P.	REFS	1					
				DEFINED	3	14	16	17	22	34
				REFS	51	65	66	75	91	130
				163	185	198		210	216	238
				243	1					
				DEFINED	175	186	DEFINED	17	78	88
1174 NNR		INTEGER		REFS	65	66	68	75	83	
1173 NR		INTEGER		REFS	91	93	112	116	122	138
				142	147	199	223	223	16	199
				217				DEFINED		

VARIABLES	SN	TYPE	RELOCATION	REFS	217	222	146	216
1222 NRS		INTEGER		151	DEFINED	222	DEFINED	
1223 NR1		INTEGER		181	DEFINED	147		
1207 NS		INTEGER		74	86	90	104	63
				90			DEFINED	74
1146 NSMAX		INTEGER		104	DEFINED	11		
1171 NW		INTEGER		55	108	137	143	197
				14				
1220 NX		INTEGER		139	154	203	DEFINED	138
1167 PSHIFT		REAL		126	DEFINED	12	128	
1227 Q		REAL		155	156	162	DEFINED	153
1224 Q1		REAL		153	155	DEFINED	148	162
O R		REAL	F.P.	3	100	113	123	139
				156	211	DEFINED	1	148
1230 S		REAL		198	167	170	179	180
				158				131
1206 SHIFT		REAL		115	117	125	126	144
				62	115	125	127	
O SMASS		REAL	F.P.	3	23	2*37	244	1
				245			DEFINED	29
O SN		REAL	F.P.	3	198	228	229	1
				219			DEFINED	160
1215 SUMD		REAL		101	115	DEFINED	97	101
1225 S2		REAL		158	168	169	170	149
1244 TEMP		REAL		241	DEFINED	239	DEFINED	
1163 TOL		REAL		104	127	128	DEFINED	8
O TRACE		REAL	F.P.	44	DEFINED	1		
O V		REAL	F.P.	3	55	65	75	117
				144	164	166	177	178
				197	1	54	108	187
				145	169	170	179	144
1176 X		REAL		24	29	113	115	190
				169	247	DEFINED	23	125
				123	244		110	168
1217 Y		REAL		167	244	124	125	131
				114	115	121	124	129
				111	114			

FILE NAMES	MODE	WRITES	219	MOTION	218	220	18	107
OUTPUT	FMT	25	READS	MOTION	137			
TAPE1	UNFMT	198	197	108				
TAPE2	UNFMT	55						
		136						
		196						

EXTERNALS	TYPE	ARGS	REFERENCES	91	118
BANSOL	REAL	6	75		
SQRT	REAL	1	129	156	158

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES	86	2*94	100
ABS	REAL	1	INTRIN	2*79			
AMAX1	REAL	0	INTRIN	115			
MINO	INTEGER	0	INTRIN	34			

STATEMENT LABELS	DEF LINE	REFERENCES	26	25
1104 12	FMT			
35 110		26	24	
40 120		29	22	28
0 130		30	32	35
0 140		37	42	
		45		

STATEMENT LABELS	DEF LINE	REFERENCES	PROPERTY	EXT REFS
110	49	41		
150	54	49		52
0	60	200		205
137	67	66		
0	69	68		
180	73	71		
0	74	70		86
203	80	78		
0	84	83		
230	88	106		119
0	89	88		
252	95	93		
0	103	98		
0	114	112		
340	117	116		
0	120	104		
406	124	122		
0	131	130		
430	141	138		
0	142	140		
465	145	142		
0	158	154		
522	180	174		
0	181	172		
601	190	184		
0	191	191		182
627	204	201		
0	210	132		
674	211	210		
0	229	214		225
800	241	238		
0	242	230		235
1022	243	212		
830	247	243		246
1027				
900				
0				
920				

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LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
567	560	J	174 180	10B	INSTACK
615	580	J	184 190	10B	INSTACK
644		I	198 198	11B	EXT REFS
666	620	N	201 204	5B	INSTACK
704	700	I	210 211	2B	INSTACK
713	800	N	214 229	64B	EXT REFS NOT INNER
724		I	219 219	13B	EXT REFS
745	800	L	222 229	27B	NOT INNER
762	800	J	225 229	7B	INSTACK
1000	830	K	230 242	27B	NOT INNER
1003	830	J	232 242	22B	NOT INNER
1016	820	I	238 241	3B	INSTACK
1030	920	I	243 247	16B	NOT INNER
1040	920	J	246 247	3B	INSTACK

STATISTICS

PROGRAM LENGTH 1327B 727  
 52000B SCM USED

```

1  SUBROUTINE EIGEN(NBNC, SMASS, XS, EV, A, W1, W2, W3, W4, CC,
    1 NEG, NMODE, MBAND, R, Z, PLOTT)
C *****
C STRUCTURAL FREE VIBRATION MODE SHAPES AND NATURAL FREQUENCIES ARE
C CALCULATED OR READ IN. MBAND+1 SETS LIMIT ON MAX MODE FURNISHED.
C *****
C
COMMON/CNTRL/NUMNP, NANGLE, MBAN, NBC, NF, NPPO, NPPI, TRACE, READFRQ
DIMENSION NBNC(1), SMASS(1), XS(1), A(NBNC, MBAND), EV(1), W1(1), W2(1),
1 W3(1), W4(1), CC(NMODE, 1), R(1), Z(1), KEEP(100),
2 ZPLOT(100, 20), NPTS(20), FIG(20), APLOT(100, 20)
LOGICAL READFRQ
LOGICAL PLOTT
IF (READFRQ) GO TO 180
READ (1) A
BACKSPACE 1
CALL BNEIGN(NEG, MBAND, NMODE, NBC, EV, NBNC, SMASS, A, W1, A, W2, W3, W4
1
C
C COMPUTE EIGENVALUES AND EIGENVECTORS
PRINT 2006
DO 90 I=1, NMODE
EV(I)=SQRT(EV(I))
90 PRINT 2005, I, EV(I)
CALL PRINTA(A, NEG, NMODE)
IF (.NOT. PLOTT) GO TO 108
ZPREV=100000.
IND=0
92 ZMAX=0.
IND=IND+1
DO 94 I=1, NUMNP
94 IF (Z(I).GT.ZMAX. AND. Z(I).LT.ZPREV) ZMAX=Z(I)
RMAX=0.
DO 96 I=1, NUMNP
IF (Z(I).NE.ZMAX) GO TO 96
IF (R(I).GT.RMAX) KEEP(IND)=I
IF (R(I).GT.RMAX) RMAX=R(I)
96 CONTINUE
ZPREV=ZMAX
IF (ZMAX.NE.0.) GO TO 92
C
DO 102 I=1, IND
DO 100 N=1, NMODE
100 ZPLOT(I, N)=Z(KEEP(I))
102 KEEP(I)=I+3*(KEEP(I)-1)
CALL OPLT
DO 106 J=1, 3
IF (J.EQ.1) YTITLE="R DISPL. "
IF (J.EQ.2) YTITLE="Z DISPL. "
IF (J.EQ.3) YTITLE="T DISPL. "
DO 104 K=1, NMODE
NPTS(K)=IND
IFIG(K)=3
DO 104 I=1, IND

```

```

104 INEW=KEEP(I)+(J-1)
APLOT(I,K)=A(INEW,K)
CALL MULPLT(ZPLOT,APLOT,NPTS,NMODE,1,100,20,
1 "Z-AXIS",6,YTITLE,8,9,IFIG)
106 CONTINUE
CALL PLOT(O.,O.,999)
108 PRINT 2008
DO 150 I=1,NMODE
DO 120 J=I,NMODE
SUM=0.0
DO 110 K=I,NEQ
110 SUM=SUM+A(K,I)*SMASS(K)*A(K,J)
120 CC(I,J)=SUM
II=I-1
IF (II) 150,150,130
130 DO 140 L=1,II
140 CC(I,L)=CC(L,I)
150 CONTINUE
CALL PRINTA(CC,NMODE,NMODE)
C
C WRITE FREQUENCIES AND MODE SHAPES
C
WRITE (8) (EV(N),N=1,NMODE)
DO 170 N=1,NMODE
DO 170 M=1,NUMNP
L=3*M-2
170 WRITE (8) M,A(L,N),A(L+1,N),A(L+2,N)
RETURN
C
C READ FREQUENCIES AND MODE SHAPES
C
180 READ (8) (EV(N),N=1,NMODE)
DO 190 N=1,NMODE
DO 190 M=1,NUMNP
L=3*M-2
190 READ (8) MM,A(L,N),A(L+1,N),A(L+2,N)
PRINT 2006
DO 200 I=1,NMODE
200 PRINT 2005, I,EV(I)
PRINT 2007
CALL PRINTA(A,NEG,NMODE)
2005 FORMAT (2H W,11,2H =,F10.3)
2006 FORMAT (1H1/* STRUCTURE NATURAL FREQUENCIES IN RAD/SEC.*)
2007 FORMAT (/// * EIGENVECTORS PHI NORMALIZED W.R.T. MASS MATRIX*)
2008 FORMAT (/// " VERIFICATION OF IMPOSED ORTHOGONALITY RELATION: " /
1 (PHI)T * (M) * (PHI) = I")
RETURN
END

```

ENTRY POINTS 3 EIGEN  
 DEF LINE 1  
 REFERENCES 85 104

VARIABLES	SN	TYPE	RELOCATION	REFS	2*18	28	59	2*69	3*84	98
0 A		REAL	ARRAY	DEFINED	16	3*93	59			
4763	APLOT	REAL	ARRAY	REFS	60	DEFINED	59			
0 CC	REAL	REAL	ARRAY	REFS	74	76	DEFINED	1	70	74
0 EV	REAL	REAL	ARRAY	REFS	18	25	26	80	96	
610	I	INTEGER		DEFINED	25	89				
				REFS	2*26	3*35	38	2*39	2*40	2*47
				2*48	59	66	69	70	71	2*74
				2*96	24	34	37	45	57	65
				95						
4737	IFIG	INTEGER	ARRAY	REFS	60	DEFINED	56			
623	II	INTEGER		REFS	73	DEFINED	71			
612	IND	INTEGER		REFS	39	45	55	57		
621	INEN	INTEGER		DEFINED	33					
616	J	INTEGER		REFS	59	58	58	69	70	
				REFS	51	53				
620	K	INTEGER		DEFINED	66					
627	KEEP	INTEGER	ARRAY	REFS	55	2*59	3*69	DEFINED	54	68
624	L	INTEGER		REFS	10	48	58	DEFINED	39	48
625	M	INTEGER		REFS	2*74	3*93	DEFINED	73	83	92
2	MBAN	INTEGER		REFS	83	92	DEFINED	82	91	
0	MBAND	INTEGER		REFS	9					
626	MM	INTEGER		REFS	10	DEFINED	1			
615	N	INTEGER		REFS	93					
				DEFINED	47	3*84	89	3*93		
1	NANGLE	INTEGER	CNTRL	REFS	46	81	89	90		
3	NBC	INTEGER	F.P.	REFS	18					
0	NEBC	INTEGER		REFS	9					
0	NEG	INTEGER		REFS	18	DEFINED	1			
4	NF	INTEGER		REFS	10	28	68	98		
0	NMODE	INTEGER		REFS	9					
				REFS	10	24	28	46	54	60
				65	18	80	81	89	90	95
				98	2*76					
				DEFINED	1					
6	NPPI	INTEGER	CNTRL	REFS	9					
5	NPPO	INTEGER	CNTRL	REFS	9	DEFINED	55			
4713	NPTS	INTEGER	ARRAY	REFS	10	37	82	91		
0	NUMNP	INTEGER		REFS	34	DEFINED	1			
0	PLOTT	LOGICAL		REFS	29	2*40	DEFINED	1		
0	R	REAL		REFS	39	15				
10	READFRQ	LOGICAL		REFS	13					
614	RMAX	REAL		REFS	39	40	36	40		
0	SMASS	REAL		REFS	10	69	DEFINED	1		
622	SUM	REAL		REFS	18	DEFINED	67	69		
7	TRACE	REAL		REFS	70	DEFINED				
0	W1	REAL	CNTRL	REFS	9					
0	W2	REAL	F.P.	REFS	18	DEFINED	1			
0	W3	REAL	F.P.	REFS	10	DEFINED	1			
0	W4	REAL	F.P.	REFS	18	DEFINED	1			
0	W4	REAL	F.P.	REFS	10	DEFINED	1			
0	XS	REAL	F.P.	REFS	18	DEFINED	1			
617	YTITLE	REAL		REFS	1					
0	Z	REAL		REFS	60	51	52	53	52	47
				REFS	60	38	47	DEFINED	1	
				REFS	10	3*35				

140

VARIABLES SN TYPE RELOCATION  
 613 ZMAX REAL  
 773 ZPLOT REAL  
 611 ZPREV REAL

FILE NAMES MODE  
 OUTPUT FMT  
 TAPE1 UNFMT  
 TAPES UNFMT

EXTERNALS TYPE ARGS REFERENCES  
 BNEIGN 14 18  
 MULPLT 13 60  
 OPLT 0 49  
 PLOT 3 63  
 PRINTA 3 28  
 SQRT REAL 1 LIBRARY 25 98

STATEMENT LABELS DEF LINE REFERENCES  
 0 90 26 24  
 73 92 32 43  
 0 94 35 34  
 124 96 41 37  
 0 100 47 46  
 0 102 48 45  
 0 104 59 54  
 0 106 62 50  
 223 108 64 29  
 0 110 69 68  
 0 120 70 66  
 0 130 73 72  
 0 140 74 73  
 267 150 75 65  
 0 170 84 81  
 327 180 89 15  
 0 190 93 90  
 0 200 96 95  
 540 2005 FMT 99 26  
 543 2006 FMT 100 23  
 552 2007 FMT 101 27  
 561 2008 FMT 102 64

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES  
 47 90 I 24 26 12B EXT REFS  
 101 94 I 34 35 5B INSTACK  
 115 96 I 37 41 10B INSTACK  
 131 102 I 45 48 20B NOT INNER  
 140 100 N 46 47 3B INSTACK  
 153 106 J 50 62 47B EXT REFS NOT INNER  
 170 104 K 54 59 24B NOT INNER  
 204 104 I 57 59 5B INSTACK  
 226 150 I 65 75 44B NOT INNER  
 230 120 J 66 70 23B INSTACK  
 241 110 K 68 69 4B INSTACK  
 264 140 L 73 74 2B INSTACK  
 305 170 N 81 84 21B EXT REFS NOT INNER  
 306 170 M 82 84 16B EXT REFS  
 336 190 N 90 93 21B EXT REFS NOT INNER

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
337 190	M	91 93	16B		EXT REFS
352 200	I	95 96	10B		EXT REFS

COMMON BLOCKS LENGTH  
CNTRL 9

STATISTICS  
PROGRAM LENGTH 10741B 4577  
SCM LABELED COMMON LENGTH 11B 9  
52000B SCM USED

```

1  SUBROUTINE EXT(IJBC,R,Z,IX,IJFS,NUFNP,NUFEL,NFBAND,NUINTF,
   1  NUCOF,WLO)
C *****
C READ AND PRINT EXTERIOR WATER ELEMENT PROPERTIES
C *****
C DIMENSION R(1),Z(1),IX(NUFEL,1),IJBC(1),IJFS(1)
   10  L=0
      MB=0
      IB=0
      IS=1
      IJFS(1)=1
      PRINT 2004
   15  20 READ 1002, N, ICODE, R(N), Z(N), MOD, NLIM, FACR, FACZ
      IF (N.GT.1) GO TO 25
      IF (Z(1).LT.WLO.AND.R(1).LT.0.0001) IS=0
   25  L1=L+1
      IF (N-L1) 90,70,30
   30  IF (L.LE.0) GO TO 80
      DIV=N-L
      DR=(R(N)-R(L))/DIV
      DZ=(Z(N)-Z(L))/DIV
      M=N-1
      DO 40 K=L1,M
      R(K)=R(K-1)+DR
      Z(K)=Z(K-1)+DZ
   40  GO TO 70
      L1=N+1
   50  IF (FACR.LE.0.0) FACR=1.0
      IF (FACZ.LE.0.0) FACZ=1.0
      PRINT 2100, MOD,NLIM,FACR,FACZ
   60  N=N+1
      N1=N-MOD
      N2=N1-MOD
      IF (N1.LE.0.OR.N2.LE.0) GO TO 100
      R(N)=R(N1)+FACR*(R(N1)-R(N2))
      Z(N)=Z(N1)+FACZ*(Z(N1)-Z(N2))
      IF (N.LT.NLIM) GO TO 60
      MOD=0
   70  L=N
      DO 74 K=L1,N
      IF (R(K).LT.0.0001) GO TO 73
      IF (ICODE.EQ.0) GO TO 74
      IF (ICODE.LT.-1) GO TO 73
   72  CONTINUE
      IB=IB+1
      IF (IB.GT.NUINTF) GO TO 78
      IF (ICODE.GT.0) IJBC(IB)=ICODE
      IF (ICODE.EQ.-1) IJBC(IB)=0
      GO TO 74
   73  IS=IS+1
      IJFS(IS)=K
      IF (ICODE.GT.0) GO TO 72
   74  CONTINUE
      PRINT 2002, (K,R(K),Z(K),ICODE,K=L1,N)
      IF (MOD.GT.0) GO TO 50

```

```

60      IF (N-NUFNP) 20,120,110
78      PRINT 2120
        STOP
80      PRINT 2130
        STOP
90      PRINT 2140, N
        STOP
65      100 PRINT 2150
        STOP
110     PRINT 2160, N, NUFNP
120     CONTINUE
        PRINT 2001
        N=0
130     READ 1003, M, (IX(M,I), I=1,8)
140     N=N+1
        IF (M.EQ.N) GO TO 160
        DO 150 I=1,4
150     IX(N,I)=IX(N-1,I)+1
        DO 155 I=5,8
155     IX(N,I)=IX(N-1,I)
160     PRINT 2003, N, (IX(N,I), I=1,8)
        C
        C
        C
        DETERMINE BAND WIDTH
        DO 170 I=1,4
        DO 170 J=1,4
        MM=IABS(IX(N,I)-IX(N,J))
        IF (MM.GT.MB) MB=MM
170     CONTINUE
        IF (NUCOF.LE.0) GO TO 196
        MC=NUCOF+NUFNP
        DO 190 I=5,8
        II=I-4
        IF (IX(N,I).EQ.2) GO TO 192
190     CONTINUE
        GO TO 196
192     DO 194 I=1,2
        MM=IABS(MC-IX(N,II))
        IF (MM.GT.MB) MB=MM
        II=II+1
        IF (II.GT.4) II=1
194     CONTINUE
196     CONTINUE
        IF (N.EQ.NUFEL) GO TO 199
        IF (N.EQ.M) GO TO 130
        GO TO 140
105     199 NFBAND=MB+1
1002    FORMAT (2I5,2F10.0,2I5,2F10.0)
1003    FORMAT (16I5)
2001    FORMAT (1H1//33H EXT.FLD.EL.NO. I J K L,
1004    1 8X,2HIJ,3X,2HJK,3X,2HKL,3X,2HLI)
2002    FORMAT (17,8X,F10.3,4X,F10.3,5X,15)
2003    FORMAT (11I2,1X,4I5,5X,4I5)
2004    FORMAT (//38H EXT.FLD.N.P.
2100    FORMAT (21H GENERATION WITH MOD=13,3X,6H MLIM=14,3X,6H FACR=F10.5,
        13X,6H FACZ=F10.5)
        Z-ORD , 7X, 5HICODE//)
        R-ORD
        MOD=13,3X,6H MLIM=14,3X,6H FACR=F10.5,
        13X,6H FACZ=F10.5)

