

**Civil Engineering Study  
Structural Series 89-31**

**INRESB-3D-SUP**

**USER'S MANUAL**

**A COMPUTER PROGRAM FOR INELASTIC  
ANALYSIS OF 3-DIMENSIONAL  
REINFORCED-CONCRETE AND  
STEEL SEISMIC BUILDINGS**

by

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**Report Series  
Prepared for the National Science Foundation under Grant  
NSF ECE 8513852**

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## ABSTRACT

This report has been prepared as a user's guide for the computer program, INRESB-3D-SUP, for analyzing elastic and inelastic building systems subjected to static loadings, multi-component earthquake motions, and pseudo-static cyclic loadings. Additionally, the program is capable of calculating the elastic natural frequency and buckling load.

A joint based system is used to define the geometry of the structure. The structural members may be elastic 3D prismatic beams, nonlinear reinforced concrete shear walls, and nonlinear springs. For the shear wall elements, the hysteresis models are for bending, shear and axial force-deformation relationships for low-rise walls. The Takeda model may be used for beams, columns and slender walls. The bilinear hysteresis model is also included. The geometric matrix for large deformations is available for both the elastic 3D prismatic beam and reinforced concrete shear wall elements.

The system formulation has the following attributes: 1) joint based degrees of freedom, 2) rigid body and planar constraints, 3) incremental nonlinear static solution, 4) unbalanced load correction for overshooting, 5) incremental nonlinear dynamic solution, 6) mass and stiffness proportional damping, 7) condensation to reduce the size of a dynamic problem, 8) energy balance, 9) damage index, and 10) ductility and excursion ratio for various definitions of displacement, constant strain energy, and variable strain energy. The computer program has been developed for achieving efficiency in both the computation and data preparation. The output solutions include the static results of member forces and joint displacements as well as the dynamic results of member forces, joint displacements, ductility factors, excursion ratios,

damage indices, seismic input energies, dissipated energies, and the option of saving data for plotting.

The main features of the report include the program listing, a description of the program, instructions for data preparation, and a guide to modify the programs dynamic storage.

#### ACKNOWLEDGMENTS

This is one of a series of reports on response analysis and optimum design of building systems with multicomponent seismic input and code provisions studied at UMR. This report is based on a joint research project undertaken by a team at NCKU (National Cheng-Kung University, Taiwan) and UMR. NCKU performed experimental work and UMR carried out analytical studies. UMR work was supported by the National Science Foundation under the grant NSF ECE 8513852. The authors gratefully acknowledge the NSF support and the experimental data provided by NCKU team, particularly Dr. S.C. Liu of NSF, Drs. M.S. Sheu, W.M. Liao, and Y.T. Kuo of NCKU. Dr. Sheu is the principal investigator of the NCKU team.

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## TABLE OF CONTENTS

	Page
ABSTRACT .....	ii
ACKNOWLEDGMENTS .....	iv
LIST OF ILLUSTRATIONS .....	ix
LIST OF TABLES .....	xi
I. INTRODUCTION .....	1
II. DESCRIPTION OF INRESB-3D-SUP COMPUTER PROGRAM	2
A. STRUCT - DEFINITION OF THE STRUCTURAL MODEL	2
1. Material Library .....	4
a. Elastic 3D Prismatic Beam Material .....	4
b. R/C Axial Hysteresis Model .....	4
c. Cheng-Mertz B1 Bending Hysteresis Model .....	4
d. Cheng-Mertz S1 Shear Hysteresis Model .....	8
e. Takeda Hysteresis Model .....	8
f. Bilinear Hysteresis Model .....	8
2. Element Library .....	8
a. Elastic 3D Prismatic Beam Element .....	8
b. Spring Element .....	13
c. Reinforced Concrete Shear Wall Element .....	18
B. SOL01 - ELASTIC STATIC ANALYSIS WITH MULTIPLE LOAD CASES .....	20
C. SOL02 - ELASTIC / NONLINEAR SEISMIC TIME HISTORY RESPONSE .....	20
D. SOL03 - ELASTIC NATURAL FREQUENCY / ELASTIC BUCKLING LOAD .....	24
E. SOL04 - NONLINEAR STATIC CYCLIC RESPONSE .....	26

III.	DESCRIPTION OF PROGRAM .....	30
	A. MAIN PROGRAM AND COMMON BLOCKS .....	30
	B. DESCRIPTION OF ROUTINES .....	33
	C. DESCRIPTION OF MISCELLANEOUS ROUTINES .....	41
	D. DYNAMIC MEMORY MANAGEMENT .....	42
	1. Dynamic Memory Allocation .....	42
	2. Compact Matrix Storage .....	43
	3. Capacity of the Dynamic Memory .....	45
	E. ADDITION OF MATERIALS, ELEMENTS, AND SOLUTIONS .....	47
	1. Addition of a Material to the Material Library .....	47
	2. Addition of an Element to the Element Library .....	48
	3. Addition of a Solution .....	49
IV.	INPUT DATA FOR PROGRAM INRESB-3D-SUP .....	50
	A. STRUCTURE - DEFINE THE STRUCTURAL MODEL .....	52
	1. Joints and Degrees of Freedom .....	53
	a. Joint Coordinates .....	53
	b. Joint Direction Cosines .....	55
	c. Joint Restraints .....	55
	d. Joint Condensation .....	56
	e. Joint Constraints .....	57
	2. Materials and Hysteresis Model Information .....	58
	a. TYPE = '3D-BEAM' .....	59
	b. TYPE = 'AXLMOD' .....	59
	c. TYPE = 'BEND1' .....	60
	d. TYPE = 'SHEAR1' .....	60
	e. TYPE = 'TAKEDA' .....	61
	f. TYPE = 'BILINEAR' .....	62

3. Geometric Stiffness Data .....	62
4. Element Data .....	63
a. TYPE = '3D-BEAM' .....	64
b. TYPE = 'SPRING' .....	65
c. TYPE = 'SHEAR WALL' .....	67
5. Mass .....	68
6. Damping .....	69
B. SOL01 - ELASTIC STATIC SOLUTION .....	70
1. Joint Loads .....	71
2. Element Loads .....	72
C. SOL02 - DYNAMIC SOLUTION BY NUMERICAL INTEGRATION .....	74
1. Special Loading Mass .....	76
2. Output Data to Disk Files .....	76
3. Initial Displacements, Velocities, Accelerations and Loads .	78
4. Ground Acceleration Record .....	80
D. SOL03 - EIGENVALUE SOLUTION .....	83
E. SOL04 - INCREMENTAL STATIC SOLUTION .....	84
1. Output Data to Disk Files .....	84
2. Joint Loads .....	85
3. Element Loads .....	85
4. Load Factors .....	85
F. BUG - SET BUG OPTIONS .....	86
G. READ - READ OUTPUT FILES .....	87
H. NOECHO - INHIBIT INPUT ECHO .....	88
I. DUMP - PRINT MEMORY .....	88
J. RELEASE - RELEASE MEMORY .....	88
K. STOP - TERMINATE EXECUTION .....	89

V.	RUNNING PROGRAM INRESB-3D-SUP .....	91
	A. GENERATING THE COMMON BLOCK MACRO LIBRARY	91
	B. COMPILING THE PROGRAM .....	91
	C. RUNNING THE PROGRAM .....	92
VI.	EXAMPLE PROBLEMS .....	94
	A. CANTILEVER BEAM .....	94
	1. Description of Input Information .....	94
	2. Input Data .....	95
	3. Output .....	96
	B. ONE STORY R/C BOX TYPE BUILDING .....	99
	1. Description of Input Information .....	99
	2. Input Data .....	101
	3. Output .....	103
	C. TWO STORY UNSYMMETRIC BUILDING WITH ISOLATED SHEAR WALLS .....	107
	1. Description of Input Information .....	107
	2. Input Data .....	110
	3. Output .....	112
	BIBLIOGRAPHY .....	120
APPENDICES		
A.	Ductility and Excursion Ratio .....	122
B.	Damage Index .....	125
C.	Listing of Program INRESB-3D-SUP .....	127

## LIST OF ILLUSTRATIONS

Figure		Page
1	Block STRUCT - Define the Structural Model .....	3
2	Axial Hysteresis Model Before Tensile Yield .....	5
3	Axial Hysteresis Model After Tensile Yield .....	5
4	Low-Rise Shear Wall Cheng-Mertz Bending Hysteresis Model .....	6
5	Multiple Segment Backbone Curve .....	7
6	Low-Rise Shear Wall Shear Cheng-Mertz Hysteresis Model .....	9
7	Takeda Hysteresis Model .....	10
8	Bilinear Hysteresis Model .....	11
9	3D Prismatic Beam Element .....	12
10	Spring Element .....	14
11	Diagonal Bracing Member Modeled With an Axial Spring .....	15
12	Two DOF Model With Shear Springs .....	16
13	Member End Rotation of an Elastic 3D Prismatic Beam Modeled with a Rotational Spring .....	17
14	Shear Wall Element .....	19
15	Block SOL01 - Static Analysis .....	21
16	Block SOL02 - Elastic / Nonlinear Dynamic Analysis .....	22
17	Block SOL03 - Natural Frequency / Elastic Buckling Load .....	25
18	Block SOL04 - Nonlinear Static Cyclic Response .....	27
19	Flow Chart for Program INRESB-3D-SUP: Part A .....	31
20	Flow Chart for Program INRESB-3D-SUP: Part B .....	32
21	Dynamic Memory Example .....	44
22	Cantilever Beam .....	95
23	One Story R/C Box Type Building .....	100

24	Two-story Unsymmetric building: Dimensions, Joints and Walls . . . . .	108
25	Two-story Unsymmetric building: Degrees of Freedom . . . . .	109
26	Displacement Definition of Ductility . . . . .	123
27	Variable Strain Energy Definition of Ductility . . . . .	123
28	Constant Strain Energy Definition of Ductility . . . . .	123

## LIST OF TABLES

Table		Page
I	DEGREES OF FREEDOM FOR UT BOX B6 .....	102

## I. INTRODUCTION

This publication is to serve as the user's manual of the computer program, INRESB-3D-SUP (INelastic Analysis of REinforced Concrete and Steel Building Systems for 3-Dimensional Ground Motions). The numerical procedures of the program are described in Chapter II. In Chapter III, the description of the subroutines, the programs capacity and the addition of materials, elements and solutions are discussed. Chapter IV contains the detailed input instructions. Instructions for running the program under the CMS environment for an IBM computer are included in Chapter V. In Chapter VI, three examples are used to illustrate the preparation of the input data and the output of solutions. The ductility and excursion ratios are derived in Appendix A. The damage index is discussed in Appendix B. The program listing is given in Appendix C.



## II. DESCRIPTION OF INRESB-3D-SUP COMPUTER PROGRAM

The computer program INRESB-3D-SUP is capable of analyzing elastic and nonlinear 3D structures subject to static and seismic loadings. The nonlinear behavior of R/C shear walls is represented by a shear wall element. A nonlinear spring element is also included that may be used to represent steel and reinforced concrete members.

INRESB-3D-SUP is a modular computer program consisting of five primary blocks. The first block (STRUCT) defines the structural model. The remaining four blocks (SOL01, SOL02, SOL03 and SOL04) are independent solutions for static loading, seismic loading, natural frequency or buckling load, and static cyclic loading, respectively. The numerical procedures for each of the five program blocks are presented in this chapter.

### A. STRUCT - DEFINITION OF THE STRUCTURAL MODEL

The structural model consists of an assemblage of elements. The point where two or more elements connect is called a joint. A structure is modelled by first defining the location and orientation of each joint; then materials that describe the behavior of the elements, the elements that connect the joints, and the orientations of the elements are then defined. For dynamic analysis, the lumped mass at each joint is also defined. All of these definitions are in the program block STRUCT. The flow chart for STRUCT is shown in Figure 1.

Step 1. --- Define Joints and Determine the DOF's. The coordinates of the joints and their orientation are defined by the user. The coordinates are defined in the global coordinate system (GCS). The orientation of each joint defines its joint coordinate system (JCS). Each joint initially has six degrees of freedom (dof) in the JCS. The user also defines the joint's dof that are restrained, constrained and condensed out. The program generates the structural degrees of freedom (17).

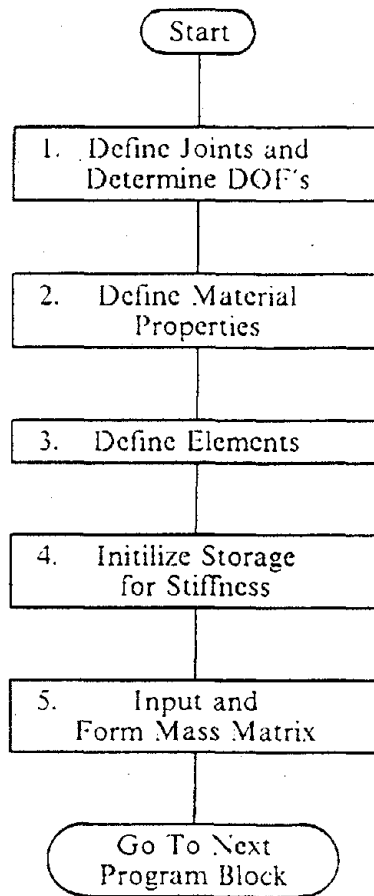


Figure 1. Block STRUCT - Define the Structural Model

Step 2. --- Define Material Properties. The material properties are input and initialized. There are six different material behaviors available, which constitute the material library, and are discussed later.

Step 3. --- Define Elements. The element data is input. The transformation matrices, initial element structural stiffness and the initial element geometric stiffness are calculated. There are three different elements available in the program, which constitute the element library, and are discussed later.

Step 4. --- Initialize Storage for Stiffness. The storage for the structural stiffness and geometric matrices is initialized.

Step 5. --- Input and Store Mass. The lumped mass at each joint is input. The structures mass matrix is stored.

#### 1. Material Library.

a. Elastic 3D Prismatic Beam Material. This material consists of the elastic section properties of a 3D prismatic beam,  $A_x$ ,  $J$ ,  $I_y$ ,  $I_z$ , and the material's moduli  $E$  and  $G$ .

b. R/C Axial Hysteresis Model. An axial hysteresis model developed for the reinforced concrete boundary columns of a shear wall (16). This hysteresis model is sketched in Figures 2 and 3 and discussed in Reference 17.

c. Cheng-Mertz B1 Bending Hysteresis Model. A bending hysteresis model developed to model the bending deformations in low-rise reinforced concrete shear walls (17). This hysteresis model is sketched in Figure 4 and uses the multiple segment backbone curve shown in Figure 5.

