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# Estimation of Seismicity Parameters Using a Computer

[Raschet Parametrov Seismicheskogo Rezhima na E'VM]

### A.I. Zakharova

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This monograph presents the methodology for machine calculations of the main seismicity indices. It is suitable for seismic zoning and for a study of the regularity of earthquakes. The current methods of determining and plotting seismic parameters are analyzed and the rationale of switching over to machine calculation justified. A number of computer programs are included for evaluating graphs of recurring earthquakes, mapping seismic activity and maximum possible earthquakes. Also included are the examples of the use of these programs to study seismicity in Uzbekistan.

The monograph is intended for seismologists and geophysicists.

Editor-in-Chief Yu.V. Riznichenko Corresponding Member of the Academy of Sciences, USSR

### Foreword

The quantitative indices and parameters of seismicity—the recurrence N(K) of earthquakes of various magnitudes  $K = \log E$  (where *E*—seismic energy of the focus), the spatial distribution of seismic activity A, and the maximum possible earthquake  $K_{\max}$ —are determined for two purposes: first, to solve problems of the general theory of the seismic process as an integral part of geodynamics; second, to qualitatively evaluate the seismic dangers for seismic zoning (delimitation) and the forecast of earthquakes.

In the present state of the development of seismology, however, seismic zoning and the establishment of long-time average indices of seismic danger happen to be the main applications of seismicity indices. This is now done not only on the basis of the old maxmium possible points but also on the new, more complete, seismic shocks—the average recurrence frequency of seismic tremors of various intensities at any given place, to the maximum possible. The intensity may be expressed in macro-seismic points, which are already considered obsolete, or in more modern spectral and time indices. The point is that knowledge of the characteristics of seismicity, N(K), A and  $K_{max}$ , is necessary to approximately calculate shocks whether the intensity is expressed in points or in spectral and time indices.

This book illustrates a method for the machine calculations of seismicity indices—N(K), A and  $K_{max}$ . The advantages of machine calculations over manual methods are well known; agitation against automation is out of place. The most important thing was to place the determination of  $K_{max}$ within the scope of machine calculation. This had been the most difficult task for manual calculation. Machine calculation also gives interpreters optimum conditions for the stable determination of this quantity where the parameters are variable. Using manual calculations the interpreters rarely had the energy or patience.

Machine calculation of seismicity indices has become especially important in view of programs developed by the Commission for the Elaboration of Qualitatively New Methods of Evaluating Seismic Danger (CESD) by the Interdepartmental Committee for Seismology and Seismological Construction (ICSSC) of the Presidium of the Academy of Sciences, USSR. This work is being done by a number of central and state organizations engaged in the problems of seismic zoning and related work in all the main seismic zones of the Soviet Union. The volume of these calculations and the necessity to standardize operations have increased recently, with the development of a new quantitative basis for seismic zoning of the USSR, and the development of seismic research during the construction of large hydroprojects in earthquake prone areas.

Programs for the machine calculation of seismic shocks have already been published. References to them are given in this monograph. However, the task of this book is to determine the feasibility of using machine calculations while interpreting actual seismological material to calculate the shocks. Since programs to determine the hypocenters and other parameters of earthquakes already exist, this book fills the last remaining gap in mechanizing seismic risk calculations arising from earthquake annals.

Besides programs for the machine calculation of seismic indices, this book provides an introduction to this problem and its study in the USSR and abroad.

It is hoped that the book will be useful to a wide range of specialists in the problems of seismicity and seismic risk. Engineers may also be interested in reading it to use the rich seismology data to design earthquake-proof structures and equipments.

> YU.V. RIZNICHENKO Corresponding Member Academy of Sciences, USSR

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## Introduction

Quantitative indices of seismicity—the so-called seismic regime parameters of one territory or another, which are necessary to delimit seismic regions are redetermined periodically in our country using the constantly gathered data. The distribution map of expected seismic effects on the earth's surface is more accurately established in this manner. This is necessary to evaluate possible earthquake dangers for buildings and installations. Average longterm values of seismicity indices are important for seismic delimitations.

Computation of the qualitative characteristics determining the seismicity of a territory over relatively short time is necessary to reveal the temporal regularity of the seismic process. This knowledge is necessary to forecast earthquakes. Besides, investigation of the change in seismicity with time is also necessary to evaluate the correctness of the seismic delimitations map since reliable determination of the average, long-term parameters of seismicity directly depends on the seismic regime.

Recently, because of an increased volume and variety of actual data, it became necessary to use the computer in seismology. Seismologists of the USSR have written numerous programs to determine the coordinates of earthquake epicenters and hypocenters and have used them successfully. Before, the computation and areawise plotting of the qualitative characteristics of seismicity were done mainly by hand and demanded considerable time.

Programs are proposed to compute graphs of the repeatability of earthquakes, seismic activity maps, and maximum possible earthquakes. The application of these programs to determine seismic parameters in Uzbekistan shows that the computation of seismic activity maps is 5-10 times faster and that of the maximum possible earthquake is more than 10 times faster than hand calculations.

The work is divided into two parts. In the first are described the main directions of the quantitative investigation of seismicity and developments in the USSR and abroad with a short survey of the application of machine methods. In the second part, computer programs are presented which can calculate seismicity characteristics for any given period of earthquake observation. Examples are given of the calculation of seismic activity maps and maximum possible earthquakes for Uzbekistan. The author is greatly indebted to Yu.V. Riznichenko and S.D. Vinogradov for their friendly discussions of the materials in this work; to E.M. Butovskaya and Y.U. Saatov for careful scrutiny; to L.M. Matasovaya, N.A. Ovechkinaya, and L.P. Kazachenko for help in the computation and formulation of the text. Quantitative Investigation of Seismicity

A qualitative description of specific features of seismicity indices, particularly in relation to the geological structure and other factors, must precede the estimation of values of these indices (Riznichenko, 1960). The works of Yu.V. Riznichenko and I.L. Nersesova (1960a, b) present a history of the development of quantitative seismicity criteria and describe the main literature before 1960. Later works are partially reviewed by Yu.V. Riznichenko (1969).

This part reviews publications on the subject, mainly between 1961– 1970. Special attention is given to the use of computers.

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### Formulation of the Problem

Attempts to qualitatively express seismicity were made at the beginning of this century (Ballor, 1900). As a measure of seismicity the quantity

$$\sigma = \sqrt{F/i},\tag{1}$$

where *i*-average yearly repeatability of the earthquakes;

F-area of the region under study, was used.

The quantity  $\sigma$  is the length of the side of the square, in which, with uniform distribution, one earthquake would have taken place in one year. However, in such determinations, the force of the earthquakes is not considered, which leads to non-comparable results for the regions in which the earthquake's frequency and force are not even approximately proportional (Toperczer, 1953). Besides, the lower limit of the acceptable earthquake force in quantity  $\sigma$  remains unclear (Riznichenko, 1961).

L. Koning proposed using magnitude as the measure of seismicity (Koning, 1952).

To map seismicity many investigators used the quantity of seismic energy or its modifications. Thus M. Bath determined seismicity as the general energy emitted in unit area in unit time (Bath, 1953) and used this characteristic for Phennoskandia. V. Sponheuer determined the seismicity of the GDR using the quantity of seismic energy of earthquakes (Sponheuer, 1953). M. Toperczer (1953) chose the average sum of seismic energy S brought to the unit area as a measure of seismicity

$$S = \frac{\sum l_i}{F \cdot P},\tag{2}$$

where  $l_i$ —the so-called "surface energy" of earthquakes, i.e., the part of

the actual energy available for observation;

F-area of the region;

P-time.

The value  $l_i$  was calculated according to the magnitude M on Richter scale in accordance with the expression:

$$1.8 \ M = \log l_i / l_0, \tag{3}$$

where  $l_0$ —the seismic energy of the standard earthquake.

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Trapp (1954) used the logarithm of the surface energy as a measure of seismicity to simplify the computations and construction of maps. P. Amand (1954) expressed seismic activity of the region under study by a specific seismicity S:

$$S = \frac{K_1}{AT} \sum_{A} \sum_{T} E_i, \tag{4}$$

where A—the chosen area;

T—time of observation;

- $K_1$ —a constant depending on unit of measurement;
- $E_i$ —summation of seismic energy of all earthquake centers in the given time.

It is clear that expression (4) is very similar to (2) proposed by M. Toperczer.

W. Ullman and R. Maaz (1967) define seismicity as the density of seismic energy emitted in the region under investigation for the entire observation period. It is true that the authors complicate their definition of seismicity by proposing that it be determined in timespace points by summing the various tremors. We prefer to compute tremors of the carth's surface brought about by earthquakes at a later stage.

G.A. Shenkareva (1967) proposed to compute a map of specific seismic energy  $E_m$  (or the power of the energy flow  $N_m$ ), which is understood as the energy emitted in 1 cm<sup>3</sup> of the earth's crust or mantle in 1 second, i.e.,

$$E_m = \frac{\sum E_i}{VT},\tag{5}$$

where  $E_i$ —the sum of the quantity of energy (in ergs) of all earthquakes, whose centers are included in the given volume V of the core or mantle;

*T*—time of observation, second.

A map of specific seismic energy has been built for the USSR (Gorshkov, Shenkareva, 1970). The volume V in this is computed as the volume of a cylinder with radius r = 50 km and height H equal to the thickness of the earth's crust; whereas, for the focal zones in the mantles, considering the depths of the centers of the earthquakes, the value of  $E_m$  varies from 0 to  $10^{-4}$  erg/cm<sup>3</sup> sec.

I.A. Sokolova (1969, 1971) found a way to compute a map of seismic energy with a prior division of equal density zones. A graph of the dependence of the linear dimensions of the focus on the quantity K of the corresponding earthquake is built for the region under investigation. Thereafter, for each K a zone of average energy  $S_K$  is chosen, the radius of which is equal to:

$$R_K = r_K + a, \tag{6}$$

where  $r_{\kappa}$ —linear dimensions of the focus;

*a*—the accuracy of epicenter determination at the reliability level 0.9.

The energy of each earthquake  $E_i$  is converted into density  $E_K = \frac{E_i}{S_K}$ , which is normalized according to time. For each K a repeatability period  $T_K$  is chosen in accordance with the graph of earthquake repeatability. Due to the small number of strong earthquakes the empirical repeatability graph is constructed theoretically. Its basis is a proposition about the normal logarithmic distribution of the linear dimensions of the focus. The energy density at any point of the map for Chatkal'skii Khrebet (spinal column) is calculated according to the formula:

$$E=\sum_{K=10}^{17}E_K,$$

where

$$E_{K} = \frac{10^{K-10} \cdot 1000}{S_{K} \cdot T_{K}}.$$
(7)

The zones of equal energy density  $E_K$  are separated by statistical methods. It is suggested that the density of seismic energy map be used to delimit the seismic region, along with maps of the seismic activity and intensity of modern tectonic movements.

H. Benioff (1951) proposed, as a measure of the temporary seismic changes, a quantity related to the released elastic strain expressed as  $\sum \sqrt{E_i}$ , where  $E_i$ —carthquake energy. Some investigators used it to study the spatial distribution of seismic activity. Thus, A. Ritzema (1954) related the quantity  $\sum \sqrt{E_i}$  to the unit area and unit time while investigating the seismicity of Sunda-Arc, whereas, P. Amand (1956), using the Benioff's terms, proposed to measure seismicity by tectonic flow  $F_f$  from the expression

$$F_f = \frac{1}{AT} \int_A \int_T E^{1/2} \, dA \, dT, \qquad (8)$$

entirely analogous to the application by Benioff and Ritzema.

The quantitative characteristics of seismicity most widespread in the USSR were worked out by Yu.V. Riznichenko in 1958 to understand the seismic regime, which, according to his definition, is the distribution of any region's earthquakes in space and in time. In recent years Riznichenko, Nersesov, and others have worked out methods to investigate seismic regime parameters based mainly on the instrumental observations of TKSE\* (Nersesov, Riznichenko, 1959; Riznichenko, Nersesov, 1960a; Riznichenko, ed., 1960).

\*The Tashkent Complex Seismological Expedition—General Editor.

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The main point of the investigation of the seismic regime of any region is to explain the law of the repeatability of earthquake, i.e., the dependence between the number N of earthquakes and their seismic energy E. This dependence is expressed usually in biologarithmic scale as a linear curve:

$$\log N = \log N_0 + \gamma (K - K_0), \qquad (9)$$

here  $K = \log E$ —the class of the earthquake energy;

- log  $N_0$  and  $\gamma$ —coefficients of the curve (9), its level and inclination, respectively;
  - $(K-K_0)$ —argument of the function log N, its present coordinate;
    - $K_0$ —the constant part of argument, representing the fixed class of energy.

It may be noticed that the first investigation about the distribution of earthquake repeatability was done by Japanese (Kawasumi, 1952, a, b; Tsuboi, 1952), seismologists using the dependence of the number of carthquakes N on their magnitude M in a form similar to (9):

$$\log N = a + bM. \tag{10}$$

V.N. Gaiskii (1970) observes that only in TKSE was the dependence between the repeatability of earthquakes of different energies subsequently used to describe and compare the seismic regimes of various areas of the seismo-active region. This was further promoted to a large extent by the earthquake energetics classification introduced by T.G. Rautian (1960, 1964) which made possible the objective construction of seismic regime. This classification uses instrumental data recordings of earthquakes, according to which energy fluxes are evaluated, which pass through the sphere of a given radius-the so-called reference sphere. This method of evaluating earthquake quantities using the energy flux of seismic waves, first proposed in 1911 by B.B. Golitsyn (1960), was adopted for the mass determination of foci energy by V.I. Bune (1955, 1956, a, b, c; 1957), who built nomograms which simplified the computations considerably. T.G. Rautian investigated methods to compute the density of the energy flux at the observation point earthquake and the energy flux through the reference sphere, damping the density of the energy flux with distance. On this basis she worked out a practical system to determine the energetics class K of the earthquake, presenting a logarithm of the seismic energy E. T.G. Rautian's classification is now used in many seismic regions of the Soviet Union.

If in the formula of the repeatability law (9) the number of earthquakes N is normalized according to area and time, then we get  $N^* \equiv A$ , i.e., an expression for the seismic activity (Riznichenko, 1958). According to the definition, the seismic activity is the average number of earthquakes of a particular class of energy K which occur in unit area in unit time. The value

of the seismic activity  $A_K$  may be found for any class K of earthquake energy according to the formula

$$A_{K} = N_{K}^{*} = 10^{-\gamma} (K - K_{0}) \cdot N_{0}, \qquad (11)$$

which immediately arises out of (9).

Most widespread is the determination of seismic activity A according to the energy class K = 10, since in most seismically dangerous regions, these earthquakes are most numerous (Riznichenko, Gorbunova, 1968) and give the most promising values of  $A_{10}$ . Substituting the actual value for K in the expression (11), one gets the earthquake repeatability of various classes of seismic energy up to  $K = K_{max}$ , i.e., the maximum energy class in the region of investigation. Maps of seismic activity give substantially more stable pictures of seismicity distribution along the area, than maps of totaled or specific energies, which are mainly dependent on powerful but rare earthquakes. From seismic activity maps one may pass on to the maps of the repeatability of earthquakes of any class K, even the greatest possible. Thus the maps of earthquake repeatability are constructed from K = 15 for Fergana valley and the River Narin basin (Nersesov and others, 1960, Butovskaya and others, 1961).

The repeatability period  $T_K$  is computed in accordance with the expression

$$T_K = \frac{S_1 \cdot 10^{(K-K_0)}}{S \cdot 10^{-\gamma} A_K},$$
 (12)

where S-area of the territory investigated;

 $S_1$ —unit of area, for which the seismic activity  $A_K$  is normalized.

The law of earthquake repeatability (9) is defined by three main parameters of the seismic regime, which may be used to quantitatively describe the seismicity of any territory: the inclination  $\gamma$  of the curve of repeatability, seismic activity A, and the maximum earthquake  $K_{max}$ . The determination of these parameters of the seismic regions of the Soviet Union and its other isolated areas have been logged by many investigators, e.g., while conducting experiments on the seismic region delimitation of the USSR (Medvedev, ed., 1968).

While studying the seismicity of active zones of the Soviet Union, a tendency was noticed toward associating epicenters of strong earthquakes with zones of increased seismic activity (Riznichenko, 1962, 1964b). A correlation was made showing a dependence between the value observed in strong earthquakes and the value of activity computed at the peaks of its epicenters (Yu.V. Riznichenko, 1966, 1967a). Establishing the correlational dependence shows it is possible to estimate the quantity of maximum earthquakes  $K_{max}$  at any point under investigation according to the level of seismicity, independent of whether or not any strong earthquake had occurred there.

Distribution of the quantity  $K_{\text{max}}$  according to the territory may be shown as a map of the maximum possible earthquakes, first prepared for Eastern Sayan and Jungariya (Riznichenko, 1966) according to the relation:

$$\log \bar{A} = \alpha + \beta \ (K_{\max} - K_{\alpha}), \tag{13}$$

where  $\bar{A}$ —average seismic activity;

 $K_{\alpha}$ —15;

 $\alpha$  and  $\beta$ —numerical coefficients in which  $\alpha = 2.84$ ;  $\beta = 0.21$ .

The quantity  $\overline{A}$  in the formula (13) is calculated for some area responsible for the generation of strong earthquakes. Its dimensions are in accordance with the quantity of energy  $E_{\text{max}}$  emitted in the focus and are proportional to the volume of the region and its formation

$$E_{\max} = 10^{K_{\max}} = cr^3,$$
 (14)

where *r*—radius of this region;

*c*—proportionality coefficient =  $3 \times 10^{10}$  J/km<sup>3</sup>.

Later maps of  $K_{\text{max}}$  by the Riznichenko's method were compiled for many areas of the USSR and beyond its boundaries (see Chapter IV).

Thus, until the present time, the quantitative evaluation of seismicity took two main directions (Riznichenko, 1969). In the USSR, Europe, China, and India, the seismicity of isolated regions, and often of an entire territory under consideration, was mapped by seismic activity A. Earthquake repeatability was investigated in space as well as time. In many regions of the Soviet Union, a new method of compiling a maximum possible earthquakes  $K_{\text{max}}$  map, as proposed by Riznichenko, is now being successfully assimilated (1962, 1964b, 1967a).

Foreign authors, particularly in America and Japan, formerly expressed seismicity either as a summation of the quantity of seismic energy  $\sum E$  emitted by the foci in unit area of the region in unit time or as the quantity of Benioff stress release, presented as the sum of the square roots from the seismic energy of the foci  $\sum E^{1/2}$ . Besides, here is investigated the spatial distribution of the number of earthquakes along the magnitude M (Miyamura, 1969). Mapping the quantities  $\sum E$  and  $\sum E^{1/2}$  and often also the earthquake distribution along M is carried out by computer. We present here one of the investigations on the law of the repeatability of earthquakes, carried out by H. Neunhöfer without a computer.

The representation of the law of distribution of the number of earthquakes according to their energies in the double logarithmic scale for an approximation of a straight line is being practiced in the USSR (Riznichenko, 1958). H. Neunhöfer (1970) considers that such a representation does not give a true picture of the seismic process and suggests a logarithmic distribution normal for its representation. This representation has the form:

$$n_i = \frac{N}{\varphi E_0 \sigma \sqrt{2\pi}} \exp \left\{-\frac{\ln^2 E_i/E_0}{2 \sigma^2}\right\},$$
 (15)

where  $n_i$ —frequency of representation of energy  $E_i \pm 1/2$  ( $\Delta E_i$ );

- ln  $E_0$ —indirect measure of the application of maximum repetition frequency of these earthquakes;
  - N—common energy in ergs of all earthquakes in the theoretical distribution (here the elementary volume in  $10^5$  km<sup>3</sup> and time of 1 year is connected);
  - $\varphi$ -normalized factor for conducting the quantity of energetic classes and observation times in the corresponding units;
  - $\sigma$ —parameter of distribution.

The distribution of earthquakes in the various epicentral zones for various time periods is calculated according to formula (15). In all cases, it is established that the form of the distribution curve depends on the parameter N, which is the common sum of the energies of all earthquakes taking place in the epicentral region under investigation in unit volume and unit time. Thus, the law of the distribution of earthquakes according to their energies can be reduced to obtain specific energy. The quantity of the total energy of earthquakes is insufficiently stable to represent long-term or transient maps of earthquake distribution in the region under study. It depends on rare, strong earthquakes and is entirely determined by their energies.

In all probability the quantity of seismic activity A happens to be the most promising index of the long-term mean distribution of seismicity. As compared to  $\Sigma E$  or  $\Sigma E^{1/2}$ , it changes to a lesser extent with time. According to Riznichenko's data (1969) obtained from investigations of the mean yearly values of the quantities A,  $\Sigma E$ , and  $\Sigma E^{1/2}$  for the crustal foci of the Baikal Rift region during 1961–1966, Tajikistan during 1956–1966, and also the deep foci of Pamir-Hindukush, 1956–1965, the quantity of  $\Sigma E^{1/2}$  fluctuates about the mean 2–3 times and  $\Sigma E$ —10 times more than A.

Until now the discussion was on the spatial distribution of seismicity, although along with it also developed the time aspect of the investigation of earthquakes. V.N. Gaiskii (1970), using probability theory and mathematical statistics, investigated the general properties of the seismic field and established necessary parameters or functions for its quasi uniformity. These are the temporal and quantitative distribution of earthquakes and maps of seismic activity. The seismic regime of crust and deep-focus earthquakes was investigated by instrumental observations in Tajikistan and Pamir-Hindukush.

Quantitative methods to evaluate seismic danger according to data of focal seismicity are now being widely used in the USSR (Riznichenko). The basis of this evaluation is to calculate the frequency of seismic tremor repetitions (Riznichenko, 1965, 1966, 1968, 1969, 1970, 1971). The problems of the distribution of tremors at a point under investigation as functions of earthquake energy and on the earth's surface depending on epicentral distance and damping of seismic waves were investigated long ago. Thus, Ishimoto and Iida (1939) established the law of the distribution of the number of tremors according to the maximum amplitude of recording in the form:

$$N(a) \ da = k \cdot a^{-m} \ da, \tag{16}$$

where a—amplitude of recording;

N(a)—number of earthquakes with the amplitudes of recording between a and da;

m and k—constant values.

S.V. Medvedev, remembering the surface effect, proposed that seismic delimitation should consider not only the earthquake's possible maximum force but also the frequency of its repetition. For this purpose, the seismic region was divided into different activity zones for different points-high, medium, and low—according to the expected repeatability through 10-15, 40-60 and 120-150 years (Medvedev, 1947). According to this classification, buildings, in terms of their longevity, are classified as temporary, massive and monumental. It may be noted here that the understanding of seismic activity expresses the repeatability effect of earthquakes of a certain force independent of its energies. Somewhat later (Riznichenko, 1958) seismic activity was called the frequency of carthquake repetitions of a certain energy class independent of their surface effect, referred to unit area. This definition was accepted by seismologists of the Soviet Union. In 1948–1949, S.V. Medvedev (1949) used his method to evaluate seismic danger in Moldavia. For this purpose, separate seismo-statistical maps were compiled for 6-, 7-, 8-, and 9-point earthquakes, on which were superimposed isoscists of the same point value, referring to all known earthquakes. Each isoline on the map represented one earthquake, e.g., an area limited by this 6thpoint earthquake isoline was considered a 6th-point type, independent of the presence here of higher seismic point values (7, 8, 9 points). Thus, for the specific region the frequency of earthquakes with the intensity under consideration or higher was estimated. To determine the frequency of earthquakes of *n*th point, at a given point a summation was given of the number of earthquakes of nth as well as higher point values occurring here. The delimitation map of Moldavia prepared by Medvedev had three isolines for each point, e.g., 6H, 6M, and 6L (the letters mean high, medium, and low activity, expressing the repeatability of 6-point earthquakes through 10-15, 40-60 and 120-150 years). Thus, Medvedev attempted a direct computation of Moldavia's shakeability according to the number of tremors of various forces, depending on strong earthquakes taking place there. Computing the

repeatability of tremors allows a differentiated evaluation of the seismic danger; whereas, in the usual delimiting practically all points of the area transferred to one point are considered equally dangerous. Besides, it is possible to determine more correctly the necessary and minimum degree of seismic protection for various classes of constructions and to consider repeated seismic actions. It is regrettable that the application of Medvedev's method is limited due to its use of data about strong but rare earthquakes; their limited data does not permit the necessary detailed, direct calculations of shocks in large areas (Riznichenko, 1969). Apparently, therefore, seismostatistical maps which used the frequency of previous earthquakes of different forces did not develop. Thus, on the seismic delimitation map of the USSR for 1957 (Medvedev, 1960) only the boundaries of regions with expected surface tremors are shown in points. It is true that Medvedev indicated the limitations of his method: (1) the absence of the time factor and the evaluation of the probability of earthquakes of a given force for each point; (2) the absence of regional differentiation according to the spectral condition of the earth's oscillations and also along the depth of the foci bedding and the mechanism of the earthquake. However, the repetition periods of corresponding tremors and other necessary characteristics were also not shown on the latest seismic delimitation map (Medvedev, ed., 1968).

M. Toperczer (1953) made one of the first attempts to evaluate the probability of the appearance of destructive earthquakes in a region under consideration. He proposed a measure, the so-called relative seismicity Sof the region, connected it with the seismic action W, equal to the product of the scale points I in the epicenter by the area  $f_j$  of the region undergoing tremors:

$$W = I f_j. \tag{17}$$

If during the observation period P on the surface F, n earthquakes took place, then the relative seismicity S is expressed by the formula:

$$S = \frac{\sum_{i=1}^{n} W}{F \cdot P}.$$
 (18)

If an area F is sectioned into basic areas  $f_{ik}$ , a quantity  $S_{ik}$  can be defined for each—the surface density of the seismicity. Besides, it is possible to compute the frequency of tremors  $n_{ik}$  for angular points for the period under observation and the sum  $\sum j_{ik}$  which shows the intensity of each separate tremor and the distribution of its force in the area. Toperczer also proposes to evaluate seismic danger by the probability that a destructive earthquake may take place in a given region during a given time interval. Thus, since the main values of the region's seismicity are only strong earthquake foci, all surrounding territories with no strong earthquakes would be considered non-seismic, irrespective of whether or not tremors of various strengths reach there. Seismic danger here would seem minimal, according to the calculation. This may not be the actual condition of the area, as regions without their own foci may have very strong tremors due to the seismic activity of adjoining territories.

V.I. Keilis-Borok, I.L. Nersesov and A.M. Yaglom (1962) considered the economical problems connected to shocks. First, they computed the number of tremors of different values released by the earthquakes with epicenters beyond its limits for each basic area and then added tremors from the foci within it. Such an approximate computation of the number of tremors, it appears, is actually not correct, since shocks are related not to the area but to each separate point (Riznichenko, 1969).

The first general solution to the computation of shocks was found by Riznichenko (1965) who later (1968) described it in detail.

Shocks  $B_I$  is the mean frequency of the repetition of tremors of a given intensity I at a given point, to the maximum possible intensity. These tremors result from activity from close and far earthquake foci, i.e., all foci producing tremors with the intensity I at the point under investigation. Thus, when calculating the shocks, it is necessary to consider the total action of the tremors, and therefore, the mention of the total shock  $B_I$ , representing the seismic effect on the surface. Its computation is carried out on the basis of given earthquake foci in accordance with the expression:

$$B_{\Sigma_I} = \int \int_{V} \int N_{\Sigma_I} \, dx \cdot dy \cdot dz, \qquad (19)$$

where  $N_{\Sigma_I}$ —transferred to the unit time and volume, the total number of earthquakes with hypocenters in the elementary volume  $V = dx \cdot dy \cdot dz$ , which at this point cause tremors of intensity *I* and above. Integration is extended to the entire volume of the region where the earthquake foci are met (Riznichenko, 1966).

When the law of earthquake repeatability is established in the following form:

$$N = A \cdot 10^{-\gamma} \, (K - K_0), \tag{20}$$

where N—mean number of earthquakes in the energy class  $K \pm 0.5$  and on the unit space and time;

A--seismic activity, i.e., spatial density of the earthquakes of a given class of energy;

 $\gamma$ —inclination of the curve of repeatability;

 $K_0$ —fixed quantity of the energy class of the earthquake to which the seismic activity definition is related.

In formula (19), the following expression is obtained for the total shocks

$$B_{\mathcal{Z}_{I}} = \frac{1}{10^{0.5\gamma} - 10^{-0.5\gamma}} \iint A \left[ 10^{-\gamma(K_{1} - K_{0})} - 10^{-\gamma(K_{\max} - K_{0})} \right] dS,$$
(21)

- where S—area surrounding the point of the region with epicenters in all basic areas— $dS = r_0 dr \cdot d\alpha$ , existing on the various hypocentral distances  $r = \sqrt{r_0^2 + h^2}$  and in various azimuths  $\alpha$  from this point;
  - $r_0$ —epicentral distance;
  - h-mean foci depth which explains the change in formula (19) from triple to double integral;
  - $K_1$ —index of the seismic energy degree emitted in the focus, resulting in tremors of the given intensity I and higher at the point under consideration;
  - $K_{\max}$ —maximum possible earthquake on area dS.

Shocks may be computed for seismic tremor intensity expressed in any form, e.g., in the density of earthquake energy flux (Riznichenko and others, 1967, 1971a), or in points of standard seismic scale (Riznichenko and others, 1969, 1970). In both cases formula (21) may be used initially, in which the quantity  $K_1$  is expressed in accordance with the accepted intensity. [If tremor intensity I is expressed by the density  $\Xi$  of the seismic energy flux then the law of damping of  $\Xi$  with distance r, is used in the form

$$\log \Xi = \log \Xi_R - n \; (\log r - \log R), \tag{22}$$

where  $\Xi_R$ —density of the energy flux on the reference sphere with radius R;

*n*—damping coefficient of the energy flux density with the hypocentral distance *r*;

 $\Xi$ —density of the seismic energy flux, i.e., the energy flux arriving on 1 km<sup>2</sup> at the observation point.

For  $K_1$ , in the formula (22), the following expression may be brought in:

$$10^{K_2} = 4\pi R^2 \left(\frac{r}{R}\right)^n \cdot \Xi.$$
(23)

Putting in expression (21), the value of  $K_1$  from (23), and changing the integration to machine summation, one gets the computed shakeability formula  $B_{2g}$  in the final form

$$B_{\Sigma_{\Xi}} = \sum_{S} A \frac{\left\{ \left[ 4 \pi R^{2} \left( \frac{r}{R} \right)^{n} \cdot \Xi \right]^{-\gamma} - (10^{K \max})^{-\gamma} \right\} \cdot 10^{\gamma \cdot K_{0}}}{10^{0.5 \gamma} - 10^{-0.5 \gamma}} \Delta S.$$
(24)

The double integral along variable r and  $\alpha$  is replaced by one summation, since the change in the tremor intensity is now considered dependent on distance only.

The given value of the density E of the seismic energy flux during calculations for a shock map of Eastern Uzbekistan (Riznichenko and others, 1967; Zakharova, Seiduzova, 1969) was changed to approximate points. For this was used the relation between the energy flux density and value of points obtained by Nersesov and others (1960). Here, the term point value means the point value  $I_0$  in the epicenters of strong earthquakes.

It is evident, that it is not entirely correct to use the relations between the quantities  $\Xi$  and  $I_0$  to evaluate tremors according to point values at observation points any distance from the epicenter. Therefore, it was important to construct maps of shocks of the same intensity territory expressed immediately in points.

To determine the value  $K_1$  in formula (21), one may use the law of damping point values with distance, as obtained by N.V. Shebalin (1968):

$$bM - I = S \log r - C, \tag{25}$$

where b, S, and C are coefficients.

Expressing the magnitude M through the energy class  $K_1$  according to the formula

$$K_1 = pM + q, \tag{26}$$

where p and q—coefficients, one gets the following expression for  $K_1$ :

$$10^{K_1} = r \frac{SP}{b \cdot 10} q - \frac{cP}{b} \cdot 10 \frac{P}{b} \cdot I.$$
 (27)

Putting the value of  $K_1$  from (27) in (21) one gets the computed formula for shocks  $B_{\Sigma_T}$ :

$$B_{\Sigma_{I}} = \sum A \frac{\left\{ \left[ 10^{q} - \frac{cP}{b}, r \frac{SP}{b}, \frac{P}{b}, 10^{-\gamma} - (10^{K_{\max}})^{-\gamma} \right\} 10^{\gamma}, \kappa_{0}}{10^{0.5 \gamma} - 10^{-0.5 \gamma}} \right\} \Delta S.$$
(28)

With the given formulas one may compute the shocks for any earthquake distribution according to quantity and for any distribution of intensity around the epicenter (Riznichenko, 1966). At the present time maps of shock waves are computed by assuming the linearity of the curve of earthquake repeatability and the circular form of isoseists. The initial material for the computations are: the map of seismic activity A, the mean depth hof the foci of earthquakes, the inclination of the curve of repeatability  $\gamma$ , the map of maximum possible earthquakes  $K_{\text{max}}$ , and the law of damping seismic intensity with distance. Since maps of shock waves are computed by computer, proofs about the computer programs and their results in the territory investigated are given in the next part.

The illustrated method of computing maps of seismic shocks makes it

possible to quantitatively evaluate seismic danger, having added to the determined intensity of the tremors in the studied zone, e.g., in points and also the frequency of their repetition. While transferring the map of shocks to a given interval of time it may be possible to compute the probability of seismic dangers. Thus the main deficiency of existing seismic delimitation methods noticed by Medvedev (1960) is avoided—the absence of a time factor and the evaluation for each point of the probability of earthquakes of a given force.

Further development of the Riznichenko's method suggests that the intensity of the seismic effect be expressed in spectral-temporal frame (Riznichenko, 1970, 1971). Then one may also remove the other deficiency of the existing method of seismic delimitation—the absence of regional differentiation according to the spectral nature of the earth's oscillations.

#### Chapter II

# Use of the Computer to Quantitatively Investigate Seismicity

All the above methods use as initial data information about the occurrence of earthquakes of various energies in the region under investigation to determine quantitative seismicity features. To construct a repeatability curve, one should limit the information about earthquake energy and its effect in the territory. Also, to construct a map of seismic activity or the maximum possible earthquakes, it is necessary to know their spatial or area distribution, i.e., to have a map of epicenters. This is related also to the methods of registering seismicity accepted abroad. Mapping either as units of the density of total seismic energy or as stress release (seismic flow) demands knowledge about the places of the emission of earthquake's energy.

Thus the quantitative investigation of seismicity in any region should begin by establishing the foci coordinates of local earthquakes. Because of the necessity of this step, it seems, computer methods in seismology were developed.

One of the first programs was for a IBM-704 (Bolt, 1960 a, b), to correct the hypocenter coordinates and times of emergence, which were computed by hand and stated as first estimates. The problem was solved with information about the minimum differences between the observed times of the appearance of waves P, PKP, and  $\rho P$  (for deep points) and calculated by the Jeffrevs-Bullen hodograph. The least squares method was used, along with right-angled coordinates and observations from more than 50 seismic stations, each of which was weighted in accordance with the seismic wave time discrepancies. In the final results, corrections were introduced for the earth's ellipticity. In 1961 B. Bolt wrote a new program for the IBM-709 and IBM-7090 in which, besides finding the location of the epicenters, the seismic wave hodograph was corrected (Bolt, 1961). To Bolt's program, accepted for assessing earthquake parameters by the Coast and Geodetic Survey of the USA, was added an initial search for the hypocenter coordinates according to data from five seismic stations. The program was written for the IBM-650 (Gunst, Brazee, 1962) and envisaged eliminating transit times of seismic stations with large discrepancies from further computations.

The subsequent program (Gunst, Engdahl, 1962) was divided in two parts. First the data was grouped by hand to determine the hypocenters and about 15% of the descriptive data was discarded; two-fifths of the stations were chosen along two initial hypocenter approximations, one of which was usually required for further computations. The second part of the program automatically found the hypocenter coordinates as well as the emergence time of the focus and station residual. The depth of the focus was located without confidence, especially when no data existed closer than 20°. With observations from not less than 50 stations the accuracy of the epicenters was 0.1° whereas, the focus depth was  $\pm 25$  km. Later, the first part of the program was also automated (Engdahl, Gunst, 1966). To select coordinated data, the times were compared by pairs to get the arrival of the longitudinal waves at various stations. If their difference was more than the time of run between them, they were considered nonconcurrent and discarded by the computer. As a theoretical base the Jeffreys-Bullen hodograph was used, the experimental data were presented by the arrival time of the P and PKP waves. The first approximation was determined from five stations and corrections were introduced concerning the height of each and the ellipticity of earth. Besides the hypocenter coordinates, the program determined azimuths, epicentral distances, magnitudes, and corrections to the hodograph.

In 1962, a program was written to determine earthquake hypocenters on the UNIVAC 1103 (Herrin, Taggart, Brown, 1962) according to data from 200 seismic stations. Its main difference from the Bolt program was the determination of time discrepancies, in which corrections are introduced for the absolute height of the station and ellipticity of earth. The accuracy of the epicenter determination found from four nuclear explosions, was 2.5-7 km and that of the focus depth from waves was 3-16 km. According to nuclear explosion and earthquake data in the USA, the regional changes in the velocities of Pn waves were investigated and, as a result, a map was constructed showing Pn velocities from 7.6-8.1 km/sec for the western part of the country and 8.1-8.4 km/sec for the eastern. This *Pn* velocities map was used to prepare a new program to determine earthquake epicenters, increasing the computation accuracy considerably (Herrin, Taggart, 1962). For example, the calculation of the focus location of a nuclear explosion (Herrin, Taggart, 1966) showed that, using data from 91 stations, taking into account regional and station corrections, the coordinates were determined ten times more accurately.

A program to determine the epicenter coordinates of remote earthquakes by an analytical method was written for the IBM-704 (Ullmann, Maaz, 1964). It was a solution of the spherical triangles system. Each determines one possible value of the epicenter coordinates, whereas, the most probable of their values is found by computing the weighted mean (average). The above programs were meant for analyzing remote earthquakes. The method to determine epicenter coordinates of close earthquakes was first proposed by Flinn (1960). The program to determine coordinates of hypocenter and time of emergence of the focus of close earthquakes was worked out for a station network at a Pasadena laboratory (Nordquist, 1962). The arrival time of the direct and two head waves, recorded by not more than 24 stations, was entered in the computers. Hodographs were computed for a three-layer model of the earth's crust with the focus lying above a basalt layer. The hypocenter was found by the least squares method, in which the observation weight depended on the residual. Uniform distribution of stations in the azimuth relative to its position is necessary to accurately determine the epicenter; whereas, for the focus depth each quadrant of stations must be sufficiently distant to record the direct and head waves. The main drawback of the program is the absence of a hodograph for foci below the Konrad boundary and the limited initial data (not more than 24 stations).

The program (Nordquist, Gardner, 1963) was meant to determine the epicentral coordinates and emergence time of the focus of southern California earthquakes. Approximate epicenter coordinates, emergence of the focus, and the arrival time of not less than six phases of longitudinal and transverse waves for the closer stations were entered in the computer. This program proposed a two-layer section of the earth's crust. Corrections to the first estimates were made by the method of least squares.

The Cisternas program (1963) was designed for the Benuiks G-15. It used a two-layer section and longitudinal wave travel time, corrected for the structure of the earth's crust. The accuracy of the coordinates determination was 1-3 km.

Arrival times of the direct longitudinal and transverse waves not more than 200 km from the epicenter, were used as initial data in the program to determine close earthquakes in southeast Australia (Cleary, Doyle, 1962). The depth of the focus was not determined-the main drawback of this program. The program to analyze local earthquakes recorded by eight seismic stations in Nevada (Ryall, Jones, 1964) was prepared for the IBM-1620. The arrival times of P and S waves were entered in chronological order. Here the arrival of the transverse wave was used only to eliminate earthquakes taking place outside the area under investigation. The program also excluded earthquake data registered by less than three stations. The choice of the initial estimate of the epicentral coordinates was made by comparing the observed differences of the P waves and the timings for three pairs of stations with tables stored in the computer memory. These were then computed for the given model of the earth's crust for epicenters at the corners of a rightangled grid for every 50 km. Thereafter the position of the epicenter was made more accurate by the method of least squares according to all available data about the arrival times of the P waves. This correction used a model of the crust with a layer boundary inclination found by the refracted waves method. In this program as in the previous one, the depth of the focus was not established.

A program to determine the hypocenters of Japanese local earthquakes (Aki, 1965a) gives the time the P and S waves first arrive at the station and an initial estimate of the focus. These are corrected by the least squares method, in which the theoretical time of arrival is computed along the two-layer section. Inside the section layer the propagation velocity of the elastic waves is varied according to Bullen's step rule. After determining the hypocenter, the emission angles of the seismic rays from the focus are computed. These are necessary to study the earthquake's dynamic parameters. A computer evaluation of the accuracy of the hypocenter positions (Aki, 1965b) showed that there were many errors in the times of emergence of the focus and its depth. With a sufficient number of observational stations these errors are insignificant when determining the coordinates of epicenters.

Seismic observations were automated by the Japanese meteorological agency in the following manner (Ichikawa, 1965): using the hand measured times of the first arrivals of P and S wave groups, recorded by agency stations, a first estimate of the coordinates of the epicenter and time of emergence of the focus were determined by computers. Thereafter, using the method of least squares the epicenter and the time in the focus were found by successive estimates leading to the minimum mean square residual time of the arrival of P and S. The magnitude of the earthquake M is determined on the computer first for each station from the hand calculated maximum amplitudes of P and S waves (using Tsuboi's formula) and then the average value of M is found from the data of all stations. Also introduced are the relative weights of the arrival times of the P and S waves. If necessary, the output gives, besides coordinates of epicenter and M, the discrepancies of travel time in the function of epicentral distance. An important drawback of the program is the absence of data on the depth of the earthquakes foci.

In the USSR, the first program for the machine search for the coordinates of focus (EPI-1) appeared in 1963 (Pyatetskii-Shapiro, Jelankina, Keilis-Borok, and others, 1963). This program, different from the abovementioned ones, does not require a first estimate. It uses the arrival times of P and PKP waves and the Jeffreys-Bullen hodograph. Calculating the focus position and the time of emergence of the focus leads to a search of the minimum mean square discrepancies of the arrival times of longitudinal waves in the space of the hypocentral coordinates. Observations with large discrepancies are excluded; since the earth is non-spherical the geographical coordinates are changed to geocentral. Later this program was improved, (the new model—EPI-2); use of pP and sP wave data gave a more accurate focus depth and epicenter position (Vartanova, Jelankina, Keilis-Borok and others, 1966). The EPI-1 and EPI-2 programs were mainly for analyzing remote earthquakes with epicentral distances higher than 20°. The final computations include the earthquake dates, time of emergence of the focus in hours, minutes, and seconds, the epicenter coordinates in degrees and minutes, focus depth in kilometers, and the mean-square error of the coordinates in seconds.