```



115 2120 FORMAT (/31H INTERFACE NODAL NUMBER ERROR /)  
 2130 FORMAT (28H FIRST JOINT CARD IS MISSING)  
 2140 FORMAT (31H COORDINATE CARD FOR JOINT NO. 15,16H NOT IN SEQUENCE)  
 2150 FORMAT (42H INSUFFICIENT INFORMATION TO GENERATE MESH)  
 2160 FORMAT (14H JOINT NUMBER 15,21H EXCEEDS GIVEN NUFNP= 15)  
 120 RETURN  
 END

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS    DEF LINE    REFERENCES  
 3 EXT            1            120

VARIABLES    SN    TYPE    RELOCATION

615	DIV	REAL	REFS	22	DEFINED	21	DEFINED		
616	DR	REAL	REFS	26	DEFINED	22			
617	DZ	REAL	REFS	27	DEFINED	23			
612	FACR	REAL	REFS	30	37	DEFINED	15	30	
613	FACZ	REAL	REFS	31	38	DEFINED	15	31	
624	I	INTEGER	REFS	72	2*78	79	84	85	91
			92	DEFINED	75	77	79	83	90
			95						
604	IB	INTEGER	REFS	47	48	49	50	DEFINED	47
607	ICODE	INTEGER	REFS	44	45	2*49	50	54	56
			DEFINED	15					
630	II	INTEGER	REFS	96	98	99	DEFINED	91	98
0	IJBC	INTEGER	REFS	8	DEFINED	1	49	50	
0	IJFS	INTEGER	REFS	8	DEFINED	1	13	53	
605	IS	INTEGER	REFS	52	53	DEFINED	12	17	52
0	IX	INTEGER	REFS	8	76	78	79	2*85	96
			DEFINED	1	72	76	78		
625	J	INTEGER	REFS	85	DEFINED	84			
621	K	INTEGER	REFS	2*26	2*27	43	53	3*56	
			DEFINED	25	42	56			
602	L	INTEGER	REFS	18	20	21	22	23	
			DEFINED	9	41				
614	L1	INTEGER	REFS	19	25	42	56	DEFINED	29
620	M	INTEGER	REFS	25	72	74	103	DEFINED	72
603	MB	INTEGER	REFS	86	97	105	DEFINED	10	97
627	MC	INTEGER	REFS	96	DEFINED	89			
626	MM	INTEGER	REFS	2*86	2*97	DEFINED	85	96	40
610	MOD	INTEGER	REFS	32	34	35	57	DEFINED	24
606	N	INTEGER	REFS	2*15	16	19	21	22	23
			29	33	34	37	38	39	42
			56	58	63	67	73	74	2*76
			2*79	2*85	92	96	102	103	
			DEFINED	15	33	71			
0	NFBAND	INTEGER	DEFINED	1	105				
611	NLIM	INTEGER	REFS	32	39	DEFINED	15		
0	NUCOF	INTEGER	REFS	88	89	DEFINED	1		
0	NUFEL	INTEGER	REFS	8	102	DEFINED	1		
0	NUFNP	INTEGER	REFS	58	67	89	DEFINED	1	
0	NUINTF	INTEGER	REFS	48	DEFINED	1			

VARIABLES	SN	TYPE	RELOCATION	REFS	35	36	2*37	2*38	DEFINED	34
622 N1		INTEGER		REFS	35	36	2*37	2*38	DEFINED	34
623 N2		INTEGER		REFS	36	37	38	DEFINED	35	
0 R		REAL	ARRAY F.P.	REFS	8	17	2*22	26	3*37	43
				DEFINED	1	15	26	37		56
0 WLO		REAL	F.P.	REFS	17	DEFINED	1			
0 Z		REAL	ARRAY F.P.	REFS	8	17	2*23	27	3*38	56
				DEFINED	1	15	27	38		

FILE NAMES	MODE	READS	15	72	56	59	61	63	65	67
INPUT	FMT	WRITES	14	32						
OUTPUT	FMT	70	79							

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
IABS	INTEGER	1	INTRIN	85

STATEMENT LABELS	DEF LINE	REFERENCES
16 20	15	58
36 25	18	16
0 30	20	19
0 40	27	25
67 50	29	57
101 60	33	39
123 70	41	19
133 72	46	54
145 73	52	43
152 74	55	42
176 78	59	48
201 80	61	20
204 90	19	63
207 100	65	36
212 110	67	58
215 120	69	58
220 130	72	103
235 140	73	104
0 150	76	75
0 155	78	77
262 160	79	74
0 170	87	83
0 190	93	90
337 192	95	92
0 194	100	95
360 196	101	88
364 199	105	102
475 1002	106	15
501 1003	107	72
503 2001	108	70
513 2002	110	56
517 2003	111	79
522 2004	112	14
531 2100	113	32
542 2120	115	59
547 2130	116	61
554 2140	117	63
563 2150	118	65
571 2160	119	67

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
61	40	K	25 27	4B	INSTACK
126	74	K	42 55	27B	EXITS
160		K	56 56	10B	EXT REFS
223		I	72 72	11B	EXT REFS
246	150	I	75 76	2B	INSTACK
257	155	I	77 78	2B	INSTACK
265		I	79 79	11B	EXT REFS
300	170	I	83 87	22B	NOT INNER
311	170	J	84 87	6B	INSTACK
327	190	I	90 93	10B	INSTACK
344	194	I	95 100	13B	EXITS

STATISTICS

PROGRAM LENGTH 646B 422

52000B SCM USED

```

1  SUBROUTINE SOLEXT(SMASS,W,A,BI,BII,D,IJBC,R,Z,IX,IJFS,
    1 HB,HL,HM,NMD,NEG,NUFNP,NUFEL,NUINTF,NUFSF,NFBAND,NEGF)
    C
    C*****
    C COMPUTE GENERALIZED FORCE VECTOR AND MASS MATRIX
    C FROM EXTERIOR WATER
    C*****
    C
    DIMENSION SS(2),RR(4),ZZ(4),H(4,4),HH(4,4),FK(50)
    DIMENSION SMASS(1),W(1),A(NEG,1),HM(NEGF,1),HB(1),HL(NEGF,1),
    1 D(NMD,1),BI(1),BII(NMD,1),IJFS(1),IJBC(1),R(1),Z(1),IX(NUFEL,1),
    COMMON/CNTRL/NUMNP, NANGLE, MBAND, NBC, NF, NPPD, NPPI, TRACE
    COMMON/FCONST/PI, ROW, HS
    DATA SS/ -0.57735026918963, 0.57735026918963/

15  PRINT 2006, (IJBC(I),I=1,NUINTF)
    PRINT 2008, (IJFS(I),I=1,NUFSF)

    C
    C GENERATE BOUNDARY DISPLACEMENTS
    C
    DO 97 K=1,NUINTF
    II=IJBC(K)
    IF(K.EQ. NUINTF) GO TO 92
    KK=K+1
    91 JJ=IJBC(KK)
    IF(JJ.NE.0) GO TO 92
    KK=KK+1
    GO TO 91
    92 DO 96 M=1,NMD
    IF(II.EQ.0) GO TO 94
    DO 93 I=1,3
    KI=3*K-I+1
    93 D(M,KI)=A(3*II-I+1,M)
    GO TO 96
    94 S=(R(K-1)-R(K))*2+(Z(K-1)-Z(K))*2
    S1=SQRT(S)
    S1=SQRT(S1)
    RS=S/S1
    DO 95 I=1,3
    KI=3*K-I+1
    D(M,KI)=D(M,KI-3)+(A(3*JJ-I+1,M)-D(M,KI-3))*RS
    95 CONTINUE
    96 CONTINUE
    97 CONTINUE

    C
    C FORM MATRIX H
    C
    DO 100 I=1,NEGF
    DO 100 J=1,NFBAND
    HM(I,J)=0.
    100 NUCOF=NEGF-NUFNP
    NUF1=NUFNP+1
    B=0.5*PI/HS
    DO 600 N=1,NUFEL
    DO 150 I=1,4
    II=IX(N,I)

```

```

60      RR(I)=R(II)
      150 ZZ(I)=Z(II)
      C
      DO 200 I=1,4
      DO 200 J=1,4
      200 HH(I,J)=0.
      DO 300 II=1,2
      DO 300 JJ=1,2
      CALL FORMH(SS(II),SS(JJ),RR,ZZ,H)
      DO 250 I=1,4
      DO 250 J=1,4
      HH(I,J)=HH(I,J)+H(I,J)
      250 HH(J,I)=HH(I,J)
      300 CONTINUE
      DO 320 I=1,4
      II=IX(N,I)
      DO 320 J=1,4
      JJ=IX(N,J)-II+1
      IF(JJ.LT.1) GO TO 320
      HM(II,JJ)=HM(II,JJ)+HH(I,J)
      320 CONTINUE
      IF (NUCOF.LE.0) GO TO 600
      DO 350 I=5,8
      II=I-4
      IF (IX(N,I).EQ.2) GO TO 370
      350 CONTINUE
      GO TO 600
      370 GO TO (371,371,372,373),II
      371 II=IX(N,II)
      I2=IX(N,II+1)
      GO TO 375
      372 II=IX(N,4)
      I2=IX(N,3)
      GO TO 375
      373 II=IX(N,1)
      I2=IX(N,4)
      375 SIJ=ABS(Z(II)-Z(I2))
      BR=B*(R(II)
      DO 380 K=1,2
      A2=(1.0-SS(K))/2.0
      A3=(1.0+SS(K))/2.0
      ZIJ=Z(II)*A2+Z(I2)*A3
      DO 380 M=1,NUCOF
      J1=NUF1+M-11
      J2=NUF1+M-12
      EIG=(2.0*M-1.0)*BR
      CALL BESNKS(EIG,3,FK)
      HK=0.5*SIJ*EIG*(FK(1)+FK(3))+FK(3)*COS(B*ZIJ)
      HM(II,J1)=HM(II,J1)+HK*A2
      HM(I2,J2)=HM(I2,J2)+HK*A3
      380 CONTINUE
      M=0
      DO 400 I=NUF1,NEGF
      M=M+1
      EIG=(2.0*M-1.0)*BR
      CALL BESNKS(EIG,3,FK)
      HM(I,1)=EIG*HS/4.0*FK(2)*(FK(1)+FK(3))
  
```

```

115 400 CONTINUE
    600 CONTINUE
    C
    C FREE-SURFACE BOUNDARY CONDITION
    C
120 DO 650 I=1,NUFSF
    II=JFS(I)
    HM(II,1)=1.0
    IF(II.EQ.1) GO TO 640
    KM=MINO(II,NFBAND)
    DO 630 K=2,KM
    IK=II-K+1
    630 HM(IK,K)=0.0
    640 DO 650 J=2,NFBAND
    650 HM(II,J)=0.0
    C
    C FORM MATRICES DO AND DJ
    C
130 DO 700 I=1,NEGF
    HB(I)=0.
    DO 700 J=1,NMD
    HL(I,J)=0.
    700 NN=NUINTF-1
    DO 750 I=1,NN
    J=I+1
    RIJ=-R(I)+R(J)
    ZIJ=Z(I)-Z(J)
    SIJ=SQRT(RIJ**2+ZIJ**2)
    CSN=ZIJ/SIJ
    SSN=RIJ/SIJ
    DO 750 K=1,2
    A1=(1.0-SS(K))/2.0
    A4=(1.0+SS(K))/2.0
    RF=(R(I)*A1+R(J)*A4)*ROW
    HB(I)=HB(I)+RF*A1*ZIJ/2
    HB(J)=HB(J)+RF*A4*ZIJ/2
    DO 750 M=1,NMO
    TI=D(M,3*I-2)*CSN+D(M,3*I-1)*SSN
    TJ=D(M,3*J-2)*CSN+D(M,3*J-1)*SSN
    AF=TI*A1+TJ*A4
    HL(I,M)=HL(I,M)+RF*A1*SIJ*AF/2.0
    HL(J,M)=HL(J,M)+RF*A4*SIJ*AF/2.0
    750 CONTINUE
    C
    C INITIALIZE BI AND BII
    C
160 DO 770 M=1,NMO
    BI(M)=0.
    DO 770 N=1,NMO
    770 BII(M,N)=0.
    CALL BANS1(R,NEGF,NFBAND,HM,HB,1)
    CALL BANS1(R,NEGF,NFBAND,HM,HB,2)
    DO 780 I=1,NUINTF
    DO 780 M=1,NMO
    780 D(M,I)=HL(I,M)/ROW
    DO 790 M=1,NMO
    790 CALL BANS1(R,NEGF,NFBAND,HM,HL(1,M),2)