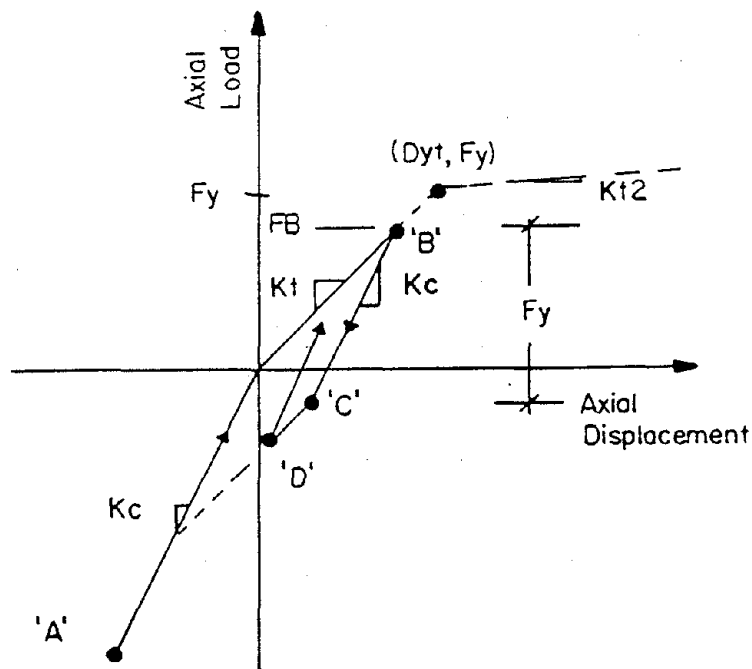


Figure 2. Axial Hysteresis Model Before Tensile Yield

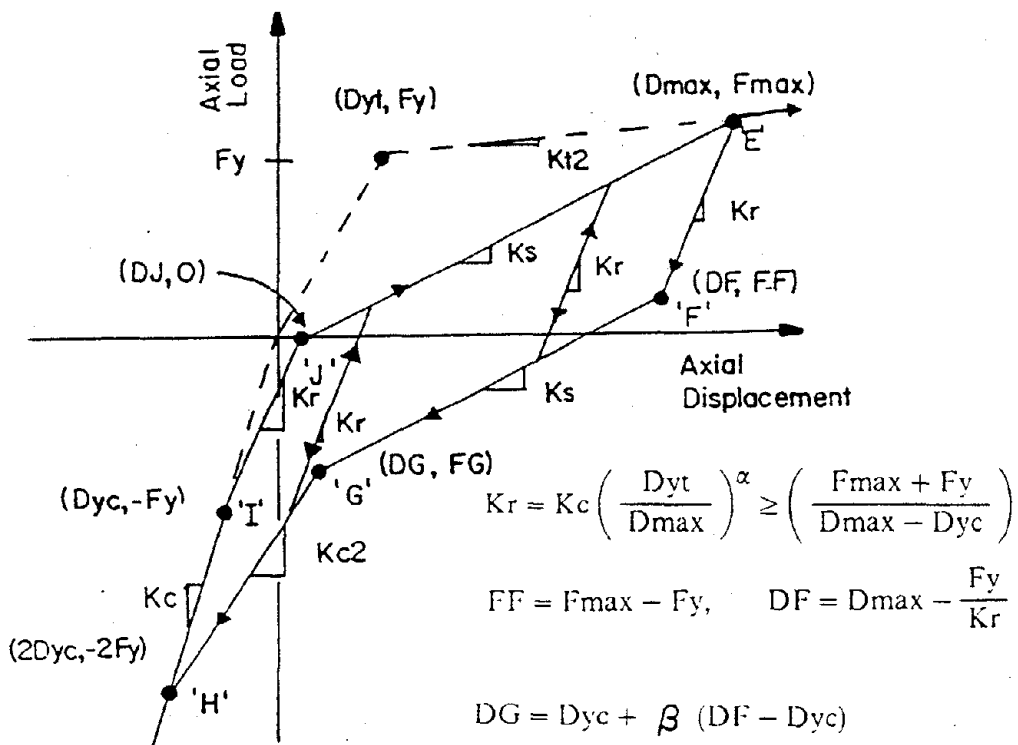


Figure 3. Axial Hysteresis Model After Tensile Yield

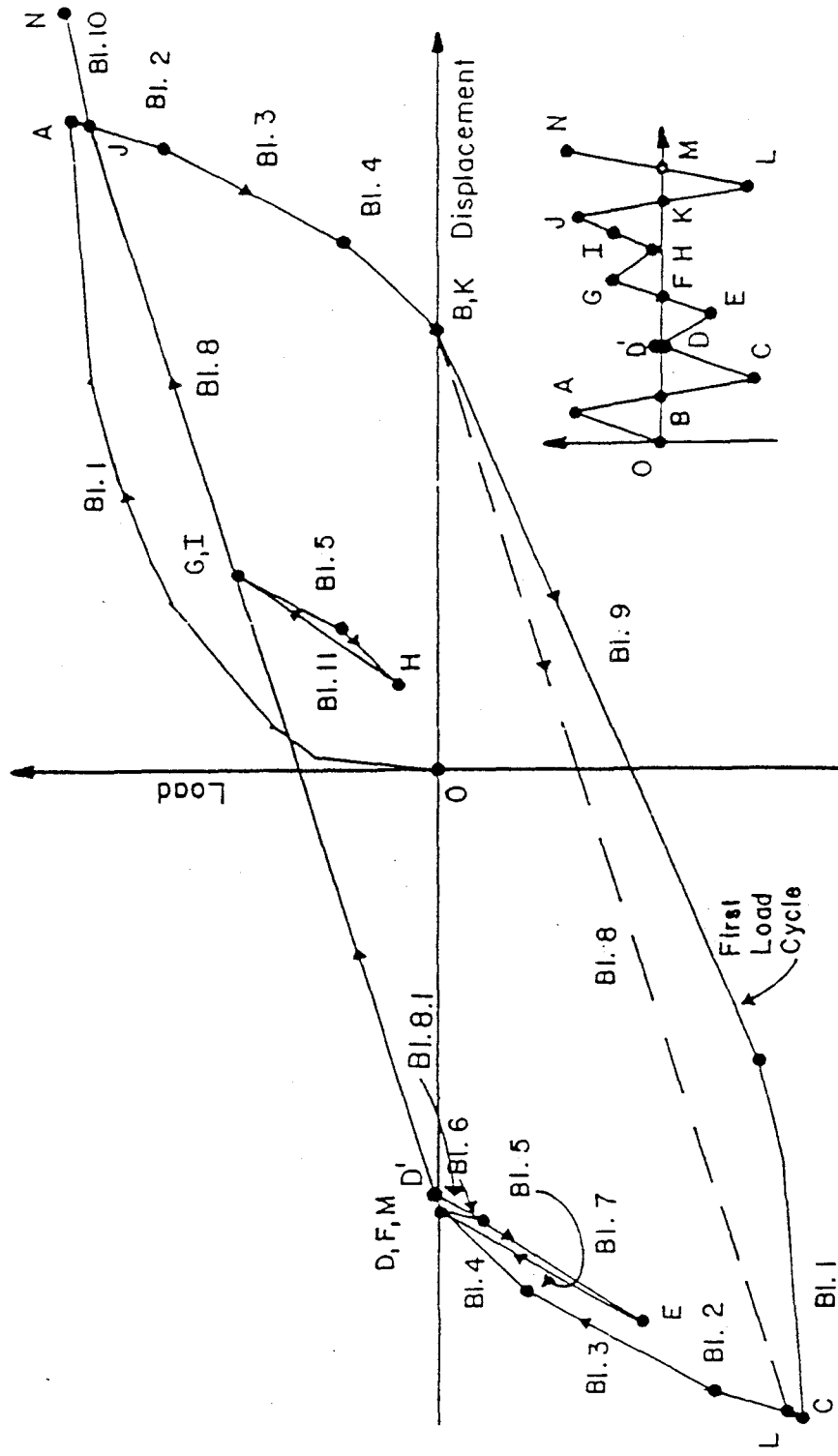


Figure 4. Low-Rise Shear Wall Cheng-Mertz Bending Hysteresis Model

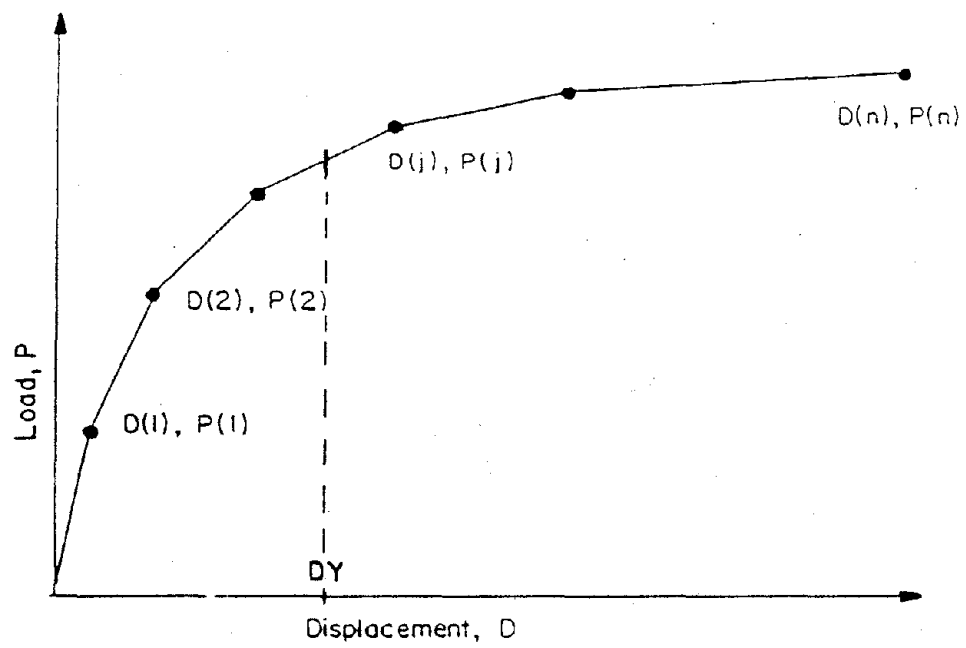


Figure 5. Multiple Segment Backbone Curve

d. Cheng-Mertz S1 Shear Hysteresis Model. A shear hysteresis model developed to model the shear deformations in low-rise reinforced concrete shear walls (17). This hysteresis model is sketched in Figure 6 and uses the multiple segment backbone curve shown in Figure 5.

e. Takeda Hysteresis Model. A bending hysteresis model developed to model the bending deformations of reinforced concrete members (21). This hysteresis model is sketched in Figure 7.

f. Bilinear Hysteresis Model. A hysteresis model that has a bilinear backbone curve and an elastic unloading and reloading curve. The model may also represent the elasto-plastic model by setting the post yielding stiffness to zero. This hysteresis model is sketched in Figure 8.

## 2. Element Library.

a. Elastic 3D Prismatic Beam Element. The elastic 3D prismatic beam element is shown in Figure 9. This beam element connects a start and end joint. At the start end of the element, a rigid body of length  $X_S$  is used to model the structural joint. A similar rigid body, of length  $X_E$  is used at the end joint. The beam's element coordinate system (ECS)  $X_e$  axis goes from end 'A' towards end 'B'. The orientation of the ECS  $Y_e$  axis is defined by a vector,  $\vec{V}$ , which lies on the ECS XY-plane. The ECS  $Z_e$  axis is perpendicular to the  $X_e$  and  $Y_e$  axes, right hand rule. There are six internal forces  $F_X, F_Y, F_Z, M_X, M_Y$  and  $F_Z$  at end 'A' in the ECS. Similarly, six internal forces also exist at end 'B'. All of the internal forces are positive in the direction of the ECS.