Closer earthquakes are analyzed by a program for the M-20 (Abutaliev, Butovskaya and others, 1967a). It uses a right-angled system of P wave coordinates and regional hodographs; the time of emergence of the focus is given by the difference S-P. The epicenter is obtained iteratively for various fixed depths of the focus. Coordinates for the minimum mean-square deviations of theoretical and observed travel times are used as solutions. The accuracy of the determined coordinates is evaluated, as a result a principal ellipse may be constructed for each epicenter (Abutaliev, Butovskaya and others, 1967b). The result is rectangular coordinates which are very inconvenient, since spherical coordinates are usually used to prepare a catalog of earthquakes. They are considerably distorted in the double transfer process, when the spherical coordinates from the stations under observation are changed to rectangular and later these rectangular epicenter coordinates are again converted back to spherical coordinates. The program to determine the earthquake hypocenters in Uzbekistan (Pavlovskaya, 1968), written for the Minsk-2, does not have this drawback. It uses special coordinates, the first arrival times of longitudinal waves at stations, the time of emergence of the focus, and regional hodographs. As initial estimates the coordinates of the nearest-to-the-epicenter stations are chosen; they are determined by the method of least squares on some fixed depths of the hypocenter; data are excluded from stations with large discrepancies. For the final result are chosen coordinates of the focus with the least mean square residual of the observed and the theoretical travel time. Another version of this program (Fadina, 1971), besides the focus coordinates, their mean square error, and epicentral distances, considers the direction of the epicenter-station azimuth, apparent velocities, and the deviation of the travel time from that tabulated.

Programs not requiring the velocity cross section of the region under investigation (Pomerantseva and others, 1971; Abutaliev, Ikramov, 1970) propose the distribution of direct waves in a uniform medium and are meant for assessing closer earthquakes, only a few hundred kilometers, thus limiting their application considerably.

One version of the azimuth method to determine the earthquake epicenter by computer according to equations of the epicentrals type  $A_i x + y + B_i = 0$ is described in the program by M.B. Vertlib (1968). The coefficients  $A_i$  and  $B_i$  are found from the differences of wave arrival times at four stations. On the surface AB, points  $A_i$   $B_i$  should lie in a straight line, on the parameters of which the coordinates of epicenters x, y are determined. For its construction by the composition method, the initial points are converted to others with fewer points also forming a straight line. The epicenters on Pribaikal were determined by this program. Its application is considerably limited due to the use of the arrival times of strictly identical phases of elastic waves. The program does not determine the earthquake's depth of the focus, which somewhat depreciates the calculated results. The program by F.V. Novomaiskaya and G.I. Perevalova (1968) may be a possible addendum to this program. It determines the foci depths of Pribaikal earthquakes by a differential method. In this method the observed arrival times of waves are corrected to agree with the hyperbolic hodograph for the given velocity distribution of the transverse waves, close to 3.5 km/sec.

The coordinates of the epicenters and foci depths of closer earthquakes are simultaneously computed from the observations of Pribaikal's seismic stations using a program by S.I. Golenetskii and G.I. Perevalova (1971). designed for BSEM-2. The arrival times of the direct transverse S waves at the registering stations and their geographical coordinates are used as initial data. The solution is found by estimates in several steps. In the first step the time of emergence of the focus or the nearest-to-the-epicenter station is computed from the S-P values and, with the given value of the velocity V, the first estimate of the epicentral coordinates is computed. In the second, according to the obtained coordinates with given values of V and focus depth h, the sum of the residual squares of the travel times and the variation direction of the coordinates is determined for the epicenter. In the third and final step the solution is corrected and the focus depth and velocity are varied with the given step. The minimum sum of residual squares is considered the solution. In the next stage the accuracy of the solution is evaluated with the introduction of unknown weights and their confidence limits, which are calculated on the basis of the student's distribution criterion. The program also determines the propagation velocity of seismic waves (if not given earlier) and the coordinates of earthquakes' foci, not only by observations of direct waves, but also according to their collection from head waves ( $\overline{P}$ ,  $P, \bar{S}, S$  during the minimization of the general sum of the residual squares of all utilized travel times. On an average, it takes two minutes of machine time to get one solution with an evaluation of the errors of the results.

A number of review works discuss the results of machine computation of foci coordinates of earthquakes. A computer was used in the seismological laboratory of California Institute of Technology to find the position of the hypocenters and to solve other seismological problems (Phinney, 1963). Studies on the computer of the 191st underwater earthquake on the Galapagos Islands during 1935–1961 with the superimposition of the distribution of epicenters were conducted by N.K. Acharya (1965). L.R. Sykes and M. Ewing (1965) present a vertical section map through the epicentral zones in the Greater and Lesser Antilles. To construct this map the foci of five hundred earthquakes during 1950–1964 were redetermined by computer, using M = 3.5-6.7. N.V. Kondorskaya and others (1966) described the results of using a computer to generalize the seismic observations. In the USSR, using the EPI-1 program to determine epicenters according to the data from a network of stations of the Unitary System of Seismic Observation (USSO), more than five thousand earthquakes were assessed by 1964. This analysis provided greater computation speed and accuracy when compared to hand determination. The possibilities for solving other problems were also made clear, and influenced improvements in the system to interpret seismic observation. Thus a mean law of the distribution of residuals (inclination from the standard Jeffreys-Bullen hodograph) was found for seismic stations in the USSR, the accuracy of determining epicenters in various parts of the earth's sphere was evaluated, and so on.

While selecting the proper method of machine processing the earthquakes in Uzbekistan and writing a corresponding program, M.P. Pavlovskaya (1968, 1971) reviewed works which also describe some of our programs.

Combining automatic computer operations, which use programs to determine coordinates of the foci of earthquakes, with some initial manual seismogram operations, enables us to develop entire systems to treat seismological data in individual regions and on a global scale. The USA's system of automated bulletins and the establishment of seismic data (Rackets, 1963) is related to it. It consists of a number of programs which guarantee seismic bulletins and determine the minimum correct information to investigate seismicity with the fewest changes of computer magnetic tapes. The operations include the manual determination of the seismic wave arrivals, and the verification of their arrivals as forecast by computer from Coast and Geodetic Survey of USA (CGS) information on the hypocenters and according to hodographs. Seismic bulletins are hand done only after that, as the CGS information becomes useful during the choice of arrivals. This makes the bulletin more complete especially when the interpreter is not very experienced.

To place the seismic wave arrivals from a number of stations, with epicenters that are determined by the CGS, a FORTRAN program was written (Fletcher, Wellen and others, 1966). Thus it is possible to identify up to 23 phases of elastic waves using data from monthly bulletins on earthquakes from five USA seismic observatories working on the VELA-UNIFORM project.

A computerized system at the International Seismological Center in Edinburgh is described by P.L. Willmore (1966) and D. Fluendy, D. Mc-Gregor and P.L. Willmore (1966). Data from separate seismic stations on the arrival time of the elastic wave phases and their amplitude are carried on special cards, with pencil notations. The franking installation converts these data into punch cards. The computer analyzes the information on the punch cards by a special correction program, which excludes erroneous records. Next the data from various stations is unified and recorded on magnetic tape in order of arrival. They are now the initial data to determine the epicenter coordinates and are used in the following manner: 110 angular, approximately uniformly distributed points are chosen. The computer figures the travel time of the waves from each point to each station registering the earthquake. The difference between the observed transit times at the stations and those calculated to the nodal point gives an estimate of the emergence time of the focus with the epicenter placed at the points. The best agreement of the differences is obtained for points at the least distance from the actual epicenter as compared to the other nodal points. This point is the initial estimate for the following accurate computation of the epicenter position using the CGS USA program (Bolt, 1960, a, b). The algorithm of the automatic identification of the seismic wave phase, reproducing the corresponding manual work, is done in FORTRAN-IV in A.L. Levshin's program for the International Seismological Center in Edinburgh (Keilis-Borok, ed., 1968).

It may be noted that the initial data to determine earthquake coordinates by computer may not be available only on punch cards which contain codified information from seismological bulletins. In modern times there are methods to directly enter information on the kinematics and dynamics of seismic waves from seismo-receivers. For this purpose systems of signals from the so-called large seismic groups (LASA) have been formed, as described by R.V. Wood and others (1965), H.W. Briscol and P.L. Fleck (1965), C.B. Forbes and others (1965), P.E. Green and others (1965), G. Dorman (1967), G. Dorman and others (1969). The work of T.I. Sokolowski and G.R. Miller (1967) discusses an automated method to quickly determine (in a few minutes after registration of longitudinal P waves) an earthquake's epicenter on a specialized computer according to the difference of the Prun to the four seismic stations. These stations are 35-40 kilometers from each other on the Hawaiian Islands. This method insures the transmission of the obtained information to the forecasting service by seismic sea waves in the USA. D.H. Weichert and E.B. Manchee (1968) described a computer method to make recordings from seismic stations in Yellowknife to obtain the automatic emission of seismic signals, the determination of epicenter coordinates, and earthquake sizes according to short period P waves.

The next step to prepare computations for quantitative seismicity indices, after determining earthquake epicenters and their dynamics, is the orderly and systematic arrangement of information. For this purpose earthquake catalogs are made and they are entered in the order of their data processing.

A catalog of punch cards with data from more than 9,000 southern California earthquakes with magnitudes M > 3 between 1934 and 1963 was made in 1964 (Nordquist, 1964). The punch cards may be analyzed by an IMB-

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7090. The available enumeration of their information is varied regarding the accurate determination of the magnitude, focus timing, and earthquake coordinates. As a result there are four accuracy gradations—A, B, C, D. To increase the speed of computation the data are initially transferred to paper punch ribbon, suitable for the Bendix-G-150. J. Nordquist (1964) illustrates examples of using a catalog of punch cards and tapes for computing seismicity and its distribution in southern California. The disposition of the data is also shown and a scheme is suggested for the most economical computation (least punching time) from punch cards.

The catalog of Nevada earthquakes between 1852 and 1961 was prepared on punch cards for an IBM computer (Slemmons, 1966). Its data can be easily converted into quantitative parameters—specific seismicity and tectonic flow—to show stress release during earthquakes. The maps on stress release during Nevada earthquakes so obtained confirm the comparability of local regional seismicity values on an area with the seismicity of western states of the USA.

V. Karnik prepared a catalog enumerating more than 10,000 European and mediterranean earthquakes with  $M \ge 3.5$  between 1901 and 1955 (Karnik, 1965 a). In the first section of the catalog information is given in chronological order; in the second it is given according to the coordinates of separate regions through  $0.5^{\circ}$  lat.  $\times 0.5^{\circ}$  long.; the third lists strong earthquakes, mainly from macroseismic data beginning in 1829. All these sections maintain a uniform order of material distribution—each line is related to one earthquake, and along the more than 40 columns, are noted the date and time of appearance, coordinates of focus, value of M, region number, number of stations to determine M macroseismic information, and so on. Each column has one figure for ease in entering data in the computer, (e.g., columns 1-4—the year of the earthquake—1901).

In the KSE IFZ\* AN USSR codification of the earthquake catalog of the Garmsk seismoactive region has been completed and holds information about more than 20,000 earthquakes which permits the simultaneous use, for thematic machine working, of a large quantity of uniform material (Sadovskii, ed., 1971).

Information on the immediate computerization of quantitative seismicity indices appeared in literature only recently. Thus, J. Nordquist (1964) introduces the program algorithm to construct a seismicity map of southern California. In it, as a measure of seismicity, the sums of the square roots of earthquake energy has been accepted; they are normalized about the area. The author thinks that his map shows the density of the release of elastic pressures. This viewpoint is supported by P. Amand (1956), and Richter

<sup>\*</sup>Complex Seismological Expedition of the Institute of Physics of the Earth-General Editor.

and Allen (1958), who conducted similar hand calculations earlier.

With a computer, D. Slemmons (1966) calculated maps of the release of elastic pressures in Nevada, using the terms specific seismicity and tectonic flow. To determine these terms earthquake energy was totaled. In the first case, it was emitted on the unit area in the unit time, and in the second as square roots from the seismic energy of the foci.

In 1966-1967, a program was prepared in the USSR for the M-20 computer and for the first time, maps of seismic shocks  $B_{Z}$ —mean repetition frequency of tremors of given intensity at a point on the earth, were computed (Riznichenko and others, 1967). Computations were made for Eastern Uzbekistan based on hand constructed maps of seismic activity and maximum possible earthquakes and on the dependence of seismic intensity I on the epicentral distance. In Riznichenko's works (1967, 1969) algorithms of  $B_{Z}$  are introduced and maps of two values of I, expressed in units of the density of seismic energy flow, are shown, viz.,  $E_1 = 10^{12}$  J/km<sup>2</sup> and  $E_2 =$  $10^{13}$  J/km<sup>2</sup>. Later seismic shock maps were computed for the intensity given as standard points. A.I. Zakharova and S.S. Seiduzova (1971) compiled shock maps for Eastern Uzbekistan for tremor intensities of I = 6, 7, 8and 9 points.

An algorithm of the shocks map program and its block-diagram is explained by S.S. Seiduzova and A.I. Zakharova (1969, 1971). This program computes the value of shocks  $B_{\Sigma_I}$ —the total frequency of seismic impulse repetitions of given intensity and higher—as well as value, inverse of  $B_{\Sigma_I}$  mean period T. In algorithmic form the relation (24) is used with the tremor intensity I expressed by the density of the seismic energy flow or (28) with the values of standard seismic scale given in points. In both cases the maps of maximum possible earthquakes  $K_{\text{max}}$  and seismic activity A, curves of damping of intensity with distance (22) or (25) constants of the formula (24) or (28) are initial computation data. A version of the computation of  $B_{\Sigma_I}$  maps for which the value of A is not entered in the data set of initial data is also available. The value of A is computer calculated according to the correlated equation (A,  $K_{max}$ ) in formula (13). The initial map  $K_{max}$ should be made from two parts-the central part represents the territory on which shocks are computed; the peripheral is the territory of which the earthquake foci call for given tremor effects in the central part. The depth h of the earthquake foci is considered a constant for the first estimate, i.e., its mean value is used for the region under investigation. For largely different depths of seismogenic layers of the earth's crust, all computations of shocks  $B_{z_I}$  may be conducted layerwise, beginning from maps A and  $K_{max}$ and the results  $B_{\Sigma_1}$  for each point on the earth should be superimposed (Riznichenko and others, 1970). The final stage of the program is to assign the number of the point,  $B_{\Sigma_I}$ , and T in years.

Vel'kner (1969), analyzing the spatial distribution of seismic parameters

in North Chile, described the results of the IBM-360 investigations of coefficients a and b in the Gutenberg-Richter statistical formula

$$\log n(M) = a + b(M),$$
 (10')

where n(M)-number of earthquakes with the magnitude between M and (M + dM).

While normalizing the quantity a along the area and timing, as conducted by Vel'kner, this coefficient happens to be analogous to the quantity of seismic activity accepted in the USSR. Coefficient b on its own is similar to the inclination  $\gamma$  of the repeatability curve of earthquakes taking into account the transfer from magnitude M to energy class K. The values of the coefficients a and b were calculated for an overlapping  $1^{\circ} \times 1^{\circ}$  section where the mean depth of focus h was also determined. In this the following formula of Aki (1965 c) was used:

$$\overline{b} = \frac{\log l}{\overline{M} - M_0},\tag{29}$$

where  $\bar{b}$ —most probable value of b for the group of earthquakes submitting

to the statistical relation of Gutenberg-Richter;

 $\overline{M}$ —mean;

 $M_0$ —lower limit of magnitude for this group so that

$$\overline{M} = \frac{\sum(\overline{M} \cdot n)}{\sum n}, \quad M \ge M_0.$$
<sup>(29')</sup>

To calculate the normalized value  $a = \tilde{a}$  (mean yearly number of earthquakes with  $M \ge 3.5$  in area (10<sup>4</sup> km) the expression used was

$$\bar{a} = \log N_{\Sigma} (M_0) + \bar{b} M_0 \log T,$$
 (30)

where  $N_{\Sigma}(M_0)$ —total number of earthquakes with magnitude  $M_0$  and higher; T—period of observation.

Statistical parameters a, b, and h correspond to each section, smoothed by dual filters, the coefficients of which are proportional to the areas of the neighboring sections which are exceeded:

$$A_{ij} = \frac{a_{ij} + 0.5 [a_{ij\pm1}; a_{ji\pm1}] + 0.25 [a_{i\pm1}, j\pm1]}{n_{ij} + 0.5 [n_{ij\pm1}; n_{i\pm1}, j] + 0.25 [n_{i\pm1}; j\pm1]}$$
(31)

where

$$n_{ij} = 1$$
, if  $a_{ij} \neq 0$ ;  $n_{ij} = 0$ , if  $a_{ij} = 0$ .

Parameters a, b, and h were calculated from earthquake observations during 1963–1966. The corresponding isoline maps were constructed according to their smoothed values. Besides, for each  $1^{\circ} \times 1^{\circ}$  section the values of the logarithm of the mean annual quantity of the released energy E were found on the basis of these parameters, i.e., according to Utsv's formula (1961):

$$E_{\Sigma} = \frac{bE}{(\beta - b) \ B \ (\beta/b, \ N)},\tag{32}$$

where E—energy of earthquake with magnitude M;

 $\beta$ —coefficient in the equation

$$\log E = \alpha + \beta M; \tag{26'}$$

B-beta-function.

Further, the isoline maps of the quantities  $\log E_{\Sigma}$ , are constructed on the distribution of extremes which appeared similar to those for seismic activity.

The curve for the distribution of earthquake magnitude was converted into the curve for the distribution of the value of tremors (intensity) using V. Karnik's equation (1965b):

$$M = \frac{2}{3}I_0 + 1.7\log h - 1.4, \tag{33}$$

from the smoothed values a, b, and h. Here  $I_0$  is the epicentral seismic intensity value. The curve for tremor distribution was used to calculate the mean yearly number of destructive earthquakes (with intensity  $I \ge 7\frac{1}{2}$  points) in each section and determine the so-called seismic risk, the probability of the appearance of at least one earthquake with  $I = 7\frac{1}{2}$  during the period T = 100, 50, 30, and 10 years using Poisson's timing interval distribution. Maps of seismic risk isolines for the first three periods are constructed according to the calculated values of probability. A comparison of these maps with the map of curve inclination b of earthquake repeatability shows an inverse correlation of the values brought in them-the b minimum corresponds to the maximum probability of an earthquake appearance and vice-versa. It may be noted that if the statistical seismicity parameters a and b are analogous to the seismic region parameters introduced by Riznichenko (1958), then the seismic risk value here considers the influence of an earthquake occurring on the  $1^{\circ} \times 1^{\circ}$  section to which the point under investigation is related. Also the probable seismic dangers, according to Riznichenko (1966b, 1971), are based on the frequency of tremors from close and far earthquake foci, at the point under investigation, i.e., from all foci which are capable of forming tremors of given intensity.

W. Sponheuer, R. Maaz and W. Ullmann (1970) introduced computer seismicity maps of central Europe. The density S(Z) of seismic energy at the point Z under investigation was considered a measure of seismicity between 1900 and 1967 and was calculated according to the formula:

$$S(Z) = \frac{E}{4\pi\hbar^2} \exp\left[-\left(\frac{\Delta}{2R}\right)^2\right],$$
(34)

where E-earthquake energy in ergs;

h—focus depth;

 $\Delta$ —epicentral distance;

R-radius of earth.

For instrumentally registered earthquakes the values of the energy were determined from the expression:

$$\log E = 1.6 M + 11.$$
 (26')

When only macroseismic data were present the magnitude M was obtained by Karnik's formula (33).

Computations of the value S(Z) were made from the data of 374 earthquakes with  $M \ge 4$  taking place between 1900 and 1967. Isolines of similar values of seismic energy density are differentiated on the map in tenfold and carried out through the corners of a square ten minute wide grid. During these 67 years the maximum seismicity level  $S(Z) = 9 \cdot 10^{17} \text{ erg/km}^2$  and maximum intensity were observed in the Swabian Alps.

Recently, using statistical methods, computer calculations were made on the probability indices of a seismic regime. Thus E.P. Tsyetkov (1969) using a BSEM-3M computer analyzed the synchronous nature of seismic regimes of various parts of the Garmsk region of Tajikistan from a combination of earthquakes between 1955 and 1965 in the energy interval classes K = 7-11. Maps were constructed of the distribution of epicenter densities with different sizes of areas of averaging-126 and 63 km<sup>2</sup>. For each the corresponding sum of earthquakes was converted into a timely order. These timely orders were paired with each other and a matrix was constructed, in which the members i and j reflect the coefficient of correlation r between the regimes *i* and *i* of the area. Since the fluctuation of the regimes in different areas may have various periods and contacts between the regimes may develop at different times, depending on the energy of earthquakes and the specific seismic life of the region, the investigated timing intervals were partitioned. As a result of this the following average time intervals were chosen: 0.25; 0.5; 1; 2 and 3 years. In each interval 104 timing orders were formed for the 126 km<sup>2</sup> area and 208 for the 63 km<sup>2</sup> area, in which from 9 to 44 members were enumerated in each order. The value of the coefficient of correlation r was determined from the expression:

$$r_{i,j} = \frac{\sum_{k} (N_i^k - \bar{N}_i) (N_j^k - \bar{N}_j)}{\sqrt{\sum_{k} (\bar{N}_i^k - N_i)^2 \sum_{k} (N_j^k - \bar{N}_j)^2}},$$
(35)

where  $N_i^k$  and  $N_j^k$ —quantity of earthquakes in *i*th and *j*th areas correspondingly in *k*th interval of time;

 $\overline{N}_i$  and  $\overline{N}_j$ —average number of earthquakes in these areas occurring in each time interval during the entire observation period.

Besides the coefficient of correlation of the paired orders, the signs of the inclinations were also established for 2- and 3-yearly intervals. The timing orders of 0.25 and 0.5 years, were grouped and correlated with the coefficient  $r \ge 0.6$ . For one year intervals chosen level r was 0.8. According to the calculated coefficients of correlation along with compact groups of contiguous sections, groups were divided into sections far from each other. To interpret these connections, a model of the actual earthquake catalog was made so that the earthquakes were distributed regionally with uniform density. The construction used a special adjunct to the computer—a random numbers sensor. It was explained that this model reflects a chaotic field of similar separate area connections in which group identification is not possible. When the actual results for the catalog and for the model were compared, it was noticed that with a decrease in the timing step, i.e., shorter periods, the differences between them are smoothed and with the smallest timing interval (0.25 year) they are practically absent. The maximum differences mentioned are clearly expressed in histograms of the distribution of the number of groups depending on their length. For collected variations of activity (density of epicenters) between blocks, that is, the unified section areas with positive connection at the level of given coefficients of correlation, the differences between the actual version and the model are also maximum for the large time intervals. It happens when longer correlative section groups exist as compared to the model. E.P. Tsvetkov explains the random connection field between separate regional sections by a general decrease in activity between 1955 and 1960 and then a general increase during 1961–1964. While analyzing the spontaneous correlation between neighboring areas for relatively longer times, it was established that the actual and the model connections differ by the total absence of a counter-phase model. In the shorter periods, there also is no connection with the negative coefficient of correlation in the actual version, i.e., during earthquake analysis. The author proposes that the negative correlations between the regions of adjacent sections may be formed by local changes in the pressure fields of the region. This is supported by the results of a comparison of the spatial distribution of positive and negative connections between neighboring sections with the strong earthquake map (K = 12-13), the epicenters of which are actually at those places where regional counter-phases are established between the connected areas. Inside the synchronous regions there are no strong earthquakes, their epicenters for K = 16-17 seemed timed to the contact zones of synchronous blocks.

E.V. Vil'kovich, V.I. Keilis-Borok and others (1970) used statistical methods on the computer to investigate the contact between earthquakes and the random changes of seismic activity with time, that is, the nonstationariness of the seismic region. To limit the number of observations of nearby earthquakes, two local statistics  $\hat{F}(d_{int})$  and  $\hat{d}(F_{int})$  were introduced.

The first indicates the time interval between the initial earthquake and the next one occurring not farther than  $d_{int}$  from it. The second is the distance between the epicenters of the initial and the next closest one to occur during the interval  $F_{int}$  after it. The thresholds ( $d_{int}$  and  $F_{int}$ ) were chosen to achieve maximum statistical sensitivity. Later the distribution of these introduced statistics was shown along the factual and random earthquake catalogs, which may be obtained by reshuffling the factual. The random catalog corresponds to the theoretical distribution. The comparison of the histograms of the distributions of these local statistics was done with non-parametrical criteria.

To introduce the influence of the initial earthquake on each successive one, the following relation was used:

$$R = K P_{\rm f} - P_{\rm r}, \tag{36}$$

where

 $P_{\rm f}$  and  $P_{\rm r}$ —are histograms constructed according to factual and random catalogs;

 $K = \int_{A}^{\infty} P_{\rm r}(S) \, dS \int_{A}^{\infty} P_{\rm f}(S) \, dS - \text{coefficient smoothing out the histograms}$ on the section  $(A, \infty)$ .

Here A is made sufficiently large, so that the influence of the initial earthquake is already damped and the conditional distributions  $P_r(S)S \ge A$  and  $P_f(S)S \ge A$  are in agreement.

The mutual correlation of the earthquakes is based on data obtained from the eastern part of Central Asia between 1952 and 1956 in the interval M from 3-44. About 2,000 earthquakes in the core (H < 75 km) and with intermediate focus depth (H = 80-250 km) were analyzed separately. For normal earthquakes an analysis of curves R(d) on the 95% reliability level shows that the initial earthquake is related to a next one farther than 50 km. The after shock of a strong earthquake has influence at a smaller distance -35 km. The curves R(F) show (99% reliability level) that after the initial earthquake there is an enhanced probability of another within 20-40 days. The construction of curves R(F) for the Presurkhoba, Pridarvaza, Eastern Tien-Shan, and Fergana regions of Central Asia testifies about the significantly different, positive influence of the initial earthquakes on the following, and negative on the next two (99% reliability level). For intermediate earthquakes, according to curves R(d) and R(F) at the 99.8% level, significant positive influence has been established of the initial earthquake on the successive one; but this influence is considerably smaller than in smaller ones. No negative influence was noticed.

Earthquake catalogs of eastern Central Asia between 1952 and 1956 show a random variation of their intensity with time. The reliability of the difference of earthquake intensities in 1952 and 1956 is very high—99.9%. The randomness of the variations of the spatial distribution of epicenters with time was also verified. For this purpose, the epicenter distributions for different durations (for example, of 5 years and of 3 months or 1 quarter) were compared using statistical criteria. In 11 of 20 quarters the distribution matched less than 5% which, according to A.I. Kolmogorov's criteria on the 99% reliability level, shows the randomness of the spatial distribution of epicenters with time. This established the nonstationariness of the temporal seismic process (variation of intensity), as well as spatial (random migration of epicenters).

A short survey of the methods to quantitatively describe seismicity and the use of the computer leads to the following conclusions. Presently in our country, a number of programs, other than those to determine the coordinates of the foci, have been written mainly to evaluate the stationariness of the seismic process in space and time. The programs to compute the values of the total seismic energy and stress release, as well as the coefficients of the Guttenberg-Richter statistical formula available abroad, belong to the seismicity characteristics which, in their physical concept, cannot fully describe the seismicity of any region, and cannot be used directly.

Programs are not available for computing and more so mapping the parameters of the seismic regime, determined by Yu.V. Riznichenko's method—a method most popular in the USSR. Subsequent chapters, therefore, are devoted to the development of such programs.

Computer Programs to Compute Main Seismicity Parameters

카고

Seismic regions for any territory are determined mainly by three parameters: inclination of the curves of earthquake repeatability, seismic activity A, and the maximum possible earthquake  $K_{max}$ . The mean long-term values of these parameters for the entire territory may be obtained by constructing a curve of earthquake repeatability, i.e., the distribution of the number of earthquakes according to their energies. For this, many years' instrumental observations of earthquakes which had a considerable range of energies are usually used as initial data. The inclination  $\gamma$  of the repeatability curve and the mean errors— $\sigma_i$  and  $\sigma_A$ —are determined by the method of least squares. This requires considerable time just to find the average long-term parameter values for the entire territory. The time requirement in manual work increases several fold during compilation of areawise maps for obtaining the spatial distribution of  $\gamma$ , seismic activity and the maximum possible earthquakes, increasing the amount of the manual work many more times. Therefore, it becomes necessary, from the point of view of time, to engage many technical personnel for these computations.

The above considerations and the need to calculate the maps and seismicity curves of Uzbekistan to study the special features of the seismic regime of separate regions, and problems of quantitatively evaluating seismic danger led us to write programs to accelerate the automatic calculation of the seismic regime parameters. While determining the seismic delimitation of the USSR in 1961-1962, and also during the recent preparation of the following seismic delimitation maps, we often came across unreliable uses of Yu.V. Riznichenko's main formulas to construct repeatability curves and seismic activity maps. The results were mainly distorted by the absence of calculations of return periods of the earthquakes of various energies. Computing the main characteristics of seismicity on the computer by standard programs averts, it seems, many errors which usually arise while comparing a seismic activity map with considerably more complex maps of maximum possible earthquakes in separate seismoactive zones. This comparison becomes necessary when constructing maps of seismic shocks for the USSR, a quantitative base for evaluating seismic danger.

In this work, programs are introduced whose aim is the computation

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of the main parameters of the seismic regime, curves of repeatability, maps of seismic activity, and maps of maximum possible earthquakes. The nomenclature of all programs begins with letters SP (seismic parameters), that is, SP-1 is the first program for computing seismic parameters, SP-2 is the second, etc. In all, there are seven programs. One is meant for computing the characteristics of the rule of earthquake repeatability, four are for maps of seismic activity, and two are for maps of maximum possible earthquakes. All the programs are for M-20, M-220, or BESM-4 computers and use the library of standard programs.

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## Chapter III

# Programs to Compute Seismic Activity Maps and Curves of Earthquake Recurrence

Seismic activity—the quantitative characteristics of seismicity—represents in itself the number of earthquakes of a particular class of energy occurring in a particular area in unit time. The first seismic activity maps were constructed by Riznichenko and Nersesov during 1958–1960. During the last twelve years, the seismicity of all scismically dangerous regions of the USSR has been evaluated using this most important parameter (Medvedev, ed., 1968, Riznichenko, ed., 1971). For this purpose seismic activity maps were prepared to present an objective distribution of the density of the epicenters of earthquakes in the region under study brought to one energy level. The mapping of seismic activity is a necessary step in the quantitative evaluation of the seismicity of any territory.

While computing the seismic delimitation of the USSR in 1961–1962, maps of the seismic activity A were compared with maps of the vertical gradients of the velocity of tectonic movements to specify the boundaries of zones of various intensities (Medvedev, ed., 1968). Currently, the computation of A is also necessary to prepare maps of the possible maximum earthquakes and seismic shocks (Riznichenko, ed., 1971).

Map A computations for large territories are very difficult and require considerable manual work and time. Therefore, it is necessary to use fast computers.

Nowadays, seismologists generally use several methods to compute seismic activity. The most widespread is the summation of earthquakes in a zone of averaging (Riznichenko, 1964a). In some seismoactive zones the classwise distribution of earthquakes method is most used (Butovskaya and others, 1966; Flenova, 1969). Seismic activity maps are constructed depending on the specific problems of studying one or another seismicity aspect with given details or accuracy by the distribution or summation method (Riznichenko, Gorbunova, 1968). There are several programs for computing seismic activity maps—SP-1; SP-2; SP-3, and SP-4.

### PROGRAM SP-1 FOR COMPUTING A MAPS WITH CONSTANT RESOLUTION BY THE SUMMATION METHOD

The constant resolution of the computation of seismic activity maps is insured by maintaining constant the areas of the zone of averaging. To construct such a map, the zone of averaging is usually split around each node of the given grid. In the zones the number of epicenters are totaled and later converted to unit area and time. The obtained activity A value is related to the nodes of the map grid in this method.

While writing the SP-1 program Zakharova (1970) proposed to define for the zone of averaging the activity by the computation interval a, i.e., the distance between two neighboring nodes of the given grid.

The catalogs of earthquake epicenters are usually published in spherical coordinates. For convenience of computation, we use these coordinates to compile maps of the established earthquake epicenters and during the actual computation of seismic activity maps—during transit from one node of the grid to another. Therefore, this computation interval is in fractions of geographical degrees; whereas the zone of averaging is right-angled, almost trapezoidal and its area is  $S = 2a \times 2a$ , km<sup>2</sup>.

The Riznichenko formula (1964a) was used to determine quantity A by the summation method in algorithmic form. It has the following form to normalize the number of earthquakes in 1,000 km<sup>2</sup> and for one year:

$$A = N_{\Sigma} \frac{1 - 10^{-\gamma}}{10^{-\gamma} (K_{\min} - K_0)} \cdot \frac{1000}{S \cdot T},$$
(37)

where  $N_2$ —number of earthquake epicenters in zone of averaging with

area  $S \text{ km}^2$ , in the period T of the establishment of earthquakes of energy class  $K_{\min}$ ;

 $K_{\min}$ —the least energy class of earthquakes in the region;

 $K_0$ —Energy class, about which the seismic activity is determined;

 $\gamma$ —inclination of the repeatability curve.

The SP-1 program is standard: with suitable built-in instructions based on the above formulas, it may be used to compute A in any territory, with any computation interval and any dimensions of averaging zones, with two initial data sets. These data sets fully determine the amount of machine computation.

The first set of the initial map of epicenters,  $M_1$ , is given as matrix  $A_{mn}$ . The number of lines of the matrix m is equal to the number of earthquake epicenters on the map. The number of columns n is the number of parameters determining each epicenter. In principle, m may be any number (to the limit of the computer memory), i.e., map A may be computed for any sufficiently large area. The number n in the computation of map A for the earth is limited by three parameters for each earthquake: the spherical

-------\_\_\_\_\_ - --A1  $\mathbf{A}_2$  $A_3$ Address Command \_\_\_\_ - --- ---- ----\_\_\_\_ ----0500 A ì 0513 A 0526 A 0541 A б 

PROGRAM SP-1

(Contd.)

| Address | Command | <b>A</b> <sub>1</sub> | A2   | A <sub>3</sub> |
|---------|---------|-----------------------|------|----------------|
|         | ,       | 551                   |      |                |
| 1       | 013     | 0560                  | 1045 | 0560           |
| 2       | 056     | 0000                  | 0560 | 0000           |
| 3       | 001     | 6026                  | 1030 | 6034           |
|         | 1       | 0554 A                |      |                |
| 0554    | 002     | 6026                  | 1030 | 6035           |
| 5       | 001     | 6027                  | 1030 | 6036           |
| 6       | 002     | 6027                  | 1030 | 6037           |
| 7       | 075     | 0                     | 0    | 6040           |
| 0560    | 077     | 0                     | 0    | 0              |
| 1       | 077     | 0                     | 0    | 0              |
| 2       | 002     | 6034                  | 6032 | . 0            |
| 3       | 076     | 0                     | 0565 | 0              |
| 4       | 056     | 0                     | 0624 | 0              |
| 5       | 002     | 6032                  | 6035 | 0              |
| 6       | 076     | 0                     | 0570 | 0              |
|         |         | 0567 A                | -    |                |
| 0567    | 056     | 0                     | 0624 | 0              |
| 0570    | 002     | 6036                  | 6033 | 0              |
| 1       | 076     | 0                     | 0573 | 0              |
| 2       | 056     | 0                     | 0624 | 0              |
| 3       | 002     | 6033                  | 6037 | 0              |
| 4       | 076     | 0                     | 0576 | 0              |
| 5       | 056     | 0                     | 0624 | 0              |
| 6       | 077     | 0                     | 0    | 0              |
| 7       | 001     | 6040                  | 0101 | 6040           |
| 0600    | 0       | 0                     | 0    | 0              |
| 1       | 0       | 0                     | 0    | 0              |
|         |         | 0602 A                |      |                |
| 0602    | 075     | 0                     | 1040 | 6041           |
| 3       | 056     | 0604                  | 0605 | 0620           |
| 4       | 077     | 0                     | 0    | 0              |
| 5       | 056     | 0606                  | 0607 | 0621           |
| 6       | 077     | 0                     | 0    | 0              |
| 7       | 056     | 0610                  | 0613 | 0613           |
| 0610    | 075     | 0                     | 1000 | 6030           |
| 1       | 013     | 0620                  | 0772 | 0620           |
| 2       | 013     | 0613                  | 0772 | 0613           |
| 3       | 077     | 0                     | 0    | 0              |
| 4       | 002     | 6030                  | 6031 | 0              |
|         |         | 0615 A                |      |                |
| 0615    | 076     | 0                     | 0620 | 0              |
| 6       | 002     | 6041                  | 0101 | 6041           |
| 7       | 076     | 0                     | 0611 | 0              |
| 0620    | 077     | 0                     | 0    | 0              |
| 1       | 077     | 0                     | 0    | Õ              |
| 2       | 013     | 0604                  | 0773 | 0604           |

| Address | Command |        | A2           | A <sub>3</sub> |
|---------|---------|--------|--------------|----------------|
| 3       | 013     | 0606   | 0773         | 0606           |
| 4       | 112     | 0      | 0547         | 0001           |
| 5       | 075     | 0      | 6040         | 6056           |
| 6       | 0       | 0      | 0            | 0              |
| 7       | 075     | 0      | 1037         | 6057           |
|         |         | 0630 A |              |                |
| 0630    | 077     | 0      | 0            | 0              |
| 1 .     | 002     | 6040   | 1031         | 0              |
| 2       | 076     | 0      | 0640         | 0              |
| 3       | 002     | 6040   | 0101         | 0              |
| 4       | 076     | 0      | 0637         | 0              |
| 5       | 075     | 0      | 0            | 6054           |
| 6       | 056     | 0      | 0723         | 0              |
| 7       | 0       | 0      | 0            | 0              |
| 0640    | 075     | 0      | 1011         | 6044           |
| 1       | 002     | 6040   | 1033         | 6043           |
| 2       | 075     | 0      | 1025         | 6045           |
|         |         | 0643 A |              |                |
| 0643    | 075     | 0      | 0            | 6046           |
| 4       | 056     | 0645   | 0647         | 0647           |
| 5       | 004     | 6045   | 6113         | 6050           |
| 6       | 013     | 0647   | 0772         | 0647           |
| 7       | 077     | 0      | 0            | 0              |
| 0650    | 001     | 6046   | 6050         | 6046           |
| 0651    | 002     | 6043   | 0101         | 6043           |
| 2       | 076     | 0      | 0646         | 0              |
| 3       | 075     | 0      | 6046         | 6056           |
| 4       | 075     | õ      | 1035         | 0140           |
| 5       | 016     | 0656   | 7714         | 0007           |
| -       |         | 0656 A |              |                |
| 0656    | 075     | 0      | 0160         | 6047           |
| 7       | 075     | 0      | 0101         | 6050           |
| 0660    | 075     | 0      | 1034         | 6051           |
| 1       | 005     | 6051   | 6047         | 0140           |
| 662     | 016     | 0663   | 7711         | 0007           |
| 3       | 002     | 6050   | 0160         | 6050           |
| 4       | 075     | 0      | 6044         | 6052           |
| 5       | 002     | 6052   | 012          | 6052           |
| 6       | 005     | 6051   | 6052         | 6052           |
| 7       | 005     | 6052   | 6047         | 0140           |
| 0670    | 016     | 0671   | <b>771</b> 1 | 0007           |
|         |         | 0671 A |              |                |
| 0671    | 075     | 0      | 0160         | 6052           |
| 2       | 005     | 6046   | 6050         | 6050           |
| 3       | 004     | 6050   | 6052         | 6050           |
| 4       | 005     | 6050   | 1036         | 6050           |
|         |         |        |              | (Court d)      |

| Address | Command | A1     | . A <sub>2</sub> | A3   |
|---------|---------|--------|------------------|------|
| 5       | 005     | 6057   | 1025             | 6051 |
| 6       | 004     | 6050   | 6051             | 6054 |
| 0677    | 044     | 6046   | 0                | 6050 |
| 0700    | 004     | 1036   | 1035             | 6051 |
| 1       | 004     | 6051   | 6050             | 6055 |
| 2       | 056     | 0      | 0724             | 0    |
| 3       | 075     | 0      | 6051             | 6055 |
|         |         | 0704 A |                  |      |
| 0704    | 001     | 6053   | 0101             | 6053 |
| 5       | 016     | 0707   | 7751             | 0007 |
| 6       | 000     | 6053   | 4000             | 6056 |
| 7       | 075     | 0      | 6034             | 6026 |
| 0710    | 112     | 0000   | 0533             | 0001 |
| 1       | 077     | 0      | 0                | 0    |
| 2       | 075     | 0      | 1026             | 6026 |
| 3       | 075     | 0      | 6036             | 6027 |
| 4       | 112     | 0000   | 0531             | 0001 |
| 5       | 077     | 0      | 0                | 0    |
|         |         | 0770 A |                  |      |
| 0770    | 777     | 0      | 7777             | 7777 |
| 1       | 777     | 7777   | 7777             | 0    |
| 2       | 0       | 0      | 0001             | 0    |
| 3       | 0       | . 0    | 0                | 0001 |

coordinates of its epicenter, latitude  $\varphi_i$  and longitude  $\lambda_i$  in degrees, and the energy class  $K_i$ .

The second data set of the constants  $M_2$  includes coordinates of the initial point of computation— $\varphi_0$ ,  $\lambda_0$ , computation step latitudinally— $a_{\varphi_i}$  and longitudinally— $a_{\lambda_i}$ , area of the averaging zone  $S = 2a_{\varphi_i} \times 2a_{\lambda_i}$ , the value of the inclination of the repeatability curve  $\gamma$ , and the establishment period of earthquakes of class  $K_{\min}$ —7. Besides, included here are the number of lines m and columns n of the initial matrix, the corresponding numbers q and r of the resulting matrix (maps of activity of the region under investigation), a set of fixed classes of energies  $K_{f_i}$  (about which A is computed) and their corresponding periods of presentation  $T_{f_j}$ ; and the number P of these classes (here and further  $j = 1, 2, \ldots p$ ). In the set  $K_{f_j}$  are included the classes of energies presented by the earthquakes of the region, beginning from  $K_{\min}$ —least of them, therefore,  $K_{f_1} = K_{\min}$ ;  $K_{f_2} = K_{\min} + 1$ ;  $K_{f_3} = K_{\min} + 2 \ldots$ ;  $K_{f_p} = K_{\min} + (P-1)$ .

The SP-1 program occupies memory cells 0500-0773; the data sets of constant and informational lines—1000-1045; the initial data sets of epicenters are in the machine memory from cell 1100. The remaining memory cells are operational and contain the intermediate results.

The SP-1 program moves in accordance with the block diagram and begins with loading the actual program and data sets of initial data in the machine. The control is in block 1, where the command address is given depending on the information. In block 2, data sets  $M_1$  and  $M_2$  are converted from the decimal system to the binary. Here the printer lists data sets  $M_1$  and  $M_2$  to control the numerical information entered in the machine. Further control is on blocks 3 and 4 to load the instruction addresses necessary for successive blocks, and further to block 5.