```

```

C
C
C
175      RESET FREE-SURFACE BOUNDARY CONDITION
      DO 800 I=1,NUFSF
      II=IJFS(I)
      IF(II.GT.NUINTF) GO TO 800
      HB(II)=0.
      DO 799 M=1,NMO
      HL(II,M)=0.
      799 HL(II,M)=0.
      800 CONTINUE
      PRINT 2001
      CALL PRINTA(HB,NEGF,1)
      PRINT 2002
      CALL PRINTA(HL,NEGF,NMO)
      NWALL=0
      DO 805 J=1,NUINTF
      IF (IJBC(J).GT.0) NWALL=NWALL+1
      805 CONTINUE
      WRITE (9) NWALL
      DO 810 J=1,NUINTF
      IF (IJBC(J).GT.0) WRITE (9) IJBC(J),HB(J),(HL(J,M),M=1,NMO)
      DO 810 M=1,NMO
      BI(M)=BI(M)+D(M,J)*HB(J)
      DO 810 N=M,NMO
      BII(M,N)=BII(M,N)+D(M,J)*HL(J,N)
      810 BII(N,M)=BII(M,N)
      PRINT 2010
      PRINT 2050, (BI(I),I=1,NMO)
      PRINT 2012
      PRINT 2050, ((BII(I,J),I=1,NMO),J=1,NMO)
      DO 850 I=1,NMO
      BII(I,I)=1.+BII(I,I)
      850 BII(I,I)=1.+BII(I,I)
      DO 870 I=1,NMO
      DO 870 M=1,NUMNP
      K=3*M
      TERM=-A(K,I)*SMASS(K)+A(K-2,I)*SMASS(K-2)
      870 BI(I)=BI(I)+TERM
      PRINT 2003
      CALL PRINTA(BI,NMO,1)
      PRINT 2004
      CALL PRINTA(BII,NMO,NMO)
      2001 FORMAT (///** PRES. COEFF. OF RIGID MODE**)
      2002 FORMAT (///** PRES. COEFF. OF FLEX MODES**)
      2003 FORMAT (///** GENERALIZED FORCE VECTOR (EXT) ---- A+BI**)
      2004 FORMAT (///** GENERALIZED MASS MATRIX (EXT) ---- M+BII**)
      2006 FORMAT (IH1//** STRUCTURAL NODAL POINTS ON THE WATER-TANK*,
      1 * INTERFACE*/(10I5))
      2008 FORMAT (//40H WATER NODAL POINTS ON THE FREE SURFACE /(10I5))
      2010 FORMAT (///5H BI )
      2012 FORMAT (///6H BII )
      2050 FORMAT (5X,2E15.6)
      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS 3 SOLEXT 1 DEF LINE 1 REFERENCES 223

VARIABLES	SN	TYPE	RELOCATION	10	33	42	2*207	DEFINED	1
O A		REAL	ARRAY	10	33	42	2*207	DEFINED	1
1430 AF		REAL		155	156	DEFINED	154		
1423 A1		REAL		148	149	154	155	DEFINED	146
1406 A2		REAL		99	99	DEFINED	97		
1407 A3		REAL		99	107	DEFINED	98		
1424 A4		REAL		148	150	154	156	DEFINED	147
1400 B		REAL		95	105	DEFINED	54		
O BI		REAL	ARRAY	10	194	199	208	210	
				DEFINED	1	162	208		
O BII		REAL	ARRAY	10	196	197	201	203	212
				DEFINED	1	164	197	203	
1405 BR		REAL		103	112	DEFINED	95		
1421 CSN		REAL		152	153	DEFINED	143		
O D		REAL	ARRAY	10	2*42	2*152	2*153	194	196
				DEFINED	1	42	169		
1413 EIG		REAL		104	105	113	114	DEFINED	103
1505 FK		REAL	ARRAY	9	104	2*105	113	3*114	
1445 H		REAL	ARRAY	9	66	69			
O HB		REAL	ARRAY	10	149	150	165	166	183
				DEFINED	1	134	149	150	178
1465 HH		REAL	ARRAY	9	69	70	77	DEFINED	63
				70					69
1414 HK		REAL		106	107	DEFINED	105		192
O HL		REAL	ARRAY	10	155	156	169	171	185
				DEFINED	1	136	155	156	180
O HM		REAL	ARRAY	10	77	106	107	165	171
				DEFINED	1	77	106	107	122
				129	51				
2 HS		REAL	FCONST	13	54	114	33	41	51
1363 I		INTEGER		16	17	32	68	3*69	73
				58	59	63	121	134	139
				81	82	114	2*152	2*155	176
				141	148	2*149	2*208	DEFINED	17
				201	4*203	2*207	61	67	80
				40	49	56	167	175	201
				120	133	138			
				204					
1365 II		INTEGER		30	33	58	59	66	75
				86	87	122	123	124	129
				178	180	DEFINED	22	57	73
				121	176				
O IJBC		INTEGER	ARRAY	10	16	22	25	188	2*192
				DEFINED	1				
O IJFS		INTEGER	ARRAY	10	17	121	176	DEFINED	1
1416 IK		INTEGER		127	DEFINED	126			
O IX		INTEGER	ARRAY	10	57	73	75	82	86
				90	92	93	DEFINED	1	
1402 I1		INTEGER		94	95	99	101	2*106	
				DEFINED	86	89			
1403 I2		INTEGER		94	99	102	2*107	DEFINED	87
				99					90



VARIABLES SN TYPE RELOCATION

VARIABLES	SN	TYPE	RELOCATION	93	51	63	3*69	2*70	75	77	129
1375 J		INTEGER		REFS 140	141	2*196	201	2*150	2*153	2*156	188
1367 JJ		INTEGER		4*192 74	135	139	187	DEFINED	50	62	68
1411 J1		INTEGER		REFS 26	42	66	76		2*77		
1412 J2		INTEGER		25	65	75					
1364 K		INTEGER		2*106	DEFINED	101					
1371 KI		INTEGER		2*107	DEFINED	102					
1366 KK		INTEGER		REFS 22	23	24					
1415 KM		INTEGER		97	126	127		32	4*35	2*37	41
1370 M		INTEGER		DEFINED	21	96		146	147	4*207	
2 MBAND		INTEGER		REFS 33	3*42	27	DEFINED	32	41		
1401 N		INTEGER	CNTRL	REFS 25	27	2*37		DEFINED	24	27	
1 NANGLE		INTEGER		REFS 125	DEFINED	124					
3 NBC		INTEGER	CNTRL	REFS 2*33	4*42	101		102	103	111	112
0 NEG		INTEGER	F.P.	REFS 2*153	2*155	2*156		162	164	2*169	171
0 NEGF		INTEGER	F.P.	180	3*194	195		3*196	2*197	206	
4 NF		INTEGER	CNTRL	DEFINED	100	109		111	151	161	168
0 NFBAND		INTEGER	F.P.	170	192	193		205			
0 NMO		INTEGER	F.P.	REFS 12	73	75		82	86	87	89
1417 NN		INTEGER		REFS 97	93	164		3*196	2*197		
6 NPPI		INTEGER		90	163	195					
5 NPPO		INTEGER	CNTRL	DEFINED	55						
1376 NUCOF		INTEGER	CNTRL	REFS 12	12						
0 NUFEI		INTEGER	F.P.	REFS 10	REFS						
0 NUFNP		INTEGER	F.P.	REFS 2*10	49	52		110	133	165	166
0 NUFSF		INTEGER	F.P.	REFS 171	185	DEFINED		1			
1377 NUFI		INTEGER	CNTRL	183		DEFINED					
0 NUINTF		INTEGER	F.P.	REFS 12	124	128		165	166	171	
0 NUMNP		INTEGER		REFS 50	29	135		151	161	163	168
1431 NWALL		INTEGER		2*10	185	192		193	195	199	2*201
0 PI		REAL		170	210	2*212		DEFINED	1		
0 R		REAL	ARRAY	202	DEFINED	137					
1425 RF		REAL		REFS 138							
1420 RIJ		REAL		REFS 12	100	DEFINED		52			
1 ROW		REAL		REFS 12	55	DEFINED		1			
1435 RR		REAL		REFS 79	53	DEFINED		1			
1374 RS		REAL		REFS 10	120	175		DEFINED	1		
1372 S		REAL		REFS 52	17	110		DEFINED	53		
1404 SIJ		REAL	ARRAY	REFS 101	102	110		137	167	177	187
		REAL		REFS 16	21	23					
		REAL		191	DEFINED	1					
		REAL		REFS 12	205						
		REAL		REFS 188	190	DEFINED		186	188		
		REAL		REFS 13	54						
		REAL		REFS 10	2*35						
		REAL		165	171	DEFINED		58	95	2*140	2*148
		REAL		REFS 149	150	155		156	DEFINED	148	
		REAL		REFS 142	144	DEFINED		140			
		REAL		REFS 13	148	169					
		REAL		REFS 9	66	DEFINED		58			
		REAL		REFS 42	39	DEFINED					
		REAL		REFS 36	39	DEFINED		35	36		
		REAL		105	143	144		155	156		

VARIABLES	SN	TYPE	RELOCATION	DEFINED	REFS	94	142	2*207	DEFINED	1	98	146	147
0 SMASS		REAL	ARRAY	REFS	10	10	2*207	2*66	97	98	98	146	147
1433 SS		REAL	ARRAY	REFS	9	9	2*66						
1422 SSN		REAL		DEFINED	14	14							
1373 S1		REAL		REFS	152	152	153	DEFINED	144	144	144		
1432 TERM		REAL		REFS	38	38	39	DEFINED	37	37	37	38	
1426 T1		REAL		REFS	208	208	DEFINED	207					
1427 TJ		REAL		REFS	154	154	DEFINED	152					
7 TRACE		REAL		REFS	154	154	DEFINED	153					
0 W		REAL	ARRAY	REFS	12	12							
0 Z		REAL	ARRAY	REFS	10	10	DEFINED	1					
1410 ZIJ		REAL	ARRAY	REFS	10	10	2*35	2*37	59	59	59	2*94	2*141
1441 ZZ		REAL	ARRAY	REFS	105	105	142	143	149	149	149	150	
FILE NAMES		MODE		DEFINED	99	99	141						
OUTPUT		FMT		REFS	9	9	66	DEFINED	59	59	59		
TAPE9		UNFMT		REFS	17	17	182	184	198	198	198	199	200
EXTERNALS		TYPE		WRITES	16	16							
BANSL1				209	211	211							
BESNKS				WRITES	190	190							
COS		REAL		REFERENCES	171	171							
FORMH				165	166	166							
PRINTA				104	113	113							
SGRT				105									
INLINE FUNCTIONS		TYPE		66									
ABS		REAL		183	185	185							
MINO		INTEGER		36	38	38							
STATEMENT LABELS				DEF LINE	210	210	212						
36 91				REFERENCES	142	142							
42 92				25	28	28							
0 93				29	23	23							
65 94				33	31	31							
0 95				35	30	30							
130 96				43	40	40							
0 97				44	29	29							
0 100				45	21	21							
0 150				51	49	49							
0 200				59	56	56							
0 250				63	61	61							
0 300				70	67	67							
263 320				71	64	64							
0 350				78	72	72							
303 370				83	80	80							
314 371				85	82	82							
322 372				86	2*85	2*85							
330 373				89	85	85							
335 375				92	85	85							
0 380				94	88	88							
0 400				108	96	96							
434 600				115	110	110							
				116	55	55							

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STATEMENT LABELS	DEF LINE	REFERENCES	PROPERTY	INDEX	FROM-TO	LENGTH	PROPERTIES
0 630	127	125		K	21 45	104B	
463 640	128	123		M	29 44	70B	
0 650	129	120	128	I	31 33	3B	INSTACK
0 700	136	133	135	I	40 43	6B	INSTACK
0 750	157	138	145	I	49 51	12B	
0 770	164	161	151	J	50 51	2B	INSTACK
0 780	169	167	168	N	55 116	260B	EXT REFS NOT INNER
0 790	171	170		I	56 59	5B	NOT INNER
0 799	180	179		I	61 63	12B	INSTACK
725 800	181	175	177	I	62 63	2B	INSTACK
0 805	189	187		I	64 71	32B	EXT REFS NOT INNER
0 810	197	191	193	JJ	65 71	27B	EXT REFS NOT INNER
0 850	203	202		I	67 70	16B	NOT INNER
0 870	208	204	205	J	68 70	4B	INSTACK
1275 2001	213	204		J	72 78	26B	NOT INNER
1302 2002	214	184		I	74 78	10B	INSTACK
1307 2003	215	209		J	80 83	10B	INSTACK
1315 2004	216	211		I	96 108	47B	EXITS
1323 2006	217	16		M	100 108	33B	EXT REFS
1334 2008	219	17		I	110 115	17B	EXT REFS
1343 2010	220	198		I	120 129	35B	NOT INNER
1346 2012	221	200		I	125 127	3B	INSTACK
1351 2050	222	199	201	K	128 129	2B	INSTACK
				J	133 136	14B	NOT INNER
				I	135 136	2B	INSTACK
				J	138 157	102B	INSTACK
				K	145 157	63B	EXT REFS NOT INNER
				M	151 157	22B	NOT INNER
				M	161 164	14B	OPT
				M	163 164	2B	INSTACK
				N	167 169	16B	NOT INNER
				I	168 169	3B	INSTACK
				M			INSTACK

SUBROUTINE SOLEXT 76/176 OPT=1 STATIC

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXT REFS
674	790	M	170 171	14B		NOT INNER
711	800	I	175 181	17B		
722	799	M	179 180	2B	INSTACK	
752	805	J	187 189	4B	INSTACK	
761	810	J	191 197	57B		NOT INNER
772		M	192 192	11B		EXT REFS
1005	810	M	193 197	30B		NOT INNER
1025	810	N	195 197	5B	INSTACK	
1066	850	I	202 203	3B	INSTACK	
1073	870	I	204 208	22B		NOT INNER
1103	870	M	205 208	7B	INSTACK	

COMMON BLOCKS LENGTH  
 CNTRL 8  
 FCONST 3

STATISTICS

PROGRAM LENGTH 1736B 990  
 SCM LABELED COMMON LENGTH 13B 11  
 52000B SCM USED

```

1      SUBROUTINE BESNKS(X,KMAX,FK)
C*****
C      MODIFIED BESSEL FUNCTIONS OF THE SECOND KIND (K)
C*****
C      DIMENSION FI(50), FK(50)
      IF(X-2.) 2,3,3
2      T=.5*X
      T=T*T
      FK(1)= ((((.00000740*T+.00010750)*T+.00262698)*T+.03488590)*T+
1      .23069756)*T+.42278420)*T-.57721566
      FK(2)= ((((-.00004686*T-.00110404)*T-.01919402)*T-.18156897)*T-
1      .67278579)*T+.15443144)*T+1.
      CALL BESNIS (X,20,FI)
      T2=.5*ALOG(T)
      FK(1)=FK(1)-T2*FI(1)
      FK(2)=FK(2)/X+T2*FI(2)
      T=2./X
      GO TO 5
3      T=2./X
      FK(1)= ((((.00053208*T-.00251540)*T+.00587872)*T-.01062446)*T+
1      .02189568)*T-.07832358)*T+1.25331414
      FK(2)= ((((-.00068245*T+.00325614)*T-.00780353)*T+.01504268)*T-
1      .03659620)*T+.23498619)*T+1.25331414
      T1=EXP(-X)/SQRT(X)
      FK(1)=FK(1)*T1
      FK(2)=FK(2)*T1
5      DO 6 N=3,KMAX
      DK=N-2
6      FK(N)=T*DK*FK(N-1)+FK(N-2)
      RETURN
      END
    
```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	DEFINED	30	18	28	22	24
3	BESNKS	1	32							
VARIABLES	SN	TYPE								
164	DK	REAL		REFS	31	7	15	18		
165	FI	REAL	ARRAY	REFS	7	17	18	27	2*31	
0	FK	REAL	ARRAY	REFS	1	11	13	17	22	
			F.P.	DEFINED	1	31				
0	KMAX	INTEGER		REFS	28	29	31			
163	N	INTEGER	F.P.	REFS	30	30	3*31	29	6*22	31
160	T	REAL		REFS	2*10	2*11	6*11	16	6*24	
			F.P.	DEFINED	9	10	19	21		
162	T1	REAL		REFS	27	28	28	26		
161	T2	REAL		REFS	17	18	18	16		
0	X	REAL	F.P.	REFS	8	9	9	19	21	2*26
				DEFINED	1			15		

EXTERNALS  
 ALOG TYPE ARGS REFERENCES  
 REAL 1 LIBRARY 16  
 BESNIS 3 15  
 EXP REAL 1 LIBRARY 26  
 SORT REAL 1 LIBRARY 26

STATEMENT LABELS  
 0 2 INACTIVE 9 8  
 47 3 21 2\*B  
 101 5 29 20  
 0 6 31 29

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES  
 106 6 N 29 31 6B INSTACK

STATISTICS  
 PROGRAM LENGTH 247B 167  
 52000B SCM USED

```

1      SUBROUTINE BESNIS(X,NMAX,FI)
C
C *****
C      MODIFIED BESSEL FUNCTIONS OF THE FIRST KIND (I)
C *****
C
C      DIMENSION FI(50), PI(200)
SUM=0.
I=X
JMAX=I+21
TZ=2./X
JM2=JMAX+2
DO 4 J=JM2,NMAX
  PI(J)=0.
4 CONTINUE
PI(JMAX+1)=1.E-20
DO 6 J=1,JMAX
  K=JMAX+2-J
  DK=K-1
  PI(K-1)=DK*TZ*PI(K)+PI(K+1)
6 SUM=SUM+PI(K)
SUM=SUM+SUM
A=EXP(X)/(PI(1)+SUM)
DO 8 N=1,NMAX
  FI(N)=A*PI(N)
  RETURN
  END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
3 BESNIS	1	26

VARIABLES	SN	TYPE	RELOCATION	REFS	DEFINED	REFS	DEFINED
70 A		REAL		25	DEFINED	23	DEFINED
67 DK		REAL		20	DEFINED	19	DEFINED
0 FI		REAL		7	DEFINED	1	DEFINED
61 I		INTEGER	ARRAY	10	DEFINED	9	DEFINED
65 J		INTEGER		14	18	17	17
62 JMAX		INTEGER		12	16	18	DEFINED
64 JM2		INTEGER		13	DEFINED	12	DEFINED
66 K		INTEGER		19	3*20	21	18
71 N		INTEGER		2*25	DEFINED	24	DEFINED
0 NMAX		INTEGER		13	24	21	1
72 PI		REAL	ARRAY	7	2*20	23	25
60 SUM		REAL		14	16	20	
63 TZ		REAL		21	2*22	23	8
0 X		REAL		20	DEFINED	11	21
EXTERNALS		REAL		9	11	23	1
EXP		REAL	REFERENCES				22
			1 LIBRARY				
			23				

STATEMENT LABELS	DEF LINE	REFERENCES
0 4	15	13
0 6	21	17
0 8	25	24

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
16 4	J	13 15	2B	INSTACK
30 6	J	17 21	10B	INSTACK
52 8	N	24 25	3B	INSTACK

STATISTICS  
 PROGRAM LENGTH 402B 258

52000B SCM USED



```

1      SUBROUTINE INT(R, Z, ICODE, IX, OIL, DUMMY1, INTE, ROIL,
      1      NUNPIN, NUELIN, NUNPIN, NUELIN)
C*****
C      READ AND PRINT INTERIOR FLUIDS ELEMENT PROPERTIES
C*****
C      DIMENSION R(NUNPIN), Z(NUNPIN), IX(NUELIN, 4), OIL(NUELIN)
      DIMENSION DUMMY1(NUELIN), INTE(NUELIN)
      INTEGER DUMMY1
      LOGICAL OIL, INTE
C
C      INPUT NODAL POINT DATA--
C      IF NODAL POINT IS ON STRUCTURAL WALL, THEN ICODE IS NO. OF
C      CORRESPONDING STRUCTURAL NODE;
C      IF NODAL POINT IS ON BOTH WALL AND INTERFACE,
C      THEN ICODE IS -(NO. OF CORRESPONDING STRUCTURAL NODE)
C
      L=0
      20 READ 1002, N, ICODE(N), R(N), Z(N), MOD, N LIM, FACR, FACZ
      LI=L+1
      IF (N-LI) 90, 70, 30
      30 IF (L. LE. 0) GO TO 80
      DIV=N-L
      DR=(R(N)-R(L))/DIV
      DZ=(Z(N)-Z(L))/DIV
      M=N-1
      DO 40 K=L1, M
      R(K)=R(K-1)+DR
      40 Z(K)=Z(K-1)+DZ
      GO TO 70
      50 LI=N+1
      IF (FACR. LE. 0. 0) FACR=1. 0
      IF (FACZ. LE. 0. 0) FACZ=1. 0
      PRINT 2100, MOD, N LIM, FACR, FACZ
      60 N=N+1
      NI=N-MOD
      N2=N1-MOD
      IF (N1. LE. 0. OR. N2. LE. 0) GO TO 100
      R(N)=R(N1)+FACR*(R(N1)-R(N2))
      Z(N)=Z(N1)+FACZ*(Z(N1)-Z(N2))
      ICODE(N)=0
      IF (N. LT. N LIM) GO TO 60
      MOD=0
      70 L=N
      IF (MOD. GT. 0) GO TO 50
      IF (N-NUNPIN) 20, 120, 110
      80 PRINT 2130
      STOP
      90 PRINT 2140, N
      STOP
      100 PRINT 2150
      STOP
      110 PRINT 2160, N, NUNPIN
      STOP
      120 CONTINUE