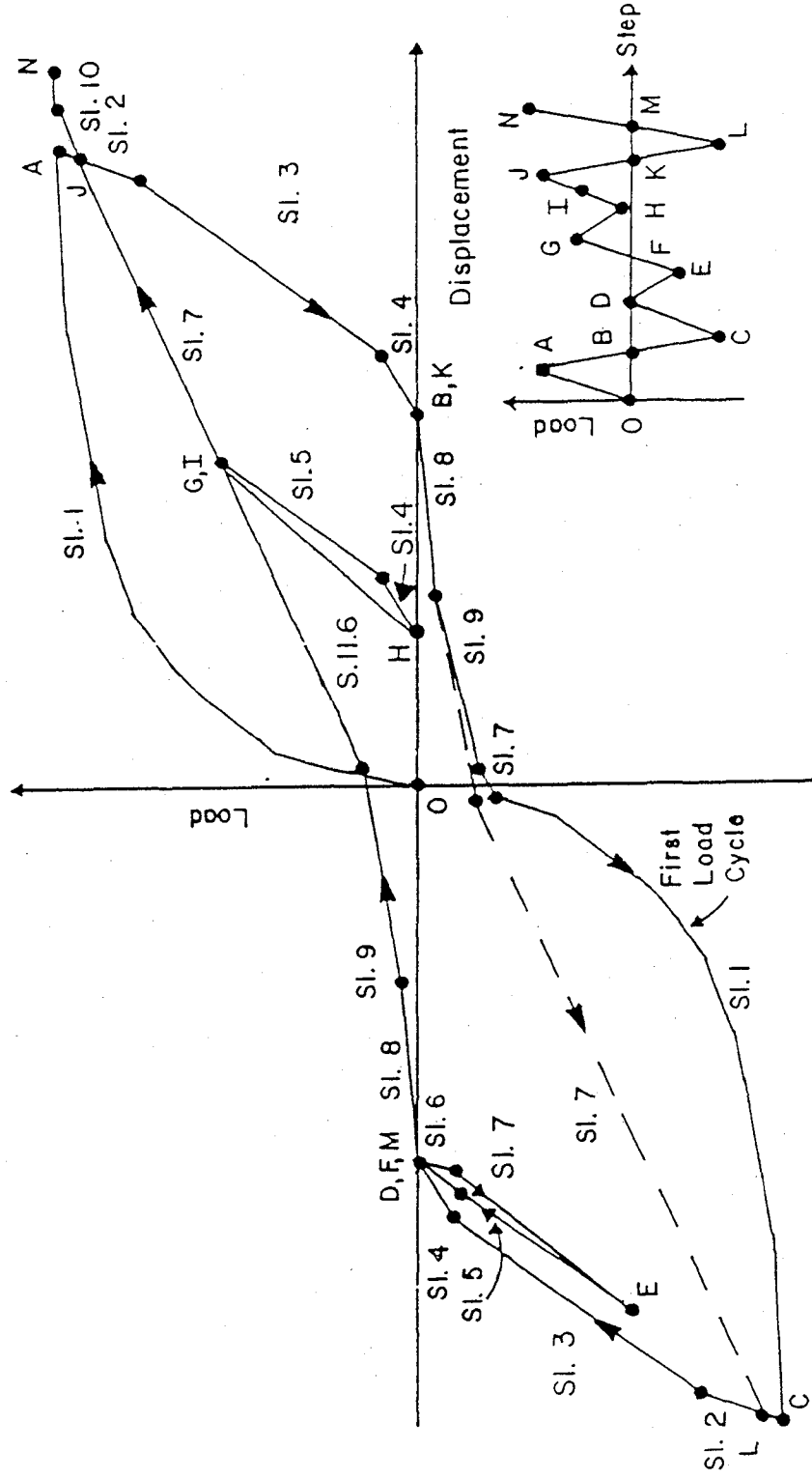


Figure 6. Low-Rise Shear Wall Shear Cheng-Mertz Hysteresis Model



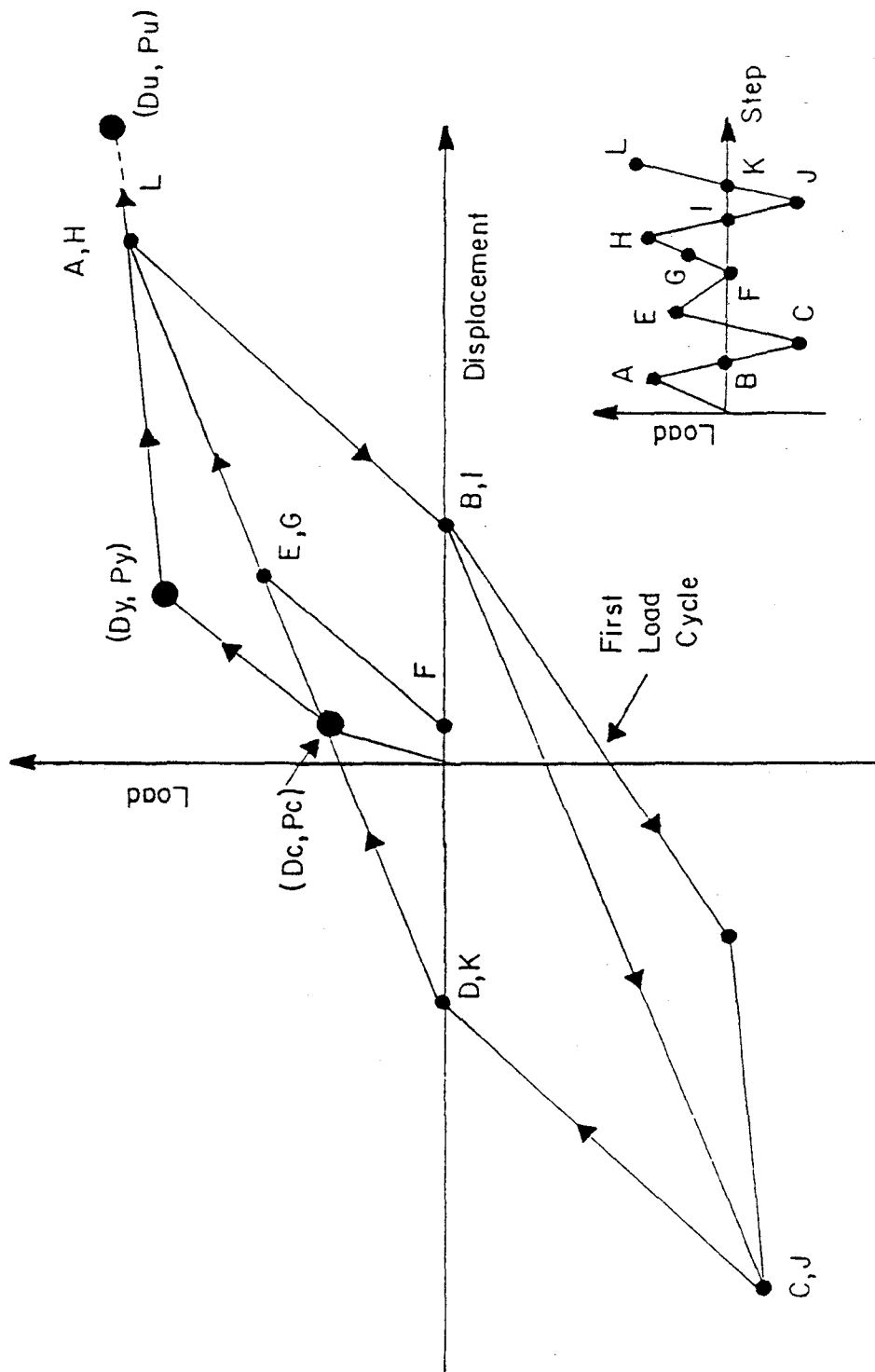


Figure 7. Takeda Hysteresis Model

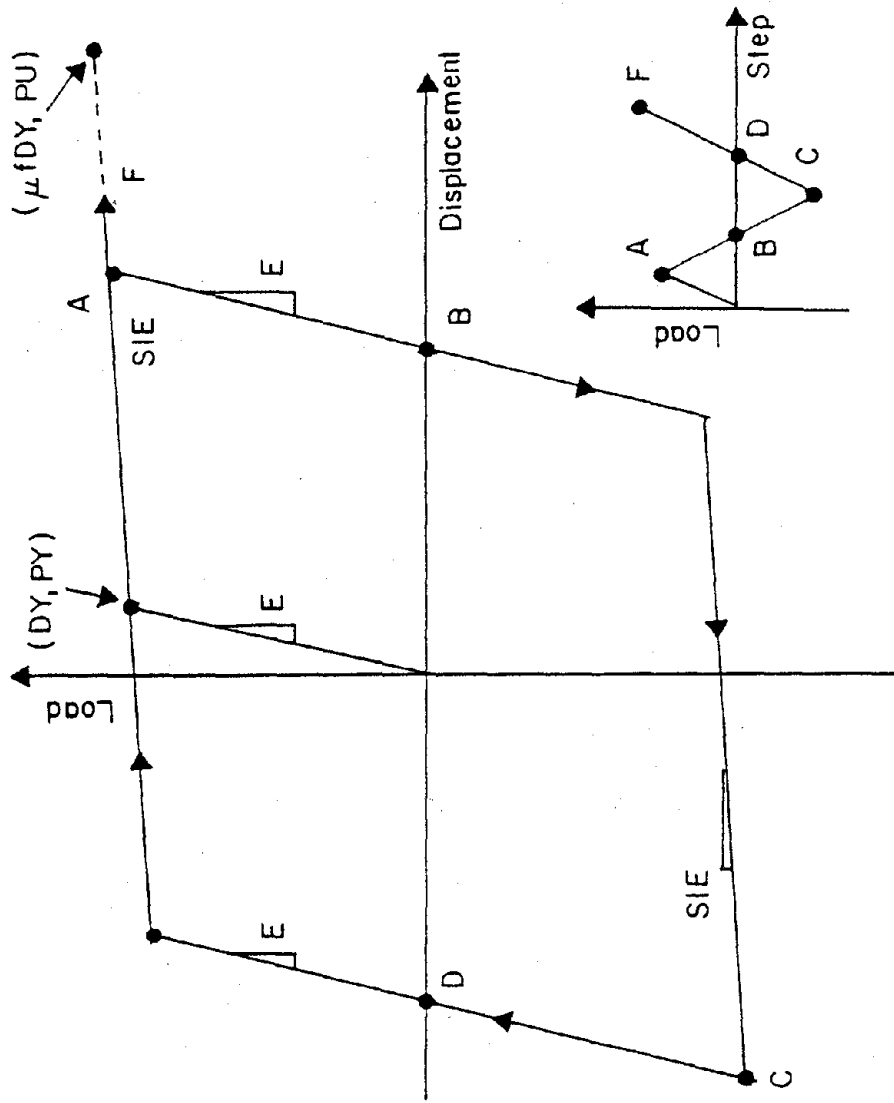


Figure 8. Bilinear Hysteresis Model

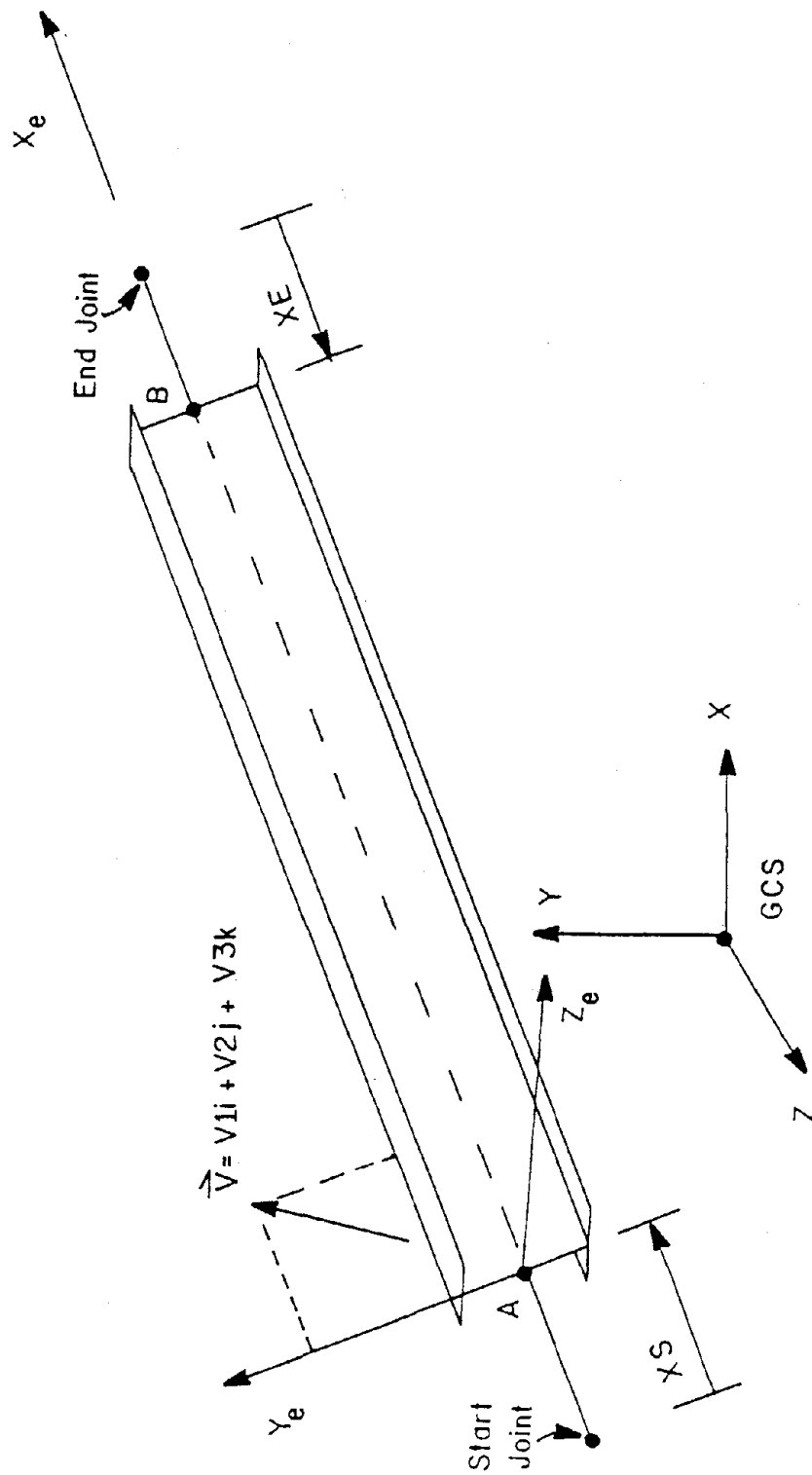


Figure 9. 3D Prismatic Beam Element

The beam element considers axial deformation, torsional deformation, and bending deformations about the  $Y_e$  and  $Z_e$  axes. Warping torsion and shear deformation are not considered. Two formulations of the geometric stiffness are also available. The 'lumped parameter' formulation only considers the second order shears at the end of the beam, while the 'consistent parameter' formulation considers the second order moments and shears at the end of the beam. The 3D-beam material is used with the beam element.

b. Spring Element. The spring element consist of an isolated spring that connects the start and end joints. At the start end of the spring, a rigid body of length  $X_S$  is used to model the joint depth. A similar rigid body, of length  $X_E$  is used at the end joint. The spring element coordinate system (ECS)  $X_e$  axis goes from end 'A' towards end 'B'. The orientation of the ECS  $Y_e$  axis is defined by the user. The ECS  $Z_e$  axis is perpendicular to the  $X_e$  and  $Y_e$  axes, right hand rule. When the distance between the start and end joints is zero, the orientation of the ECS is identical to the start joint's JCS. The distance between the start and end joints less the length of the rigid bodies, is the length of the spring element. Optionally, the user may define the length of the spring element. The spring element may behave elastically or nonlinearly depending on the material properties used and the magnitude of forces acting on the spring. Second order P- $\Delta$  forces are not calculated for the spring element.

The spring may be orientated in one of six positions as shown in Figure 10. Examples of axial, shear and rotational spring applications are shown in Figures 11, 12 and 13, respectively. The axial spring is parallel to the elements  $X_e$  axis. The rigid bodies at the ends of the spring reduce the length of the axial spring. The springs axial force,  $F_X$ , at end 'A' is positive in the  $X_e$  direction.