Block 5 contains the choice of epicenters with the coordinates of averaging zones—the coordinates  $\varphi_i$ ,  $\lambda_i$  of all epicenters of the first data sets  $M_1$ are sorted and only those falling within the limits of this zone are retained. For example, for the beginning point of the computation with coordinates  $\varphi_0$ ,  $\lambda_0$  these limits are limited by the lat.  $\varphi_0 \pm a_x$  and long.  $\lambda_0 \pm a_\lambda$ . The choice of each epicenter in the averaging zone is fixed by a special counter. The energy class  $K_i$ , corresponding to each chosen epicenter, is transferred to block 7, i.e., identification K, where it is determined by comparing with  $K_{f_i}$  stored in the memory. The transfer of control from block 5 to 7 takes place through block 6 where the instruction addresses of block 7 are loaded. Thereafter control is transferred to block 8, where the instruction addresses for block 9 are loaded, and further to block 9. Here for the energy class  $K_i$  of each epicenter in the averaging zone a corresponding presentation period  $T_{\rm fr}$  is chosen, which is necessary during unequal observation periods of earthquakes of various energy classes. Further, the number of earthquakes of various energy classes in the averaging zone are brought to the presentation period T of earthquakes of class K, and the control is transferred to block 10, where the total number  $N_{\Sigma}$  of earthquakes in the averaging zone is computed according to the expression:

$$N_{\mathcal{E}} = \sum_{j=1}^{l} \frac{T_{\min}}{T_{f_j}},$$
 (38)

where *l*—number of epicenters in the averaging zones.

Here, the numbers  $N_E$  are compared with the given  $N_{\sigma}$ , determining the number of epicenters in the averaging zones, necessary to calculate seismic activity with the desired accuracy. When  $N_E \ge N_{\sigma}$  the control is transferred to block 11 to compute seismic activity A and error  $\sigma_A$  in the averaging zone. The computation of A is carried out according to formula (37). The quantity  $\sigma_A$  is inversely proportional to the square-root of the number of earthquake epicenters of various energy classes in the averaging zone, brought to one observation period T. It is computed according to the following formula (Riznichenko, ed., 1960).

$$\sigma_A = \frac{100}{\sqrt{N_E}} \%. \tag{39}$$

If, as a result of the work in block 10 it appears that  $N_E \le N_{\sigma}$ , the control is transferred directly to printing block 12, bypassing 11. In this case, A = 0. As a result of the work in block 12, the point number and the values A and  $\sigma_A$  (%) are printed.

After printing the results of computation A for the first point of the activity map (the first averaging zone) control is transferred to block 13—preparation for computation at the next point. Here crossing to the next averaging zone of activity is achieved with step a, if the point number  $N_T < qr$ . If  $N_T = qr$  the computation stops.

Application of the above-described program to compute seismic activity maps considerably saves time. The automatic computation of value A according to formula (37) requires much less time than the manual method. Besides, here constructing the epicenter map is excluded, since for machine computation lists of epicenters are sufficient initial material. Using the SP-1 program a seismic activity map of a thousand points can be computed in 40 min. During this time the initial epicenter list enumerates these points not less than 500 times.

One more important feature is automatically done when computing the seismic activity map using the SP-1 program. Determining the computation errors  $A-\sigma_A$ , considered in the program, permits accurate computations for each point, separately for its section and for the map as a whole. It is necessary to compare these maps with the tectonics of the territory under investigation to compute the more complex quantitative evaluations of seismic danger—seismic shock maps.

#### **Illustrative Example**

The SP-1 program is standard and remains unchanged for any region. Only the contents of the initial data  $M_1$  and  $M_2$  sets and the control information may change. In this illustrative example, which may be used as a concurrent version of the program to verify that it works, the form to record initial data on standard blanks is shown, as well as the results of seismic activity computation using SP-1.

The set of epicenters  $M_1$  (Table 1) holds the data of seven earthquakes and is recorded in decimal code along triads, beginning from cell 1100. The characteristic of each earthquake uses three cells: in the first the energy class K is placed, in the second—latitude  $\varphi$ , and in the third the longitude  $\lambda$  of epicenter in degrees.

The data set of the constant  $M_2$  (Table 2) is placed in cells 1000-1041.

The control information lines (Table 3) is written in octal code along

note-books, beginning from cell 1042 to 1046, and holds the following data: line number of matrix  $A_{mn}$  less one (m-1); number of columns of this matrix (n); corresponding numbers for the resulting matrix  $A_{qr}(q-1)$  and (r-1); address of the last cell of the data set  $M_1(A_{mn})$ .

Further the results of computing the seismic activity of two columns of the map are placed by SP-1 for the initial data sets  $M_1$  and  $M_2$  and groups of control information (Tables 1-3) are placed (Table 4).  $N_T$ —serial number of the map point;  $A_{10}$ —value of the seismic activity about  $K_0 = 10$ ;  $\sigma_A$ —error of the computation  $A_{10}$  (%); *n*—number of epicenters in the averaging zone.

The placement of the epicenters relative to the computation points  $A_{10}$  conditions the value  $A_{10} > 0$  only at four points: 1, 2, 10 and 11. At the remaining points  $A_{10} = 0$  and  $\sigma_A = 100\%$ , since either  $N_E < N_\sigma$ , or n = 0 at those points.

|         |     |                  | Commands | and numb | er   |     | ·                     |
|---------|-----|------------------|----------|----------|------|-----|-----------------------|
| Address | Sig | n of             | Order    | A1       | A2   | A3  | Remarks               |
|         | No. | Order            |          |          |      |     |                       |
|         |     |                  | 1100     | A        |      |     |                       |
| 1100    | ++  | +                | 02       | 130      | 000  | 000 | $K_1 = 13$            |
| 1       | ++  | +                | 02       | 400      | 100  | 000 | $p_1 = 40.01$         |
| 2       | ++  | +                | 02       | 700      | 100  | 000 | $\lambda_1 = 70.01$   |
| 3       | ++  | +                | 02       | 130      | 000  | 000 | $K_2 = 13$            |
| 4       | ++  | +-               | 02       | 401      | 100  | 000 | $\varphi_2 = 40.11$   |
| 5       | ++  | - <del>1</del> - | 02       | 700      | 100  | 000 | $\lambda_2 = 70.01$   |
| 6       | ++  | +                | 02       | 100      | 000  | 000 | $K_3 = 10$            |
| 7       | ++  |                  | 02       | 401      | 500  | 000 | $\varphi_3 = 40.15$   |
| 1110    | ++  | +                | 02       | 702      | 1000 | 000 | $\lambda_3 = 70.21$   |
| 1       | ++  | +                | 02       | 110      | 000  | 000 | $K_4 = 11$            |
| 2       | ++  | +                | 02       | 402      | 120  | 000 | $\varphi_4 = 40.21$   |
|         |     |                  | 1113     | Α        |      |     |                       |
| 1113    | ++  | +                | 02       | 701      | 800  | 000 | $\lambda_4 = 70.18$   |
| 4       | ++  | +                | 02       | 120      | 000  | 000 | $K_{5} = 12$          |
| 5       | ++  | +                | 02       | 400      | 500  | 000 | $\varphi_{5} = 40.05$ |
| 6       | ++  | +                | 02       | 701      | 200  | 000 | $\lambda_{5} = 70.12$ |
| 7       | ++  | +                | 02       | 100      | 000  | 000 | $K_{6} = 10$          |
| 1120    | ++  | +                | 02       | 401      | 100  | 000 | $\varphi_6 = 40.11$   |
| 1       | ++  | +                | 02       | 698      | 100  | 000 | $\lambda_6 = 69.81$   |
| 2       | ++  |                  | 02       | 120      | 000  | 000 | $K_7 = 12$            |
| 3       | ++  | +                | 02       | 401      | 100  | 000 | $\varphi_2 = 40.11$   |
| 4       | ++  | +                | 02       | 701      | 100  | 000 | $\lambda_7 = 70.11$   |

TABLE 1. DATA SET M<sub>1</sub> FOR SP-1

| Address | Sig                       | n of         | Order | A1  | A <sub>2</sub> | A <sub>3</sub>        | Remarks              |
|---------|---------------------------|--------------|-------|-----|----------------|-----------------------|----------------------|
|         | No.                       | Order        |       |     |                |                       |                      |
|         |                           |              | 1000  | A   |                | · · · · · · · · · · · |                      |
| 1000    | ++                        | - -          | . 02  | 100 | 000            | 000                   | $K_{f_1} = 10$       |
| 1       | ++                        | -1.          | 02    | 110 | 000            | 000                   | $K_{f_1} = 11$       |
| 2       | ++                        | <b> </b> ·   | 02    | 120 | 000            | 000                   | $K_{t_3} = 12$       |
| 3       | -+ -+-                    |              | 02    | 130 | 000            | 000                   | $K_{f_4} = 13$       |
| 4       |                           | +            | 00    | 000 | 000            | 000                   | -                    |
| 5       | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 6       | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 7       | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 1110    | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 1       | ++                        | +            | 02    | 100 | 000            | 000                   | $K_{\rm rep} = 10$   |
| 2       | -+· <b>-</b> +-           | +            | 02    | 100 | 000            | 000                   | $K_0 = 10$           |
|         |                           |              | 1013  | A   |                |                       |                      |
| 1013    | ++                        | +            | 02    | 160 | 000            | 000                   | $T_{t_1} = 16$       |
| . 4     | - <u>+</u> - + <u>+</u> - | +            | 02    | 160 | 000            | 000                   | $T_{f_0} = 16$       |
| 5       | ++                        | +            | 02    | 160 | 000            | 000                   | $T_{f_0}^2 = 16$     |
| 6       | ++                        | +            | 02    | 380 | 000            | 000                   | $T_{f} = 38$         |
| 7.      | ++                        | +            | 00    | 000 | 000            | 000                   | -4                   |
| 1020    | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 1       | ++                        | -}-          | 00    | 000 | 000            | 000                   |                      |
| 2       | ++                        | +            | 00    | 000 | 000            | 000                   |                      |
| 3       | ++                        | -  -         | 00    | 000 | 000            | 000                   |                      |
| 4       | -+                        | +            | 00    | 000 | 000            | 000                   |                      |
| 5       | ++                        | +            | 02    | 160 | 000            | 000                   | $T_{rep}=16$         |
|         |                           | ·            | 1026  | A   |                |                       |                      |
| 1026    | ++                        | +            | 02    | 401 | 000            | 000                   | $\varphi_0 = 40.1$   |
| 7       | ++                        | +            | 02    | 701 | 000            | 000                   | $\lambda_0 = 70.1$   |
| 1030    |                           | +            | 00    | 100 | 000            | 000                   | Q = 0.1              |
| 1       | ++                        | -+-          | 01    | 300 | 000            | 000                   | $N_6 = 3$            |
| 2       | ++                        | +            | 01    | 150 | 000            | 000                   | const = 1.5          |
| 3       | ++                        |              | 00    | 500 | 000            | 000                   | const = 0.5          |
| 4       | ++                        | +-           | 00    | 430 | 000            | 000                   | $\gamma = 0.43$      |
| 5       | ++                        | -+-          | 02    | 100 | 000            | 000                   | const = 10           |
| 6       | ++                        | +            | 04    | 100 | 000            | 000                   | S <sub>0</sub> =1000 |
| 7       | ·                         | -+-          | 03    | 352 | 000            | 000                   | S=352                |
| 1010    | - <del>-</del>            | - <b>-</b> - | 01    | 350 | 000            | 000                   | P = 0.5 = 3.         |

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BLOCK DIAGRAM OF PROGRAM SP-1

BLOCK DIAGRAM OF PROGRAM SP-2



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|         | Cc      |                |                |      |                  |
|---------|---------|----------------|----------------|------|------------------|
| Address | Command | A <sub>1</sub> | $\mathbf{A}_2$ | A3   | Remarks          |
|         |         | 1042 A         |                |      |                  |
| 1042    | 000     | 0006           | 0000           | 0000 | (m-1, 0, 0)      |
| 3       | 000     | 0010           | 0000           | 0000 | (q-1, 0, 0)      |
| 4       | 000     | 0010           | 0000           | 0000 | (r-1, 0, 0)      |
| 5       | 000     | 0000           | 0003           | 0000 | (0, n, 0)        |
| 6       | 000     | 0000           | 0000           | 1124 | $(0, 0, A_{mn})$ |

TABLE 3. CONTROL INFORMATION FOR SP-1

Different values of  $A_{10}$  at points 2, 10, and 11 with an identical number n of epicenters in the averaging zones is explained thus: earthquakes, corresponding to these epicenters, differ in energy class K and, therefore, in the presentation period T. As a result, different numbers  $N_{\Sigma}$  in the averaging zone and different values of  $A_{10}$  are obtained in accordance with expressions (37) and (38).

#### PROGRAM SP-2 OF THE COMPUTATION OF A MAPS WITH CONSTANT ACCURACY BY THE SUMMATION METHOD

In the SP-2 program, the value of seismic activity at each point of the resulting map is computed by averaging around the circular varying area zone (Zakharova, 1971) unlike SP-1, where it was trapezoidal. In this the area of the averaging zone of activity A was left unchanged, which, with the usual heterogeneous distribution of epicenters, leads to unequal accuracy in computing A at various map points. A different number of epicenters fall on area S whereas the error of computing seismic activity  $\sigma_A$ , according to (39), is inversely proportional to the sum of epicenters  $N_E$  in the averaging zone.

While studying the seismic region it is often important to get a seismic activity map with uniform accuracy of all values of A (Riznichenko, Gorbunova, 1968).

The method of computing the map of seismic activity A with uniform accuracy (Gorbunova, 1964) suggests of an equal number of earthquake epicenters  $N_{\Sigma}$  at each averaging zone A. The number  $N_{\Sigma}$  represents a certain error  $\sigma_A$  of the computation of A according to (39). Then, after calculating the seismic activity A according to formula (37) by the earthquake summation method (Riznichenko, 1964a), one may compute the number of epicenters  $N_{\sigma}$  according to (39) and search it around each point, given the certain error  $\sigma_A$ . The larger the area S to contain  $N_{\sigma}$ , the lesser the level of seismic activity A.

# TABLE 4. RESULTS OF COMPUTATION OF $A_{10}$ ACCORDING TO SP-1

| N <sub>T</sub>     | A <sub>10</sub>                       | ° <sub>A</sub> %   | · 11                                  |
|--------------------|---------------------------------------|--------------------|---------------------------------------|
| +++ 01 10000000    | ++- 00 372117298                      | +++ 02 593171014   | +++ 01 40000000                       |
| +++ 01 20000000    | ++-00316988809                        | +++ 02 642684586   | +++ 01 30000000                       |
| +++ 01 30000000    | $+++00\ 000000000$                    | +++ 03 100000000   | +++ 01 10000000                       |
| +++ 01 40000000    | $+++00\ 000000000$                    | $+++03\ 100000000$ | $+++00\ 000000000$                    |
| +++ 01 50000000    | +++0000000000000000000000000000000000 | +++ 03 10000000    | $+++00\ 000000000$                    |
| +++ 01 60000000    | $+++00\ 000000000$                    | +++ 03 10000000    | +++ 00 00000000                       |
| +++ 01 70000000    | +++ 00 00000000                       | +++03100000000     | +++0000000000000000000000000000000000 |
| +++ 01 80000000    | $+++00\ 000000000$                    | +++ 03 100000000   | +++00000000000                        |
| +++01 900000000    | $+++00\ 000000000$                    | +++ 03 10000000    | +++ 00 00000000                       |
| +++ 02 10000000    | ++- 00 392790481                      | +++02577350269     | +++ 01 30000000                       |
| +++ 02 110000000   | ++- 00 392790481                      | +++02577350269     | +++ 01 30000000                       |
| +++ 02 120000000   | +++ 00 00000000                       | $+++03\ 100000000$ | $+++01\ 10000000$                     |
| $+++02\ 130000000$ | +++ 00 000000000                      | +++ 03 10000000    | $+++00\ 000000000$                    |
| +++02 140000000    | $+++00\ 000000000$                    | +++ 03 100000000   | +++0000000000                         |
| +++02 150000000    | +++0000000000000000000000000000000000 | +++ 03 10000000    | $+++00\ 000000000$                    |
| $+++02\ 160000000$ | +++ 00 00000000                       | +++ 03 10000000    | +++ 00 00000000                       |
| +++ 02 170000000   | $+++00\ 000000000$                    | +++ 03 100000000   | +++ 00 00000000                       |
| ++++ 02 180000000  | +++ 00 00000000                       | +++ 03 100000000   | $+++00\ 000000000$                    |

PROGRAM SP-2

| Address | Command | A <sub>1</sub> | A <sub>2</sub> | A3   |
|---------|---------|----------------|----------------|------|
|         |         | 0500 A         |                |      |
| 0500    | 055     | 0545           | 0770           | 0545 |
| 1       | 013     | 0545           | 1051           | 0545 |
| 2       | 055     | 0665           | 0770           | 0665 |
| 3       | 013     | 0665           | 1051           | 0665 |
| 4       | 055     | 0633           | 0770           | 0633 |
| 5       | 013     | 0633           | 1052           | 0633 |
| 6       | 055     | 0615           | 0770           | 0615 |
| 7       | 013     | 0615           | 1051           | 0615 |
| 0510    | 055     | 0730           | 0770           | 0730 |
| 1       | 013     | 0730           | 1043           | 0730 |
| 2       | 055     | 0734           | 0770           | 0734 |
|         |         | 0513 A         |                |      |
| 0513    | 013     | 0734           | 1044           | 0734 |
| 4       | 055     | 0520           | 0774           | 0520 |
| 5       | 013     | 0520           | 1041           | 0520 |
| 6       | 000     | 0000           | 0000           | 0000 |
| 7       | 016     | 0521           | 7741           | 0007 |
| 0520    | 000     | 1100           | 1100           | 0000 |
| 1       | 016     | 0523           | 7741           | 0007 |
| 2       | 000     | 1000           | 1000           | 1040 |
| 3       | 016     | 0525           | 7741           | 0007 |
| 4       | . 000   | 1054           | 1054           | 1066 |
| 5       | 056     | 0000           | 0656           | 0000 |
|         |         | 0526 A         |                |      |
| 0526    | 052     | 0000           | 0000           | 0000 |
| 7       | 275     | 0000           | 1100           | 6031 |
| 0530    | 056     | 0531           | 0532           | 0535 |
| 1       | 002     | 1000           | 6031           | 0000 |
| 2 .     | 056     | 0533           | 0534           | 0543 |
| 3       | 075     | 0000           | 1013           | 6045 |
| 4       | 075     | 0000           | 1040           | 6041 |
| 5       | 077     | 0000           | 0000           | 0000 |
| 6       | 076     | 0000           | 0543           | 0000 |
| 7       | 013     | 0535           | 0771           | 0535 |
| 0540    | 013     | 0543           | 0772           | 0543 |
|         |         | 0541 A         | ·              |      |
| 0541    | 002     | 6041           | 0101           | 6041 |
| 2       | 076     | 0000           | 0535           | 0000 |
| 3       | 017     | 0000           | 0000           | 0000 |
| 4       | 104     | 1025           | 6045           | 1100 |
| 5       | 112     | 0000           | 0527           | 0003 |
| 6       | 052     | 0000           | 0000           | 0000 |
| 7       | 075     | 0000           | 1027           | 6027 |
| 0550    | 075     | 0000           | 1026           | 6026 |
| 1       | 452     | 0000           | 0000           | 0731 |
|         |         |                |                |      |

(Contd.)

| - |       |     | A1             | A2   | A3           |
|---|-------|-----|----------------|------|--------------|
|   |       |     | 0552 A         |      |              |
|   | 2     | 452 | 0000           | 0000 | 0654         |
|   | 3     | 004 | 6026           | 6070 | 6032         |
|   | -     |     | 0554 A         |      |              |
|   | 0554  | 004 | 6027           | 6070 | 6022         |
|   | 0,554 | 004 | 0556           | 0557 | 0033         |
|   | 5     | 050 | 1065           | 6050 | 4550         |
|   | 07    | 005 | 1005           | 6032 | . 4550       |
|   | 0560  | 015 | 0561           | 7712 | 0140         |
|   | 1     | 075 | 0000           | 0161 | 6067         |
|   | 1     | 075 | 0000           | 0160 | 6061         |
|   | 2     | 075 | 0000           | 6022 | 0140         |
|   | 3     | 015 | 0565           | 7712 | 0140         |
|   | 4     | 075 | 0000           | 0161 | 6067         |
|   | 6     | 075 | 0000           | 0160 | 6063         |
|   | , U   | 075 | 0500           | 0100 | 000.         |
|   |       |     | 0567 A         |      |              |
|   | 0567  | 275 | 0000           | 1101 | 014(         |
|   | 0570  | 016 | 0571           | 7712 | 0007         |
|   | 1     | 075 | 0000           | 0161 | <b>60</b> 64 |
|   | - 2   | 075 | 0000           | 0160 | 6065         |
|   | 3     | 275 | 0000           | 1102 | 0140         |
|   | 4     | 016 | 0575           | 7712 | 0007         |
|   | 5     | 075 | 0000           | 0161 | 6066         |
|   | 6     | 075 | 0000           | 0160 | 6063         |
|   | 7     | 005 | 6060           | 6064 | 6050         |
|   | 0600  | 005 | 6061           | 6063 | 6051         |
|   | 1     | 005 | 6051           | 6065 | 6051         |
|   |       |     | 0602 A         |      |              |
|   | 0602  | 005 | 6051           | 6067 | 6051         |
|   | 3     | 001 | 6050           | 6051 | 6050         |
|   | 4     | 005 | 6061           | 6062 | 6051         |
|   | 5     | 005 | 6051           | 6065 | 6051         |
|   | 6     | 005 | 6051           | 6066 | 6051         |
|   | 7     | 001 | 6050           | 6051 | 6050         |
|   | 0610  | 075 | 0000           | 6050 | 0140         |
|   | · 1   | 016 | 0612           | 7716 | 0007         |
|   | 2     | 005 | 0160           | 6070 | 6050         |
|   | 3     | 017 | 0000           | 0000 | 0000         |
|   | 4     | 013 | 0613           | 0773 | 0613         |
|   |       |     | 061 <b>5</b> A |      |              |
|   | 0615  | 112 | 0000           | 0567 | 0003         |
|   | 6     | 075 | 0000           | 0000 | 6017         |
|   | 7     | 075 | 0000           | 0000 | 6046         |
|   | 0620  | 052 | 0000           | 0000 | 0000         |
|   |       |     | 0621 A         |      |              |
|   | 1     | 075 | 0000           | 0000 | 6072         |
|   | · ·   |     | 2000           |      | 0074         |

| Address | Command | A1     | A <sub>2</sub> | A3   |
|---------|---------|--------|----------------|------|
| 2       | 075     | 0000   | 0000           | 6073 |
| 3       | 075     | 0000   | 4550           | 6074 |
| 4       | 013     | 6072   | 1045           | 6072 |
| 5       | 013     | 6073   | 0773           | 6073 |
| 6       | 402     | 4551   | 6074           | 0000 |
| 7       | 076     | 0000   | 0633           | 0000 |
|         | 0.0     | 0630 A | 0000           |      |
| 0630    | 075     | 0000   | 6072           | 6075 |
| 1       | 075     | 0000   | 6072           | 6076 |
| ,<br>,  | 075     | 0000   | 4551           | 6070 |
| 2       | 273     | 0000   | 4.531          | 0074 |
| 3       | 112     | 0000   | 0624           | 0001 |
| 4       | 050     | 0035   | 0030           | 0643 |
| 5       | 001     | 6046   | 1100           | 6040 |
| 0       | 056     | 0637   | 0640           | 0644 |
| 1       | 075     | 0000   | 1036           | 4550 |
| 0640    | 075     | 0000   | 6074           | 6057 |
| 1       | 013     | 0643   | 6075           | 0643 |
| 2       | 013     | 0644   | 6076           | 0644 |
|         |         | 0643 A |                |      |
| 0643    | 077     | 0000   | 0000           | 0000 |
| 4       | 077     | 0000   | 0000           | 0000 |
| 5       | 001     | 6077   | 0101           | 6072 |
| 6       | 002     | 6077   | 1066           | 0000 |
| 7       | 036     | 0000   | 0620           | 0000 |
| 0650    | 005     | 6057   | 6057           | 6050 |
| 1       | 005     | 6050   | 1064           | 605  |
| 2       | 075     | 0000   | 6046           | 605  |
| 3       | 075     | 0000   | 1011           | 6044 |
| 4       | 077     | 0000   | 0000           | 0000 |
| 5       | 056     | 0000   | 0671           | 0000 |
|         |         | 0656 A |                |      |
| 0656    | 0000    | 0000   | 0000           | 0000 |
| 7       | 0000    | 0000   | 0000           | 000  |
| 0660    | 0000    | 0000   | 0000           | 000  |
| 1       | 004     | 1062   | 1063           | 607  |
| 2       | 052     | 0000   | 0000           | 000  |
| 3       | 504     | 1101   | 6070           | 110  |
| 4       | 504     | 1102   | 6070           | 110  |
| 5       | 112     | 0000   | 0663           | 000  |
| 6       | 0000    | 0000   | 0000           | 000  |
| 7       | 075     | 0000   | 0000           | 605  |
| 0670    | 056     | 0000   | 0526           | 000  |
|         |         | 0671 A | •              |      |
| 0671    | 0000    | 0000   | 0000           | 000  |
| 001 K   | 0000    | 0000   | 0000           | 000  |
| 2       | 0000    | 0000   | ~~~~           |      |

| Address   | Command | A <sub>1</sub> | $A_2$        | A <sub>3</sub> |
|-----------|---------|----------------|--------------|----------------|
| 3         | 0000    | 0000           | 0000         | 0000           |
|           |         | 0674 A         |              |                |
| 4         | 075     | 0000           | 1035         | 0140           |
| 5         | 016     | 0676           | 7714         | 0007           |
| 6         | 075     | 0000           | 0160         | 6047           |
| 7         | 075     | 0000           | 0101         | 6050           |
| 0700      | 075     | 0000           | 1034         | 6051           |
| 1         | 005     | 6051           | 6047         | 0140           |
| 2         | 016     | 0703           | 7711         | 0007           |
| 3         | 002     | 6050           | 0160         | 6 <b>05</b> 0  |
|           |         | ° 0704 A       |              |                |
| 0704      | 075     | 0000           | 6044         | 6052           |
| 5         | 002     | 6052           | 1012         | 6052           |
| 5         | 005     | 6051           | 6052         | 6052           |
| Ť         | 005     | 6052           | 6047         | 0140           |
| 0710      | 016     | 0711           | 7711         | 0007           |
| 1         | 075     | 0000           | 0160         | 6052           |
| $\hat{2}$ | 005     | 6046           | 6050         | 6050           |
| 3         | 004     | 6050           | 6052         | 6050           |
| 4         | 005     | 6050           | 1036         | 6050           |
| 5         | 005     | 6057           | 1025         | 6051           |
| 6         | 004     | 6050           | 6051         | 6054           |
|           | 001     | 0717 A         |              |                |
| 0717      | 044     | 6046           | 0000         | 6050           |
| 072()     | 004     | 1036           | 1035         | 6051           |
| 1         | 004     | 6051           | 6050         | 6055           |
| 2         | 000     | 0000           | 0000         | 0000           |
| - 3       | 000     | 0000           | 0000         | 0000           |
| 4         | 000     | 6053           | 0101         | 6053           |
| 5         | 016     | 0727           | 7751         | 0007           |
| 6         | 000     | 6053           | 4000         | 6056           |
| 7         | 001     | 6026           | 1030         | 6026           |
| 0730      | 112     | 0000           | 0552         | 0001           |
| 1         | 077     | 0000           | 0000         | 0000           |
|           | 011     | 0732 A         |              |                |
| 0732      | 075     | 0000           | 1026         | 6026           |
| 3         | 001     | 6027           | 1020         | 6020           |
| 3         | 112     | 0027           | 0551         | 0001           |
|           | 077     | 0000           | 0000         | 0000           |
|           | 077     | 0770 A         | 0000         | 0000           |
| 0770      | 777     | 0000           | 7777         | 7777           |
| 1         | 000     | 0000           | 0000         | 0000           |
| 1         | 000     | 0001           | 0000         | 0000           |
| 2         | 000     | 0000           | 0001         | 0000           |
| Э<br>А    | 777     | 0000<br>7777   | 0000<br>7777 | 0001           |
| 4         |         |                |              |                |

To compile map A by the uniform accuracy method, the averaging zone S is usually considered circular. Therefore,  $S = \pi r^2$  where r is the radius of the averaging zone.

In the SP-2 program, two sets of data are used as initial material. The first,  $M_1$ , as in SP-1, is given by the matrix  $A_{mn}$ , the number of lines *m* for which equals the number of epicenters of represented earthquakes in the region under investigation; whereas, the number of columns *n* is the number of parameters of each epicenter. When computing map *A* for the earth's surface, these parameters would be as follows: the coordinates of earthquake epicenters  $\varphi$  and  $\lambda$  in degrees and its energy class  $K_i$ . The second set of initial data  $M_2$  includes the seismic regime characteristics of the region under investigation according to (37),  $\gamma$ ,  $K_{\min}$ ,  $K_0$ ,  $T_{\min}$ , set of fixed classes of energy  $K_{l_j}$ , and their periods of presentation  $T_{r_j}$ , the computation interval —latitudinally— $a_{\varphi}$  and longitudinally— $a_{\lambda}$ , the number of lines *m* and columns *n* of initial matrices, and the corresponding numbers *q* and *r* of the resulting matrices (the product  $q \cdot r$  gives the number of points of the activity map).

Unlike the data sets of parameters  $M_2$  for the SP-1 program, the area of the averaging zone is not given, but rather the number of epicenters in it— $N_{\sigma}$ . While using the program for each point of the map beginning from the first, the coordinates of which  $\varphi_0$ ,  $\lambda_0$  are also fixed in the data sets  $M_2$ , the epicenter  $N_{\sigma}$  is found. The distance to the farthest epicenter of the number  $N_{\sigma}$  is taken as the radius r of the averaging zone of activity. Besides, constants are added to data sets  $M_2$  which are necessary to convert the scale from degrees to radians: size of the surrounding area in degrees, number  $2\pi$  and  $\pi$ ; to change radians into kilometers, while measuring the epicentral distances— $\hat{r} = 111.199$ ; and the value  $\Delta_{\max} = 1,000$  km. The SP-2 program is stored in cells 0500-0735 of MOZV, constants  $M_2$  set and control information engage cells 0770-1066, initial set  $M_1$  of the epicenters is written in the memory, from cell 1100. The remaining MOZV cells are used for the working area in which the intermediate results are written.

#### Block Diagram SP-2 (see p. 50)

SP-2 flows in a block diagram and begins with entering the actual program and the data sets of initial data into the machine. After control is given to block 1 the addresses of the commands are formed, depending on the control information. In block 2 the sets of initial data are converted from the decimal system to binary. Further control is transferred to block 3 (combined). In it the operations related to the two blocks of the program SP-1 are carried out: identification of the energy class  $K_i$  and introduction of the representative time  $T_i$  of the class  $K_i$  of each earthquake of the initial set to the period  $T_{min}$ . For this purpose the energy classes  $K_i$  of all earthquakes are successively compared with a set of fixed energy classes  $K_{f_j}$  (j = 1, 2, 3, ..., p). If  $K_i = K_{f_j}$ , the earthquake is written as the corresponding period  $T_{f_j}$ . Thereafter with the division of  $T_{\min}$  by  $T_{f_j}$  the number of earthquakes of energy class  $K_{f_j}$  during the period  $T_{\min}$  is obtained, corresponding to earthquakes during the period  $T_{f_j}$ :

$$N_j = \frac{T_{\min}}{T_{\mathbf{f}_j}}.$$

Thus, the work of blocks 1-3 ends with the preparation of the first set of initial data  $M_1$  toward the computation of seismic activity A. In blocks 4-11 A is automatically computed at each point of the map. From block 3 control is transferred to block 4, where the addresses of the block 5 cells are loaded to compute epicentral distances.

Block 5 calculates the distances  $\Delta$  between the computation point of activity and the epicenters of all the earthquakes of initial data set  $M_1$ . The calculation of  $\Delta$  is carried out according to the formula:

$$\cos \Delta = \sin \varphi_i \cdot \sin \varphi_0 + \cos \varphi_i \cdot \cos \varphi_0 \cdot \cos (\lambda_i - \lambda_0), \tag{40}$$

where  $\varphi_i$ ,  $\lambda_i$ —coordinates of the epicenter;

 $\varphi_0$ ,  $\lambda_0$ —coordinates of the point in which the seismic activity is counted.

Formula (40) was used by P. Pavlovaskaya (1968) while programing the determination of the foci coordinates Uzbekistan earthquakes.

Control is then transferred to block 6, where are loaded the addresses of the instructions of the selection block of least epicentral distances  $\Delta_{\min}$ and the computation of summated number  $N_z$  of the epicenters in the averaging zone of activity. Thereafter control is transferred to block 7.

In block 7, the least distance— $\Delta_{\min}$  is chosen from those measured in block 5. For this, all the *m* distances of  $\lambda$  are compared successively with each other. Selection of the least  $\Delta = \Delta_{\min_1}$ , is accompanied by the computation of the number  $N_{\Sigma_1}$ , corresponding to this  $\Delta_{\min_1}$ , and by its storage in the cell where the number of epicenters  $N_{\Sigma_1}$  in the averaging zone is formed, which is brought to one observation period  $T_{\min}$ . The number  $N_{\Sigma}$  is shifted to block 8, where it is analyzed by comparison with  $N_{\sigma}$ , representing the number of earthquake epicenters in accordance with the error of determining seismic activity  $\sigma_A$ , according to the formula (39).

When  $N_{\Sigma} \ge N_{\sigma}$  control is shifted to block 9 and is returned to block 7 when  $N_{\Sigma} \le N_{\sigma}$ , where the next least  $\Delta$  is chosen from those remaining.

For this purpose, in place of the previous  $\Delta_{\min} = \Delta_{\min_1}$ ,  $\Delta_{\max}$  is selected; in most cases its previously known value is used (e.g., in Uzbekistan when epicentral distance did not exceed 500-700 km on an average,  $\Delta_{\max} = 1,000$  km). All the remaining values of  $\Delta$  are again compared with each other until the selection of the least of them  $\Delta_{\min_2}$ . Then follows again the computation of  $N_{\Sigma}$  and transfer of control to block 8. If the comparison of the new number  $N_{\Sigma}$  again shows the inequality  $N_{\Sigma} < N_{\sigma}$ , control is returned to block 7 and  $\Delta_{\max}$  is dispatched in place of  $\Delta_{\min_2}$ . The process is repeated until  $N_{\Sigma} \ge N_{\sigma}$ .

|         |      | Com   | nands an | 1 numbe | ers   |                |                       |
|---------|------|-------|----------|---------|-------|----------------|-----------------------|
| Address | Sign | of    | Order    | $A_1$   | $A_2$ | A <sub>3</sub> | Remarks               |
|         | No.  | Order | :<br>    |         |       |                |                       |
|         |      |       |          | 1061 A  |       |                |                       |
| 1061    | ++   | -1-   | 04       | 100     | 000   | 000            | $\Delta_{max} = 1000$ |
| 2       | ++   | · [-  | 03       | 360     | 000   | 000            | $2\pi = 360^{\circ}$  |
| 3 -     | ++   | +     | 01       | 628     | 318   | 600            | $2\pi = 6.283186$     |
| 4       | ++   |       | 01       | 314     | 150   | 300            | $\pi = 3.141593$      |
| 5       | -+-+ | +     | 03       | 111     | 199   | 000            | 1°=111.199 km         |
| 6       | ++   | +     | • • 10   | 300     | 000   | 000            | No=3                  |

TABLE 5. ADDITIONAL CONSTANTS  $M_2$  FOR SP-2

TABLE 6. CONTROL INFORMATION FOR SP-2

|         | Co      | ommands and        | numbers                   |         | D                    |
|---------|---------|--------------------|---------------------------|---------|----------------------|
| Address | Command | <br>A <sub>1</sub> | $A_1$ $A_2$ $A_3$ Remarks | Remarks |                      |
|         |         | 1041               | A                         |         |                      |
| 1041    | 000     | 000                | 000                       | 1124    | $(0, 0, A_{mn})$     |
| 2       | 000     | 0006               | 000                       | 000     | ( <i>m</i> -1, 0, 0) |
| 3       | 000     | 0010               | 000                       | 000     | (q-1, 0, 0)          |
| 4       | 000     | 0010               | 000                       | 000     | (z-1, 0, 0)          |
| 5       | 000     | 000                | 0003                      | 000     | (0, n, 0)            |
| 6       | 000     | 000                | 0001                      | 000     | (0, 1, 0)            |
| 7       | 000     | 000                | 000                       | 0001    | (0, 0, 1)            |
| 1050    | 000     | 0001               | 000                       | 000     | (1, 0, 0)            |
| 1       | 000     | 0022               | 000                       | 000     | [3(m-1), 0, 0]       |
| 2       | 000     | 0005               | 000                       | 000     | (m-2, 0, 0)          |

As a result of block 7, a series of distances  $\Delta$  is chosen answering the condition:  $\Delta_{\min_{l}} < \Delta_{\min_{2}} < \Delta_{\min_{3}} \dots < \Delta_{\min_{N_{\sigma}}}$ , the number of these  $\Delta$  would be  $N_{\Sigma} \ge N_{\sigma}$ . After the choice of the least  $\Delta = \Delta_{\min_{N_{\sigma}}}$ , control is transferred to block 8 where  $N_{\Sigma} \ge N_{\sigma}$ . Further, control is transferred to block 9.

The computation of seismic activity A according to formula (37) is carried out in block 9. The area of the averaging zone S was found before from the expression  $S = \pi r^2$ , where  $r = \Delta_{\min N_c}$ .

TABLE 7. RESULTS OF COMPUTATION OF  $A_{10}$  ACCORDING TO SP-2

| N <sub>T</sub>     | A <sub>10</sub>    | σ <sub>A</sub>     | $N_{\Sigma}$       |
|--------------------|--------------------|--------------------|--------------------|
| +++ 01 100000000   | ++- 00 505839551   | +++ 02 642684586   | +++ 01 242106268   |
| +++01 200000000    | ++- 00 317147752   | +++02577350269     | +++ 01 30000000    |
| +++01 300000000    | ++- 01 838902168   | +++ 02 577350269   | $+++01\ 300000000$ |
| +++- 01 40000000   | ++-01 360430929    | +++ 02 577350269   | +++ 01 30000000    |
| +++ 01 50000000    | ++-01 199357111    | +++ 02 577350269   | $+++01\ 300000000$ |
| $+++01\ 600000000$ | ++-01 126308151    | +++ 02 577350269   | +++01 300000000    |
| +++ 01 700000000   | ++-02871270444     | +++02577350269     | +++01 300000000    |
| +++ 01 80000000    | $++-02\ 637057144$ | +++ 02 577350269   | +++ 01 300000000   |
| +++ 01 90000000    | ++- 02 485999108   | +-1-+ 02 577350269 | +++ 01 30000000    |
| +++ 01 100000000   | ++-00486605219     | +++02577350269     | +++ 01 300000000   |
| +++ 01 110000000   | ++-00236393739     | +++ 02 577350269   | +++ 01 30000000    |
| +++01 120000000    | ++-01743027819     | +++ 02 577350269   | +++ 01 30000000    |
| +++ 01 130000000   | ++- 01 341530739   | +++ 02 577350269   | +++ 01 300000000   |
| +++ 01 14000000    | ++-01 193443057    | +++ 02 577350269   | +++ 01 30000000    |
| $+++01\ 150000000$ | ++-01 123911577    | +++ 02 577350269   | +++ 01 300000000   |
| $+++01\ 160000000$ | ++-02859813598     | +++ 02 577350269   | +++ 01 30000000    |
| +++ 01 17000000    | $++-02\ 630920910$ | +++ 02 577350269   | +++ 01 30000000    |
| +++ 01 180000000   | ++-02482425038     | +++02577350269     | +++ 01 30000000    |

60

In block 10, the results from the binary representation system are converted to decimal and value A at the point is printed. With the serial number of point  $N_T = qr$  the computation is complete; when  $N_T < qr$  the control is transferred to block 11 where the preparation goes on to compute A at the next point, and further in block 5.

As a result of SP-2, the serial number of the map point  $N_T$  and the value of its seismic activity A is printed. This program accelerates the construction of seismic activity maps with several times greater accuracy when compared with manual computation.

#### **Illustrative Example**

The illustrative example for computing seismic activity maps according to the SP-2 program is meant mainly for the same initial data as in SP-1. Therefore, the Table 1 data may be used for loading SP-2 also. The change is related to data set  $M_2$  and the control information group. The set  $M_2$ consists of two parts. The first occupies cells 1000-1040 and fully duplicates Table 2; in the second, additional constants are introduced (Table 5), which are placed in cells 1061-1065.

The control information begins in cell 1041 in the same manner as in SP-1, but with the addition of other lines (Table 6).

In Table 7, where the results of the seismic activity computation are placed, unlike Table 4, the number of epicenters in the averaging zones  $N_{\Sigma}$  brought to the period of observation,  $T_{\min}$  is placed in the last column. The computation data are given for two map columns  $A_{10}$ , i.e., for 18 points.

While discussing the results of the computation of  $A_{10}$  according to the SP-1 program (Table 4) the differences in the activity values with similar n in the averaging zones of the same area were given different values of  $N_{\Sigma}$ . Different values of  $A_{10}$  for point numbers 2–18 (Table 7) with similar numbers of  $N_{\Sigma}$  are explained by the variable value of the averaging zone of activity, depending on the distance  $\Delta$  between the computation point and the last epicenter, fulfilling the condition  $N_{\Sigma} < N_{\sigma}$ .