```

```

60      N=0
130     READ 1003, M, (IX(M,I), I=1,4)
140     N=N+1
      IF (M.EQ.N) GO TO 160
      DO 150 I=1,4
150     IX(N,I)=IX(N-1,I)+1
160     CONTINUE
65     IF (N.EQ.NUELIN) GO TO 180
      IF (N.EQ.M) GO TO 130
      GO TO 140

      C
      C
      C
70     C INITIALIZE LOGICAL ARRAYS
180     DO 274N=1,NUELIN
      OIL(N)=.FALSE.
274     INTE(N)=.FALSE.
      DO 280N=1,NUELOIL
280     OIL(N)=.TRUE.
75     READ 1020, (DUMMY1(I), I=1,NUINTIN)
      DO 300I=1,NUINTIN
      N=DUMMY1(I)
      INTE(N)=.TRUE.
80     CONTINUE

      C
      C
      C
85     C PRINT INPUT PARAMETERS
      PRINT 1000
      PRINT 400, ROIL
      PRINT 600
      DO 310 NOD=1,NUNPIN
310     PRINT 700, NOD, R(NOD), Z(NOD), ICODE(NOD)
      PRINT 800
      DO 320 N=1,NUELIN
320     PRINT 900, N, (IX(N,I), I=1,4), OIL(N), INTE(N)
400     FORMAT (7X, #ROIL=#, F12.5, * --- DENSITY OF OIL*)
600     FORMAT (/6X, #NODE#, 15X, #R-ORD#, 15X, #Z-ORD#, 15X, #ICODE#/)
700     FORMAT (110, 2F20.5, I20)
800     FORMAT (/73X, #ELEMENT#, 5X, #NODE1#, 5X, #NODE2#, 5X, #NODE3#, 5X,
1     #NODE4#, 12X, #OIL#, * INTERFACE#/)
900     FORMAT (5110, 5X, 2L10)
1000    FORMAT (1H1, * FINITE ELEMENT ANALYSIS OF TANK INTERIOR: #/)
1002    FORMAT (215, 2F10.0, 2I5, 2F10.0)
1003    FORMAT (16I5)
1020    FORMAT (16I5)
2100    FORMAT (21H GENERATION WITH MOD=13, 3X, 6H MLIM=14, 3X, 6H FACR=F10.5,
13X, 6H FACZ=F10.5)
2130    FORMAT (28H FIRST JOINT CARD IS MISSING)
2140    FORMAT (31H COORDINATE CARD FOR JOINT NO. 15, 16H NOT IN SEQUENCE)
2150    FORMAT (42H INSUFFICIENT INFORMATION TO GENERATE MESH)
2160    FORMAT (14H JOINT NUMBER 15, 21H EXCEEDS GIVEN NUNPIN= 15)
      RETURN
      END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
3 INT	1	108

VARIABLES	SN	TYPE	RELOCATION
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542 DIV	26	REAL	REFS	27	DEFINED	25	DEFINED	26	DEFINED	27	DEFINED	28	DEFINED	29	DEFINED	30	DEFINED	31	DEFINED	32	DEFINED	33	DEFINED	34	DEFINED	35	DEFINED	36	DEFINED	37	DEFINED	38	DEFINED	39	DEFINED	40	DEFINED	41	DEFINED	42	DEFINED	43	DEFINED	44	DEFINED	45	DEFINED	46	DEFINED	47	DEFINED	48	DEFINED	49	DEFINED	50	DEFINED	51	DEFINED	52	DEFINED	53	DEFINED	54	DEFINED	55	DEFINED	56	DEFINED	57	DEFINED	58	DEFINED	59	DEFINED	60	DEFINED	61	DEFINED	62	DEFINED	63	DEFINED	64	DEFINED	65	DEFINED	66	DEFINED	67	DEFINED	68	DEFINED	69	DEFINED	70	DEFINED	71	DEFINED	72	DEFINED	73	DEFINED	74	DEFINED	75	DEFINED	76	DEFINED	77	DEFINED	78	DEFINED	79	DEFINED	80	DEFINED	81	DEFINED	82	DEFINED	83	DEFINED	84	DEFINED	85	DEFINED	86	DEFINED	87	DEFINED	88	DEFINED	89	DEFINED	90	DEFINED	91	DEFINED	92	DEFINED	93	DEFINED	94	DEFINED	95	DEFINED	96	DEFINED	97	DEFINED	98	DEFINED	99	DEFINED	100	DEFINED
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FILE NAMES	MODE	REFERENCES
INPUT	FMT	21
OUTPUT	FMT	36
		88
		89

STATEMENT LABELS	DEF LINE	REFERENCES
11 20	21	48
0 30	24	23
0 40	31	29
55 50	33	47
67 60	37	44

STATEMENT LABELS  
 112 70  
 120 80  
 123 90  
 126 100  
 131 110  
 134 120  
 135 130  
 152 140  
 0 150  
 166 160  
 172 180  
 0 274  
 0 300  
 0 310  
 0 320  
 414 400  
 432 600  
 431 700  
 434 800  
 446 900  
 451 1000  
 460 1002  
 464 1003  
 466 1020  
 470 2100  
 501 2130  
 506 2140  
 515 2150  
 523 2160

DEF LINE REFERENCES  
 46 23  
 49 24  
 51 23  
 53 40  
 55 48  
 57 48  
 59 66  
 60 67  
 63 62  
 64 61  
 71 65  
 73 71  
 75 74  
 80 77  
 88 87  
 91 90  
 92 85  
 93 86  
 94 88  
 95 89  
 97 91  
 98 84  
 99 21  
 100 59  
 101 76  
 102 36  
 104 49  
 105 51  
 106 53  
 107 55

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LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
47	40	K	29 31	48	INSTACK
140		I	59 59	11B	EXT REFS
163	150	I	62 63	2B	INSTACK
177	274	N	71 73	2B	INSTACK
206	280	N	74 75	2B	INSTACK
223	300	I	77 80	3B	INSTACK
235	310	NOD	87 88	13B	EXT REFS
252	320	N	90 91	24B	EXT REFS
255		I	91 91	11B	EXT REFS

STATISTICS  
 PROGRAM LENGTH 565B  
 52000B SCM USED 373

```

1  SUBROUTINE BNDWTH(R, Z, IX, OIL, INTE, NUMEL, NUMNOD, NBAND)
   DIMENSION R(NUMNOD), Z(NUMNOD), IX(NUMEL, 4), OIL(NUMEL), INTE(NUMEL)
   LOGICAL OIL, INTE
   MAXDIF=0
   DO 10 N=1, NUMEL
   DO 10 I=1, 3
   JMIN=I+1
   DO 10 J=JMIN, 4
   IDIF=IABS(IX(N, I))-IX(N, J)
   IF (IDIF.GT. MAXDIF) MAXDIF=IDIF
10  CONTINUE
C
C  CHECK FOR INCREASE IN BANDWIDTH DUE TO INTERELEMENT
C  COMBINATIONS OF NODE POINTS NEAR INTERFACE
C
15  N1=0
   N2=0
20  N1=N1+1
   N2=N2+1
   IF (N1.GT. NUMEL) GO TO 40
   IF (.NOT. INTE(N1)) GO TO 20
   IF (OIL(N1)) I1=1
   IF (OIL(N1)) J1=2
   IF (OIL(N1)) I2=4
   IF (.NOT. OIL(N1)) I1=4
   IF (.NOT. OIL(N1)) J1=3
   IF (.NOT. OIL(N1)) I2=1
   R1=R(IX(N1, I1))
   Z1=Z(IX(N1, I1))
30  N2=N2+1
   IF (N2.GT. NUMEL) PRINT 100
   IF (N2.GT. NUMEL) STOP
   R2=R(IX(N2, I2))
   Z2=Z(IX(N2, I2))
   IF (R1.NE. R2. OR. Z1.NE. Z2) GO TO 30
C
C  "MATCHING" ELEMENT ALONG INTERFACE FOUND
C
40  IDIF1=IABS(IX(N1, I1))-IX(N2, 1)
   IDIF2=IABS(IX(N1, I1))-IX(N2, 2)
   IDIF3=IABS(IX(N1, I1))-IX(N2, 3)
   IDIF4=IABS(IX(N1, I1))-IX(N2, 4)
   IDIF5=IABS(IX(N1, J1))-IX(N2, 1)
   IDIF6=IABS(IX(N1, J1))-IX(N2, 2)
   IDIF7=IABS(IX(N1, J1))-IX(N2, 3)
   IDIF8=IABS(IX(N1, J1))-IX(N2, 4)
   IDIF=MAX0(IDIF1, IDIF2, IDIF3, IDIF4, IDIF5, IDIF6, IDIF7, IDIF8)
   IF (IDIF.GT. MAXDIF) MAXDIF=IDIF
   N2=0
   GO TO 20
C
45  GO TO 20
C
50  CONTINUE
   NBAND=2*MAXDIF+1
100 FORMAT (* ELEMENT NOT FOUND*)
   RETURN
   END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	7	9	6	46	2*38
3 BNDWTH	1	53			2*10	2*47	9		
VARIABLES	SN	TYPE							
227 I	INTEGER			REFS	2*40	2*41	2*43	1	2*45
232 IDIF	INTEGER			REFS	27	28	39	40	41
244 IDIF1	INTEGER			REFS	21	24			
245 IDIF2	INTEGER			REFS	32	33	23	26	
246 IDIF3	INTEGER			REFS	9	DEFINED			
247 IDIF4	INTEGER			REFS	8	DEFINED			
250 IDIF5	INTEGER			REFS	42	43	45	DEFINED	25
251 IDIF6	INTEGER			REFS	10	47	51	DEFINED	47
252 IDIF7	INTEGER			REFS	2*9	DEFINED			
253 IDIF8	INTEGER			REFS	1	51			
0 INTE	LOGICAL	F. P.		REFS	3*2	5	30	31	
0 IX	INTEGER	F. P.		REFS	1				
235 I1	INTEGER			REFS	2*2	DEFINED			
237 I2	INTEGER			REFS	18	DEFINED			
231 J	INTEGER			REFS	25				
230 JMIN	INTEGER			REFS	26				
236 J1	INTEGER			REFS	43				
225 MAXDIF	INTEGER			REFS	29				
226 N	INTEGER			REFS	41				
0 NBAND	INTEGER	F. P.		REFS	17				
0 NUMEL	INTEGER	F. P.		REFS	2				
0 NUMNOD	INTEGER	F. P.		REFS	26				
233 N1	INTEGER			REFS	2				
234 N2	INTEGER			REFS	26				
0 OIL	LOGICAL	F. P.		REFS	1				
0 R	REAL	F. P.		REFS	2				
240 R1	REAL			REFS	34				
242 R2	REAL			REFS	34				
0 Z	REAL	F. P.		REFS	2				
241 Z1	REAL			REFS	34				
243 Z2	REAL			REFS	34				

FILE NAMES	MODE	WRITES	30	39	40	41	42	43	44
OUTPUT	FMT								
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES					
IABS	INTEGER	1	INTRIN	9					
MAXO	INTEGER	0	INTRIN	45					

STATEMENT LABELS	DEF LINE	REFERENCES	6	8
0 10	11	5		
42 20	18	20	49	
106 30	29	34		
207 40	50	19		
220 100	52	30		

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
12 10	N	5 11	27B	NOT INNER
13 10	I	6 11	23B	NOT INNER
25 10	J	8 11	6B	INSTACK

STATISTICS

PROGRAM LENGTH 260B 176  
 52000B SCM USED

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```

1 SUBROUTINE SOLINT(A,BI,BII,R,Z,ICODE,IX,D,HM,HB,HL,
    RO1,NUMEL,NBAND,NP,NEG,NMO,NUELOIL)
    C
5 DIMENSION A(NEG,1),BI(NMO),BII(NMO,NMO),IX(NUMEL,4),R(NP),Z(NP),
    ICODE(NP),HM(NP,NBAND),HB(NP),HL(NP,NMO),D(NMO,1)
    COMMON /FCONST/ PI,ROW,HS
    DATA SS /-.57735026918963, .57735026918963/
10 DO 30 I=1,NP
    HB(I)=0.
    DO 22 M=1,NMO
    D(M,1)=0.
22 HL (I,M)=0.
30 HM(I,J)=0.
    DO 100 N=1,NUMEL
    IJ(1)=0
    IJ(2)=0
    IJ(3)=0
    IK=0
    RO=ROW
    IF (N.LE. NUELOIL) RO=RO1*ROW
    DO 60 I=1,4
    II=IX(N,I)
    IF (ICODE(II).EQ.0) GO TO 52
    IK=IK+1
    IJ(IK)=II
52 RR(I)=R(II)
60 ZZ(I)=Z(II)
    DO 65 I=1,4
    DO 65 J=1,4
65 HH(I,J)=0.
    DO 70 II=1,2
    DO 70 JJ=1,2
    CALL FORMH(SS(II),SS(JJ),RR,ZZ,H)
    DO 68 I=1,4
    DO 68 J=1,4
    HH(I,J)=HH(I,J)+H(I,J)
68 HH(J,I)=HH(I,J)
70 CONTINUE
    DO 80 I=1,4
    II=IX(N,I)
    DO 80 J=1,4
    JJ=IX(N,J)-II+1
    IF (JJ.LT.1) GO TO 80
80 CONTINUE
    HM(II,JJ)=HM(II,JJ)+HH(I,J)/RO
    IF (IK.LT.2) GO TO 100
    NN=IK-1
    DO 85 I=1,NN
    II=IJ(I)
    JJ=IJ(I+1)
    I1=IABS(ICODE(II))
    J1=IABS(ICODE(JJ))
    RIJ=-R(II)+R(JJ)
    ZIJ=Z(II)-Z(JJ)
    SIJ=SGRT(RIJ**2+ZIJ**2)*SIGN(1.,ZIJ)

```

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```

60      CSN=-ZIJ/SIJ
        SSN=-RIJ/SIJ
        CSN=ABS(CSN)
        IF (ZIJ.GT.O.) SSN=-SSN
        ZIJ=ABS(ZIJ)
        DO 85 K=1,2
          A1=(1.-SS(K))/2.
          A4=(1.+SS(K))/2.
          RF=R(II)*A1+R(JJ)*A4
          RRR=RF*SIJ*CSN/2.
          HB(II)=HB(II)+RRR*A1
          HB(JJ)=HB(JJ)+RRR*A4
        DO 85 M=1,NMO
          TI=A(3*II-2,M)*CSN + A(3*II-1,M)*SSN
          TJ=A(3*JI-2,M)*CSN + A(3*JI-1,M)*SSN
          AF=(TI*A1+TJ*A4)*SIJ/2.*RF
          HL(II,M)=HL(II,M)+AF*A1
          HL(JJ,M)=HL(JJ,M)+AF*A4
          D(M,II)=D(M,II)+AF*A1
          D(M,JJ)=D(M,JJ)+AF*A4
        85 CONTINUE
        100 CONTINUE
        CALL BANSL1(R,NP,NBAND,HM,HB,1)
        CALL BANSL1(R,NP,NBAND,HM,HB,2)
        DO 110 M=1,NMO
          110 CALL BANSL1(R,NP,NBAND,HM,HL(1,M),2)
              NWALL=0
        DO 130 I=1,NP
          130 IF (ICODE(I).NE.O) NWALL=NWALL+1
              WRITE (9) NWALL
              PRINT 1020
        DO 200 I=1,NP
          IF (ICODE(I).EQ.O) GO TO 200
          WRITE (9) IABS(ICODE(I)),HB(I),(HL(I,M),M=1,NMO)
          PRINT 1025, I,HB(I),(HL(I,M),M=1,NMO)
        DO 150 M=1,NMO
          BI(M)=BI(M)+D(M,I)*HB(I)
        DO 150 N=M,NMO
          BII(M,N)=BII(M,N)+D(M,I)*HL(I,N)
        150 BII(N,M)=BII(M,N)
        200 CONTINUE
        PRINT 1030
        CALL PRINTA(BI,NMO,1)
        PRINT 1031
        CALL PRINTA(BII,NMO,NMO)
        1020 FORMAT (1H1/6X,4HNODE,5X,*PRES. COEFF. UNDER RIGID MODE*,6X,
        1 *PRES. COEFF. UNDER FLEX MODES*/)
        1025 FORMAT (5X,14,15X,E10,3,15X,5E15,3,/(49X,5E15,3))
        1030 FORMAT (///5X,*GENERALIZED FORCE VECTOR (EXT + INT) --- A+BI*)
        1031 FORMAT (///5X,*GENERALIZED MASS MATRIX (EXT + INT) --- M+BII*)
        RETURN
        END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES																		
3 SOLINT	1	108																		
VARIABLES	SN	TYPE	RELOCATION	REFS	ARRAY	F.P.														
0 A		REAL		REFS																
704 AF		REAL		REFS																
676 A1		REAL		DEFINED																
677 A4		REAL		REFS																
0 BI		REAL	F.P.	DEFINED																
0 BII		REAL	F.P.	REFS																
673 CSN		REAL		97																
0 D		REAL		REFS																
736 H		REAL		REFS																
0 HB		REAL	F.P.	REFS																
716 HH		REAL		94																
0 HL		REAL	F.P.	REFS																
0 HM		REAL	F.P.	39																
2 HS		REAL		REFS																
655 I		INTEGER	FCONST	REFS																
0 ICODE		INTEGER	F.P.	REFS																
663 II		INTEGER		DEFINED																
760 IJ		INTEGER		REFS																
661 IK		INTEGER		REFS																
0 IX		INTEGER	F.P.	REFS																
666 II		INTEGER		REFS																
657 J		INTEGER		DEFINED																
664 JJ		INTEGER		REFS																
667 J1		INTEGER		REFS																
675 K		INTEGER		REFS																
656 M		INTEGER		REFS																
660 N		INTEGER		REFS																
0 NBAND		INTEGER	F.P.	REFS																

VARIABLES	SN	TYPE	RELOCATION	REFS	4	DEFINED	1	82	91	92	93
0 NEQ		INTEGER	F.P.	REFS	5*4	DEFINED	1				
0 NMO		INTEGER	F.P.	REFS	100	2*102	70	82	91	92	93
665 NN		INTEGER		REFS	50	DEFINED	49	1			
0 NP		INTEGER	F.P.	REFS	6*4	9	80	81	83	85	87
0 NUOLOIL		INTEGER	F.P.	DEFINED	1						
0 NUMEL		INTEGER	F.P.	REFS	22	DEFINED	1				
705 NHALL		INTEGER	F.P.	REFS	4	DEFINED	16	1			
0 PI		REAL	FCONST	REFS	86	87		84	86		
0 R		REAL	F.P.	REFS	7						
		ARRAY		REFS	4	28	2*55	2*66	80	81	83
		REAL		DEFINED	1						
700 RF		REAL		REFS	67	73	DEFINED	66			
670 RIJ		REAL		REFS	57	59	DEFINED	55			
662 RO		REAL		REFS	46	DEFINED	21	22			
1 ROW		REAL	FCONST	REFS	7	21	22				
0 RO1		REAL	F.P.	REFS	22	DEFINED	1				
706 RR		REAL	ARRAY	REFS	6	35	DEFINED	28			
701 RRR		REAL		REFS	68	69	DEFINED	67			
672 SIJ		REAL		REFS	58	59	DEFINED	73	DEFINED	57	
756 SS		REAL	ARRAY	REFS	6	2*35	64	65	DEFINED	59	61
674 SSN		REAL		REFS	61	71	72	DEFINED	59	61	
702 TI		REAL		REFS	73	DEFINED	71				
703 TJ		REAL		REFS	73	DEFINED	72				
0 Z		REAL	F.P.	REFS	4	29	2*56	DEFINED	1		
671 ZIJ		REAL	ARRAY	REFS	2*57	58	61	62	DEFINED	56	
712 ZZ		REAL	ARRAY	REFS	6	35	DEFINED	29	DEFINED		

FILE NAMES	MODE	WRITES	88	92	99	101
OUTPUT	FMT	WRITES	87	91		
TAPE9	UNFMT					

EXTERNALS	TYPE	ARGS	REFERENCES	81	83
BANSL1		6	80		
FORMH		5	35		
PRINTA		3	100		
SGRT	REAL	1 LIBRARY	57		

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES	62	91
ABS	REAL	1	INTRIN	60		
IABS	INTEGER	1	INTRIN	53		
SIGN	REAL	2	INTRIN	57		

STATEMENT LABELS	DEF LINE	REFERENCES	45	70	95
0 22	13	11			
0 30	15	9			
66 52	28	25	14		
0 60	29	23			
0 65	32	30	31		
0 68	39	36	37		
0 70	40	33	34		
165 80	47	41	43		
0 85	78	50	63		
316 100	79	16	48		
0 110	83	82			
0 130	86	85			
0 150	97	93			

STATEMENT LABELS	DEF LINE	REFERENCES	90
466 200	98	89	
613 1020	103	88	
625 1025	105	92	
632 1030	106	99	
641 1031	107	101	

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
15	30	I	9 15	26B	NOT INNER
26	22	M	11 13	2B	INSTACK
36	30	J	14 15	2B	INSTACK
44	100	N	16 79	255B	EXT REFS NOT INNER
62	60	I	23 29	10B	INSTACK
75	65	I	30 32	12B	NOT INNER
101	65	J	31 32	2B	INSTACK
110	70	II	33 40	32B	EXT REFS NOT INNER
111	70	JJ	34 40	27B	EXT REFS NOT INNER
117	68	I	36 39	16B	NOT INNER
126	68	J	37 39	4B	INSTACK
143	80	I	41 47	27B	NOT INNER
156	80	J	43 47	11B	INSTACK
176	85	I	50 78	120B	EXT REFS NOT INNER
226	85	K	63 78	65B	NOT INNER
265	85	M	70 78	23B	EXT REFS
342	110	M	82 83	14B	OPT
363	130	I	85 86	3B	INSTACK
373	200	I	89 98	76B	EXT REFS NOT INNER
403		M	91 91	11B	EXT REFS
423		M	92 92	11B	EXT REFS
436	150	M	93 97	30B	NOT INNER
456	150	N	95 97	5B	INSTACK

COMMON BLOCKS LENGTH 3  
FCONST

STATISTICS  
PROGRAM LENGTH 1053B 555  
SCM LABELED COMMON LENGTH 3B 3  
52000B SCM USED