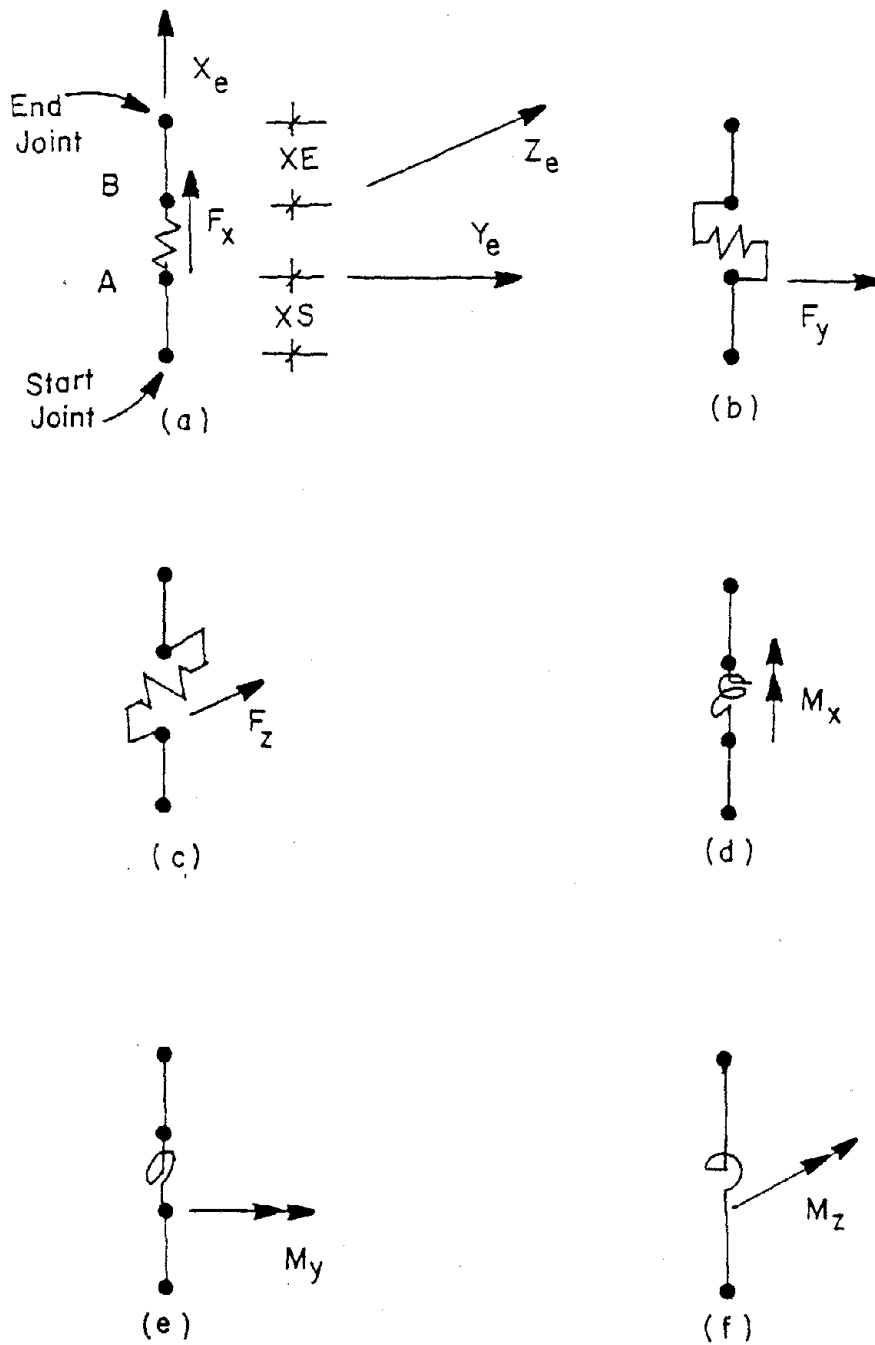


Figure 10. Spring Element: (a) Axial Spring and ECS, (b) Y-axis Shear Spring, (c) Z-axis Shear Spring, (d) Torsional Spring, (e) Y-axis Rotational Spring, (f) Z-axis Rotational Spring

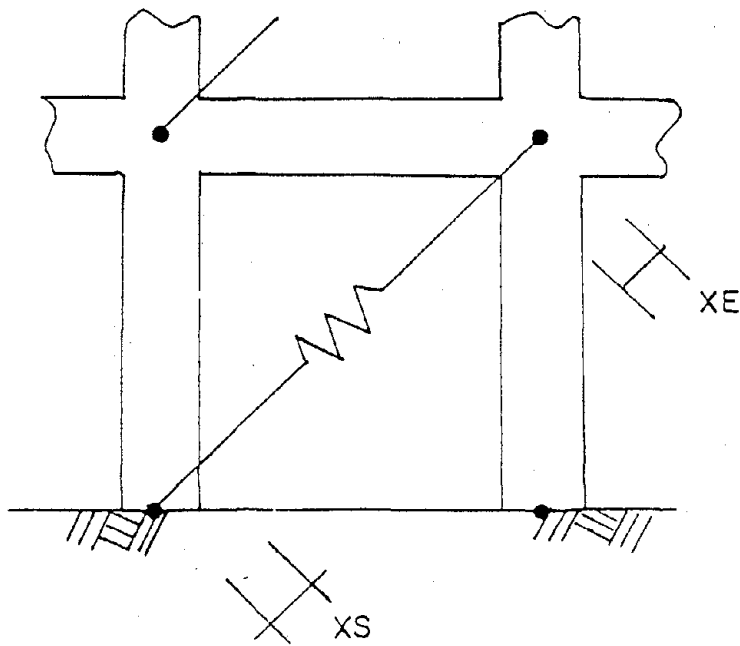


Figure 11. Diagonal Bracing Member Modeled With an Axial Spring

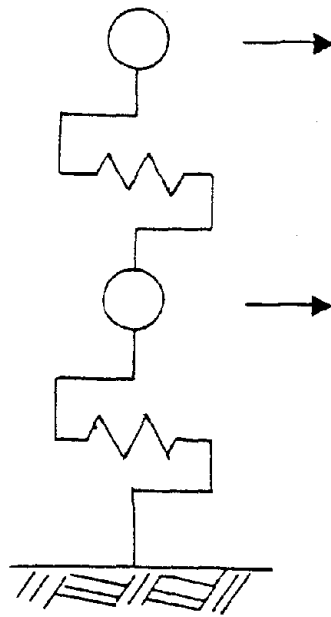


Figure 12. Two DOF Model With Shear Springs

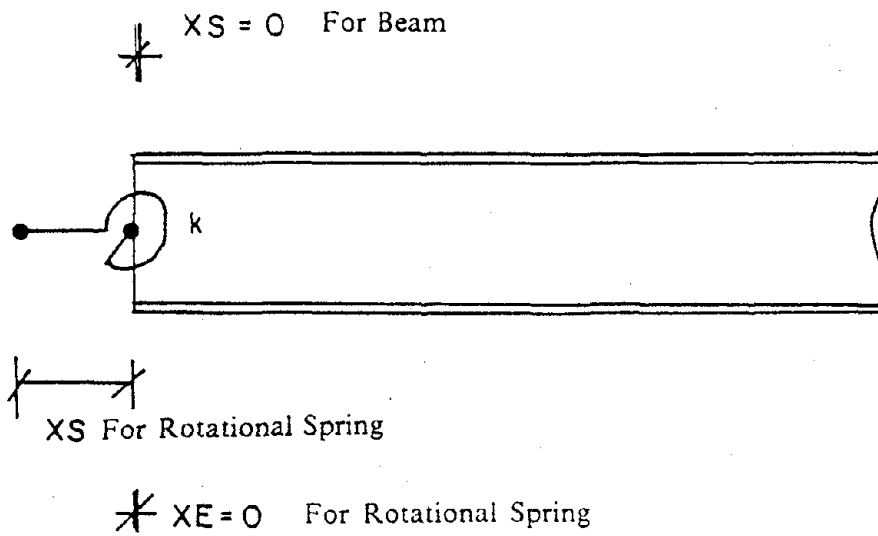


Figure 13. Member End Rotation of an Elastic 3D Prismatic Beam Modeled with a Rotational Spring



The Y-axis shear spring and Z-axis shear spring are orientated parallel to the elements  $Y_e$  and  $Z_e$  axes, respectively. The rigid bodies at the ends of the spring reduce the length of the shear spring and induce moments at the joints. The springs internal shears,  $F_Y$  and  $F_Z$ , at end 'A' are positive in the  $Y_e$  and  $Z_e$  directions.

The torsional spring is parallel to the elements  $X_e$  axis. The rigid bodies reduce the length of the torsional spring. The spring's internal torsion,  $M_X$ , at end 'A' is positive in the  $X_e$  direction.

The Y-axis rotational spring and the Z-axis rotational spring are rotational springs about the  $Y_e$  and  $Z_e$  axes, respectively. The rigid bodies at the ends of the spring reduce the length of the rotational spring. The spring's internal moments,  $M_Y$  and  $M_Z$  at end 'A' are positive in the  $Y_e$  and  $Z_e$  directions.

c. Reinforced Concrete Shear Wall Element. The reinforced concrete shear wall element consists of a panel linking four joints as shown in Figure 14. Bending and shear deformations in the plane of the wall are considered, along with axial deformation. The bending, shear and axial deformations are lumped into three springs. A rigid body, of length  $\alpha$ , connects the joints at the top of the wall with the springs, while a second rigid body, of length  $\beta$ , connects the joints at the bottom of the wall with the springs. Bending and shear stiffness perpendicular to the plane of the wall are neglected. A 'lumped parameter' formulation of the geometric stiffness considers both in-plane and out of plane  $P-\Delta$  effects.

The wall has 10 dof at the corner joints as shown in Figure 14. Fixing the bottom of the shear wall and applying a positive load to degree of freedom 1, the sign convention yields a positive moment and shear at end 'A' of the springs. Fixing the bottom of the shear wall and applying a positive load to degrees of freedom 2 and 4, yield a positive axial load at end 'A' of the spring.

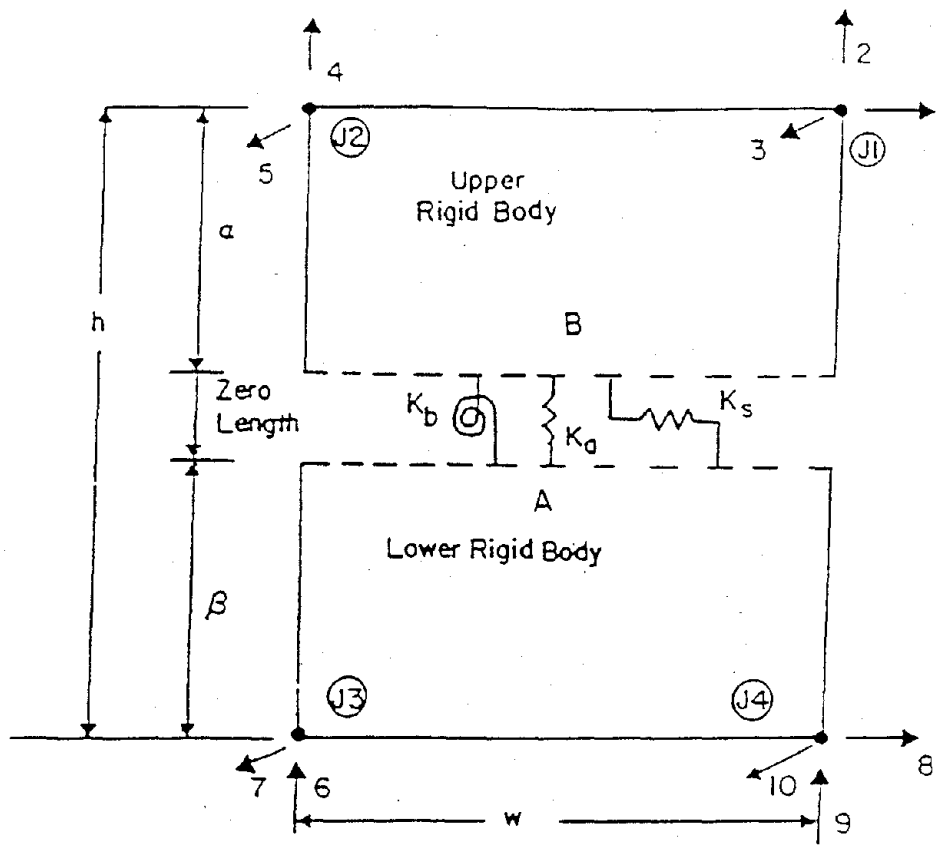


Figure 14. Shear Wall Element

Different materials are used to describe the stiffness of the bending, shear and axial springs. Typically the bending stiffness is defined by the B1 bending hysteresis model, the shear stiffness is defined by the S1 shear hysteresis model and the axial stiffness is defined by the axial hysteresis model.

## B. SOL01 - ELASTIC STATIC ANALYSIS WITH MULTIPLE LOAD CASES

This block performs the elastic static analysis with multiple load cases. The flow chart for SOL01 is shown in Figure 15.

Step 1. --- Input Joint and Element Loadings. The joint loads and imposed displacements are input for each load case. Uniform and concentrated element loadings are input for each load case on the 3D-beam element.

Step 2. --- Form the Structural Stiffness and Load Matrices. The structural stiffness matrix is formed. Optionally, the geometric stiffness matrix, based on the user's input axial loads, is subtracted from the structural stiffness matrix. Joint loadings are determined for the imposed displacements (support settlements) and combined with the input joint loadings and element loadings for each load case.

Step 3. --- Calculate Displacements. The displacements for each load case are calculated by Gauss elimination.

Step 4. --- Calculate Reactions. The reactions at restrained degrees of freedom and the summation of reactions are calculated for each load case.

Step 5. --- Calculate Element Forces. The element forces are calculated for each load case.

## C. SOL02 - ELASTIC / NONLINEAR SEISMIC TIME HISTORY RESPONSE

This block performs the elastic or nonlinear analysis of a structure subject to multiple ground accelerations. The flow chart for SOL02 is shown in Figure 16.