## PROGRAM SP-3 FOR COMPUTING A MAPS BY THE COMBINATIONAL METHOD

While calculating the seismic activity A of any territory by the uniform resolution method in each averaging zone of activity, a different number of earthquake epicenters appears, depending on the density of their distribution in the area. With small computation intervals in detailed investigations, not a single epicenter may be seen in certain zones and then a zero value of A is written at that point—the averaging zone center. This leads to a large variation in the activity map, which is, seemingly, less true with the existing

| Address     | Command | A <sub>1</sub> | $A_2$ | A <sub>3</sub> |
|-------------|---------|----------------|-------|----------------|
|             |         | 0500 A         |       |                |
| 0500        | 055     | 0521           | 1102  | 0521           |
| 1           | 013     | 0521           | 1117  | 0521           |
| 2           | 055     | 0545           | 1103  | 0545           |
| 3           | 013     | 0545           | 1116  | 0545           |
| 4           | 055     | 0620           | 1103  | 0620           |
| 5           | 013     | 0620           | 1112  | 0620           |
| 6           | 015     | 0661           | 1103  | 0661           |
| 7           | 013     | 0661           | 1114  | 0661           |
| 0510        | 015     | 0665           | 1103  | 0665           |
| 1           | 012     | 0665           | 1115  | 0665           |
| 2           | 013     | 0005           | 1115  | 0005           |
| 2           | U       | 0512 A         | U     | 0              |
|             |         | 0015 A         |       |                |
| 0513        | 0       | 0              | 0     | 0              |
| 4           | 0       | 0              | 0     | 0              |
| 5           | 0       | 0              | 0     | 0              |
| 6           | 0       | 0              | 0     | 0              |
| 7           | 0       | 0              | 0     | 0              |
| 0520        | 016     | 0522           | 7741  | 0007           |
| 1           | 000     | 2361           | 2361  | 0              |
| 2 .         | 016     | 0524           | 7741  | 0007           |
| 3           | 000     | 1021           | 1021  | 1074           |
| 4           | 0       | 0              | 0     | 0              |
| 5           | 0       | 0              | 0     | 0              |
|             |         | 0526 A         |       |                |
| 0526        | 052     | 0              | • 0   | 0              |
| 7           | 275     | 0              | 2361  | 1120           |
| 0530        | 056     | 0531           | 0532  | 0535           |
| 1           | 002     | 1021           | 1120  | 0              |
| 2           | 056     | 0533           | 0534  | 0543           |
| 3           | 075     | 0              | 1034  | 1122           |
| 4           | 002     | 1047           | 1062  | 1121           |
| 5           | 077     | -0             | 0     | . 0            |
| 6           | 076     | 0              | 0543  | Õ              |
| $\tilde{7}$ | 013     | 0535           | 1075  | 0535           |
| 0540        | 013     | 0543           | 1076  | 0543           |
|             |         | 0541 A         | 10/0  |                |
| 0541        | 002     | 1121           | 0101  | 1121           |
| 2           | 074     | 1121           | 0525  | 1121           |
| . 2         | 070     | 0              | 0000  | 0              |
| 1           | 104     | 1057           | 1100  | 0261           |
| 4           | 104     | 1032           | 1122  | 2301           |
|             | 112     | U              | 0327  | 0003           |
| 0<br>7      | U       | U              | U     | 0              |
| 0550        | U       | U              | 0     | 0              |
| 0000        | 075     | 0              | 0     | 1115           |
| 1           | 052     | 0              | 0     | 0              |

PROGRAM SP-3
| Address | Command | A <sub>1</sub> | $A_2$ | $A_3$ |
|---------|---------|----------------|-------|-------|
|         |         | 0552 A         |       |       |
| 2       | 075     | 0              | 1050  | 1124  |
| 3       | 075     | 0              | 1051  | 1125  |
| -       |         | 0554 A         |       |       |
| 0554    | 0       | 0              | 0     | (     |
| 5       | 452     | 0              | 0     | 0662  |
| 6       | 452     | 0              | õ     | 062   |
| 7       | 056     | 0560           | 0561  | 060(  |
| 0560    | 075     | 0              | 2362  | 1120  |
| 1       | 056     | 0562           | 0563  | 060   |
| 2       | 075     | 0              | 2363  | 112   |
| 3       | 056     | 0564           | 0565  | 061   |
| 4       | 001     | 1130           | 2361  | 1130  |
| 5       | 075     | 0              | 0     | 1153  |
| 6       | 056     | Ő              | 0573  | (     |
|         |         | 0567 A         |       |       |
| 0567    | 013     | 0600           | 1100  | 060   |
| 0570    | 013     | 0601           | 1100  | 060   |
| 1       | 013     | 0616           | 1100  | 0610  |
| 2       | 056     | 0              | 0600  | (     |
| 3       | 001     | 1124           | 1060  | 113   |
| 4       | 002     | 1124           | 1060  | 1134  |
| 5       | 001     | 1125           | 1061  | 113:  |
| 6       | 002     | 1125           | 1061  | 113   |
| 7       | 075     | 0              | 0     | 1130  |
| 0600    | 077     | 0              | 0     |       |
| · 1     | 077     | 0              | 0     | (     |
|         |         | 0602 A         |       |       |
| 0602    | 002     | 1133           | 1126  | (     |
| 0603    | 076     | 0              | 0605  | (     |
| 4       | 056     | 0              | 0620  | . (   |
| 5       | 002     | 1126           | 1134  | (     |
| 6       | 076     | 0              | 0610  | (     |
| 7       | 056     | 0              | 0620  | (     |
| 0610    | 002     | 1135           | 1127  | (     |
| 1       | 076     | 0              | 0613  | (     |
| 2       | 056     | 0              | 0620  | (     |
| 3       | 002     | 1127           | 1136  | (     |
| 4       | 076     | 0              | 0616  | (     |
|         |         | 0615 A         |       |       |
| 0615    | 056     | 0              | 0620  | (     |
| 6       | 077     | 0              | 0     | (     |
| 7       | 001     | 1157           | 0101  | 1157  |
| 0620    | 112     | Û              | 0567  | 000   |

(Contd.)

| Address | Command | A1     | A <sub>2</sub>    | $A_3$ |
|---------|---------|--------|-------------------|-------|
|         |         | 0621 A | , ,, WAX HAN ,, , |       |
| 1       | 002     | 1157   | 1053              | 0     |
| 2       | 076     | 0      | 0624              | C     |
| 3       | 056     | 0      | 0671              | C     |
| 4       | 075     | 0      | 1157              | 1167  |
| 5       | 075     | 0      | 1130              | 1132  |
| 6       | 075     | 0      | 1054              | 1137  |
| 7       | 077     | 0      | 0                 | (     |
|         |         | 0630 A |                   |       |
| 0630    | 075     | 0      | 1063              | 0140  |
| 1       | 016     | 0632   | 7714              | 0007  |
| 2       | 075     | 0      | 0160              | 1160  |
| 3       | 075     | õ      | 0101              | 1161  |
| 4       | 075     | õ      | 1055              | 1162  |
| 5       | 005     | 1162   | 1160              | 0140  |
| 6       | 016     | 0637   | 7711              | 0007  |
| 7       | 002     | 1161   | 0160              | 116   |
| 0640    | 002     | 1056   | 1057              | 1163  |
| 0641    | 005     | 1162   | 1163              | 1163  |
| 2       | 005     | 1163   | 1160              | 0140  |
|         |         | 0643 A |                   |       |
| 0643    | 016     | 0644   | 7711              | 0007  |
| 4       | 075     | 0      | 0160              | 1163  |
| 5       | 005     | 1132   | 1161              | 1161  |
| 6       | 004     | 1161   | 1163              | 1161  |
| 7       | 005     | 1161   | 1064              | 1161  |
| 0650    | 005     | 1137   | 1052              | 1162  |
| 1       | 004     | 1161   | 1162              | 1165  |
| 2       | 004     | 1157   | 0                 | 1161  |
| 3       | 004     | 1064   | 1063              | 1162  |
| 4       | 004     | 1162   | 1161              | 1166  |
| 5       | 001     | 1164   | 0101              | 1164  |
|         | ,       | 0656 A |                   |       |
| 0656    | 016     | 0660   | 7751              | 0007  |
| 7       | 000     | 1164   | 4000              | 1167  |
| 0660    | 075     | 0      | 1133              | 1124  |
| 1       | 112     | 0      | 0556              | 0001  |
| 2       | 077     | 0      | 0                 | (     |
| 3       | 075     | 0      | 1050              | 1124  |
| 4       | 075     | 0      | 1135              | 1125  |
| 5       | 112     | 0      | 0555              | 0001  |
| 6       | 077     | 0      | 0                 | 0     |
| 7       | 0       | . 0    | 0                 | 0     |
| 0670    | 0       | 0      | 0                 | 0     |

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0671 A 0751

| Address | Command | A <sub>1</sub> | A <sub>2</sub> | A3   |
|---------|---------|----------------|----------------|------|
| 2       | 013     | 0751           | 1116           | 0751 |
| 3       | 055     | 0770           | 1103           | 0770 |
| 4       | 013     | 0770           | 1113           | 0770 |
| 5       | 056     | 0676           | 0677           | 0707 |
| 6       | 004     | 2362           | 1140           | 1141 |
| 7       | 056     | 0700           | 0701           | 0710 |
| 0700    | 004     | 2363           | 1140           | 1142 |
| 1       | 004     | 1066           | 1067           | 1040 |
| 2       | 004     | 1124           | 1140           | 1126 |
| 3       | 004     | 1125           | 1140           | 1127 |
|         |         | 0704 A         |                |      |
| 0704    | 052     | 0              | 0              | 0    |
| 5       | 056     | 0706           | 0707           | 0745 |
| 6       | 005     | 1065           | 1161           | 1171 |
| 7       | 077     | 0              | 0              | 0    |
| 0710    | 077     | Ő              | Ő              | 0    |
| 1       | 075     | Ô              | 1126           | 0140 |
| 2       | 016     | 0713           | 7712           | 0007 |
| 3       | 075     | 0              | 0161           | 1143 |
| 4       | 075     | ŏ              | 0160           | 1144 |
| 5       | 075     | Ő              | 1127           | 0140 |
| 6       | 016     | 0717           | 7712           | 0007 |
|         |         | 0717 A         |                |      |
| 0717    | 045     | 0              | 0161           | 1145 |
| 0720    | 075     | 0              | 0160           | 1146 |
| 1       | 075     | 0              | 1141           | 0140 |
| 2       | 016     | 0723           | 7712           | 0007 |
| 3       | 075     | 0              | 0161           | 1147 |
| 4       | 075     | 0              | 0160           | 1150 |
| 5       | 075     | 0              | 1142           | 0140 |
| 6       | 016     | 0727           | 7712           | 0007 |
| 7       | 075     | 0              | 0161           | 1151 |
| 0730    | 075     | 0              | 0160           | 1152 |
| 1       | 005     | 1143 .         | 1147           | 1161 |
|         |         | 0732 A         |                |      |
| 0732    | 005     | 1144           | 1146           | 1162 |
| 3       | 005     | 1162           | 1150           | 1162 |
| 4       | 005     | 1162           | 1152           | 1162 |
| 5       | 001     | 1161           | 1162           | 1161 |
| 6       | 005     | 1144           | 1145           | 1162 |
| 7       | 005     | 1162           | 1150           | 1162 |
| 0740    | 005     | 1162           | 1151           | 1162 |
| 1       | 001     | 1161           | 1162           | 1161 |
| 2       | 075     | 0              | 1161           | 0140 |

(Contd.)

| Address      | Command | A <sub>1</sub> | A <sub>2</sub> | A3   |
|--------------|---------|----------------|----------------|------|
|              |         | 0743 A         | · · · ·        |      |
| 3            | 016     | 0744           | 7716           | 0007 |
| 4            | 005     | 0160           | 1140           | 1161 |
|              |         | 0745 A         |                |      |
| 0745         | 077     | 0              | 0              | 0    |
| 6            | 013     | 0745           | 1077           | 0745 |
| 7            | 013     | 0707           | 1101           | 0707 |
| 0750         | 013     | 0710           | 1101           | 0710 |
| 1            | 112     | 3272           | 0707           | 0003 |
| 2            | 0       | 0              | 0              | 0    |
| 3            | 075     | 0              | 0              | 1170 |
| 4            | 075     | 0              | 0              | 1131 |
| 5            | 052     | 0              | 0              | 0    |
| 6            | 075     | 0              | 0              | 1153 |
| 7            | 075     | 0              | 0              | 1154 |
|              |         | 0760 A         |                |      |
| 0760         | 075     | 0              | 1171           | 1123 |
| 1            | 013     | 1153           | 1100           | 1153 |
| 2            | 013     | 1154           | 1077           | 1154 |
| 3            | 402     | 1172           | 1123           | 0    |
| 4            | 076     | 0              | 0770           | 0    |
| 5            | 075     | 0              | 1153           | 1155 |
| 6            | 075     | 0              | 1154           | 1156 |
| 7            | 275     | 0              | 1172           | 1123 |
| <b>077</b> 0 | 112     | 1075           | 0761           | 0001 |
| 1            | 0       | 0              | 0              | 0    |
| 2            | 0       | 0              | 0              | 0    |
|              |         | 0773 A         |                |      |
| 0773         | 056     | 0774           | 0775           | 1003 |
| 4            | 001     | 1131           | 2361           | 1131 |
|              |         | 0775 A         |                |      |
| 5            | 056     | 0776           | 0777           | 1004 |
| 6            | 075     | 0              | 1064           | 1171 |
| 7            | 005     | 1123           | 1123           | 1160 |
| 1000         | 005     | 1070           | 1160           | 1137 |
| 1            | 013     | 1003           | 1155           | 1003 |
| 2            | 013     | 1004           | 1156           | 1004 |
| 3            | 077     | 0              | 0              | 0    |
| 4            | 077     | 0              | 0              | Õ    |
| 5            | 0       | 0              | 0              | Õ    |
|              |         | 1006 A         |                | -    |
| 1006         | . 001   | 1170           | 0101           | 1170 |
| 7            | 002     | 1170           | 1053           | 0    |
| 1010         | 036     | 0              | 0755           | Ô    |
| 1            | 075     | Ő              | 1170           | 1167 |
| 2            | 075     | ů              | 1170           | 1157 |

(Contd. on p. 69)





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BLOCK DIAGRAM OF PROGRAM SP-4

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| Address | Command | A1     | A2            |      |
|---------|---------|--------|---------------|------|
| 3       | 075     | 0      | 1131          | 1132 |
| 4       | 056     | 0      | 0627          | 0    |
|         |         | 1075 A |               |      |
| 1075    | 000     | 0001   | 0             | 0    |
| 6       | 000     | 0000   | 0001          | 0    |
| 7.      | 000     | 0      | 0             | 0001 |
| I100    | 000     | 0      | 0003          | 0    |
| 1       | 000     | 0003   | 0             | 0    |
| 2       | 777     | 7777   | 7 <b>77</b> 7 | 0    |
| 3       | 777     | 0      | 7777          | 7777 |
| 4       | 0       | 0      | 0             | 0    |
| 5       | 0       | 0      | 0             | 0    |
| 6       | 0       | 0      | 0             | . 0  |
| 7       | 0       | 0      | 0             | 0    |

PROGRAM SP-3 (Contd.)

accuracy of determining the epicenter coordinates ("Earthquakes in the USSR", 1962–1967). Therefore, I.V. Gorbunova's method (1964) is used when it is necessary to use the constant resolution method, i.e., the constant value of averaging zone A at low activity places, where in each zone less than a given minimum number of epicenters may fall (e.g., less than 3). This is connected with the change of averaging zone A and an increase in the computation accuracy, although, it is true, at the cost of its detailing (Riznichenko, Gorbunova, 1968).

To compute activity maps on the computer by the methods described above, taking into account, if necessary, the constant resolution and constant accuracy methods, we formed a combination program—SP-3, unifying certain blocks of the earlier SP-1 and SP-2 programs. As in SP-1 and SP-2, it uses the method of totaling earthquake epicenters in the averaging zone of activity (Riznichenko, 1964a). The initial information for computing Ais given by two sets. The first  $M_1$  is formed by the matrix of epicenters  $A_{mn}$ , similar to SP-1 and SP-2.

The second set  $M_2$  mainly holds the constants necessary to compute the seismic activity in the region under investigation: viz., a list of presented energy classes of earthquakes  $K_{f_j}$ ; number  $K_{f_j}$  equal to P; schedule of presentation periods  $T_{f_j}$  corresponding to  $K_{f_j}$ ; value of the zone  $S_1$  of averaging the seismic activity during its calculation with constant detailing;  $N_{\sigma_2}$  is the least number of earthquakes in zone  $S_1$ , giving the value A with given reliability;  $N_{\sigma_2}$  is the least number of earthquakes in the averaging zone, corresponding to given error  $\sigma_A$  of computing activity with constant accuracy;  $\varphi_0$ ,  $\lambda_0$ —coordinates of the initial point of computation A;  $a_{\varphi}$ ,  $a_{\lambda}$  is the step of computing activity latitudinally and longitudinally, in this, the pro-

duct  $2a_{\varphi} \cdot 2a_{\lambda}$  determines the area of averaging zone  $S_1$ ; some numerical constants, e.g., the numbers  $2\pi$  and 360 to change from degree scale to radians and so on. Besides, control information is available with data about the volume of the initial matrix  $A_{mn}$  and the volume of the resulting matrix  $A_{qr}$ . Here, also are situated data about some concrete cell numbers of memory necessary to calculate the construction sequence. Control information standardizes the program, which may be accepted unchanged to compute seismic activity with any stipulated accuracy for any region with any computation interval and with any averaging zone dimensions. Only the contents of the data sets of the initial data are changed.

The SP-3 program uses the library of standard programs, which is in cells 0-0477 and 6200-7777 of the memory. The SP-3 program itself engages cells 0500-1020 of the memory; the data set of constants and control information is in 1021-1117, the data set of epicenters in 2361-6177, the remaining cells are used for recording intermediate computation results.

## Block Diagram SP-3 (see p. 67)

The work flows through blocks 1-16 of the SP-3 program as seen in the block diagram. After the introduction of the actual program and initial data sets to the memory, control is given to block 1. Here the addresses of the first part of the program are calculated for the instructions sequence to compute seismic activity with a constant resolution using the control information. Control is transferred to block 2, where the initial data is converted from decimal to binary. Next control is shifted to block 3 where the addresses of the instructions for block 4 are loaded.

In this block the representative periods  $T_i$ , corresponding to the energy class  $K_i$  of each earthquake given in  $M_1$ , are brought to the period  $T_{\min}$  in accordance with the least energy classes of the representative earthquake of the region under investigation. Then control is shifted to block 5 where the addresses of instructions of block 6 are loaded. Computation A begins from the point using the given coordinates  $\varphi_0$ ,  $\lambda_0$ . For this, the averaging zone of activity  $S_1 = 2a_{\varphi} \cdot 2a_{\lambda}$  is taken around the initial point  $(\varphi_0, \lambda_0)$  and from data set  $M_1$  all earthquake epicenters are chosen, whose coordinates are included in  $S_1$ . In block 7, the number of these earthquakes  $N_{\Sigma_1}$  is calculated, which is then compared with the given minimum  $N_{\sigma_1}$  that is necessary to obtain a reliable value of activity at the point ( $\varphi_0, \lambda_0$ ). If  $N_{\Sigma_1} \ge N_{\sigma_1}$ then control is shifted to block 8, where the values of A and  $\sigma_A$  are automatically computed according to formulas (37) and (39). If  $N_{\Sigma_1} < N_{\sigma_1}$ , then the number of earthquakes inside the averaging zone is insufficient to obtain a reliable value of activity at point ( $\varphi_0$ ,  $\lambda_0$ ) in the calculations with constant resolution and it becomes necessary to increase the area of the averaging zone so that  $N_{\Sigma_1} = N_{\sigma_1}$ . For this purpose control is shifted from block 7

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o block 11 which begins the second part of the program. The addresses of he commands for the blocks of the second part of the program are autonatically formed in block 11, after which control is shifted to block 12. The ddresses of the cells of the next two blocks—13 and 14—are loaded there.

Computation of the epicentral distances  $\Delta$  from the point with coordirates  $\varphi_0$ ,  $\lambda_0$  to all epicenters ( $\varphi_i$ ,  $\lambda_i$ ) as in the first data set of initial data, akes place in block 14. The computation of  $\Delta$  is carried out according to ormula (40), which needs all the arguments to be expressed in radians. The onversion of degrees to radians for the corresponding coordinates of the omputation points ( $\varphi_0$ ,  $\lambda_0$ ) and epicenters ( $\varphi_i$ ,  $\lambda_i$ ) is carried out in block 13. Control is shifted from block 14 to block 15 where the computed  $\Delta$ , the number m of which is equal to the number of epicenters in the first data set of initial data, are compared with one another and the least distant  $\Delta_{\min}$ from the computation point of activity ( $\varphi_0$ ,  $\lambda_0$ ) to the nearest earthquake epicenter of the initial set, is selected from among them. In block 16 the selection of  $\Delta_{\min}$  is accompanied by the selection of the corresponding value of  $N_{\Sigma_{a}}$ , i.e., the total number of earthquakes in the averaging zone with area  $S_1 = \pi \Delta^2_{\min}$ , brought to the observation period  $T_{\min}$ . Here, it is compared with the earlier given value  $N_{\sigma_2}$ , defining the accuracy of the seismic activity computation according to expression (39). If  $N_{E_{s}} \ge N_{\sigma}$  control is shifted to block 8 to compute activity; if  $N_{\Sigma_2} > N_{\sigma_2}$  control goes to block 15. Here again all the remaining  $\Delta$  are compared with each other without the chosen  $\Delta_{\min}$ , which is replaced by number  $\Delta_{\max}$  larger than all possible in the region under study. As a result of the comparison, a new  $\Delta_{\min}$  is selected. The procedure of selecting the least epicentral distances  $\Delta_{\min}$  in block 15 is accompanied by the selection and summation of the corresponding N<sub>i</sub> in block 16 and this is repeated as long as  $\sum N_i =$  $N_{\Sigma}$  does not equal  $N_{\sigma}$ —the number of earthquakes in the averaging zone. This insures the given accuracy of the activity computation. (In this case, the last  $\Delta_{\min}$  among the values chosen in block 15 is taken to be the radius r of the zone  $S_2$  of averaging activity.) After the computation of  $S_2$  control is shifted to block 8, where, according to the summation formula of earthquakes (37) the activity and the error of computation  $\sigma_{4}$ —according to (39)-are calculated.

From block 8, control is shifted to block 9 where the results of computation are printed. The print-out gives the point number  $(N_T)$  and values A and  $\sigma_A$ . The number  $N_T$  is analyzed in the same block and if  $N_T = q \cdot r$ (the number of points of the resulting matrix  $A_{qr}$ ) then the computation is finished. If  $N_T < qr$  then control is shifted to block 10 where the computation for seismic activity is made ready for the successive point, for which its coordinates are formed using constants  $a_{\varphi}$  and  $a_{\lambda}$ . Further, control is shifted to block 5 and the entire process is fully repeated for each point of the seismic activity map.

# **Illustrative Example**

The initial data of sets  $M_1$ ,  $M_2$  and the control information may be used to test the SP-3 program. Set  $M_1$  is similar to that in the SP-1 and SP-2 programs (see Table 1), but here the entry address is changed from 1100 to 2361. The set of the constants  $M_2$  includes the contents of the same-named sets for SP-1 and SP-2 and engages cells 1021-1074. The recording of the constants  $M_2$  for the concurrent version of the program is on standard tabulation sheets (Table 8). Here cells 1021-1033 are meant for the energy classes  $K_{fj}$  of the representative earthquakes in set  $M_1$ . The illustrative example uses only the first four cells (1021-1024) of the nine put forth in accordance with the number P = 4 of the class  $K_{fj}$  of the set  $M_1$  (Table 1). In accordance with the class  $K_{fj}$ ; for the placement of the presentation

| TABLE 8 | 3. DATA | SET $M_2$ | FOR | SP-3 |
|---------|---------|-----------|-----|------|
|         |         | _         |     |      |

|                 |              | (               | Commands | s and numb | ers |     |                  |
|-----------------|--------------|-----------------|----------|------------|-----|-----|------------------|
| Address Sign of |              | l of            | Order    |            | Δ.  | A - | Remarks          |
|                 | No.          | Order           | Older    | A1         | A2  | A3  |                  |
|                 |              |                 |          | 1021 A     |     |     |                  |
| 1021            | ++           | ÷               | 02       | 100        | 000 | 000 | $K_{t_1} = 10$   |
| 2               | ++           | +               | 02       | 110        | 000 | 000 | $K_{f_0} = 11$   |
| 3               | ° ++         | +               | 02       | 120        | 000 | 000 | $K_{t_{3}} = 12$ |
| 4               | ++           | +               | 02       | 130        | 000 | 000 | $K_{t_{A}} = 13$ |
| 5               | +++          | - <del> -</del> | 00       | 000        | 000 | 000 | 2                |
| 6               | ++           | +               | 00       | 000        | 000 | 000 |                  |
| 7               | ++           | +               | 00       | 000        | 000 | 000 |                  |
| 1030            | ++++++       | -+              | 00       | 000        | 000 | 000 |                  |
| 1               | ++           |                 | 00       | 000        | 000 | 000 |                  |
| 2               | · +- +-      | +               | 00       | 000        | 000 | 000 |                  |
| 3               | ·+ <b>{-</b> | +               | 00       | 000        | 000 | 000 |                  |
|                 |              |                 |          | 1034 A     |     |     |                  |
| 1034            | ++           | +               | 02       | 160        | 000 | 000 | $T_{f_1} = 16$   |
| 5               | ++           | +               | 02       | 160        | 000 | 000 | $T_{t_{a}} = 16$ |
| 6               | ++           | +               | 02       | 160        | 000 | 000 | $T_{t_2} = 16$   |
| 7               | ++           | +               | 02       | 380        | 000 | 000 | $T_{t} = 38$     |
| 1040            | . ++         | +               | 00       | 000        | 000 | 000 | 4                |
| 1               | ++           | -1-             | 00       | 000        | 000 | 000 |                  |
| 2               | ++           | -1-             | 00       | 000        | 000 | 000 |                  |
| 3               | ++           | -†-             | 00       | 000        | 000 | 000 |                  |
| 4               | +++          | •   •           | 00       | 000        | 000 | 000 |                  |
| 5               | ++           | +               | 00       | .000       | 000 | 000 |                  |
| - 6             | ++           | +-              | 00       | 000        | 000 | 000 |                  |

|         |      | C     | ommands a | and numbe | ers |            |                           |
|---------|------|-------|-----------|-----------|-----|------------|---------------------------|
| Address | Sigr | 1 of  | Order     | Δ.        |     |            | Remarks                   |
|         | No.  | Order | Order     |           | 732 | <b>F13</b> |                           |
|         |      |       |           | 1047 A    |     |            |                           |
| 1047    | ++   | - -   | 01        | 400       | 000 | 000        | P=4                       |
| 1050    | +-+  | +     | 02        | 401       | 000 | 000        | $\varphi_0 = 40.1$        |
| 1       | ++   | -]-   | 02        | 701       | 000 | 000        | $\lambda_0 = 70.1$        |
| 2       | ++   | +     | 02        | 160       | 000 | 000        | $T_{\rm rep} = 16$        |
| 3       | ++   | +     | 01        | 300       | 000 | 000        | $N_{\sigma} = 3$          |
| .4      | ++   | +-    | 03        | 352       | 000 | 000        | S=352                     |
| 5       | ++   | +     | 00        | 500       | 000 | 000        | $\gamma = 0.5$            |
| 6       | ++   | +     | 02        | 100       | 000 | 000        | $K_{\rm rep} = 10$        |
| 7       | ++   | +     | 02        | 100       | 000 | 000        | $K_0 = 10$                |
| 1060    | ++   | +.    | 00        | 100       | 000 | 000        | $d\varphi = 0.1$          |
| 1       | ++   | +-    | 00        | 100       | 000 | 000        | $a_{\lambda} = 0.1$       |
|         |      |       |           | 1062 A    |     |            |                           |
| 1062    | ++   | -+-   | 00        | 500       | 000 | 000        | const = 0.5               |
| 3       | ++   | +     | 02        | 100       | 000 | 000        | const=10                  |
| 4       | ++   | -1-   | 04        | 100       | 000 | 000        | $\Delta_{\rm max} = 1000$ |
| 5       | ++   | +     | 03        | 111       | 199 | 000        | 1°=111.199                |
| 6       | ++   | +     | 03        | 360       | 000 | 000        | $2\pi = 360$              |
| 7       | ++   | +     | 01        | 629       | 318 | 600        | $2\pi = 6.283186$         |
| 1070    | +-1- | +     | 01        | 314       | 159 | 300        | $\pi = 3.141593$          |
| 1       | ++   | +     | 04        | 100       | 000 | 000        | $S_0 = 1000$              |
| 2       | ++   | +-    | 01        | 150       | 000 | 000        | const = 1.5               |
| 3       |      | ÷     | 00        | 000       | 000 | 000        |                           |
| 4       | ++   | +     | 00        | 000       | 000 | 000        |                           |

| TABLE 9. | CONTROL | INFORMATION | FOR | SP-3 |
|----------|---------|-------------|-----|------|

| Addussa |         | Commands and numbers |                |                |                  |
|---------|---------|----------------------|----------------|----------------|------------------|
| Address | Command | A <sub>1</sub>       | A <sub>2</sub> | A <sub>3</sub> | Kentarks         |
|         |         |                      | 1112 A         |                |                  |
| 1112    | 000     | 0006                 | 0000           | 0000           | (m-1, 0, 0)      |
| 3       | 000     | 0005                 | 0000           | 0000           | (m-2, 0, 0)      |
| 4       | 000     | 0010                 | 0000           | 0000           | (q-1, 0, 0)      |
| 5       | 000     | 0010                 | 0000           | 0000           | (r-1, 0, 0)      |
| 6       | 000     | 0022                 | 0000           | 0000           | [(3(m-1), 0, 0]] |
| 7       | 000     | 0000                 | 0000           | 2406           | $(0, 0, A_{mn})$ |

# TABLE 10. RESULTS OF COMPUTATION OF A10 ACCORDING TO SP-3

.

|                  | A10                | ° <sub>A</sub>   | <i>n</i>         |
|------------------|--------------------|------------------|------------------|
| +++ 01 100000000 | ++- 00 37217298    | +++ 02 593171014 | +++ 01 40000000  |
| +++ 01 200000000 | ++- 00 316988809   | +++ 02 642684586 | +++ 01 30000000  |
| +++ 01 300000000 | ++- 01 838902168   | +++ 02 577350269 | +++ 01 30000000  |
| +++ 01 40000000  | ++- 01 360430929   | ·++ 02 577350269 | +++ 01 30000000  |
| +++ 01 50000000  | ++-01 199357111    | +++02577350269   | +++ 01 30000000  |
| +++ 01 60000000  | ++- 01 126308151   | +++02 577350269  | +++ 01 30000000  |
| +++ 01 70000000  | ++- 02 871270444   | +++ 02 577350269 | +++ 01 30000000  |
| +++ 01 80000000  | ++- 02 637057144   | +++ 02 577350269 | +++ 01 30000000  |
| +++01 900000000  | ++- 02 485999108   | +++ 02 577350269 | +++ 01 30000000  |
| +++02 100000000  | + + - 00 392790481 | +++ 02 577350269 | +++ 01 30000000  |
| +++02 110000000  | ++-00392790481     | +++ 02 577350269 | +++ 01 30000000  |
| +++02 120000000  | ++-01 743027819    | +++ 02 577350269 | +++ 01 30000000  |
| +++ 02 130000000 | ++-01 341530739    | +++ 02 577350269 | +++ 01 30000000  |
| +++02 140000000  | ++-01 193443057    | +++ 02 577350269 | +++ 01 30000000  |
| +++ 02 15000000  | ++-01 123911577    | +++ 02 577350269 | -+++ 01 30000000 |
| ++++ 02 16000000 | ++-02859813598     | +++02577350269   | +++ 01 30000000  |
| +++ 02 170000000 | ++-02690920910     | +++ 02 577350269 | +++01 300000000  |
| +++ 02 180000000 | ++-02482425038     | +++ 02 577350269 | +++ 01 300000000 |

periods  $T_{f_j}$ , cells 1034-1046 are set aside; whereas, only four (1034-1037) are engaged in our example. In general, without changing the program, the activity computation may be carried out even with P = 9, i.e., in a wider range of earthquake energy classes. In cells 1047-1072 the remaining constants of  $M_2$  are recorded, the values of which are shown in the remarks. If data set  $M_2$  (Table 8) is enumerated in decimal code, then the next table containing control information to the illustrative example is given in octal code (Table 9), as in the SP-1 and SP-2 programs, where m-number of lines of the matrix  $A_{mn}$  of the initial set  $M_1$ , q-number of lines, and r-number of columns of the resulting matrix  $A_{qr}$ ;  $A_{mn}$ -the last cell of the set  $M_1$ . The control information engages cells 1112-1117.

Table 10 shows the results of the seismic activity computations of the SP-3 program for the initial data given in Tables 1, 8 and 9. Here the values of activity  $A_{10}$  are found for two columns of the map;  $N_T$ —serial number of the computational point;  $\sigma_A$ —computation error of  $A_{10}$  (%); *n*—number of epicenters in the averaging zone of activity.

# PROGRAM SP-4 FOR COMPUTING A MAPS BY THE DISTRIBUTION METHOD

The distribution method (Nersesov, Riznichenko, 1959; Riznichenko, Nersesov, 1960b) was applied during the construction of the first seismic activity maps, and also during the attempts to quantitatively evaluate seismic dangers for the seismic zoning of Uzbekistan in 1962 (Atabaev and others, 1968). The computation was conducted by the expression

$$A = \frac{\sum_{k=10}^{13} n_k^2 c_k^{10} \frac{1000}{T \cdot S}}{\sum_{k=10}^{13} n_k},$$
(41)

where  $n_k$ —number of energy class K earthquakes during T years in the area S. km<sup>2</sup>;

 $c_k^{10}$ —coefficient of transition from the activity according to class K to the activity of energy class 10.

The computation of the activity maps of many seismic zones is conducted by the earthquake summation method (Riznichenko, 1964a; Gorbunova, Riznichenko, 1965; Zakharova, Seiduzova, 1969; Riznichenko, Bune and others, 1969; Riznichenko, Zakharova, Seiduzova, 1970; Drumya and others, 1969, 1971a, b; Kallaur, 1971; Jibladze, 1971 and others). There is a commutative function in the basic construction by the summation method used in the SP-1, 2, and 3 programs, which presents itself as a dependence

PROGRAM SP-4

| 0500<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0510 | 055<br>013<br>055<br>013<br>055<br>013<br>055<br>013<br>055  | 0500 A<br>0522<br>0522<br>0537<br>0537<br>0621<br>0621 | 0764<br>0777<br>0765<br>1000<br>0765                  | 0522<br>0522<br>0537                                   |
|---|--|--|---|--|
| 0500<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0510 | 055<br>013<br>055<br>013<br>055<br>013<br>055  | 0522<br>0522<br>0537<br>0537<br>0621                   | 0764<br>0777<br>0765<br>1000<br>0765                  | 0522<br>0522<br>0537                                   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>0510         | 013<br>055<br>013<br>055<br>013<br>055   | 0522<br>0537<br>0537<br>0621                           | 0777<br>0765<br>1000<br>0765                          | 0522<br>0537   |
| 2<br>3<br>4<br>5<br>6<br>7<br>0510              | 055<br>013<br>055<br>013<br>055  | 0537<br>0537<br>0621<br>0621                           | 0765  | 0537   |
| 3<br>4<br>5<br>6<br>7<br>0510                   | 013<br>055<br>013<br>055   | 0537<br>0621<br>0621                                   | 1000  | DE0H   |
| 4<br>5<br>6<br>7                                | 055<br>013<br>055  | 0621<br>0621   | 0765  | 0337   |
| 5<br>6<br>7<br>0510                             | 013<br>055   | 0621   | 0705  | 0621   |
| 6<br>7<br>0510                                  | 055  | 10021  | 1003  | 0621   |
| 7   |  | 0671   | 0765  | 0671   |
| 0510  | 013  | 0671   | 1001  | 0671   |
|   | 055  | 0675   | 0765  | 0675   |
| 1   | 013  | 0675   | 1002  | 0675   |
| 2   | 000  | 0000   | 0000  | 0000   |
| -   |  | 0513 A   |   |  |
| 0513  | 000  | 0000   | 0000  | 0000   |
| 4   | 000  | 0000   | 0000  | 0000   |
| 5   | 000  | 0000   | 0000  | 0000   |
| 6   | 000  | 0000   | 0000  | 0000   |
| 7   | 055  | 0701   | 0765  | 0701   |
| 0520  | 013  | 0701   | 1000  | 0701   |
| 0520  | 015  | 0701   | 7741  | 0007   |
| 2   | 010  | 1100   | 1100  | 0007   |
| 2   | 016  | 0525   | 7741  | 0007   |
| · 3<br>A  | 010  | 0710   | 0710  | 0763   |
| 4<br>'5   | 000  | 0710   | 07/10   | 1010   |
| 5   | 015  | 0526 4   | 0745  | 1010   |
| 0526  | 000  | 0000   | 0000  | 0000   |
| 7 0528  | 000  | 0000   | 0000  | 1062   |
| 0520  | 073  | 0000   | 0000  | 1063   |
| 0330  | 052  | 0000   | 0000  | 1011   |
| 1   | 402  | 0/10   | 0/44  | 1011   |
| 2   | 005  | 1010   | 1011  | 1011   |
| 3   | 004  | 1011   | 0/52  | 1011   |
| 4   | 075  | 0000   | 1011  | 0140   |
| 5   | V16  | 0536   | //10  | 0007   |
| 6   | 175  | 0000   | 0160  | 1021   |
| 7   | 112  | 0000   | 0000  | 0000   |
| 0040  | 052  | 0541 A   | 0000  | 0000   |
| 0541  | 075  | 0000   | 0737  | 1012   |
| 2   | 075  | 0000   | 0737  | 1013   |
| 2   | 450  | 0000   | 0000  | 0672   |
| 3   | 432  | 0000   | 0000  | 0672   |
| 4.  | 452  | 0000   | 0000  | 0022   |
| 2   | 056  | 0000   | 0550  | 0000   |
| 6   | 036  | V34/   | 0550  | U262   |
| 1   | 0/5  | 0000   | 1102  | 1015   |
| 0550  | 056  | 1660   | 0552  | 0366   |
|   | 0513<br>4<br>5<br>6<br>7<br>0520<br>1<br>2<br>3<br>4<br>5<br>0526<br>7<br>0530<br>1<br>2<br>3<br>4<br>5<br>0526<br>7<br>0530<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0540<br>0541<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>0550<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>05540<br>0<br>05540<br>0<br>05540<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>1<br>2<br>3<br>4<br>5<br>6<br>7<br>05540<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ |

| Address   | Command | A1           | A <sub>3</sub> | A <sub>3</sub> |
|-----------|---------|--------------|----------------|----------------|
|           |         | 0552 A       |                |                |
| 2         | 056     | 0553         | 0560           | 0603           |
| 3         | 075     | 0000         | 1101           | 1017           |
| -         | ••••    | 0554 A       |                | -              |
| 0554      | 013     | 0565         | 0766           | 0565           |
| 0JJ4<br>5 | 013     | 0565         | 0766           | 0565           |
| 5         | 013     | 0500         | 0766           | 0500           |
| . 0       | 015     | 0003         | 0700           | 0003           |
| 0560      | 001     | 1013         | 0745           | 1034           |
| 0.000     | 001     | 1013         | 0745           | 1034           |
| 1         | 002     | 1013         | 0745           | 1035           |
| 2         | 001     | 1014         | 0740           | 1030           |
| 3         | 002     | 1014         | 0746           | 1037           |
| 4         | 045     | 0            | 0              | 1020           |
| 5         | 077     | 0            | 0              | 0              |
| 0         | 077     | 0            | 0              | U              |
| •.        |         | 0567 A       |                |                |
| 0567      | 002     | 1034         | 1015           | 0              |
| 0570      | 076     | 0            | 0572           | 0              |
| 1         | 056     | 0            | 0621           | 0              |
| 2         | 002     | 1015         | 1035           | . 0            |
| · 3       | 076     | 0            | 0575           | 0              |
| 4         | 056     | 0            | 0621           | 0              |
| 5         | 002     | 1036         | 1016           | 0              |
| 6         | 076     | 0            | 0600           | 0              |
| 7         | 056     | 0            | 0621           | 0              |
| 0600      | 002     | 1016         | 1037           | 0              |
| 1         | 076     | 0            | 0603           | 0              |
|           |         | 0602 A       |                |                |
| 0602      | 056     | 0            | 0621           | 0              |
| 3         | 077     | 0            | 0              | 0              |
| 4         | 001     | 1020         | 0101           | 1020           |
| 5         | 002     | <b>07</b> 36 | 0747           | 1040           |
| 6         | 056     | 0607         | 0610           | 0614           |
| 7         | 002     | 0710         | 1017           | 0              |
| 0610      | 056     | 0611         | 0614           | 0620           |
| 1         | 001     | 1041         | 0101           | 1041           |
| 2.        | 013     | 0614         | 0767           | 0614           |
| 3         | 013     | 0620         | 0770           | 0620           |
| 4         | 077     | 0            | 0              | 0              |
|           |         | 0615 A       |                |                |
| 0615      | 076     | 0            | 0620           | 0              |
| 6         | 002     | 1040         | 0101           | 1040           |
| 7         | 076     | 0            | 0612           | 0              |
| 0(20      | 077     | 0            | 0              | 0              |

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(Contd.)

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| Address | Command | $\mathbf{A}_{1}$ | $A_2$ | Aa   |
|---------|---------|------------------|-------|------|
|         |         | 0621 A           |       |      |
| 1       | 112     | . 0              | 0554  | 000  |
| 2       | 077     | Ő                | 0     | (    |
| 3       | 075     | Ő                | 1020  | 106  |
| 4       | 002     | 102.0            | 0753  | (    |
| 5       | 076     | 0                | 0631  |      |
| 6       | 075     | 0                | 0     | 1064 |
| 7       | 075     | 0                | 0750  | 106  |
|         |         | 0630 A           |       |      |
| 0630    | 056     | 0                | 0665  |      |
| 1       | 002     | 0736             | 0747  | 105  |
| 2       | 075     | 0                | 0     | 106  |
| 3       | 075     | 0                | õ     | 106  |
| 4       | 056     | 0635             | 0636  | 064  |
| 5       | 004     | 1041             | 0723  | 101  |
| 6       | 056     | 0637             | 0645  | 065  |
| 7       | 005     | 1012             | 1021  | 101  |
| 8       |         |                  |       |      |
| 0640    | 0       | 0                | 0     | I    |
| 1       | 0       | 0                | 0     | (    |
| 2       | 0       | 0                | 0     | (    |
|         |         | 0643 A           |       |      |
| 0643    | 013     | 0645             | 0771  | 064  |
| 4       | 013     | 0650             | 0772  | 065  |
| 5       | 077     | 0                | 0     |      |
| 6       | 001     | 1061             | 1011  | 106  |
| 7       | 005     | 1011             | 1011  | 101  |
| 0650 -  | 077     | 0                | 0     |      |
| 1       | 001     | 1062             | 1012  | 106  |
| 2       | 002     | 1054             | 0101  | 105  |
| 3       | 076     | 0                | 0643  |      |
| 4       | 0       | 0                | 0     |      |
| 5       | 0       | 0                | 0     |      |
|         |         | 0656 A           |       |      |
| 0656    | 004     | 0751             | 0742  | 101  |
| 7       | 0       | 0                | 0     |      |
| 0660    | 005     | 1062             | 1012  | 101  |
|         |         | 0661 A           |       |      |
| 1       | 004     | 1012             | 1061  | 106  |
| 2       | 045     | 0                | 0750  | 100  |
| 2       | 044     | 1020             | 0,50  | 101  |
| 3<br>A  | 004     | 1012             | 1011  | 106  |
| 5       | 001     | 1063             | 0101  | 100  |
| 6       | 016     | 0670             | 7051  | 000  |
| 7       | 000     | 1063             | 4000  | 106  |
| •       | 000     |                  |       |      |

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| Address | Command | A      | A <sub>2</sub> | A3   |
|---------|---------|--------|----------------|------|
|         |         | 0671 A |                |      |
| 0671    | 112     | 0      | 0544           | 0001 |
| 2       | 077     | 0      | 0              | 0    |
| 3       | 075     | 0      | 0737           | 1013 |
| 4       | 075     | 0      | 1036           | 1014 |
| 5       | 112     | 0      | 0543           | 0001 |
| 6       | 077     | 0      | 0              | 0    |
| 7       | 002     | 0736   | 0747           | 1055 |
| 0700    | 056     | 0701   | 0702           | 0703 |
| 1       | 075     | 0      | 0              | 1041 |
| 2       | 013     | 0703   | 0773           | 0703 |
| 3       | 077     | 0      | 0              | 0    |
|         |         | 0704 A |                |      |
| 0704    | 002     | 1055   | 0101           | 1055 |
| 5       | 076     | 0      | 0702           | 0    |
| 6       | 056     | 0      | 0546           | 0    |
|         |         | 0764 A |                |      |
| 0764    | 777     | 7777   | 7777           | 0    |
| 5       | 777     | 0      | 7777           | 7777 |
| 6       | 0       | 0      | 0003           | 0    |
| 7       | 0       | 0001   | 0              | 0    |
| 0770    | 0       | 0001   | . 0            | 0001 |
| 1       | 0       | 0001   | 0001           | 0    |
| 2       | 0       | 0      | 0001           | 0    |
| 3       | 0       | 0      | 0              | 0001 |

between energy E and the summated number  $N_{\mathcal{E}}$  of earthquakes, exceeding a given value  $E_{\min}$  according to energy. To compute the quantity A in each averaging zone the common number of earthquakes is totaled independent of their energy level, i.e., all the earthquakes are given identical weight during summation. The summation method, compared to the distribution method, has some great advantages from the technological angle as well as of principle (Riznichenko, 1964; Riznichenko, Gorbunova, 1968). However, the experiment of computing a seismic activity map of Uzbekistan's interior (Zakhanova, Seiduzova, 1969) as well as outside its boundary (Riznichenko and others, 1969, 1970) shows that these advantages are realized only if there is uniform material of several years of instrumental observations. Its adoptation for small time intervals causes the main advantage of the summation method to almost vanish, that advantage is the possibility of computing strong earthquakes along with the numerous weak ones which are usually taken into account when computing activity by the distribution method. Strong earthquakes take place rarely, therefore, they are usually estimated by individual units on the epicenter maps during short periods of instrumental observations. If it is attempted to use all or, depending on the presentation, almost all known strong earthquakes in the region under investigation, then it is necessary to consider them during various time intervals, that is, in accordance with the presentation periods of earthquakes of each energy class. In this case, the first step to compute the activity map becomes very difficult viz., to determine the number of epicenters in the averaging zones. This itself does not lead to the technical advantage of the summation method, which appears mainly in the simplicity of fulfilling this particular step of constructing the activity map.