```

1      SUBROUTINE PRINTA(A, NR, NC)
C*****
C      PRINT MATRIX A.
C*****
C      DIMENSION A(NR,1)
DO 100 J=1, NC, 8
  JH=J+7
  IF (JH-NC) 75, 75, 50
  50 JH=NC
  75 PRINT 1000, (N, N=J, JH)
DO 100 I=1, NR
  100 PRINT 1001, I, (A(I, K), K=J, JH)
  1000 FORMAT (//8I14)
  1001 FORMAT (14, 4X, BE14. 5)
RETURN
END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	VARIABLES	SN	TYPE	RELOCATION	REFS	7	14	14	13	11
3 PRINTA	1	17	0 A		REAL	ARRAY	REFS	2*14	DEFINED	DEFINED	DEFINED	DEFINED
			101 I		INTEGER	F. P.	REFS	9	DEFINED	DEFINED	DEFINED	DEFINED
			76 J		INTEGER		REFS	10	DEFINED	DEFINED	DEFINED	DEFINED
			77 JH		INTEGER		REFS	14	DEFINED	DEFINED	DEFINED	DEFINED
			102 K		INTEGER		REFS	12	DEFINED	DEFINED	DEFINED	DEFINED
			100 N		INTEGER		REFS	8	DEFINED	DEFINED	DEFINED	DEFINED
			0 NC		INTEGER	F. P.	REFS	7	DEFINED	DEFINED	DEFINED	DEFINED
			0 NR		INTEGER	F. P.	REFS	14	DEFINED	DEFINED	DEFINED	DEFINED

FILE NAMES

OUTPUT	MODE	WRITES	REFERENCES
0 50	INACTIVE	11	10
15 75		12	2*10
0 100		14	8
71 1000	FMT	15	12
73 1001	FMT	16	14

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
11	100	J	8 14	41B	EXT REFS NOT INNER
21		N	12 12	4B	EXT REFS NOT INNER
27	100	I	13 14	21B	EXT REFS
33		K	14 14	11B	EXT REFS

STATISTICS  
 PRDGRAM LENGTH 110B  
 52000B SCM USED  
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```

1      SUBROUTINE FORMH(S, T, RR, ZZ, H)
C*****
C      FORM FLUID ELEMENT MATRIX H
C*****
C      DIMENSION RR(4), ZZ(4), H(4, 4), A(4), AS(4), AT(4), AR(4), AZ(4)
SM=1. -S
SP=1. +S
TM=1. -T
TP=1. +T
A(1)=SM*TM/4.
A(2)=SP*TM/4.
A(3)=SP*TP/4.
A(4)=SM*TP/4.
AS(1)=-TM/4.
AS(2)=-AS(1)
AS(3)=TP/4.
AS(4)=-AS(3)
AT(1)=-SM/4.
AT(2)=-SP/4.
AT(3)=-AT(2)
AT(4)=-AT(1)
PZT=AT(1)*ZZ(1)+AT(2)*ZZ(2)+AT(3)*ZZ(3)+AT(4)*ZZ(4)
PZS=AS(1)*ZZ(1)+AS(2)*ZZ(2)+AS(3)*ZZ(3)+AS(4)*ZZ(4)
PRS=AS(1)*RR(1)+AS(2)*RR(2)+AS(3)*RR(3)+AS(4)*RR(4)
PRT=AT(1)*RR(1)+AT(2)*RR(2)+AT(3)*RR(3)+AT(4)*RR(4)
XJ=PRS*PZT-PRT*PZS
R=A(1)*RR(1)+A(2)*RR(2)+A(3)*RR(3)+A(4)*RR(4)
FAC=XJ*R
PSR=PZT/XJ
PTR=-PZS/XJ
PSZ=-PRT/XJ
PTZ=PRS/XJ
DO 50 I=1, 4
AR(I)=AS(I)*PSR+AT(I)*PTR
50 AZ(I)=AS(I)*PSZ+AT(I)*PTZ
DO 100 I=1, 4
DO 100 J=I, 4
H(I, J)=FAC*(AR(I)*AR(J)+AZ(I)*AZ(J))+XJ/R*A(I)*A(J)
100 H(J, I)=H(I, J)
RETURN
END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	SN	TYPE	REFS	7	4*29	2*40	DEFINED	12	13	14
3 FORMH	1	42	ARRAY			15							
VARIABLES			ARRAY			15							
204 A			REAL			REFS	7	4*29	2*40	DEFINED	12	13	14
A7			REAL			REFS	7	2*40	DEFINED	36			

VARIABLES	SN	TYPE	RELOCATION	REFS	7	17	19	4*25	4*26	36	37
210 AS		REAL	ARRAY	DEFINED	16	17	19	4*25	4*26	36	37
214 AT		REAL	ARRAY	DEFINED	7	22	23	4*24	4*27	36	37
224 AZ		REAL	ARRAY	REFS	20	21	22	37			
175 FAC		REAL	ARRAY	REFS	7	2*40	DEFINED				
0 H		REAL	ARRAY	REFS	40	DEFINED	30				
202 I		INTEGER	ARRAY	REFS	7	41	DEFINED	1	40	41	
				REFS	3*36	3*37	39	4*40	2*41		
203 J		INTEGER		DEFINED	35	38					
171 PRS		REAL		REFS	4*40	2*41	DEFINED	37			
172 PRT		REAL		REFS	28	34	DEFINED	26			
176 PSR		REAL		REFS	28	33	DEFINED	27			
200 PSZ		REAL		REFS	36	DEFINED	31				
177 PTR		REAL		REFS	37	DEFINED	33				
201 PTZ		REAL		REFS	36	DEFINED	32				
170 PZS		REAL		REFS	37	DEFINED	34				
167 PZT		REAL		REFS	28	32	DEFINED	25			
174 R		REAL		REFS	28	31	DEFINED	24			
0 RR		REAL	ARRAY	REFS	30	40	DEFINED	29			
0 S		REAL	ARRAY	REFS	7	4*26	4*27	4*29	DEFINED	1	
163 SM		REAL		REFS	8	9	DEFINED	1			
164 SP		REAL		REFS	12	15	DEFINED	8			
0 T		REAL		REFS	13	14	DEFINED	9			
165 TM		REAL		REFS	10	11	DEFINED	1			
166 TP		REAL		REFS	12	13	DEFINED	10			
173 XJ		REAL		REFS	14	15	DEFINED	16	10		
				REFS	30	31	32	33	34		40
0 ZZ		REAL	ARRAY	DEFINED	28	4*24	4*25	DEFINED	1		

STATEMENT LABELS

DEF LINE	REFERENCES
37	35
41	38
	39

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES

INDEX	FROM-TO	LENGTH	PROPERTIES
I	35 37	108	INSTACK
I	38 41	308	NOT INNER
J	39 41	118	INSTACK

STATISTICS  
PROGRAM LENGTH 233B 155  
52000B SCM USED

```

1      SUBROUTINE MSOLVE(A,B,NN,KK)
C*****
C      KK=0 TRIANGULARIZES MATRIXA AND REDUCES, BACKSUBSTITUTES VECTOR B
C      KK=1 REDCES AND BACKSUBSTITUTES VECTOR B ONLY
C*****
C      DIMENSION A(NN,1),B(1)
      DO 450 N=1,NN
        NI=N+1
        B(N)=B(N)/A(N,N)
        IF(N.EQ.NN) GO TO 500
        IF(KK.GE.1) GO TO 350
        DO 250 J=N1,NN
          A(N,J)=A(N,J)/A(N,N)
        DO 300 I=N1,NN
          DO 300 J=I,NN
            A(I,J)=A(I,J)-A(I,N)*A(N,J)
        300 A(J,I)=A(I,J)
        350 CONTINUE
        DO 400 I=N1,NN
          B(I)=B(I)-A(I,N)*B(N)
        450 CONTINUE
        500 NI=N
      N=N-1
      IF(N.EQ.0) RETURN
      DO 600 J=N1,NN
        B(N)=B(N)-A(N,J)*B(J)
      GO TO 500
      END
30

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION
3 MSOLVE	1	26	
VARIABLES	SN	TYPE	RELOCATION
0 A	REAL	ARRAY	F. P.
0 B	REAL	ARRAY	F. P.
116 I	INTEGER		
115 J	INTEGER		
0 KK	INTEGER		F. P.
113 N	INTEGER		
0 NN	INTEGER		F. P.
114 N1	INTEGER		

REFS	8	11	19	22	28
DEFINED	1	15	18	2*22	1
REFS	8	11	2*28	DEFINED	11
REFS	28				
REFS	17	3*18	2*19	2*19	21
REFS	2*15	3*18	2*28	DEFINED	17
REFS	27				
REFS	13	DEFINED	1	2*18	24
REFS	10	4*11	12	4*15	2*22
REFS	25	3*28	DEFINED	9	25
REFS	8	9	12	14	16
REFS	27	DEFINED	1		
REFS	14	16	21	27	DEFINED
REFS					10
REFS					24



SUBROUTINE MSOLVE 76/176 OPT=1 STATIC

STATEMENT LABELS	DEF LINE	REFERENCES
0 250	15	14
0 300	17	16
56 350	20	13
0 400	22	21
0 450	23	9
73 500	24	12
0 600	28	27

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES	EXITS	NOT INNER
11 450	N	9 23	62B			
27 250	J	14 15	3B	INSTACK		
34 300	I	16 19	22B		NOT INNER	
46 300	J	17 19	4B	INSTACK		
65 400	I	21 22	3B	INSTACK		
105 600	J	27 28	3B	INSTACK		

STATISTICS  
PROGRAM LENGTH 141B 97  
52000B SCM USED

```

1  SUBROUTINE BANSL1 (NA, NEG, MBAND, A, B, KK)
   DIMENSION NA(1)
   DIMENSION A(NEG,1), B(1)
   NEG = NEG - 1
   MBAA = MBAND - 1
   IF (KK.EQ.2) GO TO 250

```

REDUCE MATRIX A

```

10  NADR = 1
   DO 140 N=2, MBAA
     NADR = NADR + NEG
     JADR = NADR
     N1 = N - 1
   DO 130 I=1, N1
     IF (A(JADR, NE. O.) GO TO 140
130  JADR = JADR - NEGG
     I=N1
140  NA(N) = I
     M = 0
     NADR = NEG*MBAA
     DO 160 N=MBAND, NEG
       M = M + 1
     NADR = NADR + 1
     JADR = NADR
     N1 = N - 1
   DO 150 I=M, N1
     IF (A(JADR, NE. O.) GO TO 160
150  JADR = JADR - NEGG
     I=N1
160  NA(N) = I
     NA(1) = 1
     JI = 0
     DO 200 J=2, NEG
       IF = NA(J)
       IF1 = IF + 1
       IL = J - 1
       JI = JI + NEG
       JK = JI + NEG
       IFN = IF*NEGG
       IF (IF1.GT. IL) GO TO 185
       JIA = JI - IFN + 1
       DO 180 I=IF1, IL
         KF = MAXO(NA(I), IF)
         KL = I - 1
         KFN = KF*NEGG
         JKA = JK - KFN
         IKA = I*NEG - KFN
         AA = A(JIA)
         DO 170 K=KF, KL
           AA = AA - A(JKA)*A(IKA)
170  JKA = JKA - NEGG
         IKA = IKA - NEGG
         A(JIA) = AA
180  JIA = JIA - NEGG
185  JKA = JK - IFN
     AA = A(J)

```

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```

60 DO 190 K=IF,IL
   CC = A(JKA)/A(K)
   AA = AA - A(JKA)*CC
   A(JKA) = CC
190 JKA = JKA - NEGG
   A(J) = AA
200 CONTINUE
   GO TO 500

C
C   REDUCE VECTOR B AND BACK SUBSTITUTE
C
70 DO 270 N=1,NEGG
   IF(B(N).NE.O.) GOTO 280
270 CONTINUE
   N=NEGG
280 N1 = N + 1
   NADR = N1*NEG
   DO 290 I=N1,NEG
   KF = MAXO(NA(I),N)
   KL = I - 1
   JADR = NADR - KF*NEGG
   BB = B(I)
   DO 285 K=KF,KL
   BB = BB - A(JADR)*B(K)
285 JADR = JADR - NEGG
   B(I) = BB
290 NADR = NADR + NEG
   DO 300 I=N,NEG
300 B(I) = B(I)/A(I)
   NN = NEG
   NADR = NN*NEG
   DO 400 N=1,NEGG
   KF = NA(NN)
   KL = NN - 1
   JADR = NADR - KF*NEGG
   BB = B(NN)
   DO 390 K=KF,KL
   B(K) = B(K) - A(JADR)*BB
390 JADR = JADR - NEGG
   NADR = NADR - NEG
400 NN = NN - 1
500 RETURN
   END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS	16	28	49	57	2*59
3 BANS1	1	99		60	86	95	DEFINED	54	61
VARIABLES	SN	TYPE	ARRAY	F.P.					
0 A	REAL			63					
				81					
				3					
				2*51					
				1					

VARIABLES	SN	TYPE	RELOCATION	REFS	51	54	60	63	DEFINED	49	51
313 AA		REAL		57							
O B		REAL	ARRAY    F.P.	REFS	3	70	79	81	86	93	95
316 BB		REAL		DEFINED	1	83	86	95			
315 CC		REAL		REFS	81	83	95	DEFINED	79	81	93
274 I		INTEGER		REFS	60	61	DEFINED	59			
				REFS	19	31	44	45	48	76	77
				79	3*86	DEFINED	15	18		27	30
				43	85						
300 IF		INTEGER		REFS	36	40	44	58	DEFINED	35	
304 IFN		INTEGER		REFS	42	56	DEFINED	40			
301 IF1		INTEGER		REFS	41	43	DEFINED	36			
312 IKA		INTEGER		REFS	51	53	DEFINED	48	53		
302 IL		INTEGER		REFS	41	43	58	DEFINED	37	34	
277 J		INTEGER		REFS	35	37	57	63	DEFINED	82	95
272 JADR		INTEGER		REFS	16	17	28	29	81	78	82
				96	DEFINED	13	17	25	29		
				92	96						
276 JI		INTEGER		REFS	38	39	42	DEFINED	33	38	
305 JIA		INTEGER		REFS	49	54	55	DEFINED	42	55	
303 JK		INTEGER		REFS	47	56	DEFINED	39			
311 JKA		INTEGER		REFS	51	52	59	60	61	62	
				DEFINED	47	52	56	62			
314 K		INTEGER		REFS	59	81	2*95	DEFINED	50	58	80
				94							
306 KF		INTEGER		REFS	46	50	78	80	92	94	
				DEFINED	44	76	90				
310 KFN		INTEGER		REFS	47	48	DEFINED	46			
O KK		INTEGER	F.P.	REFS	6	DEFINED	1				
307 KL		INTEGER		REFS	50	80	94	DEFINED	45	77	91
275 M		INTEGER		REFS	23	27	20	23			
267 MBAA		INTEGER		REFS	11	21	DEFINED	5			
O MBAND		INTEGER	F.P.	REFS	5	22	DEFINED	1			
271 N		INTEGER		REFS	14	19	26	31	70	73	76
				85	DEFINED	11	22	69	72	89	
O NA		INTEGER	F.P.	REFS	2	35	44	76	90		
			ARRAY	DEFINED	1	19	31	32			
270 NADR		INTEGER		REFS	12	13	24	25	78	84	92
				97	DEFINED	10	12	21	24	74	84
				88	97						
O NEQ		INTEGER	F.P.	REFS	3	4	12	21	22	34	38
				39	74	75	84	85		87	88
266 NEQQ		INTEGER		REFS	17	29	40	46	52	53	55
				62	72	78	82	89	89	92	96
				4							
317 NN		INTEGER		REFS	88	90	91	93	98		
				87	98						
273 N1		INTEGER		REFS	15	18	27	30	74	75	
				DEFINED	14	26	73				

INLINE FUNCTIONS    TYPE    ARGOS    0    INTRIN    DEF LINE    REFERENCES    76  
 MAXO    INTEGER

STATEMENT LABELS  
 O 130    17    DEF LINE    REFERENCES  
 32 140    19    11    16

081

STATEMENT LABELS	DEF LINE	REFERENCES
0 150	29	27
57 160	31	22
0 170	53	50
0 180	55	43
135 185	56	41
0 190	62	58
0 200	64	34
161 250	69	6
0 270	71	69
167 280	73	70
0 285	82	80
0 290	84	75
0 300	86	85
0 390	96	94
0 400	98	89
265 500	99	65

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LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
16 140	N	11 19	20B	NOT INNER
23 130	I	15 17	5B	EXITS
43 160	N	22 31	20B	NOT INNER
50 150	I	27 29	5B	EXITS
66 200	J	34 64	72B	NOT INNER
101 180	I	43 55	34B	NOT INNER
121 170	K	50 53	4B	INSTACK
146 190	K	58 62	5B	INSTACK
162 270	N	69 71	4B	EXITS
173 290	I	75 84	27B	NOT INNER
210 285	K	80 82	4B	INSTACK
230 300	I	85 86	2B	INSTACK
237 400	N	89 98	26B	NOT INNER
252 390	K	94 96	4B	INSTACK

STATISTICS  
PROGRAM LENGTH 356B 238  
52000B SCM USED

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```

1      C
      SUBROUTINE QUAKE(T,XFH,K,DT,FH,NX)
      DIMENSION FH(1)
      DIMENSION T(1),XFH(1)
      DO 3 J=1,K
      3  FH(J)=0.
      PRINT 47, DT*(K-1)
      I=0
      J=1
      TE=0.
      5  I=I+1
      IF(I.GT.NX) RETURN
      10 IF(T(I)-TE) 11,14,12
      11 IF(2.*(TE-T(I))-DT) 14,5,5
      12 IF(J.GT.1) FH(J)=(T(I)-TE)*FH(J-1)+DT*XFH(I)/(T(I)-TE+DT)
      J=J+1
      IF (J.GT. K) RETURN
      TE=TE+DT
      GO TO 10
      14 FH(J)=XFH(I)
      J=J+1
      IF (J.GT. K) RETURN
      TE=TE+DT
      GO TO 5
      47 FORMAT (// * TRUNCATED EARTHQUAKE DATA LENGTH T =*,F10.4, * SEC*/)
      END

```

SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION	REFS
3	QUAKE	1	12 17 22	22
VARIABLES	SN	TYPE	F. P.	
0	DT	REAL		DEFINED
0	FH	REAL		DEFINED
106	I	INTEGER		DEFINED
105	J	INTEGER		DEFINED
0	K	INTEGER		DEFINED
0	NX	INTEGER		DEFINED
0	T	REAL		DEFINED
107	TE	REAL		DEFINED
0	XFH	REAL		DEFINED
FILE NAMES	MODE			
OUTPUT	FMT			
			WRITES	7
STATEMENT LABELS	DEF LINE	REFERENCES		
0	3	6		
24	5	11		
		2*14		
		24		

STATEMENT LABELS	DEF LINE	REFERENCES
27 10	13	19
0 11	14	13
36 12	15	13
57 14	20	13
75 47	25	7

LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
11 3	J	5 6	28	INSTACK

STATISTICS  
 PROGRAM LENGTH 110B 72  
 52000B SCM USED

PFL  
STORAGE ALLOCATION.