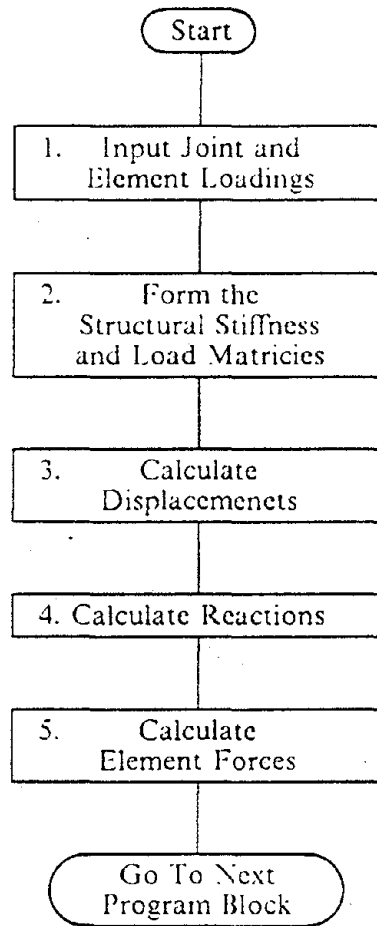


Figure 15. Block SOL01 - Static Analysis

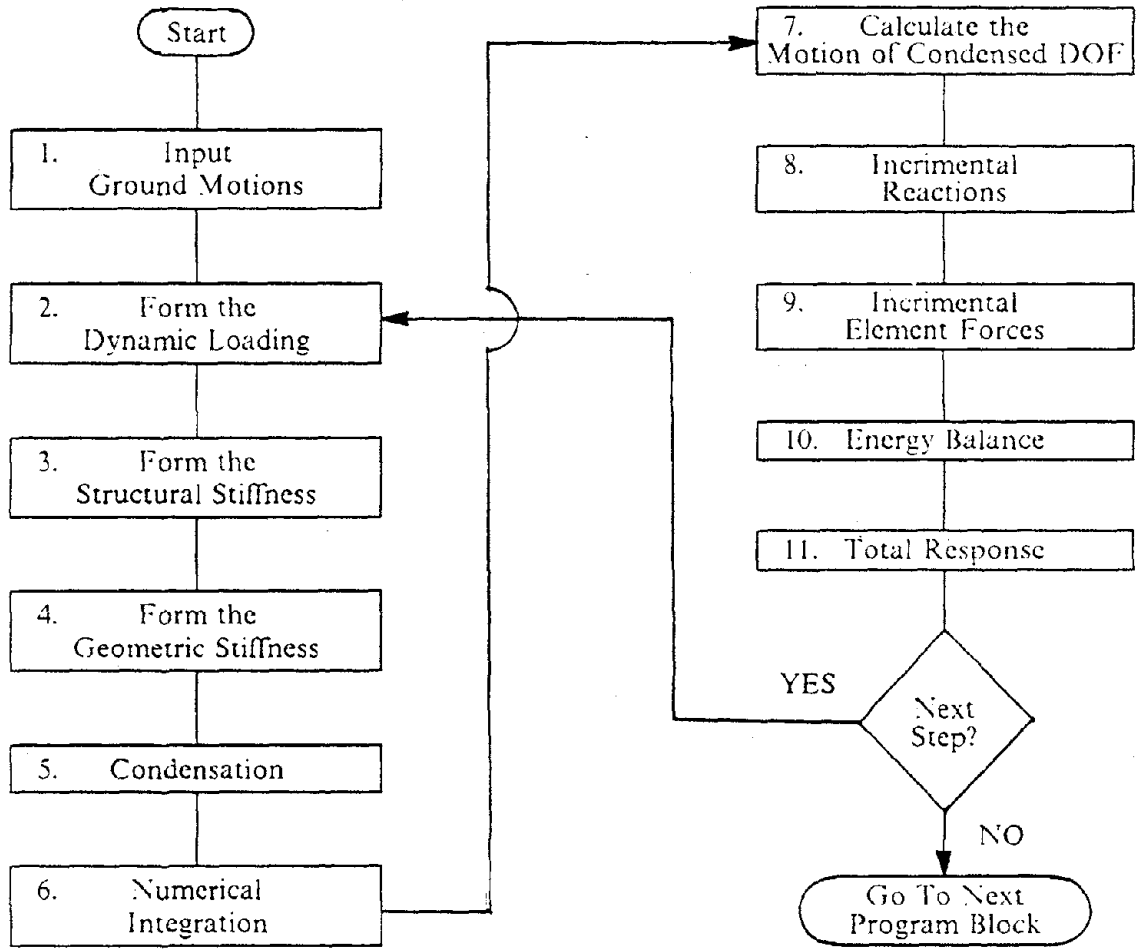


Figure 16. Block SOL02 - Elastic / Nonlinear Dynamic Analysis

Step 1. --- Input Ground Motions. The ground motions are input and stored. Transformation matrices to rotate the ground accelerations from the input coordinate system to the individual JCS are formed. The equation of motion for a dynamic loadings is

$$M\ddot{X} + C\dot{X} + KX = F(t) = - M'\ddot{X}_g \quad (1)$$

For seismic analyses,  $M = M'$ . For nonseismic analyses the special mass matrix,  $M'$ , and a pseudo-ground acceleration are input and stored. Thus the nonseismic forcing function function is equal to

$$F(t) = - M'\ddot{X}_g \quad (2)$$

Step 2. --- Form the Dynamic Loading. The dynamic loading matrix is formed and added to the unbalanced force matrix.

Step 3. --- Form the Structural Stiffness. The structural stiffness is formed 1) for the first time step, 2) for every time step that an element's stiffness is modified, and 3) for every time step that the geometric stiffness is modified. The element's stiffness is only modified during a nonlinear analysis.

Step 4. --- Form the Geometric Stiffness. The geometric stiffness is formed 1) for the first time step, and 2) for every time step if the actual element axial loads are used to calculate the geometric stiffness.

Step 5. --- Condensation. If condensed degrees of freedom exist: 1) the structural stiffness is condensed each time step that is formed, 2) the geometric stiffness is condensed each time step it is formed, if condensation of the geometric stiffness is desired, 3) the mass matrix is condensed the first time step, if needed, and 4) the dynamic loading matrix is condensed each time step.

Step 6. --- Numerical Integration. The incremental displacements, velocities and accelerations of free dof are calculated by the linear acceleration method or the average acceleration method.

Step 7. --- Calculate the Motion of Condensed DOF. The incremental displacements, velocities and accelerations of condensed dof are calculated.

Step 8. --- Incremental Reactions. The incremental reactions are calculated.

Step 9. --- Incremental Element Forces. The hysteresis models in the material library are called to calculate the incremental element forces, given the incremental displacements and previous loading history. For nonlinear analysis, if the element stiffness changes during the incremental displacement, 1) the element's unbalanced forces are calculated, and 2) a flag to reform the structural stiffness in step 3 is set for the next time step. The elastic and plastic strain energies for each element are also calculated.

Step 10. --- Energy Balance. The total input energy, kinetic energy, elastic strain energy, plastic strain energy and energy dissipated due to damping are calculated.

Step 11. --- Total Response. The total displacements, velocities, accelerations, reactions, and element forces are calculated. The unbalanced force vector for nonlinear analysis is assembled from the element's unbalanced forces. If desired, selected results may be written to output files.

Go to step 2 for the next time step.

#### D. SOL03 - ELASTIC NATURAL FREQUENCY / ELASTIC BUCKLING LOAD

This block calculates either the natural frequencies and mode shape of an elastic structure, or the buckling load and mode shape of an elastic structure. The flow chart for SOL03 is shown in Figure 17.

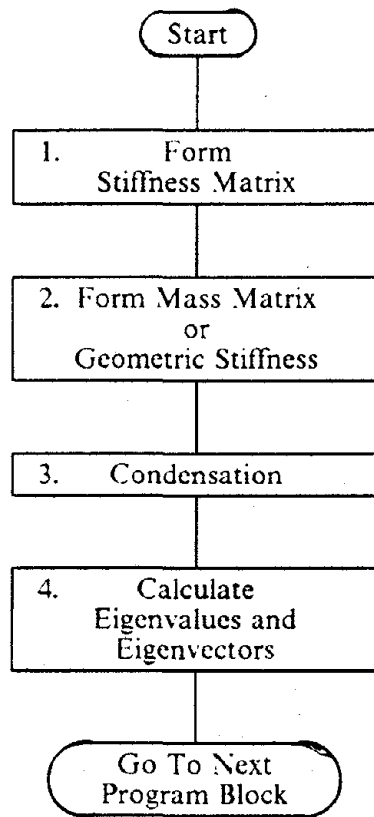


Figure 17. Block SOL03 - Natural Frequency / Elastic Buckling Load



Step 1. --- Form the Structural Stiffness Matrix. The structural stiffness matrix is formed.

Step 2. --- Form Mass Matrix or Geometric Stiffness Matrix. For the buckling solution, the geometric stiffness matrix is formed. For the natural frequency solution, the mass matrix that was formed in block STRUCT is used.

Step 3. --- Condensation. If condensed degrees of freedom exist: 1) the structural stiffness is condensed, 2) the geometric stiffness is condensed for buckling problems, if it is desired, 3) the mass matrix is condensed for natural frequency problems, if it is needed.

Step 4. --- Calculate Eigenvalue and Eigenvector. The eigenvalues and eigenvectors are calculated. Natural frequencies or buckling loads are extracted from the eigenvalues. The eigenvectors are normalized. The natural frequencies are printed along with the mode shape of each mode, or the buckling loads are printed along with the corresponding mode shape.

#### E. SOL04 - NONLINEAR STATIC CYCLIC RESPONSE

This block calculates the nonlinear static cyclic response for a given loading pattern. A loading pattern consisting of joint loads, imposed displacements and element loads is defined and stored in the vector  $\{Q\}$ . The loading pattern,  $\{Q\}$ , is multiplied by positive and negative load factors to generate cyclic loading cycles. Define  $F_j$  as the loading factor for the current cycle, and  $F_i$  as the loading factor for the previous cycle. The total loads on the structure for cycles  $i$  and  $j$  are  $F_i\{Q\}$  and  $F_j\{Q\}$ , respectively. The loading from  $F_i\{Q\}$  to  $F_j\{Q\}$  is carried out in a series of steps. A variable number of steps, with each step having incremental loads and displacements less than limiting values, may be used to load from  $F_i\{Q\}$  to  $F_j\{Q\}$  (loading option A). Alternately, a fixed number of equal load steps may be chosen to load from  $F_i\{Q\}$  to  $F_j\{Q\}$  (loading option B). The flow chart for SOL04 is shown in Figure 18.

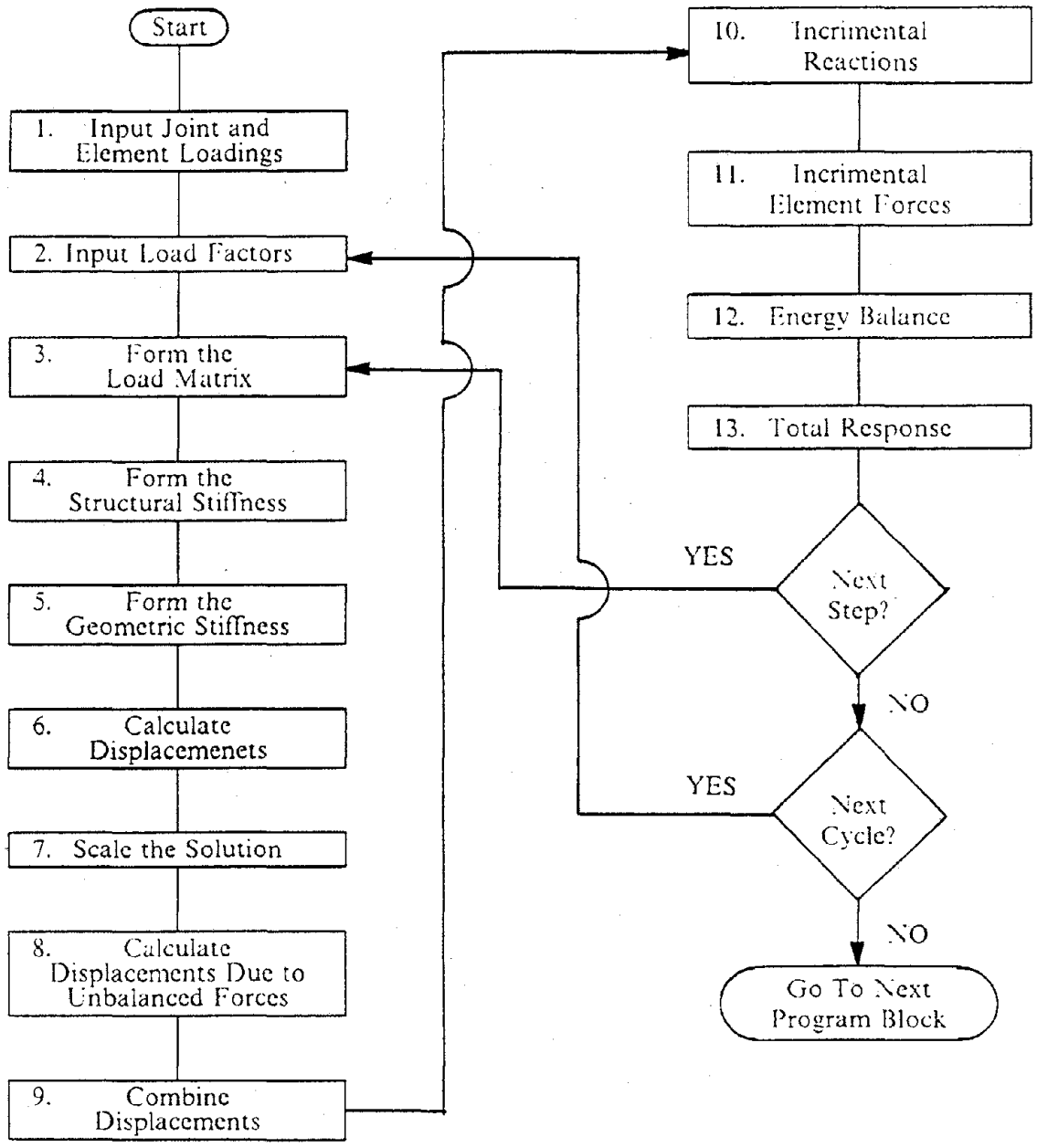


Figure 18. Block SOL04 - Nonlinear Static Cyclic Response

Step 1. --- Input Joint and Element Loadings. The joint loads and imposed displacements of the load pattern are input. Element loadings for the load pattern are input on the 3D-beam element.

Step 2. --- Input Load Factors. For each loading cycle, a load factor, and limits on the step size, or the number of load steps are input.

Step 3. --- Form the Load Matrix. The loading matrix for option A is the difference in the load at the end of the cycle and the current load. Alternately, the loading matrix for option B is the incremental load.  $\frac{F_j - F_i}{N} \times \{Q\}$ , where N is the number of load steps.

Step 4. --- Form the Structural Stiffness. The structural stiffness is formed 1) for the first load step, 2) for every load step that an element's stiffness is modified, and 3) for every load step that the geometric stiffness is modified.