As shown in the literature (Gorbunova, Riznichenko, 1965; Riznichenko, Gorbunova, 1968), the activity maps computed by the distribution and summation methods, are identical, at least within the limits of computation errors.

But this situation may be correct only for the uniform distribution of earthquake epicenters of all representative energy classes along the area, which is usually noticed in long-term instrumental observations. The maps of earthquake epicenters during short periods often have a peculiarity, which is expressed in the advantageous timing of earthquakes of large and small K in the particular region. In several regions, e.g., Pritashkent, and according to materials from relatively long-term observations, weak earthquakes are associated with one geological structure, whereas stronger ones are related to others, depending on the history of their tectonic development.

In similar cases, seismic activity maps would differ in the level as well as in the configuration of isolines A depending on the construction method. Besides, the use of the summation method gives here a distorted picture of the activity of different zones, partly of different geological structures. Actually, if earthquake epicenters with  $K \ge 8$  correspond to one structure and with  $K \ge 10$  to another and their total numbers  $N_E$  are somewhat identical, then other conditions remaining the same and the values of  $\gamma$ , Tand S,  $K_{\min}$ ,  $K_0$  remaining the same in expression (37), the seismic activity value in the limits of both structures would be identical. The classwise distribution method, however, would give considerably higher activity level on the second structure, which seems physically to be more correct. It seems that the distribution method is more correctly used here, rather than the summation method.

Computing the activity map by the distribution method is a very difficult operation. In accordance with expression (41), it demands a partial computation of the number of earthquakes of each energy class for each point of the map. Therefore, it seems, machine computation makes a sense here. The SP-4 program makes it possible to compute a seismic activity map by the classwise earthquake distribution method with constant resolution.

Initial data of the program are given by two sets  $M_1$  and  $M_2$  and a row of control information, the contents of which are analogous to those of SP-1,

2, and 3. The SP-4 program itself engages 177 memory cells—from 0500 through 0677. Cells 0700-1000 are used for the second set of initial data  $M_2$  and control information. Cells 1010-1100 are a working scratch area and in them are recorded intermediate results while the program is running. Cells 1101-6152 store the main set of initial data, i.e., the set of epicenters  $M_1$ .

# Block Diagram SP-4 (see p. 68)

The work of the program takes place according to the block diagram and begins with the entry of the initial data to the memory. Thereafter control is given to the beginning of the computation—block 1, where the row of instructions is formed using control information. In block 2 the initial data are converted from the decimal system to the binary. In blocks 3–12 the values of seismic activity  $A_{K_0}$  according to energy class  $K_0$  are computed for the corresponding map.

The formula for the computation is similar to (41) and in general is expressed in the following manner:

$$A_{K_{0}} = \frac{\sum_{K=K_{\min}}^{K_{\max}} N_{K}^{2} \cdot C_{K_{0}}^{K_{0}} \cdot \frac{1000}{S \cdot T_{\min}}}{\sum_{K=K_{\min}}^{K_{\max}} N_{K}}, \qquad (42)$$

where  $N_K$ —number of class K earthquakes taking place during  $T_{\min}$  years in the area S km<sup>2</sup>;

 $C_{K}^{K_{0}}$ —coefficient of activity transfer from class K to the activity according to class  $K_{0}$ , where K may change from the value  $K_{\min}$  to  $K_{\max}$  from the number of earthquake energy classes presented in the region under study.

In block 3 the coefficients  $C_K^{K_0}$  are computed, that is, using the SP-4 program to determine the seismic activity for any energy class  $K_0$ , with any interval of the energy classes K of the initial sets of epicenters— $K_{f_j}$  (j = 1, 2, 3, ... p). The computation of coefficients  $C_K^{K_0}$  is carried out in accordance with the curve of earthquake repeatability according to the formula:

$$C_{K}^{K_{0}} = \frac{n_{K_{0}}}{n_{K}} = 10^{\gamma \ (K-K_{0})}.$$
(43)

The computed coefficients  $C_{K_0}^{K_0}$ , the number *P* of which are put into the working cell, are stored up to the automatic computation of seismic activity.

With the work of first three blocks the preparatory operations are completed; these are common for all points of the future map. Beginning from block 4, all succeeding operations are carried out for each point.

In block 4 the addresses of the cells are loaded to select the epicenters. Control is then given to block 5 where the coordinates of the initial points of computation are entered and coordinates are formed limiting the averaging zone of activity around this point. Further the coordinates of all epicenters of the initial sets are analyzed for their affiliation to the averaging zone and only those which are inside it are selected. In block 6 the addresses of the identification block for earthquakes of energy class  $K_i$  of the initial sets are loaded. Construction of this block considers the variation of the epicenter addresses, since all the *m* epicenters of the initial data set are analyzed. The subsequent loading of the initial addresses is needed to repeat the operation for each computation point.

Control is shifted from block 6 to block 7, which analyzes or rectifies the energy class K of each earthquake, the epicenter of which is in the averaging zone. The value  $K_i$  is compared, for this purpose, with the values of each  $K_{fj}$  from the list of energy classes of the representative earthquake as given in the second set of initial data. When  $K_i = K_{fj}$  the number of earthquakes of each energy class is summated from the set of those presented—  $K_{fj}$ , i.e., the number  $N_K$  of the numerator in formula (42) is formed and is related to the corresponding K.

Since the periods of the representative earthquakes of the various classes of seismic energy may not be uniform, they are brought to a single observation period  $T_{min}$  in block 7, which is the least of the representative classes  $K_{min}$  for the earthquakes of the region, in accordance with the expression:

$$N_K = n_{K_{f_j}} \frac{T_{\min}}{T_{f_j}},$$

where  $n_{K_{f_i}}$ —total earthquakes of energy class  $K_{f_i}$  in the averaging zone dur-

ing the observation period  $T_{f_j}$ ,

 $N_{K}$ —total earthquakes of energy class  $K = K_{f_{j}}$  in the averaging zone during the observation period T.

Next control is shifted to block 8 where the number of chosen epicenters of various K are summated to form the denominator  $N_{\Sigma}$  in formula (42)

$$N_{\mathcal{E}} = \sum_{K=K_{\min}}^{K_{\max}} N_{K}$$

Here, of course, the number  $N_{\Sigma}$  is the total of earthquake epicenters of any K within the averaging zone of activity, the number of which is brought to the observation period  $T_{\min}$ , and is compared with the already given number  $N_{o}$ , which defines the required accuracy of the computation of A. When  $N_{\Sigma}$  is less than  $N_{\sigma}$  control is shifted from block 8 to printing block 10, wherein printing buffer  $N_{T_{\text{pri}}}$ ,  $A_{\text{pri}}$  and  $\sigma_{A_{\text{pri}}}$  are input with the following values: N of the point, 0 and 100%, respectively. In this case, the number of epicenters  $N_{\Sigma}$  appears to be very small for computing activity with the desired accuracy, therefore, A is considered equal to 0, whereas the error  $\sigma_A = 100\%$ . When  $N_{\Sigma} \ge N_{\sigma}$  control is shifted from block 8 to block 9, where  $A_{K_0}$  and  $\sigma_A$  are computed for the point under study in accordance with (42) and (39) and control is shifted to printing block 11, where the computation results are printed. Thereafter control is shifted to block 12, to prepare for the computation of A in the next point. Here its coordinates are formed and control is again shifted to block 4, etc. The computation process is repeated  $q \cdot r$  times and the program is stopped.

The SP-4 program is standard—it may be used to compute seismic activity A by the distribution method on any territory, with any step of computations, dimensions of the averaging zones of any earthquake energy class and with any specified accuracy of the computation of A.

#### **Illustrative Eaxmple**

To test the SP-4 program an example is formed with sets of the initial data  $M_1$ ,  $M_2$ , group of control information and computation results. It may be used as a check-out version of SP-4. The set  $M_1$  includes the parameters of 20 earthquakes and occupies cells 1100-1173 (Table 11). These parameters are the same as for the sets  $M_1$  of the previous SP-1, 2, and 3 programs.

Set  $M_2$  is meant for the seismic region parameters of the region under investigation and constants of the computation (Table 12). Here eleven cells 0710-0722 are kept for the energy classes of the representative earthquakes  $K_{f_j}$ , out of which only the first five are engaged in this example—0710-0714. In accordance with the number  $K_{f_j}$ ; five successive cells 0723-0727 are used by the numbers  $T_{f_j}$ . The parameters in cells 0736-0753 are normally the same (see Tables 2, 6 and 8). The control information (Table 13) uses cells 0777-1003 where  $A_{mn}$  is the number of the last cell of the set  $M_1$ ; *P*—number of presented earthquake classes, and *q* and *r*—number of lines and columns of the resulting matrix  $A_{qr}$ , *m*—number of lines of the initial matrix. Table 14 shows the results of the computation of seismic activity.

Here the values  $A_{10}$  for two columns of the maps are brought;  $N_T$ —serial number of the point;  $\sigma_A$ —error of computation of A (%); *n*—number of epicenters in the averaging zone of activity.

# PROGRAM SP-5 FOR COMPUTING CURVES OF EARTHQUAKE REPEATABILITY

The law of earthquake repeatability expressing the dependence between the number of earthquakes and their seismic energies is described by a linear •

# TABLE 11. DATA SET M<sub>1</sub> FOR SP-4

| •••• ••• ••• ••• ••• • |              | c     | ommands | and numb         | <br>ers        |       |                           |
|------------------------|--------------|-------|---------|------------------|----------------|-------|---------------------------|
| Address                | Sig          | m of  | 0.1     |                  | <b>-</b>       |       | Remarks                   |
|                        | No.          | Order | Order   | $\mathbf{A}_{1}$ | $\mathbf{A}_2$ | $A_3$ |                           |
|                        |              |       |         | 1100 A           |                |       |                           |
| 1100                   | ++           | +     | 02      | 110              | 000            | 000   | $K_1 = 11$                |
| 1                      | ++           | +-    | 02      | 400              | 100            | 000   | $\varphi_1 = 40.01$       |
| 2                      | + +          | +     | 02      | 690              | 510            | 000   | $\lambda_1 = 69.51$       |
| 3                      | ++           | +     | 02      | 100              | 000            | 000   | $K_2 = 10$                |
| 4                      | ++           | +     | 02      | 407              | 100            | 000   | $\varphi_2 = 40.71$       |
| 5                      | ++           | +     | 02      | 695              | 100            | 000   | $\lambda_3 = 69.51$       |
| 6                      | ++           | +     | 02      | 107              | 000            | 000   | $K_3 = 10$                |
| 7                      | ++           | +     | 02      | 406              | 100            | 000   | $\varphi_3 = 40.71$       |
| 1110                   | + +-         | +     | 02      | 695              | 100            | 000   | $\lambda_s = 69.51$       |
| 1                      | ++           | +     | 02      | 100              | 000            | 000   | $K_4 = 10$                |
| 2                      | ++           |       | 02      | 400              | 100            | 000   | $\varphi_4 = 40.01$       |
|                        |              |       |         | 1113 A           |                |       |                           |
| 1113                   | -1+-         | +     | 02      | 696              | 100            | 000   | $\lambda_4 = 69.61$       |
| 4                      | ++           | +     | 02      | 110              | 000            | 000   | $K_{5} = 11$              |
| 5                      | ++           | +     | 02      | 401              | 100            | 000   | $\varphi_5 = 40.11$       |
| 6                      | ++           | -+-   | 02      | 695              | 100            | 000   | $\lambda_5 = 69.51$       |
| 7                      | ++           | -+-   | 02      | 120              | 000            | 000   | $K_{6} = 12$              |
| 1120                   | ++           | -+-   | 02      | 401              | 100            | 000   | $\varphi_{0} = 40.11$     |
| 1                      | - -+         | +     | 02      | 695              | 100            | 000   | $\lambda_{\rm s} = 69.51$ |
| 2                      | - <b>  -</b> | +     | 02      | 110              | 000            | 000   | $K_7 = 11$                |
| 3                      | -1-+         | +     | 02      | 401              | 100            | 000   | $\varphi_{7} = 40.11$     |
| 4                      | ++           | +     | 02      | 697              | 100            | 000   | $\lambda_2 = 69.71$       |
| 5                      | ++           | -]-   | 01      | 900              | 000            | 000   | $K_8 = 9$                 |
|                        |              |       |         | 1126 A           |                |       |                           |
| 1126                   | ++           | +     | 02      | 407              | 100            | 000   | $\varphi_8 = 40.71$       |
| 7                      | +- -         | . +   | 02      | 695              | 100            | 000   | $\lambda_{s} = 69.51$     |
| 1130                   | ++           | -[ ·  | 01      | 900              | 000            | 000   | $K_9 = 9$                 |
| 1                      | ++           | +     | 02      | 400              | 100            | 000   | <i>𝒫</i> ,==40.01         |
| 2                      | ++           | +     | 02      | 695              | 100            | 000   | $\lambda_9 = 69.51$       |
| 3                      | ++           | +     | 02      | 100              | 000            | 000   | $K_{10} = 10$             |
| 4                      | +-+-         | +     | 02      | 401              | 500            | 000   | $\varphi_{10} = 40.15$    |
| 5                      | ++           | +     | 02      | 696              | 100            | 000   | $\lambda_{10} = 69.61$    |
| б                      | ++           | · +-  | 01      | 900              | 000            | 000   | $K_{11} = 9$              |
| 7                      | ++           | +     | 02      | <b>40</b> 1      | 500            | 000   | $\varphi_{11} = 40.15$    |
| 1140                   | ++           | +     | 02      | 698              | 700            | 000   | $\lambda_{11} = 69.87$    |
|                        |              |       |         | 1141 A           |                |       |                           |
| 1141                   | ++           | +     | 02      | 100              | 000            | 000   | $K_{12} = 10$             |
| 2                      | ++           | +     | 02      | 401              | 500            | 000   | $\varphi_{12} = 40.15$    |
| 3                      | ++           | -+-   | 02      | 697              | 500            | 000   | $\lambda_{12} = 69.75$    |
| 4                      | ++           | +-    | 02      | 100              | 000            | 000   | $K_{13} = 10$             |
| 5                      | ++           | +     | 02      | 400              | 100            | 000   | <b>\$\$</b> _{13}=40.01   |
| 6                      | ++           | +     | 02      | 695              | 800            | 000   | $\lambda_{13} = 69.58$    |

|         |     | Co    | mmands | and numbe | ers    |        |                        |
|---------|-----|-------|--------|-----------|--------|--------|------------------------|
| Address | Sig | gn of | Order  | <br>A.    | <br>A. | <br>A. | Remarks                |
|         | No. | Order |        |           |        |        | ·                      |
|         |     |       |        | 1147 A    |        |        |                        |
| 7       | +++ | +     | 01     | 900       | 000    | 000    | $K_{14} = 9$           |
| 1150    | ++  | +-    | 02     | 409       | 500    | 000    | $\varphi_{14} = 40.95$ |
| 1       | ++  | +     | 02     | 695       | 100    | 000    | $\lambda_{14} = 69.51$ |
| 2       | ÷   | +     | 01     | 900       | 000    | 000    | $K_{15} = 9$           |
| 3       | ++  | +     | 02     | 400       | 100    | 000    | $\varphi_{15} = 40.01$ |
| 1154    | ++  | +     | 02     | 695       | 700    | 000    | $\lambda_{15} = 69.57$ |
| 5       | ++  | 4-    | 01     | 900       | 000    | 000    | $K_{16} = 9$           |
| 6       | ++  | ÷     | 02     | 408       | 100    | 000    | $\varphi_{16} = 40.81$ |
| 7       | ++  | +     | 02     | 695       | 800    | 000    | $\lambda_{16} = 69.58$ |
| 1160    | ++  | +     | 01     | 900       | 000    | 000    | $K_{17} = 9$           |
| 1       | ++  | + .   | 02     | 409       | 300    | 000    | $\varphi_{17} = 40.93$ |
| 2       | ++  | +     | 02     | 693       | 100    | 000    | $\lambda_{17} = 69.31$ |
| 3       | ++  | +     | 01     | 900       | 000    | 000    | $K_{18} = 9$           |
| 4       |     | ÷     | 02     | 406       | 100    | 000    | $\varphi_{18} = 40.61$ |
| 5       | ++  | 4.    | 02     | 696       | 100    | 000    | $\lambda_{18} = 69.61$ |
| 6       |     | +     | 02     | 100       | 000    | 000    | $K_{19} = 10$          |
|         |     |       |        | 1167 A    |        |        |                        |
| 1167    | ++  | +-    | 02     | 401       | 500    | 000    | $\varphi_{19} = 40.15$ |
| 1170    | ++  | -+-   | 02     | 697       | 700    | 000    | $\lambda_{19} = 69.77$ |
| 1       | ++  | +     | 01     | 900       | 000    | 000    | $K_{20} = 9$           |
| 2       | ++  | +     | 02     | 402       | 200    | 000    | $\varphi_{20} = 40.22$ |
| 3       | +++ | +     | 02     | 697       | 700    | 000    | $\lambda_{20} = 69.77$ |

# TABLE 12. DATA SET M<sub>2</sub> FOR SP-4

|         |     | C     | ommands | and numbe | rs    |     |                  |
|---------|-----|-------|---------|-----------|-------|-----|------------------|
| Address | Sig | n of  | Order   |           |       | ·   | Remarks          |
|         | No. | Order | Order   | $A_1$     | $A_2$ | A3  |                  |
|         |     |       |         | 0710 A    |       |     |                  |
| 0710    | ++  | +     | 01      | 900       | 000   | 000 | $K_{f_1} = 9$    |
| 1       | ++  | +     | 02      | 100       | 000   | 000 | $K_{t_0} = 10$   |
| 2       | ++  | +     | 02      | 110       | 000   | 000 | $K_{f_{3}} = 11$ |
| 3       | ++  | +     | 02      | 120       | 000   | 000 | $K_{f_{a}} = 12$ |
| 4       | ++  | +     | 02      | 130       | 000   | 000 | $K_{f_{r}} = 13$ |
| 5       | ++  | +     | 00      | 000       | 000   | 000 | a                |
| 6       | ++  | +     | 00      | 000       | 000   | 000 |                  |
| 7       | ++  | +     | 00      | 000       | 000   | 000 |                  |
|         |     |       |         |           |       |     | (Contd.)         |

TABLE 12 (Contd.)

|         |                                 | Co        | mmands a    | nd numbe       |                   |                |                     |
|---------|---------------------------------|-----------|-------------|----------------|-------------------|----------------|---------------------|
| Address | Sig                             | <br>gn of |             |                | · · · · · · · · · |                | Remarks             |
|         | No.                             | Order     | - Order     | A <sub>1</sub> | A <sub>2</sub>    | A <sub>3</sub> |                     |
| 0720    | ++                              | +         | 00          | 000            | 000               | 000            |                     |
| 1       | ++                              | +         | 00          | 000            | 000               | 000            |                     |
| 2       | ++                              | 4-        | 00          | 000            | 000               | 000            |                     |
|         |                                 |           | 0           | 723 A          |                   |                |                     |
| 0723    | ++                              | +         | 01          | 850            | 000               | 000            | $T_{1} = 8.5$       |
| 4       | +-+-                            | +         | 02          | 180            | 000               | 000            | $T_{t_{s}} = 18$    |
| 5       | ++                              | +-        | 02          | 180            | 000               | 000            | $T_{t_{0}} = 18$    |
| 6       | ++                              | +-        | 02          | 180            | 000               | 000            | $T_{f_4} = 18$      |
| 7       | ++                              |           | 02          | 400            | 000               | 000            | $T_{f_{s}} = 40$    |
| 0730    | ++                              | +         | 00          | 000            | 000               | 000            | 5                   |
| 1       | +- <b></b> -                    | +         | 00          | 000            | 000               | 000            |                     |
| 2       | ++                              | +-        | <b>00</b> · | 000            | 000               | 000            |                     |
| 3       | ++                              | +         | 00          | 000            | 000               | 000            |                     |
| 4       | ++                              | +         | 00          | 000            | 000               | 000            |                     |
| 5       | ++                              | +         | 00          | 000            | 000               | 000            |                     |
|         |                                 |           | 0           | 736 A          |                   |                |                     |
| 0736    | ++                              | -+-       | 01          | 500            | 000               | 000            | P=5                 |
| 7       | ++                              | +         | 02          | 401            | 000               | 000            | $\varphi_0 = 40.1$  |
| 0740    | +++                             | +         | 02          | 696            | 000               | 000            | $\lambda_0 = 69.6$  |
| 1       | ++                              | +         | 01          | 850            | 000               | 000            | $T_{\rm pr} = 8.5$  |
| 2       | ++                              | +         | 03          | 352            | 000               | 000            | S=352               |
| 3       | ++                              | +         | 00          | 500            | 000               | 000            | const = 0.5         |
| 4       | ++                              | +         | 02          | 100            | 000               | 000            | const=10            |
| 5       | ++                              | +         | 00          | 100            | 000               | 000            | $a_{\omega}=0.1$    |
| 6       | - <del> -</del> - <del> -</del> | +         | 00          | 100            | 000               | 000            | $a_{\lambda} = 0.1$ |
| 7       | ++                              |           | 00          | 500            | 000               | 000            | const=0.5           |
| 0750    | ++                              | +         | 03          | 100            | 000               | 000            | const = 100         |
|         |                                 |           | (           | 0751 A         |                   |                |                     |
| 0751    | <del>- -</del> - <del> -</del>  | -+-       | 04          | 100            | 000               | 000            | $S_0 = 1000$        |
| 2       | ++                              | +         | 00          | 434            | 290               | 000            | 1=0.43429           |
| 3       | ++                              | +         | 01          | 100            | 000               | 000            | $N_{\sigma} = 1$    |

# TABLE 13. CONTROL INFORMATION FOR SP-4

| A       | (       | Commands       | and numbers |                | Den È            |
|---------|---------|----------------|-------------|----------------|------------------|
| Address | Command | A <sub>1</sub> | A2          | A <sub>3</sub> | Remarks          |
|         |         | (              | 0777 A      |                |                  |
| 0777    | 000     | 0000           | 0000        | 1173           | $(0, 0, A_{mn})$ |
| 1000    | 000     | 0004           | 0000        | 0000           | (p-1, 0, 0)      |
| 1       | 000     | 0010           | 0000        | 0000           | (q-1, 0, 0)      |
| 2       | 000     | 0010           | 0000        | 0000           | (r-1, 0, 0)      |
| 3       | 000     | 0023           | 0000        | 0000           | (m-1, 0, 0)      |

| $N_T$              | A10                                   | 𝐾 <sub>A</sub>   | n                 |
|--------------------|---------------------------------------|------------------|-------------------|
| +++ 01 10000000    | +++ 01 131071840                      | +++ 02 454858826 | +++ 01 80000000   |
| +++ 01 20000000    | +++ 00 935143140                      | +++ 02 643267520 | +++ 01 40000000   |
| +++ 01 300000000   | ++- 00 105689842                      | +++ 03 10000000  | +++ 01 10000000   |
| +++ 01 40000000    | +++ 00 000000000                      | ++++03 10000000  | +++ 00 00000000   |
| +++ 01 500000000   | +++ 00 000000000                      | +++ 03 100000000 | +++ 00 000000000  |
| +++ 01 60000000    | ++- 00 105689842                      | +++ 03 10000000  | +++ 01 100000000  |
| +++ 01 700000000   | ++- 00 357986887                      | +++ 02 582771517 | +++ 01 40000000   |
| +++ 01 80000000    | ++- 00 357986887                      | +++ 02 582771517 | +++ 01 40000000   |
| +++ 01 90000000    | ++- 00 211379685                      | +++ 02 707106781 | +++ 01 200000000  |
| $+++02\ 100000000$ | ++- 00 105689842                      | +++ 03 10000000  | +++ 01 10000000   |
| +++ 02 110000000   | +++ 00 000000000                      | +++ 03 10000000  | +++ 00 00000000   |
| +++02 120000000    | +++ 00 000000000                      | +++ 03 100000000 | +++ 00 000000000  |
| +++ 02 130000000   | ++++ 00 00000000                      | +++03 100000000  | ++++ 00 00000000  |
| +++ 02 140000000   | +++ 00 000000000                      | +++ 03 10000000  | +++ 00 000000000  |
| +++ 02 15000000    | +++ 00 00000000                       | +++ 03 100000000 | ++++ 00 000000000 |
| +++ 02 160000000   | +++0000000000000000000000000000000000 | +++ 03 100000000 | +++ 00 000000000  |
| +++ 02 17000000    | +++ 00 00000000                       | +++ 03 10000000  | +++ 00 00000000   |
| +++ 02 18000000    | +++ 00 00000000                       | +++03 100000000  | +++ 00 00000000   |

TABLE 14. RESULTS OF COMPUTATION OF A10 ACCORDING TO SP-4

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number of earthquakes  $N_K$  around the area and time an expression is obtained for the seismic activity of class K, i.e.,  $A_K$  (11). Then  $N_0 \equiv A_0$ , i.e., seismic activity, corresponding to class  $K = K_0$ . The parameters of the repeatability curve  $A_0$  and  $\gamma$  signify its level and inclination and are obtained by the method of least squares. The mean square errors of these values— $\sigma_A$ and  $\sigma_\gamma$ —are also computed in the same manner.

Arising out of the proposed linearity of the curves of earthquake repeatability, the quantity  $\gamma$  is computed as a tangent of inclination angle to the axis of abscissa, built in the coordinates  $K = \log E$  and  $\log N^*$ :

$$\log N^* = A_0 + \gamma K. \tag{44}$$

Here  $N^*$ —number of earthquakes of a particular K brought to the unit area and time. Having a system of linear equations (44), the coefficients of the straight line  $\gamma$  and  $A_0$  are found using determinants

$$\gamma = \frac{\begin{vmatrix} \sum (K \log N^*) & \sum K \\ \sum \log N^* & d \end{vmatrix}}{\begin{vmatrix} \sum K^2 & \sum K \\ \sum K & d \end{vmatrix}}.$$
 (45)

$$A_{0} = \frac{\begin{vmatrix} \sum K^{2} & \sum (K \cdot \log N^{*}) \\ \sum K & \sum \log N^{*} \end{vmatrix}}{\begin{vmatrix} \sum K^{2} & \sum K \\ \sum K & d \end{vmatrix}}.$$
 (46)

Here d is the number of equations used to construct the repeatability curve and determined by the range of presented energy classes—the so-called fixed classes  $K_{f_i}$ .

The intercept of the straight line (44) on the axis of ordinate, is characterized by the values  $A_0$ , and on the axis abscissa—by value  $b = A_0/\gamma$ , obtained from equation (44) with log  $N^* = 0$ . This value is convenient for the computation, although it may be devoid of physical sense (Butovskaya and others, 1966).

To compute the mean error of the points from the straight line equation (44) the following formula is used:

$$\sigma_{\gamma} = \sqrt{\frac{\left\{\sum \left[\log N^* - K \cdot \gamma + A_0\right]^2\right\} d}{\left|\sum_{K}^{K^2} \sum_{d}^{KK}\right| (d-2)}}.$$
(47)

The computation of the unknown quantities using formulas (45-47) by hand is very time consuming and difficult even if done only once. If these computations are repeated to establish temporal dependence, there is a PROGRAM SP-5

| Address | Command | A <sub>1</sub> | A <sub>2</sub> | A <sub>3</sub> |
|---------|---------|----------------|----------------|----------------|
|         |         | 0500 A         |                |                |
| 0500    | 055     | 0553           | 1054           | 0553           |
| 1       | 013     | 0553           | 1055           | 0502           |
| 2       | 055     | 0602           | 1054           | 0602           |
| 3       | 013     | 0602           | 1055           | 0602           |
| 4       | 055     | 0515           | 1060           | 0515           |
| . 5     | 013     | 0515           | 1061           | 0515           |
| 6       | 055     | 0517           | 1060           | 0517           |
| 7       | 013     | 0517           | 1062           | 0517           |
| 0510    | 055     | 0521           | 1060           | 0521           |
| 1       | 013     | 0521           | 1063           | 0521           |
| 2       | 055     | 0523           | 1060           | 0523           |
|         |         | 0513 A         |                |                |
| 0513    | 013     | 0523           | 1064           | 0523           |
| 4       | 0       | 0              | 0              | 0              |
| 5       | 016     | 0517           | 7741           | 0007           |
| 6       | 0       | 1000           | 1000           | 0              |
| 7       | 016     | 0521           | 7741           | 0007           |
| 0520    | 0       | 1013           | 1013           | 0              |
| 1       | 016     | 0523           | 7741           | 0007           |
| 2       | 0       | 1026           | 1026           | 0              |
| 3       | 016     | 0525           | 7741           | 0007           |
| 4       | 0       | 1041           | 1041           | 0              |
| 5       | 0       | 0              | 0              | 0              |
|         |         | 0526 A         |                |                |
| 0526    | 052     | 0              | 0              | 0              |
| 7       | 075     | 0              | 0.             | 6000           |
| 0530    | 075     | 0              | 0              | 6001           |
| 1       | 075     | 0              | 0              | 6002           |
| 2       | 075     | 0              | 0              | 6003           |
| 3       | 075     | 0              | 0              | 6004           |
| 4       | 0       | 0              | 0              | 0              |
| 5       | 405     | 1041           | 1000           | 6010           |
| 6       | 004     | 1003           | 6010           | 6010           |
| 7.      | 275     | 0              | 1026           | 6005           |
| 0540    | 105     | 6005           | 6010           | 6026           |
|         |         | 0541 A         |                |                |
| 0541    | 275     | 0              | 6026           | 0146           |
| 2       | 016     | 0543           | 7714           | 0007           |
| 3       | 0       | 0              | 0              | 0              |
| 4       | 105     | 0160           | 1004           | 604            |
| 5       | 605     | 1013           | 6041           | 6011           |
| 6       | 001     | 6001           | 6011           | 6011           |
| 7       | 201     | 6002           | 6041           | 6002           |

(Contd.)

| Address      | Command     | A1     | $A_2$ | $A_3$ |
|--------------|-------------|--------|-------|-------|
| 0550         | 201         | 6003   | 1013  | 6003  |
| 1            | 605         | 1013   | 1013  | 6012  |
|              |             | 0552 A |       |       |
| 2            | 001         | 6004   | 6012  | 6004  |
| 3            | 112         | 0      | 0535  | 0001  |
|              | ***         | 0554 4 | 0555  | 0001  |
|              | 00 <i>f</i> | 0554 A | 1001  | (010  |
| 0554         | 005         | 6001   | 1001  | 6013  |
| 5            | 005         | 6002   | 6003  | 6014  |
| 6            | 005         | 6004   | 1001  | 6015  |
| 0500         | 005         | 6003   | 6003  | 6010  |
| 0560         | 002         | 0013   | 6014  | 6013  |
| 1            | 002         | 6013   | 6010  | 6011  |
| • 2          | 004         | 6013   | 6011  | 6013  |
| 3            | 075         | 6004   | 6003  | 50021 |
| 4            | 005         | 6001   | 6002  | 5002  |
| 5            | 003         | 6007   | 6003  | 6002  |
| 0            | 002         | 0002   | 0001  | 0002  |
|              |             | 0567 A |       |       |
| 0567         | 004         | 6002   | 6011  | 6012  |
| 0570         | 075         | 0      | 6012  | 6022  |
| 1            | 004         | 6022   | 6013  | 6012  |
| 2            | 075         | 0      | 6012  | 6023  |
| 3            | 052         | 0      | 0     | 0     |
| 4            | 075         | 0      | 0     | 6001  |
| 5            | 405         | 1013   | 6013  | 6017  |
| 6            | 001         | 6017   | 6022  | 6017  |
| 7            | 202         | 6017   | 6041  | 6017  |
| 0600         | 005         | 6017   | 6017  | 6017  |
| . <b>.</b> . | 001         | 6001   | 6017  | 6001  |
|              | •           | 0602 A |       |       |
| 0602         | 112         | 0      | 0575  | 1000  |
| 3            | 005         | 6001   | 1001  | 6001  |
| 4            | 002         | 1001   | 1002  | 6020  |
| 5            | 005         | 6001   | 6020  | 6011  |
| 6            | 004         | 6001   | 6011  | 6011  |
| 7            | 044         | 6011   | 0     | 6011  |
| 0610         | 075         | 0      | 6011  | 6024  |
| 1            | 005         | 6023   | 1005  | 6006  |
| 2            | 005         | 6022   | 1005  | 6007  |
| 3            | 005         | 6007   | 1006  | 6054  |
| 4            | 005         | 6006   | 6007  | 6007  |
|              |             | 0615 A |       |       |
| 0615         | 002         | 6054   | 6007  | 6007  |
| 6            | 004         | 6007   | 6006  | 6025  |
| 7            | 016         | 0621   | 7751  | 0007  |
| 0670         | 0           | 6021   | 4000  | 6025  |

| Address | Command | $A_1$  | A <sub>2</sub> | $A_3$      |
|---------|---------|--------|----------------|------------|
|         |         | 0621 A |                |            |
| 1       | 077     | 0      | 0              | 0          |
| 2       | 0       | 0      | 0              | 0          |
| ĩ       | 0       | Ő      | 0001           | \ <b>0</b> |
| 4       | 0       | 0001   | . 0            | 0001       |
| 5       | 777     | 0      | 7777           | 7777       |
| 6       | 777     | 7777   | 7777           | 0          |
| 7       | 0       | 0001   | 0              | 0          |
| ,       | Ũ       | 0630 A |                | Ŭ          |
| 0630    | 002     | 1056   | 0101           | 0          |
| 1       | 002     | 0.01   | 0635           | 0          |
| 1       | 0/0     | 1057   | 0055           | 0          |
| 2       | 002     | 0700   | 0101           | 0525       |
| 3<br>1  | 010     | 0700   | 0500           | 0525       |
| 4       | 050     | 0643   | 0500           | 0642       |
| 5       | 033     | 0642   | 1020           | 0642       |
| 07      | 013     | 0042   | 0625           | 0672       |
| 000     | 055     | 0673   | 1060           | 0673       |
| 0640    | 015     | 0075   | 7741           | 0073       |
| 2       | 016     | 1000   | 1100           | 0007       |
| 2       | 000     | 1000   | 1100           | 0          |
|         |         | 0643 A |                |            |
| 0643    | 016     | 0645   | 7741           | 0007       |
| 4       | 000     | 1000   | 1000           | 1053       |
| 5       | 056     | 0646   | 0652           | 0652       |
| 6       | 075     | -0     | 1100           | 1077       |
| 7       | 0       | 0      | 0              | 0          |
| 0650    | 013.    | 0652   | 1066           | 0652       |
| 1       | 0       | . 0    | 0              | 0          |
| . 2     | 077     | 0      | 0              | 0          |
| 3       | 052     | 0      | 0              | 0          |
| 4       | 175     | 0      | 0              | 1026       |
| 5       | 112     | 0012   | 0667           | 0001       |
|         |         | 0656 A |                |            |
| 0656    | 002     | 1011   | 1007           | 1076       |
| 7       | 056     | 0660   | 0661           | 0666       |
| 0660    | 002     | 1077   | 1013           | 0          |
| 1       | 056     | 0662   | 0666           | 0672       |
| 2       | 001     | 1026   | 0101           | 1026       |
| 3       | 0       | 0      | 0              | 0          |
|         |         | 0664 A |                |            |
| 4       | 013     | 0701   | 0623           | 0701       |
| 5       | 013     | 0705   | 0624           | 0705       |
| 6       | 077     | 0      | 0              | 0          |
| 7       | 076     | 0      | 672            | 0          |
| 0670    | 002     | 1076   | 0101           | 1076       |
|         |         |        |                | (Contd)    |
|         |         |        |                | 100/110    |

| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | Address | Command | Å <sub>1</sub> | A <sub>2</sub> | A <sub>3</sub> |  |  |  |
|---|---------|---------|----------------|----------------|----------------|--|--|--|
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 0671 A  |         |                |                |                |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0671    | 076     | 0              | 0666           | 0              |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 2       | 077     | 0              | 0              | 0              |  |  |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 3       | 112     | 0              | 0650           | 0001           |  |  |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 4       | .016    | 0675           | 0500           | 0514           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 5       | 002     | 1067           | 0101           | 0              |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 6       | 076     | 0              | 0700           | 0              |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 7       | 056     | 0              | 0526           | 0              |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0700    | 052     | 0              | 0              | 0              |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 1       | 075     | 0              | 0              | 0              |  |  |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 2       | 075     | 0              | 0              | 6001           |  |  |  |
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $  | 3       | 075     | 0              | 0              | 6002           |  |  |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 0704 A  |         |                |                |                |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0704    | 075     | 0              | 0              | 6003           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 5       | 075     | 0              | 0              | 6004           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 6       | 401     | 1026           | 6000           | 6000           |  |  |  |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$   | 7       | 405     | 1041           | 1000           | 6010           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 0710    | 004     | 1003           | 6010           | 6010           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 1       | 075     | 0              | 6000           | 6005           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 2       | 105     | 6005           | 6010           | 6026           |  |  |  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | 3       | 275     | 0              | 6026           | 0140           |  |  |  |
| 5         0         0         0         0           6         105         0160         1004         6041           0717 A           0717         605         1013         6041         6011           0720         001         6001         6011         6001           1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004 | 4       | 016     | 0543           | 7714           | 0007           |  |  |  |
| 6         105         0160         1004         6041           0717         605         1013         6041         6011           0720         001         6001         6011         6001           1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004  | 5       | 0       | 0              | 0              | 0              |  |  |  |
| 0717 A         605         1013         6041         6011           0720         001         6001         6011         6001           1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004   | 6       | 105     | 0160           | 1004           | 6041           |  |  |  |
| 0717         605         1013         6041         6011           0720         001         6001         6011         6001           1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004   |         |         | 0717 A         |                |                |  |  |  |
| 0720         001         6001         6011         6001           1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004   | 0717    | 605     | 1013           | 6041           | 6011           |  |  |  |
| 1         201         6002         6041         6002           2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004   | 0720    | 001     | 6001           | 6011           | 6001           |  |  |  |
| 2         201         6003         1013         6003           3         605         1013         1013         6012           4         001         6004         6012         6004  | 1       | 201     | 600 <b>2</b>   | 6041           | 6002           |  |  |  |
| 3         605         1013         1013         6012           4         001         6004         6012         6004   | 2       | 201     | 6003           | 1013           | 6003           |  |  |  |
| 4 001 6004 6012 6004  | 3       | 605     | 1013           | 1013           | 6012           |  |  |  |
|   | 4       | 001     | 6004           | 6012           | 6004           |  |  |  |
| 5 112 0 0534 0001   | 5       | 112     | 0              | 0534           | 0001           |  |  |  |
| 6 056 0 0554 0  | 6       | 056     | 0              | 0554           | 0              |  |  |  |

considerable waste of time and labor. This work is considerably simplified with a computer. The SP-5 program computes the parameters of the earthquake repeatability and evaluates their errors on the basis of earlier computed numbers of earthquakes  $N_K$ , corresponding to various classes K, as usually done in long-hand calculations. It may also compute these numbers earlier, using as initial data the map or list of earthquake epicenters in the form of matrix  $A_{mn}$  (see SP-1, 2, 3, and 4). The use of the matrix  $A_{mn}$  is convenient even in the cases when, before the computation of the seismic activity map, it is necessary to fix the already existing value  $\gamma$  or compute it again for the same observation period as for map A. SP-5 program can compute the level of the repeatability curve  $A_{K_0}$  for any given class  $K_0$  of seismic energy and the values of  $\gamma$ ,  $A_0$  and  $\sigma_{\gamma}$ . Partially, with K = 10 one may find the average level of seismic activity  $A_{10}$  for the region under investigation, which, along with  $\gamma$ , is a main parameter for the seismic region.

For this purpose, the program records the equations of the repeatability curve in a straight line form, passing through two points with coordinates  $(0, A_0)$  and (b, 0):

$$\frac{K}{b} = \frac{\log N_K^* - A_0}{-A_0}.$$
 (48)

Entering the values of  $K = K_0$  in equation (48), one gets the value log  $N_K^* = \log A_{K_0}$  and further  $A_{K_0}$ .