COMPASS 3. 6-498.

03/16/81 16. 40. 14.

PAGE 1

BINARY CONTROL CARDS.

ADDRESS	LENGTH
0	15
15	

IDENT PFL  
END

ENTRY POINTS.

PFL 2+



IDENT PFL  
ENTRY PFL

\* \* FIND THE MAXIMUM FIELD LENGTH

0	206614000000000000000002 +	NAME	VFD	24/3LPFL,36/PFL
1	000000000000000000000001	SAVE		
2		PFL	BSSZ	1
3	63110		SB1	X1
4	5110000001	WAIT1	SA1	1
			NZ	X1, WAIT1
5	5110000013 +		SA1	FORM
	43600		MX6	0
6	5160000014 +		SA6	IFL
	74260		SX2	A6
			BX6	X1+X2
7	5160000001		SA6	1
10	54160	WAIT2	SA1	A6
			NZ	X1, WAIT2
11	5110000014 +		SA1	IFL
	21136		AX1	30
			BX6	X1
12	56610		SA6	B1
			EQ	B0, PFL
13	1505156000000000000000 +	FORM	VFD	18/3LMEM, 2/3, 40/0
14		IFL	BSSZ	1
15			END	

. WAIT FOR RA+1 TO CLEAR  
 . FORM THE MEM REQUEST TO ASSERTAIN  
 . PRESENT FIELD LENGTH  
 . PLACE THE CALL AND WAIT FOR RA+1  
 . TO CLEAR  
 . FIELD LENGTH

51000B SCM STORAGE USED 27 STATEMENTS 7 SYMBOLS  
 MODEL 176 ASSEMBLY 0.024 SECONDS 15 REFERENCES

FORM	13	PROGRAM*	2/12	2/25 L	
IFL	14	PROGRAM*	2/14 S	2/20	2/26 L
NAME	0	PROGRAM*	2/06 L		
PFL	2	PROGRAM*	2/02 E	2/06	2/08 L 2/24
SAVE	1	PROGRAM*	2/07 L		
WAIT1	4	PROGRAM*	2/10 L	2/11	
WAIT2	10	PROGRAM*	2/18 L	2/19	

```

1  SUBROUTINE TSTEP(W,BI,BII,DAMP,XFH,XT,C4,C5,Y,VEL,ACEL,YBUF,FH,
    1 ABUF,TEM,NMO,NT,DT,NXFH,NBUF,NBLOCK,NGRD,NTAPE,NG,PLOTT)
C *****
C SOLVE MODAL EQUATION OF MOTION USING STEP-BY-STEP TIME
C INTEGRATION TECHNIQUES.
C *****
C DIMENSION W(1),BI(1),BII(NMO,1),DAMP(1),XFH(1),FH(1),C4(1),C5(1),
    1 Y(1),ABUF(1),VEL(1),ACEL(1),YBUF(1),XT(1),TEM(NMO,1)
    DIMENSION ALINE(8)
    LOGICAL PLOTT
    REWIND NTAPE
    DO 10 I=1,NMO
    DO 10 J=1,NMO
    10 TEM(I,J)=BII(I,J)
    IF (NGRD.EQ.2.AND.NG.EQ.1) GO TO 15
C READ AND PRINT MODAL DAMPING RATIOS
C
C READ 1000, (DAMP(I),I=1,NMO)
    PRINT 2000, (I,DAMP(I),I=1,NMO)
    15 FAC=32.2
C READ AND PRINT TIME HISTORY OF GROUND ACCELERATION
C
C READ 2040, ALINE
    PRINT 2045, ALINE
    IF (ALINE(1).NE.10HCONSTANT ) GO TO 30
C CONSTANT FREQUENCY
    READ 2020, TLATE,OMEGA,HIGH
    DO 25 K=1,NXFH
    XT(K)=(K-1)*TLATE/(NXFH-1)
    XFH(K)=SIN(XT(K)*OMEGA) * HIGH
    25 CONTINUE
    GO TO 35
    30 READ 1001, (XT(K),XFH(K),K=1,NXFH)
    35 CONTINUE
    PRINT 2001, (XT(K),XFH(K),K=1,NXFH)
    IF (.NOT.PLOTT) GO TO 90
    CALL OPLT
    CALL GRAF11(XT,XFH,NXFH,1,"TIME(SEC.)","GRND. ACC.")
    CALL PLOT (0.,0.,999)
    90 DO 100 K=1,NXFH
    100 XFH(K)=XFH(K)*FAC
C GROUND ACCELERATION RECORD IS INTERPOLATED BY EQUAL TIME-INCREMENT
C
C CALL GUAKE(XT,XFH,NT,DT,FH,NXFH)
    WRITE (9) (FH(K),K=1,NT)
C
C1=DT/2.
C2=C1*DT/3.
C3=C2*2
    DO 260 I=1,NMO
    C4(I)=W(I)**2
    C5(I)=2.*DAMP(I)*W(I)

```

```

60      TEM(I,1)=TEM(I,1)+C5(I)*C1+C4(I)*C2
        ACEL(I)=-FH(I)*BI(I)
        CONTINUE
260     CALL MSOLVE(TEM,ACEL,NMD,0)
        M=0
        MC=1
        NBLOCK=0
        DO 265 I=1,NMD
            Y(I)=0.0
            VEL(I)=0.0
            M=M+1
            YBUF(M)=Y(I)
            ABUF(M)=ACEL(I)
265     CONTINUE
        C
270     MC=MC+1
        DO 280 I=1,NMD
            Y(I)=Y(I)+DT*VEL(I)+C3*ACEL(I)
            VEL(I)=VEL(I)+C1*ACEL(I)
            ACEL(I)=-FH(MC)*BI(I)-C5(I)*VEL(I)-C4(I)*Y(I)
280     CONTINUE
        CALL MSOLVE(TEM,ACEL,NMD,1)
        DO 350 I=1,NMD
            VEL(I)=VEL(I)+C1*ACEL(I)
            Y(I)=Y(I)+C2*ACEL(I)
        C
        WRITE ON TAPE2 OR TAPE7 (IN BLOCKS) OF DISPLACEMENT DATA
        M=M+1
        YBUF(M)=Y(I)
        ABUF(M)=ACEL(I)
        IF (MC.EQ.NT.AND.I.EQ.NMD) GO TO 340
        IF (M.LT.NBUF) GO TO 350
        WRITE (NTAPE) (YBUF(J),J=1,NBUF)
        WRITE (NTAPE) (ABUF(J),J=1,NBUF)
        NBLOCK=NBLOCK+1
        M=0
        GO TO 350
340     NBLOCK=NBLOCK+1
        MBUF=M
        WRITE (NTAPE) (YBUF(J),J=1,MBUF)
        WRITE (NTAPE) (ABUF(J),J=1,MBUF)
        M=0
350     CONTINUE
        IF (MC-NT) 360,400,400
360     GO TO 270
400     CONTINUE
1000    FORMAT (7F10.0)
1001    FORMAT (6(F6.3,F6.4))
2000    FORMAT (// * MODE MODAL DAMPING RATIO*/(I4,10X,F10.3))
2001    FORMAT (// * EARTHQUAKE DATA *// (2X,6(F8.4,E12.4)))
2020    FORMAT (3F10.0)
2040    FORMAT (8A10)
2045    FORMAT (I11,1X,8A10)
        RETURN
        END

```

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SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES	RELOCATION		SN	TYPE	DEF LINE	REFERENCES	SN	TYPE	DEF LINE	REFERENCES	SN	TYPE	DEF LINE	REFERENCES	
3 TSTEP	1	112	ARRAY	F.P.													
VARIABLES																	
0 ABUF			ARRAY	F.P.													
0 ACEL			ARRAY	F.P.													
576 ALINE			ARRAY	F.P.													
0 BI			ARRAY	F.P.													
0 BII			ARRAY	F.P.													
571 C1			ARRAY	F.P.													
572 C2																	
573 C3																	
0 C4			ARRAY	F.P.													
0 C5			ARRAY	F.P.													
0 DAMP			ARRAY	F.P.													
0 DT			ARRAY	F.P.													
564 FAC			ARRAY	F.P.													
0 FH			ARRAY	F.P.													
567 HIGH			REAL														
562 I			INTEGER														
563 J			INTEGER														
570 K			INTEGER														
574 M			INTEGER														
0 MBUF			INTEGER	F.P.													
575 MC			INTEGER														
0 NBLOCK			INTEGER	F.P.													
0 NBUF			INTEGER	F.P.													
0 NG			INTEGER	F.P.													
0 NGRD			INTEGER	F.P.													
0 NMO			INTEGER	F.P.													
0 NT			INTEGER														
0 NTAPE			INTEGER														
0 NXFH			INTEGER														
566 OMEGA			REAL														
0 PLOTT			LOGICAL														
0 TEM			REAL														
565 TLATE			REAL														
0 VEL			REAL														
0 W			REAL														
0 XFH			REAL														
0 XT			REAL														

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VARIABLES	SN	TYPE	RELOCATION	DEFINED REFS	33	37	69	77	82	87
0 Y		REAL	ARRAY F.P.	1	33	37	69	77	82	87
0 YBUF		REAL	ARRAY F.P.	9	66	75	91	82	1	69
					91	98		DEFINED		87

FILE NAMES	MODE	READS	WRITES	21	31	37
INPUT	FMT	42		21	31	37
OUTPUT	FMT	61		22	39	
TAPE9	UNFMT	41		50		
VARIABLES USED AS FILE NAMES, SEE ABOVE						

EXTERNALS	TYPE	ARGS	REFERENCES	79
GRAF11		6	42	
MSOLVE		4	61	
OPLT		0	41	
PLOT		3	43	
QUAKE		6	49	
SIN	REAL	1 LIBRARY	34	

STATEMENT LABELS

DEF LINE	REFERENCES	15
0 10	16	14
55 15	23	17
0 25	35	32
102 30	37	29
116 35	38	36
144 90	44	40
0 100	45	44
0 260	60	55
0 265	71	65
251 270	73	103
0 280	78	74
343 340	96	89
362 350	101	80
0 360	103	102
370 400	104	2*102
522 1000	105	21
524 1001	106	37
527 2000	107	22
535 2001	108	39
543 2020	109	31
545 2040	110	27
547 2045	111	28

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
13	10	I	14 16	158	NOT INNER
22	10	J	15 16	28	INSTACK
45		I	22 22	78	EXT REFS
67	25	K	32 35	138	EXT REFS
105		K	37 37	108	EXT REFS
121		K	39 39	108	EXT REFS
150	100	K	44 45	38	INSTACK
211	260	I	55 60	118	INSTACK
243	265	I	65 71	48	INSTACK
265	280	I	74 78	128	INSTACK
306	350	I	80 101	578	EXT REFS

STATISTICS

PROGRAM LENGTH 666B 43B  
52000B SCM USED

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1 SUBROUTINE RESPON(XANG,W,A,STRESX,IJND,IJEL,XBUF,YBUF,YM,X,Y,
 1 SIGX,SIGY,LMM,SSM,STREST,XST,XMAX,STRMAX,TX,TST,YMAX,STTMAX,TY,
 2 TTT,STRESY,HB,HL,FX,FHY,AXBUF,AYBUF,AXM,AYM,
 3 NMO,NEG,ANGLE,NPRINT,NNODE,NNEL,NUMNP,NUMEL,NUM,
 4 NBLOCK,NBUF,NIBUF,IGRAV,DT,NT,NGRD)
 5
 6 *****
 7 SUPERPOSITION OF MODES AND TIME RESPONSES OF DISPLACEMENTS
 8 AND STRESSES
 9 *****
10 COMMON/LS4ARG/LM(12),SS(6,12),XC,YC,ELM(4),S(12,12),MYPE,Q(12)
 11,C(6,6)
12 DIMENSION W(1),A(NEG,1),IJND(1),IJEL(1),XBUF(1),YBUF(1),XM(1),
13 YM(1),X(NEG),Y(NEG),SIGX(6),SIGY(6),STRESX(NUM),STRESY(NUM),
14 LMM(12,10),SSM(6,12,10),XANG(1),XMAX(1),YMAX(1),STRMAX(1),
15 STTMAX(1),TX(1),TST(1),TY(1),TTT(1)
16 DIMENSION STREST(NUM),XST(NEG)
17 DIMENSION HB(NUMNP),HL(NUMNP,NMO),FX(NT),FHY(NT)
18 DIMENSION AXBUF(NBUF),AYBUF(NBUF),AXM(NMO),AYM(NMO)
19 DATA PI/0.01745293/
20 IMAX=3*NUMNP
21 DO 5 I=1,IMAX
22 TX(I)=0.
23 TY(I)=0.
24 PRINT 2005, (W(I),I=1,NMO)
25
26 OUTPUT ANGLES
27
28 READ 1002, (XANG(N),N=1,ANGLE)
29 PRINT 2002, (XANG(N),N=1,ANGLE)
30
31 READ AND PRINT SELECTED NODE CIRCLES AND ELEMENTS FOR OUTPUT
32 PRINTING
33
34 IF (NNODE.EQ.0) GO TO 12
35 IF (NNODE.GE.NUMNP) GO TO 11
36 READ 1010, (IJND(I),I=1,NNODE)
37 PRINT 2010, (IJND(I),I=1,NNODE)
38 GO TO 12
39
40 11 PRINT 2012
41 NNODE=NUMNP
42 IF (NNEL.EQ.0) GO TO 18
43 IF (NNEL.GE.NUMEL) GO TO 15
44 READ 1010, (IJEL(I),I=1,NNEL)
45 PRINT 2020, (IJEL(I),I=1,NNEL)
46 GO TO 18
47
48 15 PRINT 2022
49 NNEL=NUMEL
50 CONTINUE
51
52 REWIND 3
53 DO 20 I=1,NUM
54 STREST(I)=0.
55 DO 21 I=1,NEG
56 XST(I)=0.
57 IF (IGRAV.NE.2) GO TO 24

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60      C
        C      READ FROM TAPE 3 THE STATIC RESPONSES
        C
        C      READ (3) XST
        C      READ (3) STREST
        C      WRITE (3) NUMNP, NUMEL, NMO, DT, NT, NPRINT, IGRAV, NGRD
        C      WRITE (3) XST
        C      WRITE (3) STREST
        C      GO TO 25
70      24 PRINT 2008
        C      WRITE (3) NUMNP, NUMEL, NMO, DT, NT, NPRINT, IGRAV, NGRD
        C      DO 28 MN=1, 10
        C      DO 28 J=1, 12
        C      LMM(J, MN)=0
        C      DO 28 I=1, 6
        C      SSM(I, J, MN)=0.
75      28 CONTINUE
        C      MN=0
        C      REWIND 1
        C      REWIND 4
        C      DO 40 N=1, NUMEL
        C      CALL READ1(LM, 283, N, NUMEL)
        C      MN=MN+1
        C      DO 31 J=1, 12
        C      LMM(J, MN)=LM(J)
        C      DO 31 I=1, 6
        C      SSM(I, J, MN)=SS(I, J)
80      31 CONTINUE
        C      IF (N.EQ.NUMEL) GO TO 32
        C      IF (MN.LT. 10) GO TO 40
        C      32 WRITE(4) LMM
        C      WRITE(4) SSM
        C      MN=0
        C      40 CONTINUE
        C      DO 50 I=1, NEQ
        C      YMAX(I)=0.
        C      Y(I)=0.
        C      50 XMAX(I)=0.0
        C      DO 60 I=1, NUM
        C      STTMAX(I)=0.
        C      60 STRMAX(I)=0.
90      C
        C      REWIND 9
        C      DO 90 I=1, NUMNP
        C      HB(I)=0.
        C      DO 90 MN=1, NMO
        C      DO 100 I=1, 2
        C      READ (9) N, HB(N), (HL(N, MN), MN=1, NMO)
        C      IF (N.WALL.LE.0) GO TO 100
        C      DO 95 J=1, N.WALL
        C      95 READ (9) N, HB(N), (HL(N, MN), MN=1, NMO)
100      100 CONTINUE
        C      READ (9) FHX
        C      IF (NGRD.EG.2) READ (9) FHY
        C
        C      READ FROM TAPE2 AND TAPE7 THE MODAL RESPONSES
        C

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115      C
      REWIND 2
      REWIND 7
      IBLOCK=0
      TS=0.
      IT=1
      NB=NBUFF
      M=0
200     IBLOCK=IBLOCK+1
      IF (IBLOCK.EQ.NBLOCK) NB=M*BUF
      READ (2) (XBUF(J), J=1, NB)
      READ (2) (AXBUF(J), J=1, NB)
      IF (NGRD.EG.2) READ (7) (YBUF(J), J=1, NB)
      IF (NGRD.EG.2) READ (7) (AYBUF(J), J=1, NB)
205     DO 210 I=1, NMD
      M=M+1
      IF (NGRD.EG.2) YM(I)=YBUF(M)
      IF (NGRD.EG.2) AYM(I)=AYBUF(M)
      AXM(I)=AXBUF(M)
210     XM(I)=XBUF (M)
      IF (NNODE.NE.0. OR. NNEL.NE.0) PRINT 2050, TS
      C
      C COMPUTE DISPLACEMENT
      C
      IF (NNODE.NE.0) PRINT 2051
      DO 250 I=1, NUMNP
      SUM1=0.
      SUM2=0.
      SUM3=0.
      DO 220 MN=1, NMD
      SUM1=SUM1+XM(MN)*A(3*I-2, MN)
      SUM2=SUM2+YM(MN)*A(3*I-1, MN)
      SUM3=SUM3+YM(MN)*A(3*I, MN)
220     X(3*I-2)=SUM1*12.
      X(3*I-1)=SUM2*12.
      X(3*I)=SUM3*12.
      DO 230 J=1, 3
      II=3*I-3+J
      XABS=ABS(X(II))
      XX=ABS(XMAX(II))
      IF (XX.GE.XABS) GO TO 230
      XMAX(II)=X(II)
      TX(II)=TS
230     CONTINUE
      IF (NGRD.EG.1) GO TO 234
      SUM1=0.
      SUM2=0.
      SUM3=0.
      DO 232 MN=1, NMD
      SUM1=SUM1+YM(MN)*A(3*I-2, MN)
      SUM2=SUM2+YM(MN)*A(3*I-1, MN)
      SUM3=SUM3+YM(MN)*A(3*I, MN)
232     Y(3*I-2)=SUM1*12.
      Y(3*I-1)=SUM2*12.
      Y(3*I)=SUM3*12.
      DO 233 J=1, 3
      II=3*I-3+J