Step 5. --- Form the Geometric Stiffness. The geometric stiffness is formed 1) for the first load step, and 2) for every load step if the actual element axial loads are used to calculate the geometric stiffness.

Step 6. --- Calculate Displacements. The incremental displacements due to the applied loadings are calculated by Gauss elimination.

Step 7. --- Scale the Solution. For loading option A, the response is scaled down such that the incremental loads and displacements for each step are less than the limiting values. This step is omitted for loading option B.

Step 8. --- Calculate Displacements due to Unbalanced Forces. The incremental displacements due to the unbalanced forces from the previous load step are calculated by Gauss elimination.

Step 9. --- Combine Displacements. The scaled down displacements due the applied loading and the displacements due to the unbalanced loadings are added together.

Step 10. --- Incremental Reactions. The incremental reactions are calculated.

Step 11. --- Incremental Element Forces. The hysteresis models in the material library are called to calculate the incremental element forces, given the incremental displacements and previous loading history. For nonlinear analysis, if the element's stiffness changes during the incremental displacement, 1) the element's unbalanced forces are calculated, and 2) a flag to reform the structural stiffness in step 4, is set for the next load step. The elastic and plastic strain energy for each element is also calculated.

Step 12. --- Energy Balance. The total input energy, elastic strain energy and plastic strain energy are calculated.

Step 13. --- Total Response. The total displacements, reactions, and element forces are calculated. The unbalanced force vector for nonlinear analysis is also calculated. If desired, selected results may be written to output files.

Go to step 3 for additional loading steps. Go to step 2 for the next loading cycle.

### III. DESCRIPTION OF PROGRAM

The computer program INRESB-3D-SUP is described in this chapter. A flow chart of the program is given in Figures 19 and 20.

#### A. MAIN PROGRAM AND COMMON BLOCKS

A brief description of the main program and the three common blocks is presented in this section.

1. MAIN - Main Program. The main program 1) reads and echoes input data, 2) initializes data, 3) calls STRUCT to define the structural model, 4) calls SOLN to perform individual solutions, 5) calls COMDMP to dump the contents of the memory, 6) sets bug options to print stiffness matrices, etc, 7) releases memory from previous solutions, and 8) stops execution of the program.

2. Common Block DATA. This common block consists of a linear array that contains the program's dynamically allocated memory. The linear array consists of a real array, Z, and an integer array, NZ. The integer array and the real array share the same storage location in memory<sup>1</sup>. Common block DATA is used by routines MAIN, CKSTOR, STRUCT, MATLIB, ELELIB, DMPDAT FORM, SOLN, SOL01, SOL02, SOL03 and SOL04.

3. Common Block ZDATA. This common block contains flags which control the execution of the routines, the number of Gdof, joints, elements, etc. and the addresses of data in the Z array that is shared between different routines. ZDATA is used by routines MAIN, CKSTOR, STRUCT, MATLIB, ELELIB, DMPDAT, FORM, SOLN, SOL01, SOL02, SOL03, SOL04, COMPT and COMDMP.

---

<sup>1</sup> This is accomplished by the Fortran EQUIVALENCE statement.

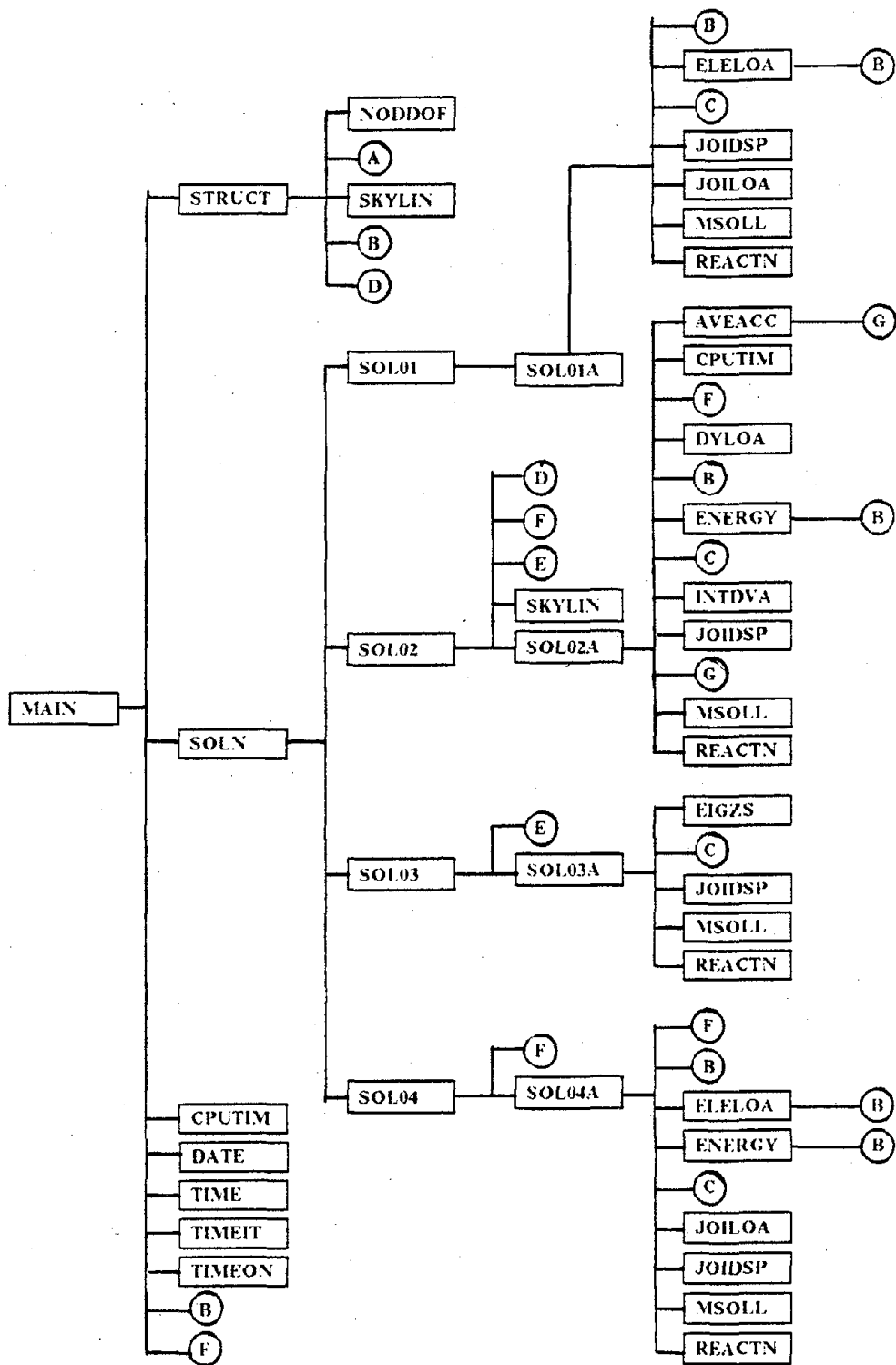


Figure 19. Flow Chart for Program INRESB-3D-SUP: Part A

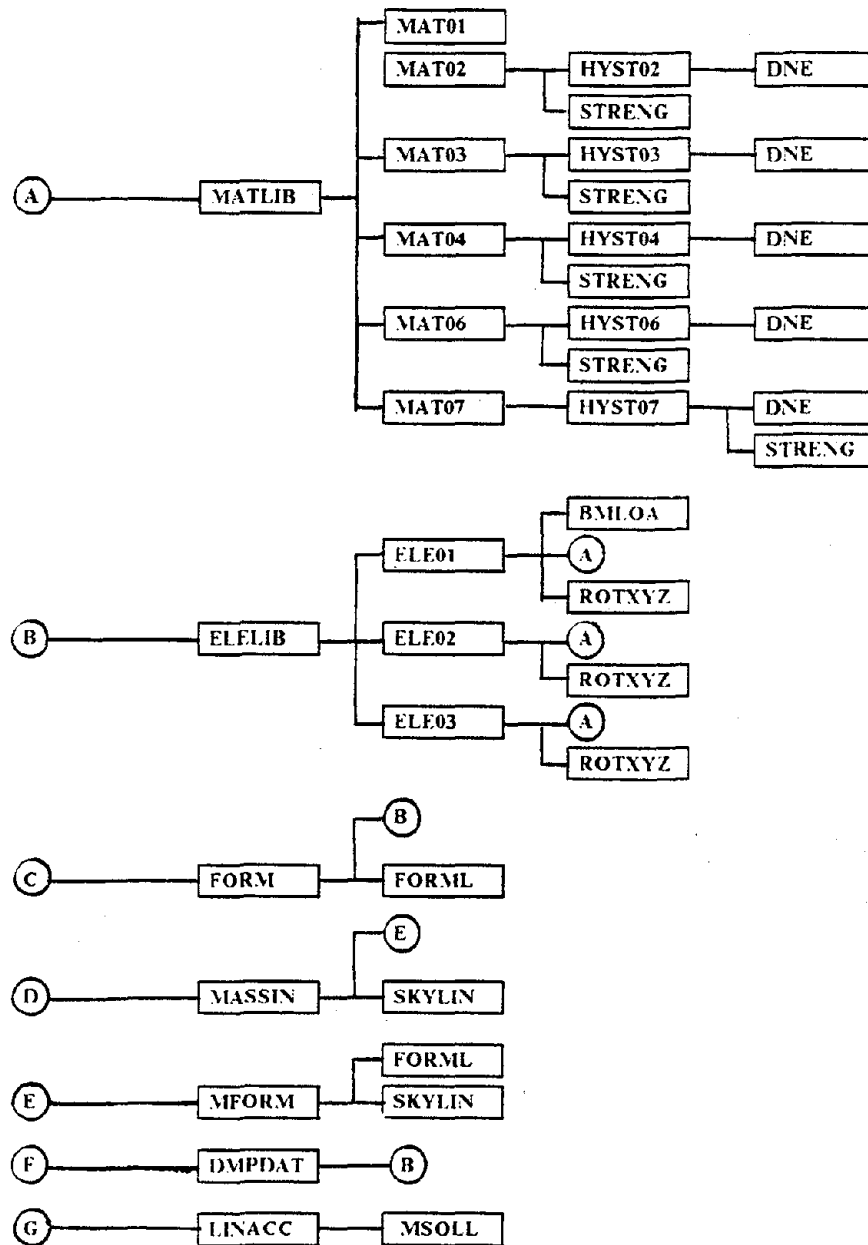


Figure 20. Flow Chart for Program INRESB-3D-SUP: Part B

4. Common Block ZDATAP. This common block contains the title, the bug options, and several other miscellaneous variables. ZDATAP is used by routines MAIN, CKSTOR, STRUCT, MATLIB, ELELIB, DMPDAT, FORM, SOLN, SOL01, SOL02, SOL03, SOL04, COMPT and COMDMP.

## B. DESCRIPTION OF ROUTINES

The program INRESB-3D-SUP includes 73 routines. These are presented in alphabetical order with a brief description.

1. AVEACC. AVEACC and LINACC calculate the dynamic response by the average acceleration method. Called by SOL02A.

2. BMLOA. Calculate the fixed end moments and shears of a prismatic beam element for uniform and concentrated element loadings. Called by ELE01.

3. CKRNG. A utility routine called by ELELOA that checks the location of element loadings.

4. CKSTOR. A utility routine that aborts the program if the problem requires more storage than is available. Called by SOL02, DMPDAT, SOL03 and SOL04.

5. COMDMP. A utility routine that prints the contents of the dynamic memory. Called by MAIN.

6. COMPT. A utility routine that initializes the addresses of the dynamic memory. Called by MAIN.

7. CROSS. Vector cross product. Called by DYLOA and NODDOF.

8. DIRECT. A utility routine called by HYST03 and HYST04 to determine the current direction of loading.



9. DMPDAT. 1) Writes the results to user defined output files. 2) Reads the results from output files and prints data. Called by SOL02, SOL02A, SOL04, SOL04A, and MAIN.
10. DNE. Calculates ductilities and excursion ratios for HYST02, HYST03, HYST04, HYST06 and HYST07.
11. DYLOA. Generates the dynamic loadings due to base acceleration for multicomponent earthquakes. Called by SOL02A.
12. ELELIB - Element Library. This subroutine is a controller that calls the members of the element library. All calls to the elements must pass through this subroutine. Called by MAIN, FORM, STRUCT, SOL01A, SOL02A, SOL04A, ELELOA, ENERGY and DMPDAT.
13. ELELOA. Calculate the element loads for the elastic 3D prismatic beam element. Called by SOL01A and SOL04A.
14. ELE01 - Elastic 3D Prismatic Beam Element. This routine calculates the stiffness, geometric stiffness, element loads, displacements, forces, etc. for the elastic 3D prismatic beam element. Called by ELELIB.
15. ELE02 - Spring Element. This routine calculates the stiffness, geometric stiffness, displacements, forces, unbalanced forces, etc. for the spring element. Called by ELELIB.
16. ELE03 - Shear Wall Stiffness Element. This routine calculates the stiffness, geometric stiffness, displacements, forces, unbalanced forces, etc. for the shear wall stiffness element. Called by ELELIB.
17. ENERGY. Calculates the energy balance. Called by SOL02A and SOL04A.

18. ETMPLY. Performs the multiplication,  $\{\dot{x}\}^t[M]\{\dot{x}\}$ , to calculate kinetic energy, for an upper triangular mass matrix. Called by ENERGY.
19. FEMREL. Modifies the fixed end forces to account for end releases. Called by BMLOA.
20. FIRST. A utility routine that performs character manipulations. Called by GETCHR.
21. FORM. FORM and FORML are used to assemble the structural and geometric stiffness matrices. Called by SOL01A, SOL02A, SOL03A and SOL04A.
22. FORML. 1) Adds the element stiffness to the global structural stiffness. 2) Adds the element geometric stiffness to the global geometric stiffness. 3) Adds the joint mass to the global mass matrix. Called by FORM and MFORM.
23. GETCHR. A Utility routine that extracts a character string from input. Called by MAIN.
24. GETINT. A utility routine that extracts an integer from character input. Called by MAIN, LMATRIX, SOLN, WMATRIX and WMTRX2.
25. HIYST02 - Axial Hysteresis Model. Calculates the axial stiffness of R/C elements based on the current load and the past loading history by the axial hysteresis model. Called by MAT02.
26. HIYST03 - B1 Bending Hysteresis Model. Calculates the bending stiffness of R/C shear walls based on the current load and the past loading history by the B1 bending hysteresis model. Called by MAT03.