The initial data for SP-5 are given by sets—mainly the same as for the previous program—and the row of control information. The first set  $M_1$ —matrix  $A_{mn}$ —formed automatically from the earthquake epicenters map, m—number of matrix lines determined by the number of earthquake epicenters of the region under study, n—number of characteristics of each epicenter, its geographical coordinates  $\varphi_i$  and  $\lambda_i$ , and  $K_i$ —earthquake energy class. It may be noted that only data about classes  $K_i$  are used in the SP-5 program, the coordinates  $\varphi_i$  and  $\lambda_i$  of the epicenters are not required. Therefore, in principle, the initial set may be given with n = 1, i.e., with information only about  $K_i$ . However, here arguments continue about the uses of the already codified and perforated matrix of epicenters  $A_{mn}$ , prepared for computing the repeatability curve and considerably reducing preparations for machine computation.

The second set of initial data  $M_2$  includes values needed to normalize the numbers  $N_K$  temporarily and spatially. Here, mainly are included parameters similar to those shown in previous programs. If it is necessary to compute the parameters of repeatability curves for already known numbers  $N_K$ , their values are also entered in the second set of initial data  $M_2$ .

Control information is the volume of initial set and some cell addresses necessary to form program instructions. The SP-5 program itself occupies cells 0500-0726 of the memory, set  $M_2$  and control information are in cells 1000-1077.

The set  $M_1$  may occupy memory cells beginning from 1100-5777. Cells 6000-6177 are kept aside for working, printing, and storing the intermediate computation results.

# Block Diagram SP-5 (see p. 101)

The SP-5 program takes place as seen in the block diagram. The indexing cell  $M_1$  is analyzed in block 1 which already contains numbers 1 and 0. When  $\mu_1 = 1$  control is shifted for the first part of the program (Blocks 2-6), which computes the classwise numbers  $N_{K_j}$  of earthquakes based on the initial set of epicenters  $M_1$ . In block 2, the addresses of block 3-6 are formed. Control is shifted to block 3, where the parameters of the earthquake epicenters are transformed from decimal to binary system.

In block 4 are loaded the addresses of the instructions for the analysis of epicenter energy classes and the automatic computation of numbers  $N_{K_i}$ .

Block 5 analyzes the energy classes of all *m* earthquakes which are given in the initial matrix  $A_{mn}$  ( $M_1$ ). When  $K_i = K_{f_j}$  control is shifted from block 5 to block 6 which computes the classwise number  $N_{K_j}$ . From block 6, control is shifted again to block 4 to load the addresses of block 5 and then on to block 5, where the value  $K_{i_n} = K_{f_j}$  is chosen for the following analysis. This goes on until all the energy classes of all epicenters of the initial set are identified and the numbers  $N_{K_j}$  corresponding to it are summated. Then control is shifted to block 7, where are formed the addresses of some instructions for blocks 8-15.

Block 7 is the first block of second part of the program in which is conducted the automatic computation of the parameters of the repeatability curves. The second part of the program may work independently; in this case, control is shifted straight from block 1 to block 7, if  $\mu_1 = 0$ —when the earthquake class numbers  $N_{K_j}$  are given in the set  $M_2$ . After compiling the addresses, control is shifted from block 7 to block 8, where the numbers are converted from decimal to binary, included in the second set  $M_2$ with the numbers  $N_{K_j}$ . If control to block 7 is shifted to block 6, i.e., the first part of the program has worked, then the numbers  $N_{K_j}$  from the conversion from decimal to binary are bypassed, since these numbers have already been input to the memory in binary-octal code.

Further the control is shifted to block 9 which determines the distribution density of the numbers of earthquakes  $N_{K_{f}}^{\bullet}$ . For this purpose, the number  $N_{K}$  is normalized for 1,000 km<sup>2</sup> area and one year.

In block 10, the index cell  $\mu_2$  is analyzed, in which the number 0 or 1 was put earlier, indicating the method of computing the repeatability curve —by distribution ( $\mu_2 = 0$ ) or by summation ( $\mu_2 = 1$ ). When  $\mu_2 = 0$ , control is shifted to block 11, where the function of the distribution of  $N_{K_j}^*$  about  $K_{f_j}$  is computed and a system of linear equations (44) is formed. This is equal to P', i.e., the number  $K_{f_j}$  in the region under investigation.

When  $\mu_2 = 1$  control is shifted from block 10 to block 12 to compute the cumulative function of the number  $N_{K_j}^*$  of earthquakes of the entire range of energy classes of representative earthquakes which are given in the initial epicenter map. It is computed by the summation of the normalized numbers of earthquakes  $N_{K_j}^*$ , which reflect various K beginning from  $K_{max}$ , taking part in the construction of the repeatability curve and further increasing the summation up to the formation of the total sum after the computation of  $K_{min}$ . These numbers  $\sum N_{K_j}^*$  of earthquakes of each energy class  $K_{f_j}$  are put in the same cell as the values  $N_{K_j}^*$  of the classwise normalized numbers of earthquakes in the distribution method for constructing the repeatability curve. Further, the systems of linear equations (44) are formed in a manner similar to block 11.

Control is shifted from blocks 11 and 12 to block 13 where are computed the inclination  $\gamma$  and other coefficients of the curve.

Block 14 computes the seismic activity level of the region  $A_{K_0}$  according to the seismic energy class  $K_0$  as well as the error of averaging  $\sigma_{\gamma}$ . The computation results are printed in block 15. The values  $\gamma$ ,  $A_0$ , b,  $A_{K_0}$  and  $\sigma_{\gamma}$  are shown on the printer. When calculating the repeatability curves by the summation method, the values  $\sigma_{\gamma}$  and  $A_{K_0}$ , apparently, have no significance unlike in the distribution method.

# **Illustrative Example**

To test the SP-5 program, its check-out version may be used, which is written with the already prepared classwise numbers of earthquakes  $N_{K_j}$  given in the initial data set  $M_2$ . The search of these numbers on the basis of initial set  $M_1$  is not difficult but its volume of  $M_1$  is so large that bringing it here is very difficult. For the illustrative example, data set  $M_2$  has been shown (Table 15) in cells 1000–1053.

In our case, the number P = 5, whereas  $K_{f_j}$  varies from 13 to 9, but the range of the classes  $K_{f_j}$  being used may be increased twice if necessary, since cells 1013–1025 have been left to record  $K_{f_j}$ . In accordance with the placement of  $K_{f_j}$  the following groups of cells, 1026–1040 and 1041–1053, are meant for recording of the classwise numbers of earthquakes  $N_{K_j}$  and presentation periods  $T_{f_i}$ .

| Commands and numbers |         |         |       |     |                |                |              |  |
|----------------------|---------|---------|-------|-----|----------------|----------------|--------------|--|
| Address              | Sig     | Sign of |       |     |                |                | Remarks      |  |
|                      | <br>No. | Order   | Order | A   | A <sub>2</sub> | $\mathbf{A}_3$ |              |  |
| *                    | 1000 A  |         |       |     |                |                |              |  |
| 1000                 | ++      | +       | 00    | 000 | 000            | 000            | 0            |  |
| 1                    | ++      | +       | 00    | 000 | 000            | 000            | 0            |  |
| 2                    | -+-+-   | +       | 01    | 200 | 000            | 000            | const=2      |  |
| 3                    | ++      | +       | 04    | 100 | 000            | 000            | $S_0 = 1000$ |  |
| 4                    | ++      | +       | 00    | 434 | 290            | 000            | l=0.43429    |  |
| 5                    | +-      | +       | 01    | 100 | 000            | 000            | const=1      |  |
| 6                    | ++-+-   | +       | 02    | 100 | 000            | 000            | const = 10   |  |

#### TABLE 15. DATA SET M<sub>2</sub> FOR SP-5

| Address | Sign of   |         |                |                |                |                 |
|---------|-----------|---------|----------------|----------------|----------------|-----------------|
|         |           |         |                |                | A <sub>3</sub> | – Remarks       |
| No      | ). Orde   | r Order | $\mathbf{A}_1$ | $\mathbf{A}_2$ |                |                 |
| 7 +     | + +       | 00      | 500            | 000            | 000            | const=0.5       |
| 1010 +  |           | 05      | 855            | 000            | 000            | S = 85,500      |
| 1 +     | + $+$     | 01      | 500            | 000            | 000            | P=5             |
| 2 +     | + +,<br>· | 00      | 000<br>1013 A  | 000            | 000            | 0               |
| 1013 +  | + +       | 02      | 130            | 000            | 000            | $K_{f_1} = 13$  |
| 4 +     | + +       | 02      | 120            | 000            | 000            | $K_{f_2} = 12$  |
| 5 +     | + +       | 02      | 110            | 000            | 000            | $K_{f_3} = 11$  |
| 6 +     | + +       | 02      | 100            | 000            | 000            | $K_{f_4} = 10$  |
| 7 +     | + +       | 01      | 900            | 000            | 000            | $K_{15} = 9$    |
| 1020    |           | 00      | 0              | 0              | 0              |                 |
| 1       |           | 00      | 0              | 0              | 0              |                 |
| 2       |           | 00      | 0              | 0              | 0              |                 |
| 3       |           | 00      | 0              | 0              | 0              |                 |
| 4       |           | 00      | 0              | 0              | 0              |                 |
| 5       |           | . 00    | 0              | 0              | 0              |                 |
|         |           |         | 1026 A         |                |                |                 |
| 1026 +  | + +       | - 02    | 100            | 000            | 000            | $N_{K_1} = 10$  |
| 7 +     | + +       | 02      | 230            | 000            | 000            | $N_{K_2} = 23$  |
| 1030 +  | + +       | - 02    | 870            | 000            | 000            | $N_{K_3} = 87$  |
| 1 +     | + +       | 03      | 224            | 000            | 000            | $N_{K_4} = 224$ |
| 2 +     | + +       | - 03    | 229            | 000            | 000            | $N_{K_5} = 229$ |
| 3       |           | 00      | 0              | 0              | 0              |                 |
| 4       |           | ··· 00  | 0              | 0              | 0              |                 |
| 5       |           | 00      | 0              | 0              | 0              |                 |
| 6       |           | 00      | 0              | 0              | 0              |                 |
| 7       |           | 00      | 0              | 0              | 0              |                 |
| 1040    |           | 00      | 0              | 0              | 0              |                 |
|         |           |         | 1041 A         |                |                |                 |
| 1041 +  | + +       | - 02    | 400            | 000            | 000            | $T_{f_1} = 40$  |
| 2 +     | + +       | - 02    | 180            | 000            | 000            | $T_{t_2} = 18$  |
| 3 . +   | + +       | - 02    | 180            | 000            | 000            | $T_{1_3} = 18$  |
| 4 +     | + +       | - 02    | 180            | 000            | 000            | $T_{f_4} = 18$  |
| 5 +     | + +       | - 01    | 850            | 000            | 000            | $T_{f_s} = 8.5$ |
| 6       |           | 00      | 0              | 0              | 0              | -               |
| 7       |           | 00      | 0              | 0              | 0              |                 |
| 1050    |           | 00      | 0              | 0              | 0              |                 |
| 1.      |           | 00      | 0              | 0              | 0              |                 |
| 2       |           | 00      | 0              | 0              | 0              |                 |
| 3       |           | 00      | 0              | 0              | 0              |                 |

| A 11      | Co      | mmands a       | Demonstra      |                |                              |
|-----------|---------|----------------|----------------|----------------|------------------------------|
| Address – | Command | A <sub>1</sub> | A <sub>2</sub> | A <sub>3</sub> | Kemarks                      |
|           |         | 1054 A         |                |                |                              |
| 1054      | 000     | 0000           | 0000           | 0000           | $(0, 0, A_{mn}) = (0, 0, 0)$ |
| 5         | 000     | 0000           | 0000           | 0000           | 0                            |
| 6         | 000     | 0000           | 0000           | 0000           | $M_1 = 0$                    |
| 7         | 000     | 0000           | 0000           | 0000           | $M_2=0$                      |
| 1060      | 000     | 0000           | 0000           | 0000           | (m-1, 0, 0) = (0, 0, 0)      |
| 1         | 000     | 0000           | 0000           | 1011           | $(0, 0, a_t) = (0, 0, 1011)$ |
| 2         | 000     | 0000           | 0000           | 1017           | $(0, 0, K_n) = (0, 0, 1017)$ |
| 3         | 000     | 0000           | 0000           | 1032           | $(0, 0, N_n) = (0, 0, 1032)$ |
| 4         | 000     | 0000           | 0000           | 1045           | $(0, 0, T_n) = (0, 0, 1045)$ |
| 5         | 000     | 0004           | 0000           | 0000           | (p-1, 0, 0) = (4, 0, 0)      |
| 6         | 000     | 0000           | 0000           | 0000           | (0, n, 0) = (0, 0, 0)        |

#### TABLE 16. CONTROL INFORMATION FOR SP-5

Control information is recorded in cells 1054–1066 (Table 16). Here  $A_{mn}$  is the number of the last cell of the set of epicenters  $M_1$ , therefore, in our case the content of the cell 1054 is equal to zero. Index cells 1056 and 1057 are marked for members  $\mu_1$  and  $\mu_2$ ;  $\mu_1 = 0$  means set  $M_1$  is absent;  $\mu_2 = 0$  indicates use of the distribution method to compute the parameters of the repeatability curves; m and n—number of rows and columns of the matrix  $A_{mn}$ , consisting of set  $M_1$ . Hence, in the cells corresponding to them here, numbers 1060 and 1066 are zero. In the remaining cells, 1061–1064, the numbers of succeeding cells are shown, which are meant to record the following data:  $a_e$ —constant of computation,  $K_n$ —classes  $K_{fj}$ ,  $N_n$ —classwise numbers of earthquakes,  $T_n$ —representative periods  $T_{fj}$  for the classes  $K_{fj}$ .

Given below are the results of the computation of the parameters of the frequency curve (data Tables 15 and 16) using the SP-5 program while running the distribution method:

| γ:         | + | +- | 00587957519  |
|------------|---|----|--------------|
| $A_0$ :    | + | ++ | 01525446148  |
| b :        | + | ++ | 01893704272  |
| $A_{10}$ : | + | +  | 00125975281  |
| σγ :       | + |    | 01426563065. |

# Chapter IV

# Programs to Compute Maps of Maximum Possible Earthquakes ( $K_{max}$ )

Hand computation of maps of maximum possible earthquakes  $K_{\text{max}}$  using correlations between  $K_{\text{max}}$  and seismic activity A has been described by Riznichenko (1966b).

I.V. Gorbunova (1969) uses, for this purpose, seismic activity maps with constant accuracy based on correlations from Northern Tien-Shan.

Value of  $K_{\text{max}}$  may be found for each node of the map grid thus (Riznichenko, 1966a, 1967a): Based on the correlated dependence (13) for each value of  $K_{\text{max}}$ , A is found, i.e., the average seismic activity in the area responsible for the strong earthquake  $K_{\text{max}}$ . In this the radius r of the area is computed with the assumption that the value of energy  $K_{\text{max}}$ , emitted in the focus of a strong earthquake, is proportional to the volume of the region of its preparation in accordance with (14).

Further, a grid is drawn on the map of earthquake epicenters. It is necessary to establish the values of  $K_{\text{max}}$  on its points. Each node of the grid becomes the center of concentric areas, whose radius r reflects the values  $K_{\text{max}}$ of the entire range of earthquakes as in formula (14). The value  $\overline{A}$  in each is computed by the summation method. The value  $K_{\text{max}}$  is assigned to the grid point which corresponds to the value  $\overline{A}$  on area  $S = \pi r^2$ , as in formulas (13) and (14).

The compilation of the  $K_{max}$  maps is the same for Eastern Sayan (Riznichenko, 1966b), Eastern Uzbekistan (Zakharova, Seiduzova, 1969), Southern Fergana (Flenova, 1971), certain regions of Turkmenia (Kallaur, 1971), Georgia and its surroundings (Jibladze, 1971), Pribaikal (Uspenskaya, 1971), and others.

Since the described computation of  $K_{\max}$  was very unwieldy and difficult (Riznichenko and others, 1970), it was simplified in the following manner: At first, the values  $\overline{A}$  were computed for each  $K_{\max}$  value for all earthquakes by formula (13), which should define the appearance of these earthquakes. Then, the total quantity N of epicenters is found by formula (37), taking into account the values of  $\overline{A}$  and S, stipulating the given quantity  $\overline{A}$ . Next the number  $N_{\Sigma}$  of epicenters of concentric areas S is computed, which is
done for each grid point. The value  $K_{\max}$  is attributed to the point under study, insuring better agreement between the computed value  $N_E$  and the observed one.

The computation of  $K_{\max}$  with value  $N_E$  may also be simplified by using the summation method with constant accuracy (Gorbunova, 1964). The values  $\overline{A}$  for each  $K_{\max}$  are also computed by formulas (13, 14) and are inserted in formula (37) along with the total number of epicenters  $N_E = N_\sigma$ , which is constant for all succeeding calculations and insures the constant accuracy of values  $\overline{A}$ . The areas S, found from expression (37) for the averaging zone of activity for each  $K_{\max}$ , are recomputed for r. Then with these r, the concentric areas about the point under study are described: r of each area corresponds to a particular  $K_{\max}$ , which is attributed to the grid node, if the number of the epicenters  $N_E$  in this area is not less than the given  $N_\sigma$ . It is usually convenient to compute the system of grids before.

The summation of earthquakes to compute maps of  $K_{\max}$  is difficult with dissimilar periods  $T_K$  for earthquakes of various energy classes. In this case the use of formula (37) can only be done after periods  $T_K$  are normalized to period  $T_{\min}$ . Therefore, to compute the numbers  $N_E$  in the averaging zone of activity or to determine its area with given  $\overline{A}$  and  $N_{\sigma}$ , it is necessary to establish the relationship of  $T_{\min}$  with  $T_K$  for each on the map of epicenters. This additional preparation for the initial epicenter map to compute the map of  $K_{\max}$  may be avoided if the program analyzes the presentation periods. The great difficulty of hand calculating step  $K_{\max}$  equal to the full value K, increases further if this step is further decreased, as is necessary in more detailed investigations. In this case, the computer reduces computation time.

The computation of the map of maximum possible earthquakes is possible when the initial information is entered as maps of earthquake epicenters and as maps of seismic activity. For this two programs—SP-6 and SP-7—have been written.

#### SP-6 PROGRAM TO COMPUTE MAPS OF K<sub>max</sub> FROM THE MAP OF EARTHQUAKE EPICENTERS

The SP-6 program works according to an algorithm based on formulas (13), (14) and (37). The main idea behind calculating the  $K_{\text{max}}$  map on the computer, as in the manual method, is to compare the values of seismic activity, calculated on one hand from the correlation dependence (13) for the series of values  $K_{\text{max}}$  (the so-called tabulated values of activity  $A_T$ ), and on the other, from the epicenter map in the variable area zones responsible for the emergence of earthquakes of different energy classes (values of activity in the averaging zones $-A_z$ ). When  $A_T = A_z$  the value  $K_{\text{max}}$  is recorded for the point under investigation in accordance with (13). The analysis of the values

of activity and transfer to the result, i.e., to determine each member of the resulting matrix  $K_{\text{max}}$ , is conducted differently for two groups of  $K_{\text{max}}$ . The first includes values beginning from the maximum proposed in the region to  $K = (15 - a_K)$ , where  $a_K$  step of computation K. In the second are all  $K_{\rm max} \leq 15$  to  $K_{\rm min}$ . This division is explained as follows: In working with the first group of  $K_{\text{max}}$ , seismic activity  $A_z$  is computed according to formula (13) in the circular variable radius zones with centers at the computation point in which the radius of the zone is reduced by the reduction in  $K_{max}$ according to formula (14). If  $K_{\text{max}} = 18r = 314$  km; then  $K_{\text{max}} = 15r =$ 31 km; and  $K_{\text{max}} = 14r = 15$  km, i.e., it decreases. It seems it would be useless to compute seismic activity in radii zones less than  $K_{max} < 14$  since they may not show a single epicenter. This leads to zero values of  $K_{max}$  and the distortion of computation results. To analyze the values of  $K_{\text{max}} \leq 15$ , therefore, a constant number  $N_{\sigma}$  of the sum of the epicenters in the averaging zone is considered in the program. This number signifies a value of activity, e.g.,  $N_{\sigma} \ge 3$ . According to known  $N_{\sigma}$  and the value  $A_T$  representing the given  $K_{\text{max}}$  using relationship (13), the program computes the radius r of the averaging zone by formula (37), where  $S = \pi r^2$ . Further, the computation is stopped in areas if, corresponding to the series of values r, the total number of epicenters  $N_{\Sigma}$  is computed and  $N_{\Sigma} = N_{\sigma}$ . The computation of the number  $N_{Z}$  in the circular zone is replaced by comparing the values r and  $\Delta_{\min}$ —distance from the point under consideration to the epicenter which, of all  $N_{\sigma}$  epicenters, is nearest to the point under study. The epicentral distances  $\Delta$  are measured according to formula (40).

Two sets,  $M_1$  and  $M_2$ , are used as initial data with several control data in the program. Set  $M_1$  is presented by a matrix of epicenters  $A_{mn}$ , which is compiled directly or automatically from the map of earthquake epicenters or from their catalog, as in the previous programs. Set  $M_2$  presents data about numbers  $N_{\sigma}$ , seismicity, and computational conditions. These numbers reflect a given accuracy of the computation of activity. It also includes a computation interval along the coordinates—lat.  $a_{\varphi}$  and long.  $a_{\lambda}$  and about the value ( $K_{\max} - a_K$ ); parameters of formula (13)—  $\log \alpha$ ,  $\beta$ ,  $K_{\alpha}$ , and values  $K_{\max}$  using computation interval  $A_K$ , which investigates the activity in the peaks of each computation point and several other data. Program control information holds information about the quantity of elements in each line and column of the initial matrix  $A_{nm}$ , about the general quantity and elements, and about the number of rows q and columns r of the resulting matrix  $K_{\max}$  in the  $K_{\max}$  map being computed.

The addresses of the initial cells for writing the instructions are also stored here. These instructions are to translate of initial data set  $M_1$ . Similarly are stored instructions for re-recording the results of the intermediate computation—e.g., values of epicentral distances  $\Delta_i$ . These distances are measured for each computation point and, during the analysis of the radii







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PROGRAM SP-6

| Address | Command | A1             | A <sub>2</sub> | A <sub>3</sub> |
|---------|---------|----------------|----------------|----------------|
|         |         | 0500 A         |                |                |
| 0500    | 055     | 0523           | 1021           | 0523           |
| 1       | 013     | 0523           | 1123           | 0523           |
| 2       | 055     | 0545           | 1022           | 0545           |
| 3       | 013     | 0545           | 1124           | 0545           |
| 4       | 055     | 0553           | 1022           | 0553           |
| 5       | 013     | 0553           | 1124           | 0553           |
| 6       | 055     | 0643           | 1022           | 0643           |
| 7       | 013     | 0643           | 1124           | 0643           |
| 0510    | 055     | 0750           | 1022           | 0750           |
| 1       | 013     | 0750           | 1125           | 0750           |
| 2       | 055     | 1010           | 1022           | 1010           |
| -       |         | 0513 A         |                | 1010           |
| 0513    | 013     | 1010           | 1126           | 1010           |
| 4       | 015     | 1010           | 1022           | 1014           |
| +<br>5  | 013     | 1014           | 1127           | 1014           |
| 5       | 015     | 1014           | 1022           | 1014           |
| 7       | 013     | 1212           | 1022           | 1212           |
| 0520    | 015     | 1212           | 1022           | 1212           |
| 0520    | 013     | 1217           | 1022           | 1217           |
| 2       | 015     | 1217           | 7741           | 1217           |
| 2       | 000     | 2212           | 2712           | 0007           |
| 3       | 000     | 0526           | 3213<br>7741   | 0007           |
| 4       | 010     | 1024           | 1024           | 1122           |
| 5       | 000     | 1034<br>0526 A | 1034           | 1122           |
| 0500    | 050     | 0020 11        | 0              | 0              |
| 0320    | 032     | 0              | 2012           | 1140           |
| 0520    | 215     | 0521           | 5215           | 1140           |
| 0530    | 030     | 1047           | 1140           | 0535           |
| 1       | 002     | 1047           | 1140           | 0540           |
| 2       | 050     | 0533           | 0534           | 0545           |
| 3       | 075     | 0              | 1062           | 1141           |
| . 4     | 002     | 1113           | 1034           | 1142           |
| 3       | 017     | 0              | 0542           | 0              |
| 6       | 076     | 0525           | 0343           | 0525           |
| 0540    | 013     | 0535           | 1024           | 0535           |
| 0540    | 013     | 0543           | 1025           | 0543           |
| 0541    | 000     | 0541 A         | 0101           | 11/0           |
| 0541    | 002     | 1142           | 0101           | 1142           |
| 2       | 017     | 0              | 0333           | U              |
| 3       | 104     | U<br>1074      | 1141           | 2012           |
| 4       | 104     | 10/4           | 1141           | 3213           |
| 5       | 112     | U              | 0527           | 0003           |
| 5       | 0/5     | 0              | U              | 1236           |
| 7       | 004     | 1035           | 1036           | 1143           |

(Cont d.)

| Address  | Command | A <sub>1</sub> | $A_2$ | $A_3$ |
|----------|---------|----------------|-------|-------|
| <br>0550 | 052     | 0              | 0     | 0     |
| 1        | 504     | 3214           | 1143  | 3214  |
| 2        | 504     | 3215           | 1143  | 3215  |
| 3        | 112     | 0              | 0551  | 0003  |
|          |         | 0554. A        |       |       |
| 0554     | 075     | 0              | 1040  | 0140  |
| 5        | 016     | 0556           | 7714  | 0007  |
| 6        | 075     | 0              | 0160  | 1231  |
| 7        | 075     | 0              | 0101  | 1151  |
| 0560     | 075     | 0              | 1077  | 1152  |
| 1        | 005     | 1231           | 1152  | 0140  |
| 2        | 016     | 0563           | 7711  | 0007  |
| 3        | 002     | 1151           | 0160  | 1151  |
| 4        | 002     | 1060           | 1061  | 1153  |
| 5        | 005     | 1153           | 1231  | 0140  |
| 6        | 016     | 0567           | 7711  | 0007  |
|          |         | 0567 A         |       |       |
| 0567     | 075     | 0              | 0160  | 1153  |
| 0570     | 005     | 1037           | 1074  | 1152  |
| 1        | 004     | 1151           | 1153  | 1151  |
| 2        | 004     | 1151           | 1152  | 1151  |
| 3        | 005     | 1151           | 1111  | 1232  |
| 4        | 052     | Ō              | 0     | 0     |
| 5        | 075     | 0              | 1075  | 1145  |
| 6        | 075     | 0              | 1076  | 1146  |
| 7        | 452     | 0              | 0     | 1011  |
| 0600     | 452     | 0              | 0     | 1006  |
| 1        | 004     | 1145           | 1143  | 1155  |
|          |         | 0602 A         |       |       |
| 0602     | 004     | 1146           | 1143  | 1156  |
| 3        | 056     | 0604           | 0605  | 0641  |
| 4        | 005     | 1041           | 1151  | 1241  |
| .5       | 075     | 0              | 1155  | 0140  |
| 6.       | 016     | 0607           | 7712  | 0007  |
| 7        | 075     | 0              | 0161  | 1147  |
| 0610     | 075     | 0              | 0160  | 1150  |
| 1        | 075     | 0              | 1156  | 0140  |
| 2        | 016     | 0613           | 7712  | 0007  |
| 3        | 075     | 0              | 0161  | 1157  |
| 4        | 075     | 0              | 0160  | 1160  |
|          |         | 0615 A         |       |       |
| 0615     | 275     | 0              | 3214  | 0140  |
| 6        | 016     | 0617           | 7712  | 0007  |
| 7        | 075     | 0              | 0161  | 1161  |
| 0620     | 075     | . 0            | 0160  | 1162  |
| 1        | 275     | 0              | 3215  | 0140  |
| 2        | 016     | 0672           | 7713  | 0007  |

| Address | Command | $\mathbf{A}_{1}$ | $\mathbf{A}_{2}$ | A <sub>3</sub> |
|---------|---------|------------------|------------------|----------------|
| 3       | 075     | 0                | 0161             | 1163           |
| 4       | 075     | 0                | 0160             | 1164           |
| 5       | 005     | 1147             | 1161             | 1151           |
| б       | 005     | 1150             | 1160             | 1152           |
| 7       | 005     | 1152             | 1162             | 1152           |
|         |         | 0630 A           |                  |                |
| 0630    | 005     | .1152            | 1164             | 1152           |
| 1       | 001     | 1151             | 1152             | 1151           |
| 2       | 005     | 1150             | 1157             | 1152           |
| 3       | 005     | 1152             | 1162             | 1152           |
| 4       | 005     | 1152             | 1163             | 1152           |
| 5       | 001     | 1151             | 1152             | 1151           |
| 6       | 075     | 0                | 1151             | 0140           |
| 7       | 016     | 0640             | 7716             | 0007           |
| 0640    | 005     | .0160            | 1143             | 1151           |
| 1       | 005     | 1041             | 1151             | 1 <b>241</b>   |
| 2       | 013     | 0641             | 1026             | 0641           |
|         |         | 0643 A           |                  |                |
| 0643    | 112     | 0                | 0615             | 0003           |
| 4       | 056     | 0                | 1210             | 0              |
| 5       | 075     | 0                | 0                | 0710           |
| 6       | 002     | 1114             | 1034             | 1154           |
| 7       | 075     | 0                | 1106             | 1140           |
| 0650    | 005     | 1231             | 1140             | 0140           |
| 1       | 016     | 0632             | 7710             | 0007           |
| 2       | 005     | 0160             | 1043             | 0140           |
| 3       | 016     | 0654             | 7714             | 0007           |
| 4       | 004     | 0160             | 1042             | 0140           |
| 5       | 016     | 0656             | 7710             | 0007           |
|         |         | 0656 A           |                  |                |
| 0656    | 075     | 0                | 0160             | 1233           |
| 7       | 075     | 0                | 1233             | 1165           |
| 0660    | 002     | 1112             | 1034             | 1166           |
| 1       | . 075   | 0                | 0                | 1167           |
| 2       | 056     | 0663             | 0664             | 0670           |
| 3       | 002     | 1165             | 1241             | 0              |
| 4       | 056     | 0665             | 0670             | 0673           |
| 5       | 001     | 1167             | 3213             | 1167           |
| 6       | 013     | 0670             | 1025             | 0670           |
| 7       | 013     | 0673             | 1027             | 0673           |
| 0670    | 017     | 0                | 0                | 0              |
|         |         | 0671 A           |                  | -              |
| 0671    | 076     | 0                | 0673             | 0              |
| 2       | 056     | 0                | 0674             | 0              |

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|            |         |        | · · · |                |
|------------|---------|--------|-------|----------------|
| Address    | Command | A1     | A2    | A <sub>3</sub> |
| 4          | 002     | 1166   | 0101  | 1166           |
| 5          | 076     | 0      | 0666  | 0              |
| 6          | 0       | 0      | 0     | 0              |
| 7          | 005     | 1231   | 1167  | 1151           |
| 0700       | 005     | 1233   | 1233  | 1152           |
| 1          | 004     | 1151   | 1152  | 1234           |
| 2          | 002     | 1140   | 1103  | 1152           |
| 3          | 005     | 1152   | 1105  | 1152           |
| -          |         | 0704 A |       |                |
| 0704       | 001     | 1104   | 1152  | 1152           |
| 5          | 005     | 1152   | 1044  | 0140           |
| 6          | 010     | 0707   | 7710  | 0007           |
| 7          | 075     | 0.07   | 0160  | 1025           |
| 0710       | 075     | 0      | 0100  | 1255           |
| 1          | 0       | 0      | 0     | 0              |
| 1          | 0       | 0      | 0     | 0              |
| 2          | 0       | 0      | 0     | 0              |
| 3          | 002     | 1235   | 1234  | 0              |
| 4          | 076     | 0      | 0716  | 0              |
| 5          | 0       | 0      | 1002  | 0              |
| 6          | 0       | 0      | 1235  | 0              |
|            |         | 0717 A | 1003  |                |
| 0717       | 076     | 0      | 1002  | 0              |
| 0720       | 002     | 1140   | 1101  | 1140           |
| 1          | 002     | 1154   | 0101  | 1154           |
| 2          | 076     | 0      | 0650  | 0              |
| 3          | 002     | 1115   | 1034  | 1170           |
| 4          | 075     | 0      | 1107  | 1140           |
| 5          | 016     | 0726   | 0702  | 0710           |
| 6          | 005     | 1232   | 1102  | 1151           |
| 7          | 004     | 1151   | 1235  | 1151           |
| 0730       | 044     | 1151   | 0     | 1151           |
| 1          | 056     | 0      | 1215  | 0              |
|            |         | 0732 A |       |                |
| 0732       | 0       | 0      | 0     | 0              |
| 3          | 075     | 0      | 0     | 1173           |
| 4          | 075     | 0      | 0     | 1167           |
| 5          | 052     | 0      | 0     | 0              |
| 6          | 075     | 0      | 0     | 1171           |
| 7          | 075     | 0      | 0     | 1172           |
| 0740       | 075     | 0      | 1241  | 1174           |
| 1          | 013     | 1171   | 1027  | 1171           |
| 2          | 013     | 1172   | 1026  | 1172           |
| 3          | 402     | 1742   | 1174  | Δ172<br>Λ      |
| 4          | 076     | 0      | 0750  | 0<br>0         |
| • <b>r</b> | 0.0     | 0745 A | 0.20  | v              |
| 0745       | 075     | 0      | 1171  | 1175           |
| 0/45       | 0/3     | U      | 11/1  | 1175           |
| 6          | 075     | 0      | 1172  | 1176           |

| Address | Command | A <sub>1</sub> | A <sub>2</sub> | A <sub>3</sub> |
|---------|---------|----------------|----------------|----------------|
| 7       | 075     | 0              | 1242           | 1174           |
| 0750    | 112     | 0              | 0741           | 0001           |
| 1       | 056     | 0752           | 0753           | 0760           |
| 2       | 001     | 1167           | 3213           | 1167           |
| 3       | 056     | 0754           | 0755           | 0761           |
| 4       | 075     | 0              | 1110           | 1241           |
| 5       | 075     | 0              | 1174           | 1177           |
| 6       | 013     | 0760           | 1175           | 0760           |
| 7       | 013     | 0761           | 1176           | 0761           |
|         |         | 0760 A         |                |                |
| 0760    | 077     | 0              | 0              | 0              |
| 1       | 077     | 0              | 0              | 0 -            |
| 2       | 001     | 1173           | 0101           | 0              |
| 3       | 002     | 1173           | 1102           | 0              |
| 4       | 036     | 0              | 0735           | 0              |
| 5       | 075     | 0              | 1151           | 1165           |
| 6       | 002     | 1177           | 1165           | 0              |
| 7       | 076     | 0              | 0773           | 0              |
| 0770    | 005     | 1101           | 1034           | 1200           |
| 1       | 001     | 1140           | 1200           | 1237           |
| 2       | 056     | 0              | 1003           | 0              |
|         |         | 0773 A         |                |                |
| 0773    | 002     | 1165           | 1177           | 0              |
| 4       | 076     | 0              | 1002           | 0              |
| 5       | 002     | 1140           | 1101           | 1140           |
| 6       | 002     | 1170           | 0101           | 1170           |
| 7       | 076     | 0              | 0725           | 0              |
| 1000    | 075     | 0              | 0              | 1237           |
| 1       | 056     | 0              | 1003           | 0              |
| 2       | 075     | 0              | 1140           | 1237           |
| 3       | 001     | 1236           | 0101           | 1236           |
| 4       | 016     | 1006           | 1751           | 0007           |
| 5       | 000     | 1236           | 4000           | 1240           |
|         |         | 1006 A         |                |                |
| 1006    | 077     | 0              | 0              | 0              |
| 7       | 001     | 1145           | 1100           | 1145           |
| 1010    | 112     | 0              | 0600           | 0001           |
| 1       | 077     | 0              | 0              | 0              |
| 2       | 075     | 0              | 1075           | 1145           |
| 3       | 001     | 1146           | 1100           | 1146           |
| Ą.      | 112     | 0              | 0577           | 0001           |
| 5       | 077     | 0              | 0              | 0              |
| 6       | 777     | 7777           | 7 <b>77</b> 7  | 0              |
| 7       | 777     | 0              | 7777           | 7777           |
| 1020    | 0       | 0001           | 0              | 0              |
|         |         | 1021 A         |                |                |
| 1021    | 0       | 0              | 0001           | 0              |

(Contd).

| Address | Command | $A_1$  | A <sub>2</sub> | A <sub>3</sub> |
|---------|---------|--------|----------------|----------------|
| 2       | 0       | 0      | 0              | 0001           |
| . 3     | 0       | 0      | 0003           | 0              |
|         | `       | 1210 A |                |                |
| 1210    | 052     | 0      | 0              | 0              |
| 1       | 375     | 0      | 1241           | 2226           |
| 2       | 112     | 0      | 1211           | 0001           |
| 3       | 056     | 0      | 0645           | 0              |
| 4       | 0       | 0      | 0              | 0              |
| 5       | 052     | 0      | 0              | 0              |
| 6       | 375     | 0      | 2226           | 1241           |
| . 7     | 112     | 0      | 1216           | 0001           |
| 1220    | 056     | 0      | 0732           | 0              |

of the averaging zones of activity, their order is changed in the memory. Re-recording restores the initial order of the value  $\Delta_i$ , which is necessary for the multiple analysis of values  $K_{\max}$  at each point, in accordance with computation step  $(K_{\max} - a_K)$ .

The program itself is located in cells 0500-1030 of the memory and set  $M_2$  in cells 1035-1120. Control information engages cells 1123-1135 and set  $M_1$  in 3200-6150. Intermediate results are in cells 1121-3177, the computed  $\Delta_i$ —epicentral distances—are dispatched to cells 1241-3177 during computation.

#### Block Diagram SP-6 (see p. 102)

The SP-6 program flows as in the block diagram. First are entered the punch cards of the program itself and the initial data set. Control is then shifted to the four preparational blocks for the main computation. Block 1 handles the instructions and their repetitions (cycles) according to the control information. In block 2, the initial data of sets  $M_1$  and  $M_2$  are converted from the decimal to the binary system. The  $M_1$  data are prepared for computation in block 3, which ends with the introduction of periods  $T_K$  of the energy class  $K_l$  emergence of each earthquake epicenter of the initial set to the period  $T_{\min}$  of the class  $K_{\min}$ , i.e., the least class from those represented in the region. For this purpose, classes  $K_l$  are compared with a set of fixed classes of energy  $K_{lj}$ . When  $K_l = K_{lj}$  the corresponding period  $T_{lj}$  is attributed to the earthquake. By dividing  $T_{\min}$  by  $T_{lj}$  the number of carthquakes of the class  $K_l$  is found (the emergence time  $T_{\min}$ ), i.e., the number  $N_l$  which is dispatched to the initial matrix  $A_{mn}$  in place of the corresponding  $K_i$ , which represents each earthquake epicenter.

Multiple computations of seismic activity are prepared in block 4 and the

constant part of the value  $\overline{A}$  is computed from formula (37), depending only on the parameters of the seismic regime, viz:

$$B = \frac{(1-10^{-\gamma}) \cdot 1000}{10^{-\gamma} (K_{\min} - K_0) \cdot \pi \cdot T_{\min}}.$$
 (37')

The value B is dispatched in the working cell and stored until the end of the computation, in the process of which periodic reference is made to it. The preparatory operations are finished in blocks 1-4. In each of the remaining the activity is computed and analyzed for each point under study for the future  $K_{\text{max}}$  map. The work of block 5 begins from the first point, situated in its lower left corner. The addresses of the cells are entered to record the intermediate results for the computation of the epicentral distances  $\Delta_i$  by formula (40). Thereafter their m values are dispatched in two series of cellsworking and storage. In block 6 the value  $K_{\max}$  is given, which at the beginning of the computation is equal to the maximum  $K_{max}$  from those proposed in the region, i.e.,  $(K_{\max})_1 = (K_{\max})_{\max}$ . Later it is reduced by computation interval  $a_K$  around  $K_{\max}$ , i.e.,  $(K_{\max})_2 = [(K_{\max})_1 - a_K]$  and so on. Next the value of radius  $r_{max}$ , of the zone responsible for the appearance of the  $K_{\text{max}}$ , earthquake is computed according to formula (14). From the list of epicentral distances  $\Delta_i$ , obtained from block 5, those compatible with  $r_{\max_i}$  are selected, i.e., those for which  $\Delta_i \leq r_{\max_i}$ . After this the sum  $N_E$  of earthquakes is found, that is, the epicentral distance  $\Delta_i$  which from the point of computation answers the condition  $\Delta_i \leq r_{\max_i}$ , i.e.,  $N_{\Sigma} = \sum N_i$ . The value of  $N_{\Sigma}$  is total number of earthquakes in the circle of radius  $r_{\max}$ , which, after multiplication by the contents of the working cell obtained from formula (37'), gives the value of seismic activity  $A_z$  in the averaging zone with  $r_{\max_{i}}$ . Activity  $A_z$  and its tabulated value  $A_T$  are computed in block 7 and later compared. If  $A_T = A_z$  then the results are printed. If  $A_T < A_z$ , then the value  $K_{\max}$  for the computation point should be larger than the given  $K_{\max}$ , but less than the earlier investigated value  $K_{\max_{i=1}}$ . In the printing cell, therefore, value  $K_{\max_i} = [K_{\max_{i=1}} - 0.5 \cdot a_K]$  is dispatched through block 12. If  $K_{\max_i} = (K_{\max})_{\max}$  the relationship  $A_T < A_z$  signifies the reduction of  $(K_{\max})_{\max}$  which may be avoided by making the first value  $K_{\max}$  as large as necessary.  $A_T > A_z$  signifies that the activity, computed about the earthquake epicenters of the initial set  $M_1$  in the averaging zone  $r_{\max}$ , is less than the tabulated one (13), and it is necessary to reduce the averaging zone  $S_{\max_i}$ in accordance with the reduction of  $K_{max}$ . In this case,  $K_{max}$ , is reduced by the value of the interval  $a_K$  about  $K_{max}$  and control is shifted to the beginning of block 6 where the value  $r_{\max_{j+1}}$  is computed  $-K_{\max_{j+1}} = [K_{\max_j} - a_K]$ . This computation is repeated until the comparison of the activity values  $A_T$ and  $A_z$ . If they are unequal, computation with the interval  $a_K$  is repeated in blocks 6 and 7 for all  $K_{\text{max}}$  up to  $K_{\text{max}} = 15 + a_K$ . When the values  $K_{\text{max}}$ in the range  $K_{\text{max}} \ge 15 + a_K$  are analyzed and all the values  $A_T$  from all the  $K_{\text{max}}$  satisfy the value  $A_z$ , control is shifted to block 8. Here and further on, in blocks 9-11, are analyzed the values  $K_{\text{max}}$  from K = 15 to  $K = K_{\text{min}}$ . In block 8,  $A_T$  is computed by formula (13) for the first value  $K'_{\text{max}} = 15$ . Next the value of the radius  $r'_{\text{max}_j}$  of the averaging zone of activity— $A'_z$ —is computed according to formula (37), where  $S = \pi r^2$  for  $\overline{A} = A'_T$  and  $N_{\Sigma} =$  $N_{\sigma}$  ( $N_{\sigma}$  given in the initial computation conditions). Thereafter control is shifted to block 9, where  $\Delta_i$ —epicentral distances from the computational point to all epicenters of set  $M_1$ —are compared with each other.