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175 XABS=ABS(Y(II))
    XX=ABS(YMAX(II))
    IF (XX.GE.XABS) GO TO 233
    YMAX(II)=Y(II)
    TY(II)=TS
233 CONTINUE
234 CONTINUE
    IF (NNODE.EQ.0) GO TO 250
    IF (NUMNP.EQ.NNODE) GO TO 237
    DO 235 II=1,NNODE
235 IF (I.EQ.IJND(II)) GO TO 237
    GO TO 250

C
C COMPUTE PRESSURE
237 CONTINUE
    SUMXP=FHX(IT)*HB(I)
    SUMYP=0.
    IF (NGRD.EQ.2) SUMYP=FHY(IT)*HB(I)
    DO 238 MN=1,NMO
    SUMXP=SUMXP+AXM(MN)*HL(I,MN)
    IF (NGRD.EQ.2) SUMYP=SUMYP+AYM(MN)*HL(I,MN)
238 CONTINUE

C
C COMPUTE AND PRINT FOR DIFFERENT ANGLES
DO 240 J=1,NANGLE
    THETA=XANG(J)*PI
    SUM1= X(3*I-2)*COS(THETA)+Y(3*I-2)*SIN(THETA)+XST(3*I-2)
    SUM2= X(3*I-1)*COS(THETA)+Y(3*I-1)*SIN(THETA)+XST(3*I-1)
    SUM3= X(3*I)*SIN(THETA)+Y(3*I)*COS(THETA)+XST(3*I)
    SUM4= SUMXP*COS(THETA)+SUMYP*SIN(THETA)
240 PRINT 2060, I, SUM1, SUM2, SUM3, SUM4, XANG(J)
250 CONTINUE

C
C WRITE ON TAPES DISPLACEMENTS OF ALL NODAL CIRCLES
WRITE(3) X
IF(NGRD.EQ.2) WRITE (3) Y
C
C COMPUTE ELEMENT STRESSES
C
REWIND 4
IF (NNEL.NE.0) PRINT 2100
N=0
305 READ (4) LMM
    READ (4) SSM
    DO 390 MN=1,10
    N=N+1
    IF (N.GT.NUMEL) GO TO 400
    DO 350 I=1,6
    SIGX(I)=0.
    SIGY(I)=0.
    DO 350 J=1,12
    JJ=LMM(J,MN)
    IF (NGRD.EQ.1) GO TO 350
    SIGY(I)=SIGY(I)+SSM(I,J,MN)*Y(JJ)

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230      350 SIGX(I)=SIGX(I)+SSM(I,J,MN)*X(JJ)
      DO 360 J=1,6
      IF (NGRD.EQ.1) GO TO 360
      SIGY(J)=0.57870*SIGY(J)
      360 SIGX(J)=0.57870*SIGX(J)
      NN=6*N
      DO 365 I=1,6
      II=NN-6+I
      STRESX(II)=SIGX(I)
      SABS=ABS(SIGX(I))
      SMAB=ABS(STRMAX(II))
      IF (SMAB.GE.SABS) GO TO 365
      STRMAX(II)=STRESX(II)
      TST(II)=TS
      365 CONTINUE
      IF (NGRD.EQ.1) GO TO 367
      DO 366 I=1,6
      II=NN-6+I
      STRESY(II)=SIGY(I)
      SABS=ABS(SIGY(I))
      SMAB=ABS(STTMAX(II))
      IF (SMAB.GE.SABS) GO TO 366
      STTMAX(II)=STRESY(II)
      TTT(II)=TS
      366 CONTINUE
      367 CONTINUE
      IF (NNEL.EQ.0) GO TO 390
      IF (NUMEL.EQ.NNEL) GO TO 369
      DO 368 II=1,NNEL
      368 IF (N.EQ.IJEL(II)) GO TO 369
      GO TO 390
      369 DO 370 J=1,NANGLE
      THETA=XANG(J)*PI
      SUM1=SIGX(1)*COS(THETA)+STREST(NN-5)+SIGY(1)*SIN(THETA)-
      SUM2=SIGX(2)*COS(THETA)+STREST(NN-4)+SIGY(2)*SIN(THETA)-
      SUM3=SIGX(3)*COS(THETA)+STREST(NN-3)+SIGY(3)*SIN(THETA)-
      SUM4=SIGX(4)*COS(THETA)+STREST(NN-2)+SIGY(4)*SIN(THETA)-
      SUM5=SIGX(5)*SIN(THETA)+STREST(NN-1)+SIGY(5)*COS(THETA)-
      SUM6=SIGX(6)*SIN(THETA)+STREST(NN)+SIGY(6)*COS(THETA)
      370 PRINT 2110, N, SUM1, SUM2, SUM3, SUM4, SUM5, SUM6, XANG(J)
      390 CONTINUE
      IF (N.LT.NUMEL) GO TO 305
      C
      C WRITE ON TAPE3 STRESSES OF ALL ELEMENTS
      C
      400 WRITE (3) STRESX
      IF (NGRD.EQ.2) WRITE (3) STRESY
      TS=TS+DI*NPRINT
      IT=IT+NPRINT
      M=M+(NPRINT-1)*NM0
      IF ((M+NM0).GT.NB) GO TO 500
      GO TO 205
      500 IF (IBLOCK.GE.NBLOCK) GO TO 550
      M=M-NB
      GO TO 200
      550 ANGLE=0.
      PRINT 2200, ANGLE
      285

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DO 570 I=1, NUMNP
570 PRINT 2205, I, (TX(3*I-3+J), XMAX(3*I-3+J), J=1,3)
PRINT 2210, ANGLE
DO 580 N=1, NUMEL
580 PRINT 2215, N, (TST(6*N-6+I), STRMAX(6*N-6+I), I=1,6)
IF (NGRD.NE.2) RETURN
ANGLE=90.
PRINT 2200, ANGLE
DO 585 I=1, NUMNP
585 PRINT 2205, I, (TY(3*I-3+J), YMAX(3*I-3+J), J=1,3)
PRINT 2210, ANGLE
DO 590 N=1, NUMEL
590 PRINT 2215, N, (TTT(6*N-6+I), STTMAX(6*N-6+I), I=1,6)
1002 FORMAT (8F10.0)
1010 FORMAT (16I5)
2002 FORMAT (//14H ANGLE OUTPUT ,/(10X,F10.0))
2005 FORMAT (// * FREQ OF SYSTEM IN RAD/SEC*/(5X,10F10.4))
2008 FORMAT (1H1/50H STATIC RESPONSES ARE NOT INCLUDED IN TIME HISTORY)
2010 FORMAT (//22H NODAL PTS FOR OUTPUT /(5X,10I10))
2012 FORMAT (//41H OUTPUTS ARE PRINTED FOR ALL NODAL POINTS /)
2020 FORMAT (//23H ELEMENT NO FOR OUTPUT /(5X,10I10))
2022 FORMAT (//37H OUTPUTS ARE PRINTED FOR ALL ELEMENTS /)
2050 FORMAT (////4H T=,F10.4,5H SEC. )
2051 FORMAT (//10X,24H DISPLACEMENT IN INCHES
1/18X,2HNP,10X,1HR,18X,1HZ,18X,1HT,15X,8HPRESSURE,
2 16X,15H ANGLE(DEGREES) /)
2060 FORMAT (15X,15,4(4X,E15.8),10X,F10.4)
2100 FORMAT (//10X,15H STRESS IN PSI
1/15X,6H EL.NO 6X 5HSIG R 7X 5HSIG Z 7X 5HSIG T 6X 6HTAU RZ
26X 6HTAU RT 6X 6HTAU ZT 7X 15H ANGLE(DEGREES) /)
2110 FORMAT (15X,15,6E12.4,5X,F10.4)
2200 FORMAT (1H1/41H DYNAMIC DISPLACEMENT ENVELOPE IN INCHES ///
1 64H -DUE TO HORIZONTAL GROUND MOTION ALONG THE DIRECTION OF ANGLE
2= ,F5.1,////
1 3X,2HNP,6X,4HTIME,11X,1HR,6X,4HTIME,11X,1HZ,6X,4HTIME,11X,1HT)
2205 FORMAT (15,3(2X,F8.2,E12.4))
2210 FORMAT (1H1/32H DYNAMIC STRESS ENVELOPE IN PSI ///
2= ,F5.1,////
1 1X,5HEL.NO,4X,4HTIME,5X,5HSIG R,4X,4HTIME,5X,5HSIG Z,4X,4HTIME,
2 5X,5HSIG T,4X,4HTIME,4X,6HTAU RZ,4X,4HTIME,4X,6HTAU RT,4X,4HTIME,
3 4X,6HTAU ZT)
2215 FORMAT (16,6(F8.2,E10.4))
RETURN
END

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SYMBOLIC REFERENCE MAP (R=2)

ENTRY POINTS	DEF LINE	REFERENCES
3	RESPON	291 329

VARIABLES	SN	TYPE	RELOCATION	REFS	14	145	146	147	164	165	166
2216	0	ANGLE	ARRAY	DEFINED	1				DEFINED	284	292
0	AXBUF	REAL		REFS	285	288	293	296	DEFINED		
0	AXM	REAL	F. P.	REFS	20	133	DEFINED	1	126		
0	AYBUF	REAL	F. P.	REFS	20	192	DEFINED	1	133		
0	AYM	REAL	F. P.	REFS	20	132	DEFINED	1	128		
367	C	REAL	LS4ARG	REFS	20	193	DEFINED	1	132		
0	DT	REAL	F. P.	REFS	12	68	276	DEFINED	1		
126	ELMASS	REAL	LS4ARG	REFS	63						
0	FHX	REAL	LS4ARG	REFS	12	188	DEFINED	1	111		
0	FHY	REAL	F. P.	REFS	19	190	DEFINED	1	112		
0	HB	REAL	F. P.	REFS	19	188	190	DEFINED	1	102	109
0	HL	REAL	F. P.	REFS	19	192	193	DEFINED	1	104	109
2164	I	INTEGER	F. P.	REFS	24	25	26	38	39	45	46
				REFS	54	73	2*84	93	94	95	97
					102	104	131	132	133	134	145
					147	148	149	150	152	164	165
					167	168	169	171	182	188	190
					193	3*200	3*201	3*202	204	223	224
					3*229	236	237	238	246	247	248
					2*290	3*295	2*298	DEFINED	23	26	38
					45	46	53	55	72	83	92
					101	105	129	140	222	235	245
2171	IBLOCK	INTEGER		REFS	290	294	298				
0	IGRAV	INTEGER		REFS	123	124	281	DEFINED	118	123	
2201	II	INTEGER	F. P.	REFS	57	63	68	DEFINED	1		
				REFS	153	154	2*156	157	172	173	2*175
					182	237	239	2*241	242	247	249
					2*251	258	DEFINED	152	171	181	236
					246						
0	IJEL	INTEGER	ARRAY	REFS	14	46	258	DEFINED	1	45	
0	IJND	INTEGER	ARRAY	REFS	14	39	182	DEFINED	1	38	
2163	IMAX	INTEGER		REFS	23	DEFINED	22				
2173	IT	INTEGER		REFS	188	190	277	DEFINED	120	277	127
2167	J	INTEGER		REFS	71	73	2*82	2*84	125	126	289
					128	171	199	204	226	228	
					2*232	261	268	2*287	2*295		
					70	81	108	125	126	127	128
2210	JJ	INTEGER		DEFINED	151	198	225	230	260	287	295
0	LM	INTEGER	ARRAY	REFS	228	229	DEFINED	226			
0	LMM	INTEGER	ARRAY	REFS	12	79	82	DEFINED	1	71	82
2175	M	INTEGER	LS4ARG	REFS	14	88	226	DEFINED			
				REFS	130	131	132	133	134	278	279
					282	122	130	278	282		
0	MBUF	INTEGER		DEFINED	124	DEFINED	1				
2166	MN	INTEGER	F. P.	REFS	71	73	80	82	84	87	104
				REFS	2*145	2*146	2*147	2*164	2*165	2*166	2*192
					226	228	229	DEFINED	69	75	80
					103	109	144	163	191	219	
					90						
352	MTYPE	INTEGER	LS4ARG	REFS	12	31	79	86	3*109	220	221
2165	N	INTEGER		REFS	30	268	270	3*290	3*298	220	281
					234	31	78	109	216	220	289
					30						
					297						

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VARIABLES	SN	TYPE	RELOCATION	REFS	30	31	198	260	DEFINED	1	282
2174 NB	O	INTEGER	F. P.	REFS	125	126	127	128	279		
		INTEGER		DEFINED	121	124					
	O	INTEGER	F. P.	REFS	124	281	DEFINED	1			
	O	INTEGER	F. P.	REFS	2*20	121	DEFINED	1			
	O	INTEGER	F. P.	REFS	3*14	18	55	92	DEFINED	1	
	O	INTEGER	F. P.	REFS	63	68	112	127	128	131	132
				REFS	159	193	210	227	231	244	275
				DEFINED	291	1					
	O	INTEGER	F. P.	REFS	19	2*20	26	63	68	103	109
				REFS	129	163	191	278	279		
				DEFINED	144	1					
2211 NN		INTEGER		REFS	236	246	262	263	264	265	266
	O	INTEGER	F. P.	REFS	267	234					
	O	INTEGER	F. P.	REFS	43	44	45	46	135	215	255
	O	INTEGER	F. P.	REFS	256	DEFINED	1	49	135	139	179
	O	INTEGER	F. P.	REFS	36	37	38	39	135		
	O	INTEGER	F. P.	REFS	180	DEFINED	1	42	278		
				REFS	63	68	276	277			
				DEFINED	1						
	O	INTEGER	F. P.	REFS	2*19	63	68	DEFINED	1		
	O	INTEGER	F. P.	REFS	2*14	18	53	96	DEFINED	1	
	O	INTEGER	F. P.	REFS	44	49	63	68	78	79	86
				REFS	221	270	289	297	DEFINED	1	
	O	INTEGER	F. P.	REFS	256	22	37	42	63	68	101
				REFS	140	286	294	DEFINED	1		
2170 NWALL		INTEGER		REFS	107	108	DEFINED	106			
1416 PI		REAL		REFS	199	261	DEFINED	21			
353 G		REAL	LS4ARG	REFS	12						
132 S		REAL	LS4ARG	REFS	12						
2212 SABS		REAL		REFS	240	250	DEFINED	238	248	262	263
O SIGX		REAL	F. P.	REFS	14	229	233	237	238	262	263
				REFS	254	266	267	DEFINED	1	223	229
				REFS	233						
O SIGY		REAL	F. P.	REFS	14	228	232	247	248	262	263
				REFS	264	266	267	DEFINED	1	224	228
				REFS	232						
2213 SMAB		REAL		REFS	240	250	DEFINED	239	249		
14 SS		REAL	LS4ARG	REFS	12	84					
O SSM		REAL	F. P.	REFS	14	89	228	229	DEFINED	1	73
				REFS	218						
O STREST		REAL	F. P.	REFS	18	65	262	263	264	265	266
				REFS	267	1	54	62			
O STRESX		REAL	F. P.	REFS	14	241	274	DEFINED	1	237	
O STRESY		REAL	F. P.	REFS	14	251	275	DEFINED	1	247	
O STRMAX		REAL	F. P.	REFS	14	239	290	DEFINED	1	98	241
O STTMAX		REAL	F. P.	REFS	14	249	298	DEFINED	1	97	251
2204 SUMXP		REAL		REFS	192	203	DEFINED	188	192	193	
2205 SUMYP		REAL		REFS	193	203	DEFINED	189	190	193	
2176 SUM1		REAL		REFS	145	148	164	167	204	268	
				REFS	141	145	160	200	204	262	
2177 SUM2		REAL		DEFINED	146	149	165	168	204	268	
				REFS	142	146	161	201	204	268	
2200 SUM3		REAL		DEFINED	147	150	166	204	204	268	
				REFS	143	147	162	166	202	264	
2207 SUM4		REAL		REFS	204	268	DEFINED	203	265		
2214 SUM5		REAL		REFS	268	DEFINED	266				

VARIABLES	SN	TYPE	RELOCATION	REFS	268	2*201	267	2*203	2*262	2*263	2*264
2215 SUM6	REAL			REFS	2*200	2*201	2*202	2*203	2*262	2*263	2*264
2206 THETA	REAL			2*265	2*266	2*267	DEFINED	199	261		
2172 TS	REAL			REFS	135	157	176	242	252	276	
	REAL			DEFINED	119	276					
0 TST	REAL	F. P.	ARRAY	REFS	14	290	DEFINED	1	242		
0 TTT	REAL	F. P.	ARRAY	REFS	14	298	DEFINED	1	252		
0 TX	REAL	F. P.	ARRAY	REFS	14	287	DEFINED	1	24	157	
0 TY	REAL	F. P.	ARRAY	REFS	14	295	DEFINED	1	25	176	
0 W	REAL	F. P.	ARRAY	REFS	14	26	DEFINED	1			
0 X	REAL	F. P.	ARRAY	REFS	14	153	156	200	201	202	209
	REAL			229	DEFINED	1	148	149	150		
2202 XABS	REAL			REFS	155	174	DEFINED	153	172		
0 XANG	REAL	F. P.	ARRAY	REFS	14	31	199	204	261	268	
	REAL			DEFINED	1	30					
0 XBUF	REAL	F. P.	ARRAY	REFS	14	134	DEFINED	1	125		
124 XC	REAL	LS4ARG	ARRAY	REFS	12						
0 XM	REAL	F. P.	ARRAY	REFS	14	145	146	147	DEFINED	1	134
0 XMAX	REAL	F. P.	ARRAY	REFS	14	154	287	DEFINED	1	95	156
0 XST	REAL	F. P.	ARRAY	REFS	18	64	200	201	202		
	REAL			DEFINED	1	56	61				
2203 XX	REAL			REFS	155	174	DEFINED	154	173		
0 Y	REAL	F. P.	ARRAY	REFS	14	172	175	200	201	202	210
	REAL			228	DEFINED	1	94	167	168	169	
0 YBUF	REAL	F. P.	ARRAY	REFS	14	131	DEFINED	1	127		
125 YC	REAL	LS4ARG	ARRAY	REFS	12						
0 YM	REAL	F. P.	ARRAY	REFS	14	164	165	166	DEFINED	1	131
0 YMAX	REAL	F. P.	ARRAY	REFS	14	173	295	DEFINED	1	93	175