27. HYST04 - S1 Shear Hysteresis Model. Calculates the shear stiffness of R/C shear walls based on the current load and the past loading history by the S1 shear hysteresis model. Called by MAT04.

28. HYST06 - Takeda Hysteresis Model. Calculates the bending stiffness of R/C elements based on the current load and the past loading history by the Takeda hysteresis model. Called by MAT06.

29. HYST07 - Bilinear Hysteresis Model. Calculates the stiffness based on the current load and the past loading history by the bilinear hysteresis model. This model is also capable of producing elasto-plastic behavior. Called by MAT06.

30. IDRECT. A utility routine that determines the current direction for HYST02 and HYST06.

31. INTDVA. Reads and stores initial displacement, velocity and accelerations for dynamic solutions. Called by SOL02A.

32. INTSCT. A utility routine that determines the intersection of two lines in point slope form. Called by HYST02, HYST03 and HYST04.

33. IQUICK. A utility routine that finds the program's internal joint number, given the joint's ID number. Called by NODDOF, ELE01, ELE02, ELE03, JOILOA, INTDVA, DMPDAT and MFORM.

34. ISORT. A utility routine that sorts the joint input. Called by NODDOF.

35. JOIDSP. Calculates and prints the displacement, velocity, acceleration or eigenvector at each joint in the JCS and GCS. Called by SOL01A, SOL02A, SOL03A and SOL04A.

36. JOILOA. Reads and calculates the joint loads. Called by SOL01A and SOL04A.

37. KMIN. A utility routine used by the hysteresis models HYST03 and HYST04 to ensure the stiffness is between zero and the initial stiffness, SI.

38. LINACC. Calculates the dynamic response by the linear acceleration method. Called by SOL02A and AVEACC.

39. LMATRIX. A utility routine that prints upper triangular mass, structural stiffness, element stiffness, geometric stiffness, etc. matrices. This routine is activated by the user input bug options, which are described later. Called by FORM, MFORM, ELE01, ELE02, ELE03, SOL01A, SOL02A, SOL03A, SOL04A, MSOLL, TMPPLY, ETMPPLY, UTMPPLY and MASSIN.

40. MASSIN. Initializes the storage for the mass matrix. Called by STRUCT and SOL02.

41. MATLIB - Material Library. This subroutine is a controller that calls the members of the material library. All calls to the materials and hysteresis models must pass through this subroutine. Called by STRUCT, ELE01, ELE02 and ELE03.

42. MAT01 - Elastic 3D Prismatic Beam Stiffness. This routine reads and stores the stiffness for the elastic 3D prismatic beam element. Called by MATLIB.

43. MAT02 - Axial Stiffness for R/C Elements. 1) Reads and stores axial input data. 2) Calculates the axial stiffness with calls to the axial hysteresis model, HYST02. 3) Calculates the strain energy with calls to STRENG. Called by MATLIB.

44. MAT03 - Bending Stiffness for R/S Shear Walls. 1) Reads and stores bending input data. 2) Calculates the bending stiffness with calls to the B1 bending

hysteresis model, HYST03. 3) Calculates the strain energy with calls to STRENG. Called by MATLIB.

45. MAT04 - Shear Stiffness for R/C Shear Walls. 1) Reads and stores shear input data. 2) Calculates the shear stiffness with calls to the S1 shear hysteresis model, HYST04. 3) Calculates the strain energy with calls to STRENG. Called by MATLIB.

46. MAT06 - Bending Stiffness for R/C Elements. 1) Reads and stores bending input data. 2) Calculates the bending stiffness with calls to the Takeda hysteresis model, HYST06. 3) Calculates the strain energy with calls to STRENG. Called by MATLIB.

47. MAT07 - Bilinear Material. 1) Reads and stores input data. 2) Calculates the stiffness with calls to the bilinear hysteresis model, HYST07. 3) Calculates the strain energy with calls to STRENG. Called by MATLIB.

48. MFORM. Reads the joint masses and forms the mass matrix with calls to FORML. Called by MASSIN, SOL02 and SOL03.

49. MSOLL. 1) Performs Gauss elimination of the stiffness matrix. 2) Condenses the mass matrix while performing Gauss elimination. 3) Condenses the geometric stiffness while performing Gauss elimination. 4) Reduces the load matrix. 5) Performs back substitution. 6) Operations 1 through 5 may be performed on partitioned matrices. 7) Stiffness, geometric stiffness and mass matrices are upper triangular matrices with skyline storage. Called by SOL01A, SOL02A, SOL03A, SOL04A and LINACC.

50. NODDOF. Reads joints, constraints, restraints and condensation information, calculates the JCS cosine matrices, and determines the global degrees of freedom. Called by STRUCT.

51. PBIT. A utility routine that prints the joint restraint and constraint code for each joint. Called by NODDOF.

52. REACTN. 1) Modifies the loading to include restraint displacements. 2) Solves for the reactions. 3) Prints the reactions in the JCS and GCS coordinate systems. 4) Calculates the summation of reactions. Called by SOL01A, SOL02A, SOL03A and SOL04A.

53. ROTYZ. 1) Calculates the local element cosine matrix. 2) Calculates the transformation from ECS to JCS. 3) Calculates the constraint transformation. 4) Calculates the transformation for a rigid body at the end of the beam element. Called by ELE01, ELE02 and ELE03.

54. SKYLIN. Determines the skyline of the structural stiffness, geometric stiffness and mass matrices. Called by STRUCT, MFORM and MASSIN.

55. SKYLN2. Determines the skyline of the dynamic stiffness matrix. Called by SOL02.

56. SMAX. A utility routine that determines and prints the the maximum and minimum input accelerations. Called by DYLOA.

57. SOLN - Solution Library. This subroutine is a controller that calls the solution requested by the user. All calls to the solutions must pass through this subroutine. Called by MAIN.

58. SOL01 - Elastic Static Analysis with Multiple Load Cases. This routine initializes the storage for the elastic static analysis. Called by SOLN.

59. SOL01A. This routine calculates the elastic static response, as described in Section B of Chapter II. Called by SOL01.

60. SOL02 - Dynamic Time History Response. This routine initializes the storage for the dynamic time history response. Called by SOLN.

61. SOL02A. This routine calculates the dynamic time history response for both elastic and nonlinear structures, as described in Section C of Chapter II. Called by SOL02.

62. SOL03 - Elastic Natural Frequency / Buckling Load. This routine initializes the storage for the elastic natural frequency or the buckling load. Called by SOLN.

63. SOL03A. This routine calls EIGZS to calculate the natural frequency or buckling load for elastic structures, as described in Section D of Chapter II. Called by SOL03.

64. SOL04 - Nonlinear Static Cyclic Response. This routine initializes the storage for the static nonlinear analysis. Called by SOLN.

65. SOL04A. This routine calculates the static nonlinear response, as described in Section E of Chapter II. Called by SOL04.

66. STRENG. Calculates the elastic and plastic strain energy. Called by MAT02, MAT03, MAT04, MAT06, HYST07.

67. STRUCT - Structural Definition. 1) Sets up storage for joints and calls NODDOF to input joint information and to generate degrees of freedom. 2) Sets up storage for materials and calls MATLIB to input materials and to initialize the hysteresis models. 3) Sets up storage for elements and calls ELELIB to input elements and to calculate initial element stiffnesses. 4) Calls SKYLIN to set up the storage for the structural stiffness, geometric stiffness and mass matrices. 5) Reads and initializes the mass matrix. These functions are described in greater detail in Section A of Chapter II. Called by MAIN.

68. TEST. A utility routine that examines character input, and sets a logical flag. Called by MAIN, STRUCT, SOL02, SOL03A, SOL04A, INTDVA and DMPDAT.

69. TMPY. A utility routine that performs multiplication for triangular matrices Called by SOL02A, SOL04A and ETMPY.

70. VCOS. A utility subroutine that calculates the angle between two vectors. Called by ROTXYZ and ELE03.

71. VCROSS. A utility subroutine that calculates the vector cross product. Called by ELE03.

72. WMATRX. A utility subroutine that prints a matrix. This routine is activated by the user input bug options which are described later. Called by ELE01, ELE02, ELE03, SOL01A, SOL04A, REACTN, MSOLL and DYLOA.

73. WMTRX2. A utility subroutine that prints a portion of a matrix. This routine is activated by the user input bug options which are described later. Called by ELE02 and ELE03.

### C. DESCRIPTION OF MISCELLANEOUS ROUTINES

Several other miscellaneous routines are used by program INRESB-3D-SUP, which are listed below.

1. EIGZS. An IMSL eigenvalue routine that is called by SOL03A to calculate the natural frequency and buckling load. This routine is only required for SOL03. Omission of this routine will not affect blocks STRUCT, SOL01, SOL02 or SOL04.

2. SDUMP. An IBM routine that prints the contents of memory with bug option K. Called by COMDMP. Omission of this routine will only effect bug option K.



3. CPUTIM, TIMEON and TIMEIT. These are three routines on the local UMR system that are used to print the results of the analysis and abort SOL02 if the CPU time limit is close to being exceeded. Equivalent routines may be substituted on other systems, or these routines may be commented out. Called by MAIN and SOL02A.

4. TIME and DATE. These are two routines on the local UMR system that are used to print the time and date of the analysis on the header. Equivalent routines may be substituted on other systems, or these routines may be commented out. Called by MAIN.

#### D. DYNAMIC MEMORY MANAGEMENT

1. Dynamic Memory Allocation. The computer program INRESB-3D-SUP stores all of the joint, material, element, mass, stiffness, response, etc. data in a large linear array, Z, that resides in the common block DATA. The Z array consists of real numbers. An integer array NZ is set equal to the Z array, by a Fortran EQUIVALENCE statement, to provide storage for integer variables. Index variables beginning with IZ, such as IZxxxx, are used to store the address of the information in the Z array. The variable IZ is used to track the next available space in the Z array. The exact amount of space required to solve a specific problem is reserved in the Z array during the execution of the program. This dynamic allocation of memory allows the program to use the computers memory efficiently.

For example, assume that the Z array is empty and  $IZ = 1$ . The joint ID numbers are integer variables that are stored in the NZ array. Thus the index for the joint ID numbers is  $IZID = IZ = 1$  and NUMJOI joint numbers are stored in the NZ array. Once the storage for the joint numbers is reserved, the next available storage location

is  $IZ = IZ + NUMJOI$ . Next the joint coordinates are stored in the Z array, beginning at  $IZCORD = IZ$ . The joint coordinates require  $3 * NUMJOI$  storage locations. Thus once the storage for the joint coordinates is reserved, the next available storage location is  $IZ = IZ + 3 * NUMJOI$ . The Z array with joint numbers and coordinates is shown in Figure 21.

2. Compact Matrix Storage. The mass, stiffness, geometric stiffness and dynamic stiffness matrices are sparse symmetric matrices. Because the matrices are symmetric, only half (the upper triangular matrix) of each matrix needs to be stored. Additionally, many of the terms in the upper triangular matrix are zero. The nonzero terms, in a given column, are typically found near the main diagonal. The level of the upper nonzero term in each column is the skyline. Thus only the terms below the skyline of the upper triangular matrix are stored in the Z array. Additionally the linear array addresses of the main diagonal elements are stored in the array MD. For example, let the matrix B be the 5x5 full symmetric matrix below

$$B = \begin{bmatrix} 1 & 3 & 0 & 0 & 12 \\ 3 & 2 & 5 & 0 & 11 \\ 0 & 5 & 4 & 7 & 10 \\ 0 & 0 & 7 & 6 & 9 \\ 12 & 11 & 10 & 9 & 8 \end{bmatrix} \quad (3)$$

where  $B_{1,3}$ ,  $B_{1,4}$  and  $B_{2,4}$  are zero. Thus the terms in the upper triangular matrix, below the skyline are

$$B_{\text{upper triangular}} = \begin{bmatrix} 1 & 3 & & & 12 \\ & 2 & 5 & & 11 \\ & & 4 & 7 & 10 \\ & & & 6 & 9 \\ & & & & 8 \end{bmatrix} \quad (4)$$

These elements are stored in the linear array by columns, beginning with the element on the main diagonal. Thus the B matrix in linear array form becomes

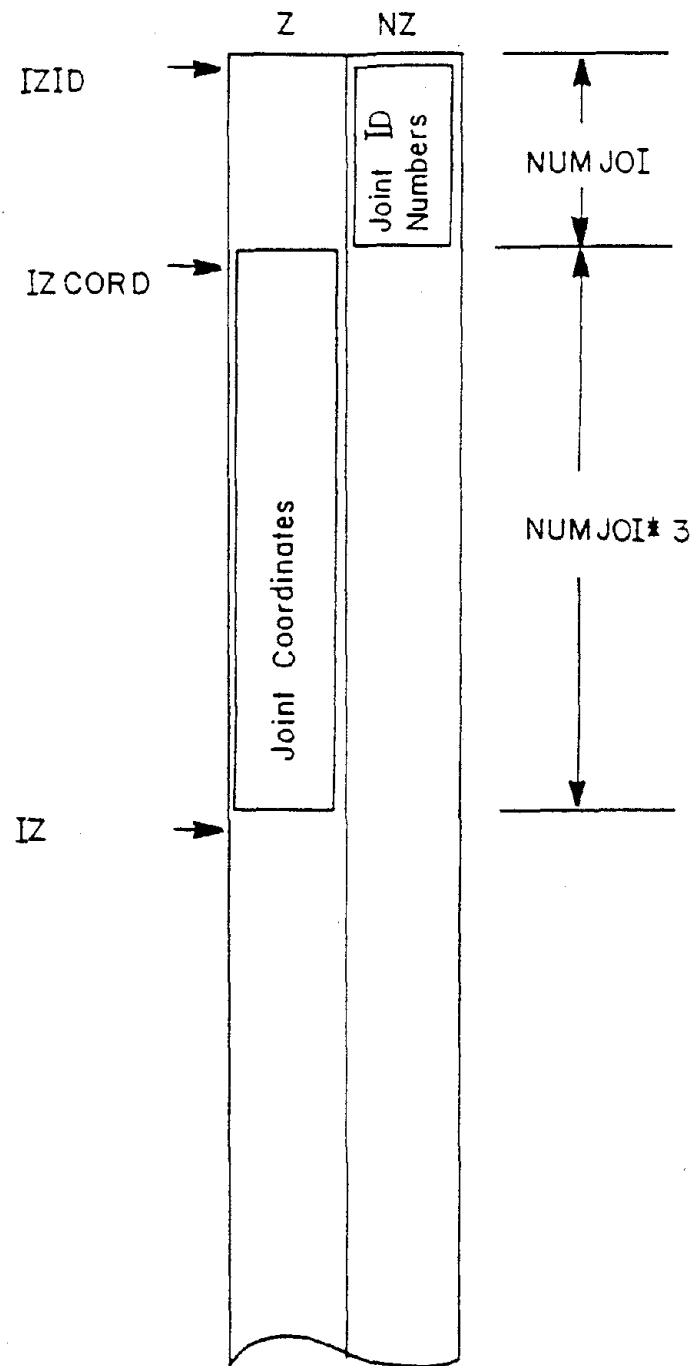


Figure 21. Dynamic Memory Example

$$A = \begin{bmatrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12 \end{bmatrix} \quad (5)$$

and the array, MD, containing the addresses of the main diagonal elements is

$$MD = \begin{bmatrix} 1 \\ 2 \\ 4 \\ 6 \\ 8 \\ 13 \end{bmatrix} \quad (6)$$

The last row of the array is a dummy element with the value  $N + 1$ , where  $N$  is the number of elements in the linear array. The  $i, j$  element of the linear array is addressed with the algorithm

$$\begin{aligned} B(I, J) &= A(MD(J) + J - I) \quad \text{If } J > I \text{ and } (MD(J) + J - I) < MD(J + 1) \\ &= 0 \quad \quad \quad \text{If } J > I \text{ and } (MD(J) + J - I) \geq MD(J + 1) \end{aligned} \quad (7)$$

This storage method was also presented by Bath and Wilson (2).