The comparison ends with the selection of the least  $\Delta_i$  from those measured; its value is now equal to  $\Delta_{\min_1}$ . Block 10 computes the number of earthquakes  $N_{\Sigma}$  which have epicenters inside the circle of radius  $\Delta_{\min_1}$  and compares  $N_{\Sigma}$  with the earlier given  $N_o$ . If  $N_{\Sigma} \ge N_o$ , the preconsidered accuracy of the computation of the activity in the circle of radius  $\Delta_{\min_1} = \Delta_{\min_0}$  is defined and control is shifted to block 11 ( $\Delta_{\min_0}$  is the radius of the optimal averaging zone where  $N_{\Sigma} = N_o$ ). When  $N_{\Sigma} < N_o$  the number of earthquakes in the circle of radius  $\Delta_{\min_1}$  is insufficient to compute activity with the given accuracy  $\sigma$ . Therefore, after the dispatch of a very large number in place of  $\Delta_{\min_1}$ , it is necessary to return to block 9. Here comparing  $\Delta_i$  is repeated with the selection of a new least distance  $\Delta_i = \Delta_{\min_2}$ ,  $\Delta_{\min_2}$  being greater than  $\Delta_{\min_1}$ . Block 10 repeats the summing of earthquakes and the following comparison of  $N_{\Sigma}$  with  $N_o$ .

The return from block 10 to 9 is repeated until the relationship  $N_{\Sigma} \ge N_{\sigma}$ is achieved for a particular  $\Delta_i = \Delta_{\min_n}$ . Then control is shifted to block 11 where the chosen value  $\Delta_{\min_a}$  is compared with the  $r_{\max_i}$  computed in block 8. The equality  $\Delta_{\min} = r_{\max}$ , signifies that the tabulated value  $A_T$ , representing the averaging zone with radius  $r_{max_i}$ , agrees with  $A_z$ . Then the value  $K_{\text{max}}$ , corresponds to the point, around which this zone is given; this is insured by the value  $A_z$  in accordance with formula (13). Then the results are printed. If  $\Delta_{\min_0} > r_{\max_j}$  then the number of epicenters equal to  $N_{\Sigma}$  defines the activity  $A_T$  on the area larger than  $\pi (r_{\max})^2$ . In this case  $K_{\max}$  of the point under study should be larger than  $K_{\max}$ , but lesser than the earlier investigated  $K_{\max} = K_{\max_{i=1}}$ . Therefore the value  $K_{\max} = [K_{\max_{i=1}} + 0.5 a_K]$ is sent to the printing cell through block 12-to correct Kmax. Control is shifted then to block 13 to print the results. If  $\Delta_{\min_0} < r_{\max_i}$  the tabulated value of activity  $A'_r$  corresponding to the zone radius  $r_{\max_i}$  is insured in the given  $N_{\sigma}$  only in a much smaller zone, i.e., the point under study answers the relation  $K_{\text{max}} < K_{\text{max}}$ . The value  $K_{\text{max}}$  is lowered by the interval  $K_{\text{max}}$  equal to  $a_K$  and the control is again shifted to block 8. The number of computation cycles in blocks 8-11 depends on the  $K_{max}$  of the point under study and on the interval computation  $a_K$ . If the relation  $\Delta_{\min} \ge r_{\max}$ , cannot be made, the process continues up to  $K_{\text{max}} = K_{\text{min}}$ . Further control is shifted to block 13 to print the results, which fixes the point serial number and value  $K_{\min}$ . Then follows block 14 which prepares the computation of  $K_{\max}$  for the succeeding point. After this computation is stopped if the number of points to study  $K_{\max}$  is exhausted. Otherwise control is shifted to block 5, where the epicentral distances from the new computation point are measured and all the above-mentioned operations are repeated.

#### **Illustrative Example**

To verify the SP-6 program its check-out version may be used as an illustrative example. It works on the basis of initial data presented by sets  $M_1$ (Table 1),  $M_2$  (Table 18) and a group of control information. The  $M_1$  address entry is changed to 3213 for SP-6.

In cells 1034-1046 the computation constants are kept; 1047-1061--classes  $K_{\rm fj}$  for the region under study; 1062-1074 the periods of presentation  $T_{\rm fj}$  representing  $K_{\rm fj}$ ; 1075-1102--coordinates of the initial point computation  $\varphi_0$ ,  $\lambda_0$ ; computation interval around  $\varphi - a_{\varphi}$  and around  $\lambda - a_{\lambda}$ ; inclination of the repeatability curve  $\gamma$ ; least number  $N_{\sigma}$  of earthquakes in the scismic activity averaging zone A, representing the given error of the computation of  $A - \sigma_A$ . In cells 1103-1105 are the constants of formula (13). In 1106-1107 are the greatest of the proposed earthquakes in the region ( $K_{1_{\rm max}}$ ) and the value of the earthquake for which the averaging zone A becomes measurable with the epicenter determination errors ( $K_{2_{\rm max}}$ ).

| N Points   | <i>K</i> max  |
|--|---|
| +++ 01 10000000  | +++ 02 150500000  |
| +++ 01 20000000  | +++ 02 150500000  |
| -+++ 01 <b>3000000</b>   | +++ 02 150500000  |
| +++ 01 40000000  | +++ 02 135499999  |
| +++ 01 5000000   | +++- 02 123499999   |
| +++ 01 60000000  | +++ 02 114499999  |
| +++ 01 70000000  | ···+··· 02 106499999  |
| +++ 01 80000000  | +++ 02 100000000  |
| +++ 01 90000000  | +++ 02 100000000  |
|  |   |
| N Points   | Kmax  |
| N Points<br>+++ 02 100000000   | $K_{\rm max}$<br>+++ 02 100000000   |
| $\frac{N \text{ Points}}{+++ 02 \ 100000000} +++ 02 \ 110000000$   | $ \frac{K_{\text{max}}}{+++ 02 \ 100000000} + ++ 02 \ 150500000 $   |
| $\frac{N \text{ Points}}{+++ 02 \ 100000000} \\ +++ 02 \ 110000000 \\ +++ 02 \ 120000000 \\ +++ 02 \ 120000000 \\ +++ 02 \ 120000000 \\ +++++ 02 \ 120000000 \\ ++++++ 02 \ 120000000 \\ +++++++++++++++++++++++++++++$ | $ \frac{K_{\text{max}}}{+++ 02 \ 100000000} \\ +++ 02 \ 150500000 \\ +++ 02 \ 150500000 $   |
| $N \text{ Points} +++ 02 \ 100000000 +++ 02 \ 110000000 +++ 02 \ 120000000 +++ 02 \ 120000000 +++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 ++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 1300000000 +++++ 02 \ 130000000 +++++ 02 \ 130000000 +++++ 02 \ 1300000000 +++++ 02 \ 1300000000 +++++ 02 \ 1300000000 +++++ 02 \ 1300000000 ++++++ 02 \ 1300000000 ++++++ 02 \ 1300000000 ++++++ 02 \ 130000000000 ++++++ 02 \ 1300000000000000000000000000000000000$   | $ \frac{K_{\text{max}}}{+++ \ 02 \ 100000000} \\ +++ \ 02 \ 150500000 \\ +++ \ 02 \ 150500000 \\ +++ \ 02 \ 144500000 $   |
| N  Points +++ 02 100000000 +++ 02 110000000 +++ 02 120000000 +++ 02 130000000 +++ 02 130000000 +++ 02 140000000  | $K_{max}$ +++ 02 100000000<br>+++ 02 150500000<br>+++ 02 150500000<br>+++ 02 150500000<br>++++ 02 144500000<br>++++ 02 131499999                                      |
| N  Points +++ 02 10000000 +++ 02 110000000 +++ 02 12000000 +++ 02 13000000 +++ 02 13000000 +++ 02 14000000 ++++ 02 15000000  | $K_{max}$ +++ 02 10000000 +++ 02 15050000 +++ 02 15050000 ++++ 02 15050000 ++++ 02 14450000 ++++ 02 131499999 ++++ 02 121499999                                       |
| N  Points +++ 02 10000000 +++ 02 110000000 +++ 02 12000000 ++++ 02 13000000 ++++ 02 13000000 ++++ 02 14000000 ++++ 02 15000000 ++++ 02 15000000 ++++ 02 16000000   | $K_{max}$ +++ 02 10000000<br>+++ 02 15050000<br>+++ 02 15050000<br>+++ 02 15050000<br>++++ 02 14450000<br>++++ 02 131499999<br>++++ 02 121499999<br>++++ 02 113499999 |
| N  Points $+++ 02 100000000$ $+++ 02 110000000$ $+++ 02 120000000$ $+++ 02 130000000$ $+++ 02 140000000$ $+++ 02 150000000$ $+++ 02 150000000$ $+++ 02 170000000$  | $K_{max}$ +++ 02 10000000 +++ 02 15050000 +++ 02 15050000 ++++ 02 15050000 ++++ 02 14450000 ++++ 02 131499999 ++++ 02 121499999 ++++ 02 113499999 ++++ 02 105499999   |

TABLE 17. RESULTS OF COMPUTATION ON SP-6

# TABLE 18. DATA SET $M_2$ FOR SP-6

| Address         Sign of<br>No.         Order         A1         A2         A3           1034 A           1034         ++         +         00         500         0         0         const = 0.5           5         ++         +         03         360         0         0         2 $\pi$ = 6.283186           7         ++         +         01         628         318         600         2 $\pi$ = 6.283186           7         ++         +         01         314         159         300 $\pi$ = 3.141593           1040         ++         +         02         100         0         const = 10           1         ++         +         01         300         0         const = 13           3         ++         -         10         300         0         const = 2.305           5         0         0         0         0         0         0           1047         +         +         02         100         0 $K_{t_2}$ = 11           1         ++         +         02         0         0         0         0           1050         ++         + |         |            | Com       | mands and | d numbers     |       |                |                              |
|--|---------|------------|-----------|-----------|---------------|-------|----------------|------------------------------|
| No.         Order         A1         A2         A3           1034         ++         +         00         0         0         const = 0.5           5         ++         +         03         360         0 $2\pi = 360$ 6         ++         +         01         628         318         600 $2\pi = 6.233186$ 7         ++         +         01         314         159         300 $\pi = 3.141593$ 1040         ++         +         01         314         159         0         1/2         =         11.199           2         ++         +         01         300         0         const = 2.30259         0         const = 2.30259           5         0         0         0         0         0         0         0           6         0         0         0         0         0         Kts = 10           1050         +         +         02         100         0         Kts = 12           2         +         +         02         120         0         Kts = 12           2         +         +         02         0                                 | Address | Si         | gn of     |           |               |       |                | Remarks                      |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |         | No.        | Order     | Order     | A1            | $A_2$ | A <sub>3</sub> |                              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |         |            |           |           | 1034 A        |       |                |                              |
| 10.1       1       1       0.3       260       0       0 $2\pi = 360$ 6       ++       +       01       628       318       600 $2\pi = 6.283186$ 7       ++       +       01       314       159       300 $\pi = 3.41593$ 1040       ++       +       02       100       0       const = 10         1       ++       +       03       315       0       0       const = 3         3       ++       -       10       315       0       1/C = 0.315 \cdot 10^{-1}         4       ++       +       01       230       259       0       const = 2.30259         5       0       0       0       0       0       0       0         1047       +       +       02       100       0 $K_{t_2} = 10$ 1050       ++       +       02       120       0 $K_{t_2} = 11$ 1       ++       +       02       100       0 $K_{t_2} = 12$ 2       ++       +       02       100       0 $K_{t_2} = 10$ 1050       ++       +       <   | 1034    | ++         | +-        | 00        | 500           | n i   | Ω              | const = 0.5                  |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 5       | 4-J.       | +         | 03        | 360           | ŏ     | õ              | $2\pi = 360$                 |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 6       | <br>-+-+-  | · •       | 01        | 628           | 318   | 600            | $2\pi = 6.283186$            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 7       | ++         | +         | 01        | 314           | 159   | 300            | $\pi = 3.141593$             |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1040    | ++         | -+-       | 02        | 100           | 0     | 0              | const = 10                   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1       |            | +         | 03        | 111           | 199   | 0              | $1^{\circ} = 111.199$        |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 2       | ++         | +         | 01        | 300           | 0     | 0              | const = 3                    |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 3       | ++         |           | 10        | 315           | 0     | 0              | $1/C = 0.315 \cdot 10^{-10}$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 4       | ++         | +         | 01        | 230           | 259   | 0              | const = 2.30259              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 5       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 6       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   |         |            |           |           | 1047 A        |       |                |                              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1047    | ++         | - <u></u> | 02        | 100           | 0     | 0              | $K_{t_1} = 10$               |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1050    | ++         | +         | 02        | 110           | 0     | 0              | $K_{f_{a}} = 11$             |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1       | ++         | +         | 02        | 120           | 0     | 0              | $K_{f_3} = 12$               |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 2       | ·+·+       | +         | 02        | 130           | 0     | 0              | $K_{t_{A}} = 13$             |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 3       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 4       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 5       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 6       |            |           | 0         | 0             | 0     | 0              | . 0                          |
| 1060 $++$ $+$ 02       100       0       0 $K_{rep} = 10$ 1 $++$ $+$ 02       100       0       0 $K_{o} = 10$ 1062       02       160       0       0 $T_{r_1} = 16$ 3       02       160       0       0 $T_{r_2} = 16$ 4       02       160       0       0 $T_{r_3} = 16$ 5       02       380       0       0 $T_{r_4} = 38$ 6       0       0       0       0       0         7       0       0       0       0       0         1070       0       0       0       0       0         10       0       0       0       0       0         1070       0       0       0       0       0         1070       0       0       0       0       0         4       02       160       0 $T_0 = 16$ 1075 A   | 7       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1060    | -++-       | +         | 02        | 100           | 0     | 0              | $K_{\rm rep} = 10$           |
| 1062       02       160       0 $T_{t_1} = 16$ 3       02       160       0 $T_{t_2} = 16$ 4       02       160       0       0 $T_{t_3} = 16$ 5       02       380       0       0 $T_{t_4} = 38$ 6       0       0       0       0       0         7       0       0       0       0       0         1070       0       0       0       0       0         1       0       0       0       0       0         4       02       160       0       0       0         1070       0       0       0       0       0         4       02       160       0       0       0         4       02       160       0 $T_0 = 16$ 1075 A  | 1       | ++         | +         | 02        | 100           | 0     | 0              | $K_0 = 10$                   |
| 1062       02       160       0 $T_{t_1} = 16$ 3       02       160       0 $T_{t_2} = 16$ 4       02       160       0       0 $T_{t_2} = 16$ 5       02       380       0       0 $T_{t_3} = 16$ 5       02       380       0       0 $T_{t_4} = 38$ 6       0       0       0       0       0         7       0       0       0       0       0         1070       0       0       0       0       0         1070       0       0       0       0       0         1070       0       0       0       0       0         2       0       0       0       0       0         3       0       0       0       0       0         4       02       160       0 $T_0 = 16$ 1075 A   |         |            |           |           | 1062 A        |       |                |                              |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1062    |            |           | 02        | 160           | 0     | 0              | $T_{f_1} = 16$               |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 3       |            |           | 02        | 160           | 0     | 0              | $T_{f_2} = 16$               |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 4       |            |           | 02        | 160           | 0     | 0              | $T_{i_3} = 16$               |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 5       |            |           | 02        | 380           | 0     | 0              | $T_{I_4} = 38$               |
| 7       0       0       0       0       0       0         1070       0       0       0       0       0       0         1       0       0       0       0       0       0         2       0       0       0       0       0       0         3       0       0       0       0       0       0         4       02       160       0       0 $T_0 = 16$ 1075 ++         1075 ++       +       02       701       0 $\lambda_0 = 70.1$ 6       ++       +       02       701       0       0 $\lambda_0 = 70.1$ 7       ++       +       0       430       0       0 $\gamma = 0.43$ 1100       ++       +       0       100       0 $a_{\varphi} = 0.1$   | 6.      |            |           | 0         | 0             | 0     | 0              | 0                            |
| 1070       0       0       0       0       0       0       0       0         1       0       0       0       0       0       0       0       0         2       0       0       0       0       0       0       0       0         3       0       0       0       0       0       0       0         4       02       160       0       0 $T_0 = 16$ 1075 A         1075       ++       +       02       701       0 $\lambda_0 = 70.1$ 6       ++       +       02       701       0       0 $\lambda_0 = 70.1$ 7       ++       +       0       430       0       0 $\gamma = 0.43$ 1100       ++       +       0       100       0 $a_{\varphi} = 0.1$  | 7       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$  | 1070    |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 1       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 2       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 3       |            |           | 0         | 0             | 0     | 0              | 0                            |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 4       |            |           | 02        | 160           | 0     | 0              | $T_0 = 16$                   |
| $6$ $++$ $+$ $02$ $701$ $0$ $0$ $\lambda_{9} = 70.1$ $7$ $++$ $+$ $0$ $430$ $0$ $0$ $\gamma = 0.43$ $1100$ $++$ $+$ $0$ $100$ $0$ $\alpha_{\varphi} = 0.1$   | 1075    | ᆂᆂ         | +         | 02        | 1075 A<br>401 | 0     | Û              | $m_{\rm c} \rightarrow 40.1$ |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 6       | 1<br>      | ا<br>ملہ  | 02        | 701           | 0     | 0              | $\lambda_0 = 70.1$           |
| $1100 + + + 0  100  0  0  a_{\varphi} = 0.1$   | 7       | - <u> </u> |           | 02        | 430           | 0     | ñ              | v = 0.43                     |
| 100 11 1 0 100 0 0 0 0 0 0 0 0 0 0 0 0   | 1100    | 1 1<br>=   |           | - A       | 100           | 0     | ñ              | $a_m = 0.45$                 |
| 1 + 1 + 0 = 100 = 0 = 01   | 1       |            | - -       | õ         | 100           | õ     | õ -            | $a_{\lambda} = 0.1$          |

| ~       |               |                       |       |        |    |    |                           |
|---------|---------------|-----------------------|-------|--------|----|----|---------------------------|
| Address | dress Sign of |                       | Order |        | ~_ | Δ. | Remarks                   |
| -       | No.           | No. Order $A_1 = A_2$ |       | A3     |    |    |                           |
| 2       | ++            | +                     | 01    | 300    | 0  | 0  | $N_{\sigma} = 3$          |
| 3       | -+·+-         | - [                   | 02    | 150    | 0  | 0  | KL = 15                   |
| 4       | · [           | -   ·                 | 01    | 116    | 0  | 0  | $\log L = 1.16$           |
| 5       | ++            | - -                   | 0     | 210    | 0  | 0  | B = 0.21                  |
| 6       | ++-           | +                     | 02    | 180    | 0  | 0  | $K_{1_{max}} = 18$        |
| 7       | ++            | +                     | 02    | 150    | 0  | 0  | $K_{2_{\text{max}}} = 15$ |
|         |               |                       |       | 1110 A |    |    |                           |
| 1110    | ++            | +                     | 04    | 100    | 0  | 0  | $\Delta_{\rm max} = 1000$ |
| 1       | ++            | +                     | 04    | 100    | 0  | 0  | $S_0 = 1000$              |
| 2       | ++            | +                     | 01    | 700    | 0  | 0  | m = 7                     |
| 3       | +-+-          | +                     | 01    | 400    | 0  | 0  | P = 4                     |
| 4       | ++            | +-                    | 02    | 300    | 0  | 0  | $K_1 = 30$                |
| 5       | ++            | +                     | 02    | 500    | 0  | 0  | $K_2 = 50$                |
| 6       | ++            | +                     | 0     | 100    | 0  | 0  | $A_K = 0.1$               |

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TABLE 19. CONTROL INFORMATION FOR SP-6

| A J.J., | Cor     | nmands a       | D 1         |      |                                 |  |  |  |
|---------|---------|----------------|-------------|------|---------------------------------|--|--|--|
| Address | Command | A <sub>1</sub> | $A_2$ $A_3$ |      | Remarks                         |  |  |  |
| 1123 A  |         |                |             |      |                                 |  |  |  |
| 1123    | 0       | 0              | 0           | 3240 | $(0, 0, A_{mn}) - (0, 0, 3240)$ |  |  |  |
| 4       | 0       | 0022           | 0           | 0    | [3(m-1), 0, 0] = (22, 0, 0)     |  |  |  |
| 5       | 0       | 0005           | 0           | 0    | (m-2, 0, 0) = (5, 0, 0)         |  |  |  |
| 6       | 0       | 0011           | 0           | 0    | (q-1, 0, 0) = (11, 0, 0)        |  |  |  |
| 7       | 0       | 0011           | 0           | 0    | (r-1, 0, 0) = (11, 0, 0)        |  |  |  |
| 1130    | 0       | 0              | 0003        | 0    | (0, n, 0) = (0, 3, 0)           |  |  |  |
| 1       | 0       | 0006           | 0           | 0    | (m-1, 0, 0) = (6, 0, 0)         |  |  |  |

Cells 1110-1117 contain:  $\Delta_{max}$ -maximum epicentral distance; S<sub>0</sub>-normalized multiplier for the computation of  $A_{10}$ ; *m*—number of lines of the matrix  $A_{mn}$  of the set  $M_1$ ; *p*-number of classes  $K_{f_i}$ ;  $K_1$ -number of cycles to compute  $A_{10}$  from  $K_{1_{\text{max}}}$  to  $K_{2_{\text{max}}}$ ;  $K_2$ —similar but from  $K_{2_{\text{max}}}$  to  $K_{\text{min}}$ ;  $a_K$ —computation interval of  $A_{10}$  about K.

The control data are in cells [123-1131 (Table 19) and mainly holds the same information as in Tables 3, 6, 9 and 13. Table 17 presents the results of the computations of 18 map points (2 columns) using the initial data of Tables 1, 17 and 18.

#### SP-7 PROGRAM TO COMPUTE THE $K_{max}$ MAP ACCORDING TO THE SEISMIC ACTIVITY MAP

While describing the SP-6 program which uses formula (13), it was mentioned that the increase in the energy class of a strong earthquake leads to a considerable increase in the zone for the computation of seismic activity  $\overline{A}$  (14).

It seems that, in the manual as well as the machine analysis of  $K_{\text{max}}$ , the values  $\overline{A}$  in the peaks of the point under study should be computed on large areas, especially for classes  $K_{\text{max}} \ge 17$ . This means that to compute the value  $K_{\rm max}$  in the outermost points on the map of the territory under investigation, there must be information about the epicenters of its peaks in the 150-300 km radius. Thus for Uzbekistan, one should have epicenter maps for Tajikistan and Kirgizia, otherwise the value  $K_{max}$  will be distorted in the periphery. Larger distortions are excluded by introducing corrections on the seismic background of the surrounding area (Zakharova, Seiduzova, 1969a). However, due to the inaccuracy of determining their value, this is not a better solution to the problem. It is preferable to use long-term observations for the epicenter maps. However, it is difficult to obtain such observations in Central Asia at the present time. There are few epicenter maps from which it is easy to get earthquake coordinates necessary for further computations. Lists of epicenters with all necessary informations have been published for only the last six years. Therefore, it is necessary to find other ways to get initial information while maintaining the accurate  $K_{\text{max}}$  computations. This may be achieved, it seems, by using seismic activity maps from the long-term observations of the seismic station network. The very first  $K_{\text{max}}$  map (Riznichenko, 1965) was actually compiled from an activity map. The seismic activity maps, constructed by various methods for the major seismo-active regions of the Soviet Union, may be found in special issues dedicated to the investigation of seismic regions (A.V. Kozlov, ed., 1969; V.N. Gaiskii, ed., 1970) and in the yearly periodical "Earthquakes in the USSR" between 1962 and 1966. From them, independent of the measurements, one can easily find the activity values of any grid, i.e., with any previously given interval, conditioned by the computation intervals of the activity map and the future map  $K_{max}$ . The SP-7 program is also based on initial information from the seismic activity map. Fig. 1 explains the method of entering the initial data set in the computer. Here, ABCD is the area of the future  $K_{max}$ map, A'B'C'D'-the area of the seismic activity map. The initial data consist of two matrices— $A_{mn}$  which reflects the area A'B'EF (Fig. 1) and  $A_{kl}$  (area FEC'D'). The entire map of activity A is covered by a graduated grid with  $a_{\varphi}$  latitudinal and  $a_{\lambda}$  longitudinal interval. At the grid nodes, the activity values are drawn and punched along the columns beginning from the left lower corner, i.e., from point A' (Fig. 1). The length of row n of the

PROGRAM SP-7

| Address | Command | A1     | A2   | $A_3$ |
|---------|---------|--------|------|-------|
|         |         | 0500 A |      |       |
| 0500    | 055     | 0522   | 1021 | 0522  |
| 1       | 013     | 0522   | 1123 | 0522  |
| 2       | 055     | 0545   | 1022 | 0545  |
| 3       | 013     | 0545   | 1125 | 0545  |
| 4       | 055     | 0552   | 1022 | 0552  |
| 5       | 013     | 0552   | 1124 | 0552  |
| 6       | .055    | 0764   | 1022 | 0764  |
| 7       | 013     | 0764   | 1126 | 0764  |
| 0510    | 055     | 0777   | 1022 | 0777  |
| 1       | 013     | 0777   | 1125 | 0777  |
| 2       | 055     | 0767   | 1022 | 0767  |
|         |         | 0513 A |      |       |
| 0513    | 013     | 0767   | 1134 | 0767  |
| 4       | 055     | 1012   | 1022 | 1012  |
| 5       | 013     | 1012   | 1127 | 1012  |
| 6       | 055     | 0771   | 1030 | 0771  |
| 7       | 013     | 0771   | 1135 | 0771  |
| 0520    | 056     | 0000   | 1014 | 0000  |
| 1       | 016     | 0523   | 7741 | 0007  |
| 2       | 000     | 0000   | 0000 | 0000  |
| 3       | 016     | 0525   | 7741 | 0007  |
| 4       | 000     | 1034   | 1034 | 1107  |
| 5       | 075     | 0000   | 1046 | 1177  |
|         |         | 0526 A |      |       |
| 0526    | 075     | 0000   | 0000 | 1206  |
| 7       | 004     | 1035   | 1036 | 1143  |
| 0530    | 016     | 0531   | 0554 | 0615  |
| 1       | 052     | 0000   | 0000 | 0000  |
| 2       | 075     | 0000   | 1045 | 1175  |
| 3       | 075     | 0000   | 1177 | 1176  |
| 4       | 452     | 0000   | 0000 | 0547  |
| 5       | 452     | 0000   | 0000 | 0543  |
| 6       | 004     | 1175   | 1143 | 1172  |
| 7       | 004     | 1176   | 1143 | 1173  |
| 0540    | 075     | 0000   | 1172 | 0140  |
| •••••   |         | 0541 A |      |       |
| 0541    | 0000    | 0000   | 0000 | 0000  |
| 2       | 056     | 0000   | 0616 | 0000  |
| 3       | 077     | 0000   | 0000 | 0000  |
| 4       | 001     | 1175   | 1072 | 1175  |
| 5       | 112     | 0000   | 0535 | 0001  |
| 6       | 075     | 0000   | 0000 | 0701  |
| v       |         | 0000   | 0000 | 0101  |

(Contd.)

| Address | Command | A1     | A <sub>3</sub> | A <sub>3</sub> |
|---------|---------|--------|----------------|----------------|
| 0550    | 075     | 0000   | 1045           | 1175           |
| 1       | 001     | 1176   | 1073           | 1176           |
| 2       | 112     | 0000   | 0534           | 0001           |
| 3       | 056     | 0000   | 0645           | 0000           |
|         |         | 0554 A |                |                |
| 0554    | 075     | 0000   | 1040           | 0140           |
| 5       | 016     | 0556   | 7714           | 0007           |
| 6       | 075     | 0000   | 0160           | 1201           |
| 7       | 075     | 0000   | 0101           | 1151           |
| 0560    | 075     | 0000   | 1077           | 1152           |
| 1       | 005     | 1201   | 1152           | 0140           |
| 2       | 016     | 0563   | 7711           | 0007           |
| 3       | 002     | 1151   | 0160           | 1151           |
| 4       | 002     | 1060   | 1061           | 1153           |
| 5       | 005     | 1153   | 0140           | 0140           |
| 6       | 016     | 0567   | 7711           | 0007           |
|         |         | 0567 A |                |                |
| 0567    | 075     | 0000   | 0160           | 1153           |
| 0570    | 005     | 1037   | 1074           | 1152           |
| 1       | 004     | 1151   | 1153           | 1151           |
| 2       | 004     | 1151   | 1152           | 1151           |
| 3       | 005     | 1151   | 1071           | 1202           |
| 4       | 052     | 0000   | 0000           | 0000           |
| 5       | 075     | 0000   | 1075           | 1145           |
| 6       | 075     | 0000   | 1076           | 1146           |
| 7       | 452     | 0000   | 0000           | 1007           |
| 0600    | 452     | 0000   | 0000           | 0762           |
| 1       | 004     | 1145   | 1143           | 1155           |
|         |         | 0602 A |                |                |
| 0602    | 004     | 1146   | 1143           | 1156           |
| 3       | 056     | 0604   | 0605           | 0641           |
| 4       | 005     | 1041   | 1151           | 1240           |
| 5       | 075     | 0000   | 1155           | 0140           |
| 6       | 016     | 0607   | 7712           | 0007           |
| 7       | 075     | 0000   | 0161           | 1147           |
| 0610    | 075     | 0000   | 0160           | 1150           |
| 1       | 075     | 0000   | 1156           | 0140           |
| 2       | 016     | 0613   | 7712           | 0007           |
| 3       | 075     | 0000   | 0161           | 1157           |
| 4       | 075     | 0000   | 0160           | 1160           |
|         |         | 0615 A |                |                |
| 0615    | 000     | 0000   | 0000           | 0000           |
| 6       | 016     | 0617   | 7712           | 0007           |
| 7       | 075     | 0000   | 0161           | 1161           |
| 0620    | 075     | 0000   | 0160           | 1162           |
| 1       | 075     | 0000   | 1173           | 0140           |

| Address | Command | A1     | A <sub>2</sub> | A_3  |
|---------|---------|--------|----------------|------|
| 2       | 016     | 0623   | 7712           | 0007 |
| 3       | 075     | 0000   | 0161           | 1163 |
| 4       | 075     | 0000   | 0161           | 1164 |
| 5       | 005     | 1147   | 1161           | 1151 |
| 6       | 005     | 1150   | 1160           | 1152 |
| 7       | 005     | 1152   | 1162           | 1152 |
|         |         | 0630 A |                |      |
| 0630    | 005     | 1152   | 1164           | 1152 |
| 1 .     | 001     | 1151   | 1152           | 1151 |
| 2       | 005     | 1150   | 1157           | 1152 |
| 3       | 005     | 1152   | 1162           | 1152 |
| 4       | 005     | 1152   | 1163           | 1152 |
| 5       | 001     | 1151   | 1151           | 1151 |
| б       | 075     | 0000   | 1151           | 0140 |
| 7       | 016     | 0640   | 7716           | 0007 |
| 0640    | 005     | 0160   | 1143           | 1151 |
| 1       | 077     | 0000   | 0000           | 0000 |
| 2       | 013     | 0641   | 1026           | 0641 |
|         |         | 0643 A |                |      |
| 0643    | 056     | 0000   | 0543           | 0000 |
| 4       | .056    | 0000   | 1210           | 0000 |
| 5       | 075     | 0000   | 0000           | 0710 |
| 6       | 002     | 1063   | 1034           | 1154 |
| 7       | 075     | 0000   | 1106           | 1140 |
| 0650    | 005     | 1201   | 1140           | 0140 |
| 1       | 016     | 0652   | 7710           | 0007 |
| 2       | 005     | 0160   | 1043           | 0140 |
| 3       | 016     | 0654   | 7714           | 0007 |
| 4       | 004     | 0160   | 1042           | 0140 |
| 5       | 016     | 0656   | 7710           | 0007 |
|         |         | 0656 A |                |      |
| 0656    | 075     | 0000   | 0160           | 1203 |
| 7       | 075     | 0000   | 1203           | 1165 |
| 60      | 002     | 1062   | 1034           | 1166 |
| 1       | 075     | 0000   | 0000           | 1171 |
| 2       | 075     | 0000   | 0000           | 1167 |
| 3       | 056     | 0664   | 0665           | 0671 |
| 4       | 002     | 1165   | 1240           | 0000 |
| 5       | 056     | 0666   | 0670           | 0674 |
| 6       | 001     | 1167   | 0000           | 1167 |
| 7       | 013     | 0671   | 1025           | 0671 |
| 0670    | 013     | 0674   | 1025           | 0674 |
|         |         | 0671 A |                |      |
| 0671    | 077     | 1165   | 2731           | 0000 |
| 2       | 076     | 0000   | 0.074          |      |

(Contd.)

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| Address | Command | A1     | A2    | A3   |
|---------|---------|--------|-------|------|
| 3       | 056     | 0000   | 0676  | 0000 |
| 4       | 077     | 0000   | 0000  | 0000 |
| 5       | 001     | 1171   | 0101  | 1171 |
| 6       | 002     | 1166   | 0101  | 1166 |
| 7       | 076     | 0000   | 0667  | 0000 |
| 0700    | 004     | 1167   | 1171  | 1204 |
| 1       | 000     | 0000   | 0000  | 0000 |
| 2       | 002     | 1140   | 1103  | 1152 |
| 3       | 005     | 1152   | 1105  | 1152 |
|         |         | 0704 A |       |      |
| 0704    | 001     | 1104   | 1152  | 1152 |
| 5       | 001     | 1152   | 1044  | 0140 |
| 6       | 005     | 0707   | 7710  | 0007 |
| 7       | 075     | 0000   | 0160  | 1205 |
| 0710    | 000     | 0000   | 0000  | 0000 |
| 1       | 000     | 0000   | 0000  | 0000 |
| 2       | 000     | 0000   | 0000  | 0000 |
| 3       | 002     | 1205   | 1204  | 0000 |
| 4       | 076     | 0000   | 0716  | 0000 |
| 5       | 056     | 0000   | 0754  | 0000 |
| 6       | 002     | 1204   | 1205  | 0000 |
| Ū       | 002     | 0717 4 |       |      |
| 0717    | 071     | 0000   | 0756  | 0000 |
| 0717    | 070     | 0000   | 0736  | 0000 |
| 0720    | 000     | 0000   | 0730  | 0000 |
| 2       | 075     | 0000   | 0000  | 0710 |
| 2       | 075     | 1064   | 1034  | 1174 |
| 3       | 075     | 0000   | 1107  | 1174 |
|         | 015     | 0726   | 0702  | 0710 |
| 5       | 010     | 1202   | 1102  | 1151 |
| 7       | 005     | 1151   | 1205  | 1151 |
| 0730    | 004     | 1151   | 1205  | 1151 |
| 0731    | 056     | 0000   | 1234  | 0000 |
| 0751    | 050     | 0722 4 | 1427  | 0000 |
|         |         | 0732 A |       |      |
| 0732    | 075     | 0000   | 0000  | 0710 |
| 3       | 016     | 0742   | 0660  | 0710 |
| 4       | 000     | 0000   | 0000  | 0000 |
| 2       | 000     | 0000   | 0000  | 0000 |
| 6       | 002     | 1140   | 1070  | 1140 |
| 1       | 002     | 1152   | 0101  | 1154 |
| 0740    | 076     | 0000   | 0650  | 0000 |
| 1       | 000     | 1205   | 0/22  | 0000 |
| 2       | 002     | 1205   | 1204  | 0000 |
| 5       | 076     | 0000   | 0/45  | 0000 |
| 4       | 056     | 0000   | 0754  | 0000 |
|         |         | 0745 A |       |      |
| 0745    | 002     | 1204   | 1 205 | 0000 |
|         |         |        |       |      |

| Address | Command | A <sub>1</sub> | A <sub>2</sub> | A <sub>3</sub> |
|---------|---------|----------------|----------------|----------------|
| 6       | 076     | 0000           | 0756           | 0000           |
| 7       | 002     | 1140           | 1070           | 1140           |
| 0750    | 002     | 1174           | 0101           | 1174           |
| 1       | 076     | 0000           | 0725           | 0000           |
| 2       | 056     | 0000           | 0756           | 0000           |
| 3       | 000     | 0000           | 0000           | 0000           |
| 4       | 005     | 1039           | 1070           | 1142           |
| 5       | 001     | 1140           | 1142           | 1140           |
| 6       | 001     | 1206           | 0101           | 1206           |
| 7       | 075     | 0000           | 1140           | 1207           |
|         |         | 0760 A         |                |                |
| 0760    | 016     | 0762           | 7751           | 0007           |
| 1       | 000     | 1207           | 4000           | 1207           |
| 2       | 077     | 0000           | 0000           | 0000           |
| 3       | 100     | 1145           | 1100           | 1145           |
| 4       | 112     | 0000           | 0600           | 0001           |
| 5       | 000     | 0000           | 0000           | 0000           |
| 6       | 000     | 0000           | 0000           | 0000           |
| 7       | 030     | 0000           | 0770           | 0000           |
| 0770    | 016     | 0772           | 7741           | 0007           |
| 1       | 000     | 0000           | 0000           | 0000           |
| 2       | 002     | 1065           | 1034           | 1170           |
|         |         | 0773 A         |                |                |
| 0773    | 056     | 0774           | 0775           | 0776           |
| 4       | 375     | 0000           | 0000           | 0000           |
| 5       | 052     | 0000           | 0000           | 0000           |
| 6       | 077     | 0000           | 0000           | 0000           |
| 7       | 112     | 0000           | 0776           | 0001           |
| 1000    | 013     | 0776           | 1032           | 0776           |
| I       | 002     | 1170           | 0101           | 1170           |
| 2       | 076     | 0000           | 0775           | 0000           |
| 3       | 0000    | 0000           | 0000           | 0000           |
| 4       | 000     | 0000           | 0000           | 0000           |
| 5       | 000     | 0000           | 0000           | 0000           |
|         |         | 1006 A         |                |                |
| 1006    | 001     | 1177           | 1073           | 1177           |
| 7       | 077     | 0000           | 0000           | 0000           |
| 1010    | 075     | 0000           | 1075           | 1145           |
| 1       | 001     | 1146           | 1101           | 1146           |
| 2       | 112     | 0000           | 0577           | 0001           |
| 3       | 077     | 0000           | 0000           | 0000           |
| 4       | 055     | 0774           | 1031           | 0774           |
| 5       | 013     | 0774           | 1121           | 0774           |
| 6       | 055     | 0666           | 1122           | 0666           |
| 7       | 013     | 0666           | 1122           | 0666           |
| 1020    | 056     | 0000           | 0521           | 0000           |

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BLOCK DIAGRAM OF PROGRAM SP-7



main matrix  $A_{mn}(A'B', Fig. 1)$  should not be less than twice the radius r of the activity averaging zone for the largest class  $K_{max}$ . The length of the column m should exceed the value 2r on the length of the future map ( $K_{max}$ — AB). Such dimensions of the matrix  $A_{mn}$  insure the computation of the value of  $K_{max}$  for column AB. The requirements for the length of the column of the additional matrix  $A_{kl}$  are the same as those for the length of the main matrix column, i.e., k = m (Fig. 1). The length of row l should insure the computation of the activity of the largest class  $K_{max}$  at points of the entire resulting map excluding column AB, i.e., should be equal to  $(AD-a_{\lambda})$ , where  $a_{\lambda}$  is the computation interval of  $K_{max}$  longitudewise.



Fig. 1. Placement of initial data for the SP-7 program:

ABCD—Area of the map  $K_{\max}$ ; A'B'C'D'—area of the map A; A'B'EF—main matrix of initial data; m—length of the column A'B'EF; n—length of the line (row) A'B'EF; FEC'D'—additional matrix of initial data; k = m—length of the column FEC'D'; l—length of the row FEC'D'; r—radius of the averaging zone A for the largest  $K_{\max}$  of the area investigated.

The matrices  $A_{mn}$  and  $A_{kl}$  constitute the main  $M_1$  and additional  $M'_1$  sets of initial data. If the main matrix is serially entered along with the SP-7 program and its members in the memory beginning from 4220, then the same addressing entry is required for each column of the additional matrix, that is, the net number after cell 4220 + kl. (Henceforth, mn and kl mean the number of members in the main and additional matrices of the initial data respectively.)

The punch cards of the additional matrix are entered only after the  $K_{max}$  values for its column AB are computed and printed. A shift of the entire matrix  $A_{mn}$  precedes the automatic introduction instruction, used in the program for this purpose. The shift is one column to the left for matrix  $A_{mn}$  representing area A'B'EF. The first column of the additional matrix  $A_{kl}$  is then entered in the empty place and  $K_{max}$  for the second column of the map ABCD is computed.

One more set of initial data  $M_2$  is considered in the computation. This matrix is characteristic of the seismic regime of the region under investigation. In them are included the inclination of the earthquake repeatability curve; the energy class  $K_0$  to which the seismic activity computation is related; class  $K_{\min}$ —the least of those in the region; period of appearance  $T_{\min}$ of the class  $K_{\min}$ ; coefficients of correlational dependence  $K_{\max} = K_{\max}$  ( $\overline{A}$ )  $\log \alpha$ ,  $\beta$  and  $K_{\alpha}$ ; and value of the maximum proposed  $K_{\max}$ . In the same data set are included the initial point coordinates of matrix  $A_{mn}$  (point A' in Fig. 1)— $\varphi_{A_0}$ ,  $\lambda_{A_0}$  and distances between the grid points on the activity map, representing matrices  $A_{mn}$  and  $A_{kl}$ — $a_{\varphi}$  and  $a_{\lambda}$ ; coordinates of the initial point computation of the map  $K_{\max}$ — $\varphi_0$  and  $\lambda_0$ ; the computation interval latitudinally  $a_{\varphi}$  and longitudinally  $a_{\lambda}$  and around  $K-a_K$ ;  $N_{\sigma}$ —number of epicenters in the averaging zone of activity,  $\overline{A}$ , defining the given accuracy and others.

Besides data sets  $M_1$ ,  $M'_1$ ,  $M_2$  the initial data include a) control data with information about the number of elements in each line and column of the matrix  $A_{ma}$  and the total number of elements in it, b) similar information about the resulting matrix  $K_{max}-K_{qr}$ ; c) addresses of the initial cells, necessary for instructions to enter and transfer the initial data sets.

The computer memory is used in the following manner: the program itself is in cells 0500-1020; 1034-1107—set  $M_2$ ; 1120-1133—control data. Set  $M_1$  (matrix  $A_{mn}$ ) is accommodated from cell 4220 and may engage all the remaining memory depending on the volume of mn excluding the number of cells m, which is necessary to record the first column of the matrix  $A_{kl}$ . Part of the memory is meant to record the intermediate data from the computation of  $K_{max}$ , e.g., the distances  $\Delta_l$  computed from each point of the computed  $K_{max}$  to the points of initial data set with activity values.