FILE NAMES	MODE	REFS	38	45	41	46	48	67	135	293
INPUT	FMT	30	38	45	41	46	48	67	135	293
OUTPUT	FMT	26	31	39	285	287	288	290		
		204	215	268						
		295	298							
TAPE1	UNFMT	76								
TAPE2	UNFMT	125	126	MOTION	116	209	210	274	275	
TAPE3	UNFMT	63	64	65	68					
		61	62	MOTION	52					
TAPE4	UNFMT	88	89	READS	217	218	MOTION	77	214	
TAPE7	UNFMT	127	128	MOTION	117					
TAPE9	UNFMT	106	109	MOTION	111	MOTION	100			

EXTERNALS	TYPE	ARGS	REFERENCES	201	202	203	262	263	264	265	266
COS	REAL	1	REFERENCES	201	202	203	262	263	264	265	266
			LIBRARY	200							
				267							
READ1	REAL	4	79								
SIN	REAL	1	LIBRARY	201	202	203	262	263	264	265	266
				267							

INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES	154	172	173	238	239	248	249
ABS	REAL	1	INTRIN	REFERENCES	154	172	173	238	239	248	249

STATEMENT LABELS	DEF LINE	REFERENCES	25	23	37	36	44
0 5	25	23					
62 11	41	37					
66 12	43	36					
106 15	48	44					

200



STATEMENT LABELS	DEF LINE	REFERENCES	
112 18	50	43	47
0 20	54	53	
0 21	56	55	
166 24	67	57	
172 25	69	66	
0 28	74	69	70
0 31	85	81	83
257 32	88	86	
264 40	91	78	87
0 50	95	92	
0 60	98	96	
0 90	104	101	103
0 95	109	108	
361 100	110	105	107
412 200	123	283	
453 205	129	280	
0 210	134	129	
0 220	147	144	
554 230	158	151	155
0 232	166	163	
623 233	177	170	174
626 234	178	159	
0 235	182	181	
637 237	187	180	182
0 238	194	191	
0 240	204	198	
743 250	205	140	179
771 305	217	270	
1025 350	229	222	225
1045 350	233	230	231
1070 365	243	235	240
1111 366	253	245	250
1114 367	254	244	
0 368	258	257	
1125 369	260	255	258
0 370	268	260	
1220 390	269	219	255
1225 400	274	221	
1256 500	281	279	
1263 550	284	281	259
0 570	287	286	
0 580	290	289	
0 585	295	294	
0 590	298	297	
1755 1002	299	30	
1757 1010	300	38	45
1761 2002	301	31	
1766 2005	302	26	
1774 2008	303	67	
2003 2010	304	39	
2010 2012	305	41	
2016 2020	306	46	
2023 2022	307	48	
2031 2050	308	135	
2035 2051	309	139	
2050 2060	312	204	
2054 2100	313	215	

201

STATEMENT LABELS	DEF LINE	REFERENCES
2071 2110 FMT	316	268
2075 2200 FMT	317	285
2120 2205 FMT	321	287
2123 2210 FMT	322	288
2154 2215 FMT	328	290

LOOPS	LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
20	5	I	23 25	2B	INSTACK
120	20	I	53 54	2B	INSTACK
127	21	I	55 56	2B	INSTACK
173	28	MN	69 74	24B	NOT INNER
174	28	J	70 74	20B	NOT INNER
207	28	I	72 74	2B	INSTACK
224	40	N	78 91	43B	EXT REFS NOT INNER
231	31	J	81 85	22B	NOT INNER
246	31	I	83 85	2B	INSTACK
275	50	I	92 95	2B	INSTACK
305	60	I	96 98	2B	INSTACK
313	90	I	101 104	14B	NOT INNER
322	90	MN	103 104	2B	INSTACK
330	100	I	105 110	34B	EXT REFS NOT INNER
335	95	J	108 109	24B	EXT REFS NOT INNER
344		MN	109 109	11B	EXT REFS
466	210	I	129 134	10B	INSTACK
511	250	I	140 205	235B	EXT REFS NOT INNER
522	220	MN	144 147	7B	INSTACK
546	230	J	151 158	10B	INSTACK
571	232	MN	163 166	7B	INSTACK
615	233	J	170 177	10B	INSTACK
632	235	II	181 182	5B	EXITS
656	238	MN	191 194	7B	INSTACK
667	240	J	198 204	54B	EXT REFS
776	390	MN	219 269	225B	EXT REFS NOT INNER
1002	350	I	222 229	33B	NOT INNER
1021	350	J	225 229	11B	INSTACK
1042	360	J	230 233	6B	INSTACK
1061	365	I	235 243	11B	INSTACK
1102	366	I	245 253	11B	INSTACK
1120	368	II	257 258	5B	EXITS
1126	370	J	260 268	72B	EXT REFS
1267	570	I	286 287	21B	EXT REFS NOT INNER
1272		J	287 287	12B	EXT REFS
1312	580	N	289 290	21B	EXT REFS NOT INNER
1315		I	290 290	12B	EXT REFS
1341	585	I	294 295	21B	EXT REFS NOT INNER
1344		J	295 295	12B	EXT REFS
1364	590	N	297 298	21B	EXT REFS NOT INNER
1367		I	298 298	12B	EXT REFS

COMMON BLOCKS LENGTH  
LS4ARG 283

STATISTICS  
PROGRAM LENGTH 2407B 1287  
SCM LABELED COMMON LENGTH 433B 283  
52000B SCM USED

202

FWA OF THE LOAD 111  
LWA+1 OF THE LOAD 173113

TRANSFER ADDRESS -- ERST 22760

PROGRAM ENTRY POINTS -- ERST 22760

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCSSR	VER LEVEL	HARDWARE	COMMENTS
/FCNST/	111	3						
/CNTRL/	114	11						
ERST	125	24765	L00	03/16/81	FTN	4. 8 498	767X I	PROGRAM OPT=1 STATIC
MSCHECK	25112	41	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
LAYOUT	25153	3364	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
/LSARG/	30537	433.						
ELEMENT	31172	203	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
SSLAW	31375	406	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
STRAIN	32003	303	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
MASTIF	32306	1627	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
/BUF/	34135	5416						
WRITE1	41553	54	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
TOTAL	41627	400	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
READ1	42227	61	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
HYDROST	42310	271	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
STATIC	42601	365	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BANSOL	43166	221	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BNEIGN	43407	1327	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
EIGEN	44736	10741	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
EXT	55677	646	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
SOLEXT	56545	1736	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BESNKS	60503	247	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BESNIS	60752	402	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
INT	61354	565	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BNDNTH	62141	260	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
SOLINT	62421	1053	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
PRINTA	63474	110	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
FORMH	63604	233	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
MSOLVE	64037	141	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
BANSL1	64200	356	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
GUANE	64556	110	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
PFL	64666	15	L00	03/16/81	COMPASS	3. 6 498	767X I	SUBROUTINEOPT=1 STATIC
TSTEP	64703	666	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
RESPON	65571	2407	L00	03/16/81	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 STATIC
/D0112B/	70200	3						
AXIS	70203	505	UL-DTCLPLOT	08/13/80	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 TRACE
DASH	70710	453	UL-DTCLPLOT	08/13/80	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 TRACE
/JBL/	71363	6						
STATJ	71371	7	UL-DTCLPLOT	08/13/80	COMPASS	3. 6 498	767X I	SUBROUTINEOPT=1 TRACE
NEWPEN	71400	35	UL-DTCLPLOT	08/13/80	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 TRACE
/D0112A/	71435	4						
OFFSET	71441	16	UL-DTCLPLOT	08/13/80	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 TRACE
QUADAX	71457	420	UL-DTCLPLOT	08/13/80	FTN	4. 8 498	767X I	SUBROUTINEOPT=1 TRACE

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCSSR	VER	LEVEL	HARDWARE	COMMENTS
SCALE	72077	170	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
SETAXIS	72267	225	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
SYMBOL	72514	747	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
PDMP	73463	471	UL-DTCPLT	10/22/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
BUFF	74154	720	UL-DTCPLT	10/22/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
/DEVICE/	75074	3							
PLOTS	75077	36	UL-DTCPLT	10/28/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
RSTR	75135	42	UL-DTCPLT	10/28/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
GRAF11	75177	261	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
JSTAT	75460	44	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
NUMBER	75524	243	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
WHERE	75787	32	UL-DTCPLT	08/13/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
SLINE	76021	121	UL-DTCPLT	08/21/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
/MULPLOT/	76142	2							
MULPLT	76144	506	UL-DTCPLT	08/21/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1 TRACE
PACK1	76552	14	UL-DTCPLT	10/22/80	COMPASS	3. 6	498		
OPLT	76666	135	UL-DTCPLT	10/28/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
PLOT	77023	414	UL-DTCPLT	10/28/80	FTN	4. 8	498	767X I	SUBROUTINEOPT=1
ALOG10	77437	6	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		CALL-BY-REFERENCE LINK TO ALOG10.
IT0J	77445	32	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		INTEGER TO INTEGER EXPONENTIATION. OPT=ALL
SIN	77477	6	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		FC L4 - EVALUATE SINE FUNCTION. CALL-BY-REFER
SINCOS	77505	60	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		TRIGONOMETRIC SINE OR COSINE OF X. OPT=ALL.
SQRT	77565	6	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		CALL-BY-REFERENCE LINK TO SQRT.
SYS=	77573	1	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		LINK BETWEEN SYS=AID AND INITIALIZATION COD
SYS=AID	77574	7	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		AUXILIARY MATH LIBRARY LINK FOR ERRORS.
TAN	77603	36	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		TRIGONOMETRIC TANGENT. OPT=ALL.
XTOI*	77641	11	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		CALL-BY-REFERENCE LINK TO XTOI.
BACKSP=	77652	55	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		BACKSPACE LOGICAL RECORD.
/GB. ID. /	77727	135							
/FCL=ENT/	100064	42							
/FCL. C. /	100126	26							
COMIO=	100154	10	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMMON CODED I/O ROUTINES AND CONSTANTS.
ENCODE=	100164	126	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FORMATTED WRITE INTO CORE.
FCL=FDL	100312	40	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FCL CAPSULE LOADING
FEIFST=	100352	3	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		CONVERTED DATA STORAGE
FLTOU=	100355	315	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMMON FLOATING OUTPUT CODE
FORSYS=	100572	464	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FORTRAN OBJECT LIBRARY UTILITIES.
INCOM=	101356	145	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMMON INPUT FORMATTING CODE
INPC=	101523	207	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FORMATTED READ FORTRAN RECORD.
KODER=	101732	476	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		OUTPUT FORMAT INTERPRETER.
NAMOUT=	102430	267	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		NAMELIST OUTPUT ROUTINE.
/IO. BUF. /	102717	227							
OUTB=	103146	205	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		BINARY WRITE FORTRAN RECORD.
OUTCOM=	103353	204	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMMON OUTPUT CODE
REWIND=	103957	33	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		POSITION FILE AT BEGINNING-OF- INFORMATION.
STLCRM=	103612	31	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOADING OF FCL CAPSULES
STLIBI.	103643	24	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR BINARY INPUT.
STLICO.	103667	16	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR CODED INPUT.
STLREW.	103705	14	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR REWIND.
CLOCK=	103721	53	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		ACCESS SYSTEM CLOCKS FOR FORTRAN.
GOTDER=	103774	14	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMPUTED GO TO ERROR PROCESSOR.
ALOG.	104010	63	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		EXPONENTIAL FUNCTION. E TO POWER X. OPT=ALL
EXP.	104073	73	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		COMMON ERROR MESSAGES FOR EXPONENTIATION.
EXP. MSG	104166	16	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		COMMON ERROR MESSAGES FOR EXPONENTIATION.
IT0J*	104204	11	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		CALL-BY-REFERENCE LINK TO IT0J.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCSSR	VER	LEVEL	HARDWARE	COMMENTS
COS	104215	6	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		FCL4 -- EVALUATE COSINE FUNCTION. CAL
SQRT.	104223	32	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		COMPUTE THE SQUARE ROOT OF X. OPT=ALL.
SYS=1ST	104255	65	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		MATH LIBRARY LINK TO ERROR MESSAGE PROCESSOR
TAN	104342	6	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		CALL-BY-REFERENCE LINK TO TAN.
XTOI	104350	63	SL-FORTRAN	09/20/79	COMPASS	3. 6	498		REAL TO INTEGER EXPONENTIATION.
/STP. END/ GENTRY=	104433	1							
FEENRY=	104434	1	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FCL INITIALIZATION ROUTINE.
FLTN=	104435	41	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		INITIALIZE CONSTANTS.
FMTAP=	104476	156	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		COMMON FLOATING INPUT CONVERTER.
FORUTL=	104654	377	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		CRACK APLIST AND FORMAT FOR KODER/KRAKER.
GETFIT=	105253	47	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FCL MISC. UTILITIES.
INPB=	105403	61	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		LOCATE AN FIT GIVEN A FILE NAME.
KRAKER=	106011	454	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		BINARY READ FORTRAN RECORD.
NAMIN=	106465	527	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		PROCESS FORMATTED FORTRAN INPUT.
OUTC=	107214	150	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		NAMELIST INPUT ROUTINE.
SPA=	107364	11	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		FORMATTED WRITE FORTRAN RECORD.
STLBAK.	107375	12	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		SPA= - SUBSTITUTE PARAMETER ADDRESSES.
STLOBI.	107407	15	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR BACKSPACE.
STLOCO.	107424	12	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR BINARY OUTPUT.
CPU. SYS	107436	40	SL-SYSLIB	04/15/80	COMPASS	3. 6	498		STATIC LOAD FOR CODED OUTPUT.
CM. KIL	107476	12	SL-SYSLIB	09/20/79	COMPASS	3. 5	470		PROCESS SYSTEM REQUEST.
CTL#PTL	107510	34	SL-SYSLIB	09/20/79	COMPASS	3. 6	498		CMM VI. 1 - DEACTIVATE CMM.
CTL#SKP	107544	57	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM CONTROLLER - PARTIAL GET/PUT.
LIST#RM	107623	67	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM CONTROLLER - SKIP PHYSICAL/FILE.
RM#SYS=	107712	5	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM - ALLOCATE SPACE FOR LIST OF FILES
CTL#RM	107717	576	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM - POST RA+1 REQUEST
CTL#NR	110515	40	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM CONTROLLING ROUTINE.
ERR#RM	110555	25	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		CRM CONTROLLER - WEOX, REWIND
ERRCAP=	110602	324	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		CRM ERROR PROCESSOR ENTRY.
RBL#RM	110602	0	SL-SYSLIB	12/11/79	COMPASS	3. 6	498		
FERCAP=	111126	227	SL-FORTRAN	04/15/80	COMPASS	3. 6	498		CRM - MANIFEST BAMLIB/AAMLIB FOR STATIC LOA
CHEK#SQ	111355	77	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
CLSV#SQ	111454	222	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
DF#CRM	111676	226	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
EF#CRM	112124	445	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#W	112571	51	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#WA	112642	175	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
PUT#SQ	113037	571	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
PUT#N	113630	213	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
REW#SQ	114235	172	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
SKBL#SQ	114362	752	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
SKIP#SQ	115334	234	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
WAR#SQ	115570	162	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
CLSF#RM	115752	425	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
COMM#WA	116377	306	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#SQ	116705	616	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#FU	117523	117	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#S	117642	505	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GET#Z	120347	166	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
GPTM#SQ	120535	442	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
LBUF#RM	121177	134	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
OPEN#RM	121333	1332	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		
PUT#CI	122665	65	SL-BAMLIB	12/11/79	COMPASS	3. 6	498		

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCSSR	VER	LEVEL	HARDWARE	COMMENTS
PUT\$S	122752	357	SL-BAMLIB	12/11/79	LOADER	1.5	498		
PUT\$Z	123331	75	SL-BAMLIB	12/11/79	LOADER	1.5	498		
RPE\$SQ	123426	166	SL-BAMLIB	12/11/79	LOADER	1.5	498		
SKFL\$SQ	123614	36	SL-BAMLIB	12/11/79	LOADER	1.5	498		
WEDX\$SQ	123652	137	SL-BAMLIB	12/11/79	LOADER	1.5	498		
FCL\$RM	124011	42	SL-BAMLIB	12/11/79	COMPASS	3.6	498		LINK/DELINK STATIC CAPSULES.
PLG\$RM	124011	0	SL-BAMLIB	12/11/79	COMPASS	3.6	498		
//	124053	47040							

.410 CP SECONDS

144500B CM STORAGE USED

176 TABLE MOVES

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UCS UCS-176 NOS/BE 1.3 REL499-14 03/16/81
16.39.36.KCCANRE FROM /AN AT P 3
16.39.36.IP 00009024 WORDS - FILE INPUT , DC 04
16.39.36.KCC.P3.T10.*****.*****.**,**,ERSTLGO
16.39.36. BUILD
16.39.38.PURGE:A,ERSTLGO, ID=DYNATECH.
16.39.39.PR ID= DYNATECH PFN=ERSTLGO
16.39.39.PR CY= 001 00013440 WORDS.
16.39.39.RETURN,A.
16.39.39.EXIT,U.
16.39.39.REQUEST,LGO,*PF.
16.39.39.FTN,R,A,STATIC.
16.40.18. 4.135 CP SECONDS COMPILATION TIME
16.40.18.CATALOG,LGO,ERSTLGO,ID=DYNATECH.
16.40.19.INITIAL CATALOG
16.40.19.RP = 999 DAYS
16.40.19.CT ID= DYNATECH PFN=ERSTLGO
16.40.19.CT CY= 001 00013440 WORDS.
16.40.19.MAP,PART.
16.40.19.ATTACH,DTCPLLOT, ID=DYNATECH,MR=1.
16.40.19.PFN 15
16.40.19.DTCPLLOT
16.40.20.PF CYCLE NO. = 004
16.40.20.LIBRARY,DTCPLLOT.
16.40.20.LOAD,LGO.
16.40.20.NOGO.
16.40.26.EXIT,U.
16.40.26.DAYCOPY.
16.40.29.OP 00043008 WORDS - FILE OUTPUT , DC 40
16.40.29.MS 53760 WORDS ( 96768 MAX USED)
16.40.30.CPA 4.605 SEC.
16.40.30.IO 20.561 SEC.
16.40.30.CM 514.698 KWS.
16.40.30.SRU
16.40.30.EJ END OF JOB, AN
16.000

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