#### Block Diagram SP-7 (see p. 120)

The SP-7 program moves according to the block diagram. After the entry of the punch cards of the program and the initial data sets  $M_1$  and  $M_2$ , control is given to block 1. Here the addresses for the instructions to translate the initial data are calculated, as well as the cycles to compute intermediate values and the exact value of  $K_{\text{max}}$  depending on the control data. In block 2, the initial data sets  $M_1$  and  $M_2$  are converted from decimal to the binary system. In block 3, the data from the multiple computations of the seismic activity values are prepared for the succeeding blocks. Here the constant part B of the value  $\overline{A}$  has been computed. It depends only on the parameters of seismic regime of the region according to formula (37').

Blocks 1-3 prepare the main computation. In the succeeding blocks 4-12 the values of  $K_{\text{max}}$  are computed for the point under study. Thereafter a concrete  $K_{\text{max}}$  is chosen and dispatched for print. The entire row of values  $K_{\text{max}}$  is computed, the number of members of which depends directly on the step  $a_k$ . Meanwhile, in blocks 4–12 all further computations are continued for the initial computation point of the resulting map and are repeated with the following point, in accordance with the given computation step  $a'_{\varphi}$  and  $a'_{\lambda}$  (latitudinally and longitudinally). Block 4 computes the distance from the initial point of computation with coordinates  $\varphi_0$ ,  $\lambda_0$  to all grid nodes on the initial map of activity, representing matrix  $A_{mn}$  (A'B'EF) as in formula (40).

Block 5 computes the radius  $r_{\max_j}$  of the averaging zone of seismic activity. Its value  $A_1$  represents  $K_{1_{\max}}$ —largest of the proposed earthquake  $K_{\max}$  in the region in accordance with the correlational dependence (13).

The value  $r_{\max_j}$  is computed by formula (14). In block 6 all values  $\Delta_i$ , computed in block 4, are compared with the values  $r_{\max_j}$ . For all  $\Delta_i \leq r_{\max_j}$  the corresponding values of seismic activity  $A_i$  are chosen and totaled in block 7. The value of activity in the averaging zone of radius  $r_{\max_j}$  is equal to

$$A_z = \frac{\sum_{i=1}^{n} A_i}{n},\tag{49}$$

where *n*—number of points—initial map of activity nodes for which

 $\Delta_i \leqslant r_{\max_i}.$ 

Block 8 computes the tabular values of activity  $A_T$  for  $K_{\max} = K_{\max_j}$  according to formula (13). Then control is shifted to block 9 where the values  $A_z$  and  $A_T$  are compared.

If  $A_z > A_T$ , the value  $K_{\max}$  is larger than  $K_{\max}$  in the *i*th point under study. On the other hand, the value  $K_{max}$  in the *i*th point is also less than  $(K_{\max_i} + a_K)$ , since at each point are analyzed all values of the maximum possible earthquakes from  $K_{\max_1}$ ,  $K_{\max_2} = (K_{\max_1} - a_K)$  and so on to  $K_{\min}$ . Therefore, control is shifted to print the values of  $K_{max}$ , intermediate between  $K_{\max_j}$  and  $K_{\max_{j-1}}$ , i.e.,  $(K_{\max_j} + 0.5 a_K)$ . The equality  $A_z = A_T$  signifies total agreement of the investigated value  $K_{max}$  to the actual  $K_{max}$ , and the computation is stopped. Control is shifted to print the point of value  $K_{max}$ . With  $A_z < A_T$  the investigated value of  $K_{\text{max}}$  is more than the actual one and it is necessary to analyze lower values of  $K_{\max}$ , viz.,  $K_{\max_2} = (K_{\max_1} - a_K)$ , and control is shifted to block 5 to measure the value  $r_{max_2}$  of the averaging zone of activity, representing  $K_{max_2}$  in accordance with relation (14). Control is shifted from block 9 to block 5 only when  $K_{\max_j} > K_{2_{\max}}$ . Values  $K_{\max_j}$  to  $K_{2_{\max}}$  are analyzed in the same manner. When  $K_{\min} < K_{\max_j} \leq K_{2_{\max}}$  the further analysis of the values  $K_{\max}$  at the point is conducted differently. Control is shifted to block 10 to compute  $A_T$ , the value of the investigated  $K_{\text{max}}$ . Further control is shifted to block 11, where the radius  $r_{max}$ , of the averaging zone of activity  $A_z$  is computed according to formula (37) with  $\overline{A} = A_T$ , obtained in block 10, and  $N_{\Sigma} = N_{\sigma}$ . The obtained values of r' are compared

with all  $\Delta_i$  for the investigated point, for which control is again shifted from block 11 to block 6. Thereafter the seismic activity  $A_z$  in the averaging zone of radius r' is computed in block 7 by superimposing separate activity values at points whose  $\Delta_i \ll r'$ . Further control is shifted from block 7 to block 9 to compare the values of activity  $A_T$  and  $A_z$ . The result is either printed (blocks 12 and 13), or lesser values of  $K_{\max}$  at the computational points are investigated.

Various methods of investigating values of  $K_{\max}$  in the intervals from  $K_{1_{\max}}$  to  $K_{2_{\max}}$  and from  $K_{2_{\max}}$  to  $K_{\min}$  are explained as in the SP-6 program.

Since the computation of  $A_z$  is conducted for the seismic activity map, actually for its discreet values  $A_i$ , forming the initial matrices  $A_{mn}$  and  $A_{kl}$ , it is important that their sum must include at least three values of  $A_i$  as in formula (49). The number *n* in formula (49) is determined by the relationship of values *r* (radius of the averaging zone of activity) and *a* (distance between the graduated grid points of the initial map of activity). With r/a >1 the number *n* would be more than 3. With this relationship, the value of activity in the averaging zone of radius *r* and its value of  $K_{max}$  are also determined.

If the values  $A_T$  and  $A_z$  do not equalize in the succeeding cycles to compute  $K_{\max_j} > K_{\min}$ , all the described operations are repeated up to  $K_{\max} = K_{\min}$ . This completes the program for the investigated point. Control is shifted to block 13 where the result is printed, and a serial number and the value of  $K_{\max}$  is issued for each point of computation. Block 13 also analyzes the number of points  $N_T$ . With  $N_T = q \cdot r$ , where  $q \cdot r$ —number of points in the columns of the resulting matrix K, control is shifted to block 15. With  $N_T < q \cdot r$  control is shifted to block 14 to compute the next point of the column. Here the coordinates of the next point are chosen and the addresses of the necessary instructions are loaded to compute  $K_{\max}$ . Next control is shifted to block 4 to compute distances  $\Delta_l$ , etc.

The column of matrix  $A_{kl}$  is entered in block 15. This is necessary to compute  $K_{\max}$  in the next column of the map. After shifting control to block 16 the addresses of the cells are restored to re-record the activity values and all the matrices  $A_{mn}$  and the columns of matrix  $A_{kl}$  introduced in block 15 are shifted one column to the left. Block 17 prepares the computation of  $K_{\max}$  in the next column of the map and computes  $N_T$ . With  $N_T = q \cdot r$ , the number of members of the resulting matrix  $K_{qr}$ , the computation is stopped; if  $N_T < qr$  control is shifted to block 4 to compute  $K_{\max}$  in the first point of the next column  $K_{qr}$ .

The SP-7 program has a series of advantages concerning the sets of initial data over SP-6. First, the seismic activity maps of large territories are more accessible for investigations than the epicenter maps or similar lists. Second, the serialized initial material system formed in the matrix form, permits the computation of  $K_{max}$  for any desired large areas without using the additional memory of the computation. The information in the main memory is automatically shifted and the cells thus made free are used for additional data as already considered in the feeding instructions of the program. SP-6 uses maps of randomly placed epicenter. The computation of  $K_{\text{max}}$  for large territories must either use drums and magnetic tapes to increase memory, or prior group the epicenter coordinates so that it is possible to shift and automatically enter additional data. Either possibility can be achieved; however, it is much more convenient to avoid this complexity as in SP-7.

#### **Illustrative Example**

Unlike the other programs, the check-out version for SP-7 is somewhat complex. In explaining the programs SP-1, 2, 3, 4, and 6 where the main initial data set  $M_1$  was codified straight from the epicenter catalog, it was sufficient to give the parameters ( $\varphi_i$ ,  $\lambda_i$ ,  $K_i$ ) for some of them. Here we have from 7 to 20 to extend the volume of  $M_1$  to 21 or 60 elements. Usually, the epicenter catalogs are formed in chronological order, therefore, the epicenters of set  $M_1$  were more or less uniformly distributed along the region. This made it possible to work with the SP program. In SP-7 the data set  $M_1$  is made of seismic activity values A from a corresponding map with a certain grid and fixed coordinates  $\varphi_{A_0}$ ,  $\lambda_{A_0}$  of the initial point to be used for further computations.

In the computation of  $K_{max}$  for each point, SP-7 requires that the values of activity are totaled in an averaging zone with a changing radius up to 300 km and more. In this zone a different number of points are accommodated, depending on the given step A of the value of  $K_{max}$  to be analyzed Since SP-7 begins with the analysis of the largest  $K_{\text{max}}$ , e.g., K = 17 or 18, then at the beginning of the computation at any map point, the activity in the zone is averaged for hundreds of values of A, which are selected successively from the nodes of the given grid. The coordinates of the node have been computed earlier using given interval A from the given point  $\varphi_{A_0}$ ,  $\lambda_{A_0}$ . Therefore, it is not possible to limit the operation by a small number of values of A in one or two columns of initial matrix  $A_{mn}$ , since in all its cells, corresponding to remaining elements, a very large number (machine  $\infty$ ) would be held and the program could not run. For the control SP-7, therefore, it is necessary to add several additional instructions, introducing zeros in the matrix cells  $A_{mn}$  which are not engaged with the values of A (Table 20). Now data set  $M_1$  may hold the activity values A of one column of matrix  $A_{mn}$ , input 4422 A; and the column of matrix  $A_{kl}$ , input 6113 (Table 21).

The data set  $M_2$  (Table 22) holds the constants and conditions of computation. The latter include the coordinates of the initial point of matrix  $A_{mn} - \varphi_{A_0}$  and  $\lambda_{A_0}$ , the given step of its elements— $a_{\varphi_A}$  and  $a_{\lambda_A}$  latitudinally and longitudinally, the number of matrix elements—mn, number of its

.

| Address | Command | A <sub>1</sub> | $\mathbf{A}_{2}$ | $\mathbf{A}_{\mathfrak{g}}$ |
|---------|---------|----------------|------------------|-----------------------------|
| 1025    | 052     | 0000           | 0000             | 0000                        |
| 7       | 175     | 0000           | 0000             | 4422                        |
| 6       | 112     | 1470           | 1026             | 0001                        |
| 1030    | 056     | 0000           | 0500             | 0000                        |

### TABLE 21. DATA SET M<sub>1</sub> FOR SP-7

| Commands and numbers |      |       |       |        |         |      |  |
|----------------------|------|-------|-------|--------|---------|------|--|
| Address              | Sig  | 1 of  |       |        | <br>A . | A    | Remarks                                |
| •                    | No.  | Order | Older | AI     | A2      | 1.12 |  |
|                      |      | •     |       | 4422 A |         |      | •••••••••••••••••••••••••••••••••••••• |
| 4422                 | ++   | _     | 02    | 250    | 000     | 000  | $A_1 = 0.0025$                         |
| 3                    | -++- | _     | 03    | 300    | 000     | 000  | $A_2 = 0.0030$                         |
| 4                    | +++  | _     | 02    | 350    | 000     | 000  | $A_3 = 0.0035$                         |
| . 5                  | ++   | -     | 02    | 400    | 000     | 000  | $A_4 = 0.0040$                         |
| 6                    | ++   | -     | 02    | 550    | 000     | 000  | $A_5 = 0.0055$                         |
| . 7                  | ++   | -     | 02    | 700    | 000     | 000  | $A_6 = 0.0070$                         |
| 4430                 | +++  |       | 02    | 800    | 000     | 000  | $A_7 = 0.0080$                         |
| . 1                  | ++   |       | 01    | 100    | 000     | 000  | $A_8 = 0.0100$                         |
| 2                    | +- - | _     | 01    | 150    | 000     | 000  | $A_9 = 0.0150$                         |
| 3                    | .++  |       | 01    | 200    | 000     | 000  | $A_{10} = 0.0200$                      |
| 4                    | +-+- | -     | 01    | 400    | 000     | 000  | $A_{11} = 0.0400$                      |
| 5                    |      |       |       | 4435 A |         |      |  |
| 4435                 | ++   | -     | 01    | 500    | 000     | 000  | $A_{12} = 0.0500$                      |
| 6                    | ++   | -     | 01    | 500    | 000     | 000  | $A_{13} = 0.0500$                      |
| 7                    | ++   | -     | 01    | 500    | 000     | 000  | $A_{14} = 0.0500$                      |
| 4400                 | ++   |       | 01    | 500    | 000     | 000  | $A_{15} = 0.0500$                      |
| 1                    | ++   | -     | 01    | 400    | 000     | 000  | $A_{16} = 0.0400$                      |
| 2                    | ++   | -     | 01    | 300    | 000     | 000  | $A_{17} = 0.0300$                      |
| 3                    | ++   |       | 01    | 250    | 000     | 000  | $A_{18} = 0.0250$                      |
| 4                    | ++   | -     | 01    | 220    | 000     | 000  | $A_{19} = 0.0220$                      |
| 5                    | ++   | _     | 01    | 210    | 000     | 000  | $A_{so} = 0.0210$                      |
| 6                    | ++   | -     | 01    | 200    | 000     | 000  | $A_{21} = 0.0200$                      |
| 7                    | ++   |       | 01    | 180    | 000     | 000  | $A_{22} = 0.0180$                      |
|                      |      |       |       | 4450 A |         |      |  |
| 4450                 | ++   | -     | 01    | 160    | 000     | 000  | $A_{23} = 0.0160$                      |
| 1                    | ++   | · _   | 01    | 140    | 000     | 000  | $A_{24} = 0.0140$                      |
| 2                    | ++   | _     | 01    | 120    | 000     | 000  | $A_{25} = 0.0120$                      |
| 3                    | ++   |       | 01    | 100    | 000     | 000  | $A_{26} = 0.0100$                      |
| 4                    | ++   | -     | 02    | 000    | 000     | 000  | $A_{27} = 0.0090$                      |

5

|         |        | C     | Commands | and numb | bers  |                |                   |
|---------|--------|-------|----------|----------|-------|----------------|-------------------|
| Address | Si     | gn of | 0.1      |          |       |                | Remarks           |
|         | No.    | Order | Order    | $A_1$    | $A_2$ | $\mathbf{A}_3$ |                   |
| 5       | <br>++ |       | 02       | 800      | 000   | 000            | $A_{28} = 0.0080$ |
| 6       | ++     | -     | 02       | 700      | 000   | 000            | $A_{29} = 0.0070$ |
| 7       | ++     |       | 02       | 600      | 000   | 000            | $A_{30} = 0.0060$ |
| 4460    | ++     |       | 02       | 500      | 000   | 000            | $A_{31} = 0.0050$ |
| 1       | ++     |       | 02       | 400      | 000   | 000            | $A_{32} = 0.0040$ |
| 2       | -++-   |       | 02       | 300      | 000   | 000            | $A_{33} = 0.0030$ |
| 3       |        |       |          | 6113 A   |       |                |                   |
| 6113    | ++     |       | 00       | 400      | 000   | 000            | $A_{34} = 0.3000$ |
| 4       | ++     |       | 00       | 500      | 000   | 000            | $A_{35} = 0.5000$ |
| 5       | ++     | ~     | 00       | 500      | 000   | 000            | $A_{36} = 0.5000$ |
| 6       | ++     |       | 00       | 500      | 000   | 000            | $A_{37} = 0.5000$ |
| 7       | ++     |       | 00       | 400      | 000   | 000            | $A_{38} = 0.4000$ |
| 6120    | ++     |       | 00       | 400      | 000   | 000            | $A_{39} = 0.4000$ |
| 1       | ++     |       | 00       | 400      | 000   | 000            | $A_{40} = 0.4000$ |
| 2       | ++     |       | 00       | 500      | 000   | 000            | $A_{41} = 0.5000$ |
| 3       | ++     | +     | 01       | 100      | 000   | 000            | $A_{42} = 1.0000$ |
| 4       | ++     | +     | 01       | 100      | 000   | 000            | $A_{43} = 1.0000$ |
| 5       | ++     | +     | 01       | 100      | 000   | 000            | $A_{44} = 1.0000$ |
|         |        |       |          | 6126 A   |       |                |                   |
| 6126    | ++     | _     | 00       | 500      | 000   | 000            | $A_{45} = 0.5000$ |
| 7       | ++     | -     | 00       | 450      | 000   | 000            | $A_{46} = 0.4500$ |
| 6130    | ++     |       | 00       | 430      | 000   | 000            | $A_{47} = 0.4300$ |
| 1       | ++     |       | 00       | 410      | 000   | 000            | $A_{48} = 0.4100$ |
| 2       | ++     | -     | 00       | 400      | 000   | 000            | $A_{49} = 0.4000$ |
| 6133    | +-+-   | +     | 00       | 380      | 000   | 000            | $A_{50} = 0.3800$ |
| 4       | ++     | _     | 00       | 350      | 000   | 000            | $A_{51} = 0.3500$ |
| 5       | +-     | _     | 00       | 300      | 000   | 000            | $A_{52} = 0.3000$ |
| 6       | ++     | _     | 00       | 270      | 000   | 000            | $A_{53} = 0.2700$ |
| 7       | ++     |       | 00       | 250      | 000   | 000            | $A_{54} = 0.2500$ |
| 6140    | ++     | _     | 10       | 700      | 000   | 000            | $A_{55} = 0.0700$ |
|         |        |       |          | 6141 A   |       |                |                   |
| 6141    | ++     | -     | 01       | 370      | 000   | 000            | $A_{56} = 0.0870$ |
| 2       | ++     |       | 01       | 250      | 000   | 000            | $A_{a7} = 0.0250$ |
| 6143    | ++     | -     | 01       | 180      | 000   | 000            | $A_{58} = 0.0180$ |
| 4       | ++     |       | 01       | 160      | 000   | 000            | $A_{59} = 0.0160$ |
| 5       | ++     | _     | 01       | 140      | 000   | 000            | $A_{60} = 0.0140$ |
| 6       | ++     |       | 01       | 120      | 000   | 000            | $A_{61} = 0.0120$ |
| 7       | ++     | _     | 02       | 800      | 000   | 000            | $A_{62} = 0.0080$ |
| 6150    | ++     |       | 02       | 600      | 000   | 000            | $A_{63} = 0.0060$ |
| 1       | ++     | _     | 02       | 500      | 000   | 000            | $A_{64} = 0.0050$ |
| 2       | ++     | _     | 02       | 300      | 000   | 000            | $A_{65} = 0.0030$ |
| 6153    | ++     |       | 02       | 700      | 000   | 000            | $A_{66} = 0.0010$ |

TABLE 22. DATA SET M<sub>2</sub> FOR SP-7

| Commands and numbers |                                 |       |       |                |       |       |   |
|----------------------|---------------------------------|-------|-------|----------------|-------|-------|---|
| Address              | Si                              | gn of |       | <b>-</b>       |       |       | -<br>Remarks  |
|                      | No.                             | Order | Order | $\mathbf{A}_1$ | $A_2$ | $A_3$ |   |
| 1034 A               |                                 |       |       |                |       |       |   |
| 1034                 | ++                              | +     | 00    | 500            | 0     | 0     | const = 0.5   |
| 5                    | ++                              | -+-   | 03    | 360            | 0     | 0     | $2\pi = 360^{\circ}$                                  |
| 6                    | ++                              | +     | 01    | 628            | 318   | 600   | $2\pi = 6283186$                                      |
| 7                    | ++                              | -ţ-   | 01    | 314            | 159   | 300   | $\pi = 3.141593$                                      |
| 1040                 | ++                              | +     | 02    | 100            | 0     | 0     | const = 10  |
| 1                    | ++                              |       | 03    | 111            | 199   | 0     | $1^{\circ} = 111190 \text{ km}$                       |
| 2                    | ++                              | +-    | 01    | 300            | 0     | 0     | const = 3   |
| 3                    | ++                              |       | 01    | 315            | 0     | 0     | $1/C = 0315 \cdot 10^{-10}$                           |
| - 4                  | ┿╋                              | +     | 01    | 230            | 259   | 0     | const = 2.30259                                       |
| 5                    | ++                              | +     | 02    | 100            | 0     | 0     | $K_{\rm rep} = 10$                                    |
| 6                    | ++                              | +     | 02    | 100            | 0     | 0     | $K_0 = 10$  |
|                      |                                 |       |       | 1062 A         |       |       |   |
| 1062                 | - <b>├</b> - /->                | +     | 03    | 825            | 0     | 0     | mn = 825  |
| 3                    | ++                              | +     | 02    | 300            | 0     | 0     | $K_1 = 30$  |
| 4                    | ++                              | +     | 02    | 510            | 0     | 0     | $K_2 = 51$  |
| 5                    | +++                             |       | 02    | 250            | 0     | 0     | n = 25  |
| 6                    | - <del> -</del> - <del> -</del> | +     | 2     | 372            | 500   | 000   | $\varphi_{A_0} = 37.25$                               |
| 7                    | ++                              | +     | 2     | 640            | 000   | 000   | $\lambda_{A_0} = 64.00$                               |
| 1070                 | ++                              | +     | 0     | 100            | 0     | 0     | $a_{K} = 0.1$   |
| 1                    | ++                              | +     | 04    | 100            | 0     | 0     | $S_0 = 1000$  |
| 2                    | ++                              |       | 00    | 250            | 0     | 0     | $a_{\Psi K} = 0.25$                                   |
| 3                    | ++                              | -     | 00    | 333            | 333   | 333   | $aK_{A} = 0.33$                                       |
| 4                    | +++                             |       | 02    | 110            | 00    | 0     | $T_{\rm rep} = 11$                                    |
|                      |                                 |       |       | 1075 A         |       |       |   |
| 1075                 | ++                              |       | 02    | 402            | 500   | 0     | $\varphi_0 = 40.25$                                   |
| 6                    | ++                              | +     | 02    | 680            | 0     | 0     | $\lambda_a = 68.00$                                   |
| 7                    | ++                              | +-    | 00    | 460            | 0     | 0     | $\gamma = 0.46$                                       |
| 1100                 | ++                              | +     | 00    | 250            | 0     | 0     | $a_{\varphi} = 0.25$                                  |
| 1                    | - <del> </del> <del> </del> -   | +     | 00    | 333            | 333   | 333   | $a_{\lambda} = 0.33 \left(\frac{1^{\circ}}{3}\right)$ |
| 2                    | +- +-                           | +     | 01    | 800            | 0     | 0     | $N_{\sigma} = 8$                                      |
| 3                    | ++                              | +-    | 02    | 150            | 0     | 0     | $K_{\alpha} = 15$                                     |
| 4                    | +                               | +     | 01    | 116            | 0     | 0     | $\log \alpha = -1.16$                                 |
| 5                    | ++                              | +     | 00    | 210            | 0     | 0     | $\beta = 0.21$  |
| 6                    | ++                              | +     | 02    | 180            | 0     | 0     | $K_{1_{max}} = 18$                                    |
| 7                    | ++                              | +     | 02    | 150            | 0     | 0     | $K_{2_{\rm max}} = 15$                                |

|         |           | Con  | nmands an        | id numbers |      | <b></b>                          |  |
|---------|-----------|------|------------------|------------|------|----------------------------------|--|
| Address | Sig       | m of |                  |            |      | Remarks                          |  |
|         | No. Order |      | $\mathbf{A}_{1}$ | Ag         | A3   |                                  |  |
|         |           |      |                  | 1120 A     |      |                                  |  |
| 1120    |           | 0    | 0                | 6113       | 6052 | $(O_1A_1, n+1, A_1, n)$          |  |
| 1       |           | 0    | 0                | 4463       | 4422 | $(O_1A_{12}A_{11})$              |  |
| 2       |           | 0    | 0                | 4422       | 0    | $(O_1A_{11}O)$                   |  |
| 1123    |           | 0    | 4422             | 4422       | 6112 | $(A_{11}, A_{11}, A_{mn})$       |  |
| 4       |           | 0    | 0030             | 0          | 0    | (n-1, 0, 0)                      |  |
| 5       |           | 0    | 0040             | 0          | 0    | (m-1, 0, 0)                      |  |
| 6       |           | 0    | 0007             | 0          | 0    | (q-1, 0, 0)                      |  |
| 7       |           | 0    | 0001             | 0          | 0    | (r-1, 0, 0)                      |  |
| 1130    |           | 0    | 0027             | 0          | 0    | (n-2, 0, 0)                      |  |
| 1       |           | 0    | 1470             | 0          | 0    | (mn-1, 0, 0)                     |  |
| 2       |           | 0    | 6113             | 0          | 0    | $(A_1, n+1 0, 0)$                |  |
| 3       |           | 0    | 6113             | 6113       | 6153 | $(A_1, n+1, A_1, n+1, A_m, n+1)$ |  |

TABLE 23. CONTROL INFORMATION FOR SP-7

columns—*n*; coordinates of the initial point of computation— $\varphi_0$ ,  $\lambda_0$ ,  $A_0$  and step of computation  $a_{\varphi}$  and  $a_{\lambda}$  latitudinally and longitudinally. The remaining cells of  $M_2$  are named as in SP-6.

The control data for the illustrative example is shown in Table 23. Here  $A_{11}$  is the number of the initial cell of the first column of the matrix  $A_{mn}$ ;  $A_{12}$ —number of initial cell at the second;  $A_1$ , *n* number of first cell of the last column;  $aA_{mn}$ —number of the last of its cells  $A_1$ , n+1—number of the initial cell of the first column of the matrix  $A_{kl}$ ,  $A_m$ , n+1—last cell. The remaining names are the same as in the previous program.

The output of SP-7, based on initial data (Tables 20-23), for all columns of the map  $K_{\text{max}}$  (16 points) follows:

| $N_T$           | $K_{\max}$       |
|-----------------|------------------|
| +++01 100000000 | +++02 100000000. |

In this only NN points change— $N_T$ , whereas the values  $K_{\text{max}}$  remain the same as for point 1, therefore, the result for the last point would be as follows:

| $N_T$          | $K_{\max}$     |
|----------------|----------------|
| +++02 16000000 | +++02 10000000 |

Thus, for all 10 points  $K_{\text{max}} = 10$ , i.e., does not exceed the energy class of the least of the representative earthquakes  $K_{\min}$  in set  $M_2$ . This is explained by the small number of values of A in  $M_1$ .

## Chapter V

# Examples of the Computation of A and $K_{max}$ Maps by SP Programs

The SP programs were used to investigate the seismicity of Uzbekistan. Thus maps of seismic activity were computed for the eastern part of the Ferghana Valley and its surrounding hilly terrain. The initial data of the SP-1, 2, 3 and 4 programs are mainly the same. Set  $M_1$  was compiled using the catalog of Eastern Uzbekistan earthquakes from the Institute of Seismology, Academy of Sciences of the UzbSSR between 1968–1969. Here earthquakes with  $K \leq 13$  were recorded according to energy when they occurred (Zakharova, Matasova, 1971). Earthquakes with K = 13 were chosen for the period 1929–1969; K = 12, = 11, = 10 from 1951 to 1969 and K = 9from 1960 to 1969. Some presentations about the density of epicenter distribution in the investigated territory provide the map of earthquake epicenters (Fig. 2). Eastern Ferghana and its hilly terrain, for which the activity map was computed is shown here by a dash-dot line.

While calculating the map A, the values of K,  $\varphi$ , and  $\lambda$  were codified for each of the 500 earthquakes of set  $M_1$ . In set  $M_2$ , common to all the maps, were the values of energy classes  $K_{f_j}$  and corresponding to them, the periods of presentation  $T_{f_j}$ , viz:

| $K_{\rm f_1}=9$    | $T_{\rm f_2} = 8.5$ |
|--------------------|---------------------|
| $K_{\rm f_2} = 10$ | $T_{\rm f_2} = 18$  |
| $K_{\rm f3} = 11$  | $T_{f_3} = 18$      |
| $K_{\rm f4} = 12$  | $Tr_{5} = 18$       |
| $K_{\rm fs} = 13$  | $T_{6_{2}} = 40$    |

 $K_0 = 10$ —class of seismic energy to which the value of activity is referred;  $T_{\rm rep} = 8.5$ —is the representative period of earthquakes with the lowest energy from those used in computation;  $\gamma = 0.5$ —inclination of earthquakes repeatability curve. All maps of A were calculated with an identical interval, longitudinally and latitudinally, equal to 0.1°. Values of A at each computation point were normalized around a 1,000 km<sup>2</sup> area and one year period. For detailed maps, computed by SP-1 and SP-4, the area of averaging zone is  $S = 0.2^{\circ} \times 0.2^{\circ}$ , i.e., about 350 km<sup>2</sup>. While using SP-2 the area was changing and depended on the density of earthquake epicenters and the given minimum number of epicenters in the averaging zone— $N_{\sigma}$ . The combined SP-3 program computed A for each point of the map using an averaging zone of S = 350 km<sup>2</sup>; whereas with fewer than  $N_{\sigma}$  epicenters in it, it used a zone of varying area, as in SP-2.

Seismic activity maps  $A_{10}$  for the eastern Ferghana Valley and its hilly surroundings (areas) were computed by the SP programs (Figs. 3-7). Isolines  $A_{10}$  are shown everywhere with values  $A_{10} = 0.01$ ; 0.02; 0.05; 0.1; 0.2; 0.5; 1.0. The maps  $A_{10}$ , computed by the summation method with constant detailing by SP-1 (Fig. 3) and the combination method by SP-3 (Fig. 6), generally present a similar picture of the distribution of seismic activity values. In the first case, for all points of the map and for their overwhelming majority in



Fig. 2. Map of earthquake epicenters of Eastern Uzbekistan between 1951 and 1969:

Seismic energy:  $I - K \ge 14$ ; 2 - K = 13; 3 - K = 12; 4 - K = 11; 5 - K = 10; Class of accuracy: 6 - A; 7 - B; 8 - n/cl; 9 - Boundary of Ferghana Valley; 10 - Seismic stations; 11 - Boundary of section for which the map  $A_{10}$  was compiled by computer.



Fig. 3. Detailed seismic activity map  $A_{10}$  for Eastern Ferghana, computed by the summation method using SP-1:

*I*—Isoline  $A_{10}$  value of activity; 2–1.0 >  $A_{10} \ge 0.5$ ; 3–0.5 >  $A_{10} \ge 0.2$ ; 4–0.2 >  $A_{10} \ge 0.1$ ; 5– $A_{10} < 0.1$ ; 6–inhabited places.



Fig. 4. Seismic activity map  $A_{10}$  with constant accuracy for Eastern Ferghana, computed by the summation method using SP-2 with  $N_{\sigma} = 5$ : For legend see Fig. 3.



Fig. 5. Seismic activity map with constant accuracy for Eastern Ferghana, computed by the method of summation using SP-2 with  $N_{\sigma} = 8$ : For legends see Fig. 3.



Fig. 6. Seismic activity map  $A_{10}$  for Eastern Ferghana. computed by the combination method using SP-3: For legend see Fig. 3.



*1*—Isolines of activity. Values of activity:  $2-A_{10} \ge 1.0$ ;  $3-1.0 > A_{10} \ge 0.5$ ;  $4-0.5 > A_{10} \ge 0.2$ ;  $5-0.2 > A_{10} \ge 0.1$ ;  $6-A_{10} < 0.1$ ; 7—inhabited places.

the second, the values of  $A_{10}$  were computed in the averaging zone of the same  $0.2^{\circ} \times 0.2^{\circ}$  area of the geographical radius with not less than three epicenters  $N_{\sigma}$ .

Computations were stopped only for those points with averaging zones of activity of  $N_o < 3$  in SP-1 (Fig. 3) and a zero value of  $A_{10}$  was recorded for them. In SP-3 (Fig. 6) computations were continued with an increase in area until  $N_o = 3$ . This explains the somewhat lesser differentiation of zone  $A_{10}$  (Fig. 6) compared to regions of lower activity values (Fig. 3) and also the difference of the minimum levels  $A_{10}$  on these maps. Their isolines  $A_{10}$ extend in two directions—northeast and northwest.

The background activity values, i.e., the values engaging a larger part of the computed territory consist of  $0.2 < A_{10} < 0.5$  and cover the central northwestern and southeastern parts. The most extended region of lower activity values is in Ferghana valley itself (between the cities Hamangan, Andijan, and Ferghana);  $A_{10}$  does not exceed 0.2. In the hilly surroundings to the north and east, the value of  $A_{10}$  increases to 0.5 but nowhere reaches 1.0. All four of the regions of increased values of activity (where  $A_{10} > 0.5$ ) are beyond the Ferghana Valley boundary.

Two are north-northeast of Namangan near the foot of Bozbutau and
Ortatokar, close to the North Ferghana flexure-fault zone. The third region is east of Osh and close to the Kurshabsk fold zone where the newest structures of the Alai and Ferghana ridges join. Finally, the fourth region of the increased value of  $A_{10}$  is between the cities of Osh and Ferghana on the northern slopes of the Alai ridge, close to the Southern Ferghana flexure-fault zone.

If the  $A_{10}$  maps are compared (Figs. 3, 6 and 4, 5), it is clear that the first is more detailed, since it was constructed mainly with constant detailing with  $N_{\sigma} = 3$ , i.e., with a small averaging zone of activity. The second was computed according to SP-2 with constant accuracy, in which, with  $N_{\sigma} = 5$  (Fig. 4) and with  $N_{\sigma} = 8$  (Fig. 5), there was a larger area of averaging zone. This also explains the increase in the zone of uniform activity on corresponding maps. This can be easily seen in Fig. 5 where are merged not only the small activity zones ( $A_{10} = 0.1$ -0.2) (Fig. 4), but also the background—0.2 <  $A_{10} < 0.5$ . The computer map of  $A_{10}$  according to SP-2 with  $N_{\sigma} = 3$  has a similar configuration of activity isolines and also the same level as the maps on Figs. 3 and 6. Still further differentiated are the regions of uniform seismic activity on the map of  $A_{10}$  constructed with constant detailing. Their computations of activity values were conducted by the distribution method according to SP-4 (Fig. 7).



Fig. 8. Tracing from the seismic activity map with constant accuracy for Central Asia, manually computed by the summation method. Legend same as in Fig. 3

except values of activity  $3-0.5 > A_{10} \ge 0.25$ ;  $4-0.25 > A_{10} \ge 0.1$ .



Fig. 9. Seismic activity map  $A_{10}$  with constant detailing for Eastern Ferghana, manually computed by the summation method: For legend see Fig. 7.



Fig. 10. Map of largest possible earthquakes  $K_{\text{max}}$  computed from the activity map using SP-7.

Here, with the same background activity the extent of the zone is considerably less with a larger increase of their values and level of the maxima of  $A_{10}$ . This depends on the method of computing the activity and the smaller value of the given number of epicenters in the averaging zone  $(N_{\sigma} = 1)$  in which the value of  $A_{10}$  is considered significant.

Let us consider the seismic activity maps computed (Figs. 3, 5), with the



maps constructed manually (Figs. 8, 9). A strict comparison, it is regretted, was not possible since the maps computed by hand were not totally analogous to those of machine computations.

Figures 8 and 9 present maps in which most computation conditions are similar to the computer computations given in Figs. 3 and 5. Fig. 8 shows a tracing from the  $A_{10}$  map for Central Asia (Bune, Vvedenskaya, Gzovskii, Gorbunova, 1970). The map with uniform accuracy was compiled by computer. The activity values in the averaging zones of the changing area, depending on the epicenter density, were attributed to the centers of  $1600 \,\mathrm{km^2}$ units. For initial data, a map of the representative earthquake epicenters with  $K \ge 10$  between 1956 and 1966 was used. It was less detailed than illustrated on Fig. 5, where under strictly identical conditions the computation interval was 0.1°, i.e., the activity values were attributed to the centers of areas approximately four times less ( $S = 350 \text{ km}^2$ ). The activity levels of the Ferghana Valley and its hilly surroundings are identical (Figs. 8 and 5). In Fig. 9. a tracing from the seismic activity map of Uzbekistan is shown (B.B. Tal'-Virskii, A.I. Zakharova and I.B. Yakovleva, 1971). This map was constructed with constant detailing with a computation interval of  $0.1^{\circ}$ . The activity values in the averaging zone were computed by the summation method. The general isolines configuration of  $A_{10}$  is comparable here with those described in Fig. 3, but the level of  $A_{10}$  is almost twice higher. This is because during manual calculations, in the averaging zone, where earthquakes with K = 9 were absent, in formula (37) we used  $K_{\min} = 10$ . So the weight of each earthquake in the zone was almost tripled as compared with  $K_{\min} = 9.$ 

Besides the above seismic activity maps, the map of maximum possible earthquakes were also computed with these programs. Fig. 10 shows a map of  $K_{\text{max}}$  for Eastern Uzbekistan computed by the SP-7 program. To compile the initial data set  $M_1$ , a seismic activity map of Central Asia was used, the main part of which was constructed according to the data from V.I. Bune and others (1970): The western part (between 64–68° E), according to B.B. Tal'-Virskii, A.I. Zakharova, and I.B. Yakovleva (1971) and the northern (between—43.5–45.5°N) were extrapolated from the values of  $A_{10} = 0.02-$ 0.005 to 0.001, since observations about earthquakes are not conducted in this territory.

The values of  $A_{10}$  were drawn from this map with an interval 0.25° latitudinally and 0.33° longitudinally, i.e., in the centers of zones with nearly 3,600 km<sup>2</sup> areas to prevent overstating the initial data detailing (values  $A_{10}$ were calculated on the map to the centers of areas S = 1,600 km<sup>2</sup>). In accordance with the plan to accommodate initial data for SP-7, the area of the activity map somewhat exceeded the area of the  $K_{\text{max}}$  map to insure the averaging of  $A_{10}$  in the zone responsible for the appearance of earthquakes with K = 18, and was limited by the following coordinates: 37-45.5°N latitude and 64–78°E longitude. The contours of the map  $K_{\text{max}}$  were denoted by the same letters ABCD (Fig. 1). The computation of the values of  $K_{\text{max}}$ was latitudinal and longitudinal with the same interval around K through 0.1 ( $a_K$ ) from which the values of seismic activity  $A_{10}$  were drawn from the initial map, i.e.,  $a_{\varphi_K} = a_{\varphi_A} = 0.25^\circ$  and  $a_{\lambda K} = a_{\lambda A} = 0.33^\circ$ . The computations and characteristics of seismicity of the investigated territory in set  $M_2$ are as follows:

1) The computation conditions of the initial map of seismic activity and codification of the values  $A_{10}$ :

| $\gamma = 0.46$    | $N_{\sigma} = 8$               | $a_{\varphi_A} = 0.25$ |
|--------------------|--------------------------------|------------------------|
| $K_0 = 10$         | $S_0 = 1000$                   | $a_{\lambda_A} = 0.33$ |
| $K_{\min} = 10$    | $\varphi_{A_0}=64^{\circ}00$   |                        |
| $T_{\rm pri} = 11$ | $\lambda_{A_0} = 37^{\circ}00$ |                        |

2) The parameters of correlational dependence  $A = A(K_{\text{max}})$  and the computation conditions of the map  $K_{\text{max}}$ :

| $\log \alpha = -1.16$ | $a_{m{\varphi}}=0.25$ | $\varphi_0 = 40^\circ 25$    |
|-----------------------|-----------------------|------------------------------|
| $\beta = 0.21$        | $a_{\lambda}=0.33$    | $\lambda = 68^{\circ}00$     |
| $K_{\alpha} = 15$     | $a_{K} = 0.1$         | $1/c = 0.315 \cdot 10^{-10}$ |
| $K_{imax} = 18$       | mn = 825              |                              |
| $K_{2\max} = 15$      |                       |                              |

On the computer  $K_{\text{max}}$  map (Fig. 10), the isolines are shown through 0.5 of the value of K analogous to the map (Fig. 11) constructed manually (Zakharova, Seiduzova, 1970). The relative distribution of the values of  $K_{\text{max}}$  on them are almost identical: increased values of  $K_{\text{max}}$  are noticed on the larger eastern part of the investigated territory (Ferghana Valley and its hilly surroundings in the north, east, and south). Here the corresponding isolines are considerably different and have the values  $K_{\text{max}} = 17-18$  (Fig. 10). The described region (Fig. 11) is contoured only by one isoline  $K_{\text{max}} =$ 17. West of it, in the transitional region from the hill to the Pritashkent Valley, the values of  $K_{\text{max}}$  are reduced to 15.5-16 on both maps; their isolines are denser and extend more or less identically.

In the Pritashkent plains the smallest  $K_{\text{max}}$  are noticed for those computed for Eastern Uzbekistan—15.5–14 (Fig. 10) and 15.5–15 (Fig. 10). The maximum differences of 1.5 K in the absolute values of  $K_{\text{max}}$  were noticed on these maps on the small section between Ferghana Valley and Pritashkent. Here  $K_{\text{max}} = 17-17.5$  by computer as against 15.5–16 by hand calculation. The maximum possible earthquake values differ considerably (in unit of  $K_{\text{max}}$ ) in the Ferghana Valley where the computer gives  $K_{\text{max}} = 18$ ; it is 17 manually. On the northwest edges of Pritashkent with the same  $K_{\text{max}}$ difference of 1.0 K the machine computations are lower than those by hand  $(K_{\text{max}} = 14 \text{ and } 15 \text{ accordingly})$ . This difference in the value of  $K_{\text{max}}$  is explained by nonuniform initial data. In the first case (Fig. 11) the map of earthquake epicenters was used as initial material. It was reliable only for the territory of the  $K_{\text{max}}$  map itself. Therefore, the seismic activity values, and also the values of  $K_{\text{max}}$ , are most accurately computed for those map points, whose averaging zones were wholly within the limits of the epicenter map. Seismic activity in the region surrounding this map was only approximate and should reflect on the results of the computation of  $K_{\text{max}}$ .



Fig. 11. Map of largest possible earthquakes  $K_{max}$ , computed from the epicenter map by hand.

The computer used initial data directly drawn from the seismic activity map. They somewhat exceeded the boundaries of the  $K_{\text{max}}$  map and made it possible to consider more accurately seismic activity in the averaging zones for each point. Therefore the values of  $K_{\text{max}}$  on Fig. 11 exceed those on Fig. 12\* almost everywhere. A reverse relationship of the values of  $K_{\text{max}}$  in the Pritashkent Valley is because the earthquakes with K = 8 were considered for this territory (Fig. 12\*). In the machine computation information about focal seismicity was taken as uniform for all of Eastern Uzbekistan, i.e., limited by the least class of energy K = 10.

Thus the programs SP-1, 2, 3, 4, and 5 may be successfully used not only to obtain long-term average values of the distribution of parameters of the seismic regime in space, but also to considerably simplify the investigation of the variation of the seismic process in time. SP-6 and SP-7, seemingly, may also be used to investigate the values of energy density in the foci of strong earthquakes.

\*Correct as per the Russian original. This figure is not available in the Russian text-General Editor.

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