### 3. Capacity of the Dynamic Memory.

The program's capacity is a function of the amount of memory available in the computer. The program instructions compiled in double precision on an IBM 4381 computer require about 0.8 megabytes of memory. Assuming 8 megabytes of total memory is available, the Z array may occupy  $8 - 0.8 = 7.2$  megabytes of memory. For

double precision, on an IBM computer, each variable is 8 bytes long. Thus for 8 megabytes of memory, the Z array may contain up to  $\frac{7.2 \times 10^6}{8} = 900,000$  variables.

The number of variables in the Z array required for a specific problem is a function of 1) the number and orientation of the joints, 2) the number of restraints, 3) the number of constraints, 4) the number and types of materials, 5) the number and types of elements and the materials each element uses, 6) the number of joint masses, 7) the amount of storage required by the structural stiffness, geometric stiffness, and mass matrices, which is a function of the bandwidth, 8) the type of solution, 9) the number of degrees of freedom, 10) the number load cases for SOL01, 11) the number of element loadings for SOL01 and SOL04, 12) the number of free dof for SOL02 and SOL03, and 13) the length of the ground acceleration record for SOL02. The actual number of variables used, and the percentage of total memory used are printed out at the end of each block. For the example in Section C of Chapter V, the following message is printed in the output.

```
*-----*
*--- MEMORY UTILIZATION ..... ---*
*--- IZ= 21965,   MEM= 4.393%  ---*
*-----*
```

This example required 21,965 variables. Four megabytes of memory are available for the Z array and the program is compiled in double precision on an IBM computer. Thus the Z array has a capacity of  $\frac{4 \times 10^6}{8} = 500,000$  variables, and  $\frac{21965}{500,000} \times 100 = 4.393\%$  of the available memory was used.

The capacity of the program is modified by changing the value of MAXZ in the PARAMETER statement

```
PARAMETER (MAXZ = 500000, MAXDZ = MAXZ/2)
```

of file ZCOMN2 COPY. The macro library GEM3 is then regenerated and the program is recompiled.

## E. ADDITION OF MATERIALS, ELEMENTS, AND SOLUTIONS

The modular form of the INRESB-3D-SUP program allows for the relatively easy addition of materials, elements and solutions. The changes required to add materials, elements and solutions are discussed below.

1. Addition of a Material to the Material Library. A subroutine with the name MATxx is written that contains the material information. The subroutine must have the following options to be consistent with the existing subroutines:

IOPT=0 Determines the number of storage spaces required for each element utilizing this material. This storage is typically used by a hysteresis model that is called by routine MATxx.

IOPT=1 Inputs and stores data. Returns the amount of storage required for the material.

IOPT=2 Calculates the initial stiffness and initializes the hysteresis model.

IOPT=3 Calculates the current stiffness and load for an incremental displacement, given the previous loading history. Calculates the strain energies, ductilities, and excursion ratios.

IOPT=4 Calculates the strain energies, ductilities, and excursion ratios.

IOPT=5 Calculates the damage index.

For nonlinear materials, the subroutine MATxx calls a companion hysteresis model, subroutine HYSTxx.

The call to MATxx is added in routine MATLIB. All communication with the subroutine MATxx is through the routine MATLIB. The name of the material and the material number (MATYP = xx) are added to routine STRUCT.

2. Addition of an Element to the Element Library. A subroutine with the name ELExx is written that contains the element information. The subroutine must have the following options to be consistent with the existing subroutines:

- IOPT = 1 Interprets the input data, calculates transformation matrices, initial structural stiffness and a unit load geometric stiffness. Determines the actual amount of storage required.
- IOPT = 2 Determines the axial load used for the geometric stiffness.
- IOPT = 3 Recalculates the structural stiffness, if one of the components of stiffness has changed.
- IOPT = 4 Calculates the incremental forces, unbalanced forces and new components of stiffness.
- IOPT = 5 Calculates the total element forces and energies.
- IOPT = 6 Calculates the fixed end forces due to element loads, if applicable.
- IOPT = 7 Writes element data to an output file.
- IOPT = 8 Reads element data from an output file and print.
- IOPT = 9 Determines the amount of storage required for the element's materials.
- IOPT = 10 Determines the strain energy.
- IOPT = 11 Determines the ductilities and excursion ratios.
- IOPT = 12 Prints out the maximum forces and/or displacements that the element was subjected to.
- IOPT = 13 Sets the internal forces and displacement equal to zero. Reinitializes the hysteresis models.
- IOPT = 14 Calculates and prints the damage index.

The call to ELEXx is added in routine ELELIB. All communication with the subroutine ELEXx is through the routine ELELIB. The name of the element, the element number (NELTYP=xx), the number of variables input for the element, and the maximum amount of storage required for the element are added to routine STRUCT.

3. Addition of a Solution. A subroutine with the name SOLxx is written that reserves and initializes the storage required by the solution. SOLxx also calls CKSTOR to ensure that the program has enough storage to execute the solution. The call to SOLxx is added to routine SOLN. All communication with the subroutine SOLxx is through the routine SOLN.

Subroutine SOLxx calls subroutine SOLxxA which performs the actual solution. Subroutine SOLxxA may call other subroutine such as FORM to form the stiffness matrix, JOILOA to generate joint loadings, MSOLL to solve for displacements or ELELIB to calculate element forces. The functions of these subroutines and others are described in the previous section.



#### IV. INPUT DATA FOR PROGRAM INRESB-3D-SUP

The input for program INRESB-3D-SUP is divided into several blocks. Each block is briefly described below. The blocks may be executed in any order, except as noted. Multiple solutions of the same structure are possible by using multiple solution blocks. Multiple structures may be analyzed by redefining the structure with the STRUCT block.

<u>BLOCK</u>	<u>DESCRIPTION</u>
STRUCT .....	Defines the structure to be analyzed. Joints, materials, elements, mass and damping are defined.
SOL01 .....	Elastic static solution of the structure with multiple load cases. SOL01 must be preceded by the block STRUCT.
SOL02 .....	Dynamic solution of linear and nonlinear structures subject to three dimensional ground motion by numerical integration. SOL02 must be preceded by the block STRUCT.
SOL03 .....	Eigenvalue solution for the natural frequency or buckling load of an elastic structure. SOL03 must be preceded by the block STRUCT.
SOL04 .....	Incremental static solution of a nonlinear structure. SOL04 must be preceded by the block STRUCT.

##### Secondary Blocks

BUG .....	Sets flags to print out detailed information.
READ .....	Reads results written to an output file during SOL02 or SOL04, and prints the results.
NOECHO .....	Inhibits the input echo.
DUMP .....	Prints out the contents of the memory.
RELEASE .....	Releases the memory used for the previous solution.
STOP .....	Terminates execution of the program.

## NOTES ON INPUT

- 1) Input is free format, unless otherwise noted.
- 2) Input variables beginning with I-N are integers, and should not contain a decimal point.
- 3) Input variables beginning with A-H, and O-Z are real and may contain a decimal point.
- 4) Logical variables are identified in the input description, and have the value .TRUE. or .FALSE..
- 5) Character variables are identified in the input description, and are enclosed in 'single quotes', except as noted.
- 6) Character and logical variables must be input in upper case.
- 7) The input data is read from unit 05, except as noted.
- 8) The output is printed on unit 06, except as noted.
- 9) Input cards are identified by a box. If that card is repeated, the entire box is repeated.

input card image.....

The data for one card may be input on one or more lines in the data file, provided that all of the character variables are on the first line.

10) Consistent units are used throughout the program. Thus, input in inches, kips, seconds yields output in inches, inch-kips etc. Mixing units will yield unpredictable results. Units are indicated parenthetically where appropriate.

Example:

Note

'BUG = K'	(1)
'STRUCT'	(2)
. Structure input is omitted.	
'SOL04'	(3)
. Solution input is omitted.	
'READ UNIT = 21'	(4)
'STOP'	(5)

- (1) The bug option is set, this prints out the hysteresis model data for each time step.
- (2) The structure is defined.
- (3) An cyclic static solution of the structure is performed.
- (4) Data printed on unit 21 during SOL04 is read from the disk file and printed in a report.
- (5) The program is terminated.

A. STRUCTURE - DEFINE THE STRUCTURAL MODEL

These cards define the structural model to be analyzed. The following cards are each input once.

'STRUCT'
TITLE

STRUCT Signifies that the structural model is to be input. Character variable, enclose in single quotes.

TITLE User input title, 80 characters maximum. Character variable, enclose in single quotes.

1. Joints and Degrees of Freedom. These cards are used to define the coordinates of the joints, joint restraints, constraints and the degree of freedom to be condensed out. The degree of freedom numbers are assigned by the program, and printed in the output. The following card is input once.

NJOINT NCOS NSUPT NCOND NCONST SCALE
--------------------------------------

NJOINT The number of joints defined by the joint coordinate cards.

NCOS The number of joint direction cosine cards input.

NSUPT The number of joint restraint cards input.

NCOND The number of joint condensation cards input.

NCONST The number of joint constraint cards input.

SCALE Scale factor that the joint coordinates are to be multiplied by. If SCALE = 12, the user inputs the joint coordinates in feet, and the structure is defined in inches.

a. Joint Coordinates. These cards are used to define the coordinates of the joints, in the global coordinate system, GCS, and identify the direction cosine of the joint. The total number of joints defined in this section is less than or equal to NJOINT. The second card is only used when the preceding card has a value of IGEN that is greater than zero. These cards are repeated until 1) NJOINT joints have been defined, or 2) An input or generated joint ID number is less than or equal to zero.

ID X Y Z ICOS IGEN
--------------------

ΔID ΔX ΔY ΔZ
--------------

ID The joint IDentification number. ID numbers can be input in any convenient order and need not be consecutive. However, the band width of

the structural stiffness matrix is dependent on the joint ID numbers. An  $ID \leq 0$  terminates the input of the joint coordinates.

- X The GCS X coordinate of the joint. (length)
- Y The GCS Y coordinate of the joint. (length)
- Z The GCS Z coordinate of the joint.(length)
- ICOS The joint's direction cosine number.
- IGEN The number of additional joints to be generated from this joint.
- $\Delta ID$  The increment between the generated ID number and the previous joint's ID number. A generated  $ID \leq 0$  terminates the input of the joint coordinates.
- $\Delta X$  The increment between the generated joint's GCS X coordinate and the previous joint's X coordinate. (length)
- $\Delta Y$  The increment between the generated joint's GCS Y coordinate and the previous joint's Y coordinate. (length)
- $\Delta Z$  The increment between the generated joint's GCS Z coordinate and the previous joint's Z coordinate. (length)

Example: NJOINT = 7

	<u>Note</u>
10 0. 0. 0. 1 2	(1,2)
10 0. 0. 3.	(2)
1 4. 3. -1. 2 0	(3)
-1 0 0 0 0 0	(4)

- (1) Joint 10 has the coordinates (0,0,0) and uses direction cosine #1.
- (2) Two joints are generated from joint 10: Joint 20 (0,0,3) and Joint 30 (0,0,6).
- (3) Joint 1 has the coordinates (4,3,-1) and uses direction cosine #2.
- (4) Input of the joint coordinates is terminated.

b. Joint Direction Cosines. These cards are used to input the joint direction cosines, which in turn define the joint coordinate system, JCS. The joint direction cosines are numbered from 1 to NCOS. This card is repeated NCOS times.

Vxi	Vxj	Vxk	Vyi	Vyj	Vyk
-----	-----	-----	-----	-----	-----

Vxi The projection on the GCS X axis of a unit vector parallel to the JCS X axis.

Vxj The projection on the GCS Y axis of a unit vector parallel to the JCS X axis.

Vxk The projection on the GCS Z axis of a unit vector parallel to the JCS X axis.

Vyi The projection on the GCS X axis of a unit vector parallel to the JCS Y axis.

Vyj The projection on the GCS Y axis of a unit vector parallel to the JCS Y axis.

Vyk The projection on the GCS Z axis of a unit vector parallel to the JCS Y axis.

c. Joint Restraints. These cards are used to define the joint restraints. This card is repeated NSUPT times.

ID	ITX	ITY	ITZ	IRX	IRY	IRZ	IGEN	ΔID
----	-----	-----	-----	-----	-----	-----	------	-----

ID The joint IDentification number. An ID of zero indicates that all the joints are restrained by this card.

ITX Restraint flag for translation in the JCS X direction.

ITY Restraint flag for translation in the JCS Y direction.

ITZ Restraint flag for translation in the JCS Z direction.

IRX Restraint flag for rotation about the JCS X axis.

IRY Restraint flag for rotation about the JCS Y axis.

IRZ Restraint flag for rotation about the JCS Z axis.

IGEN The number of additional joints, with the same restraints, to be generated from this joint.

$\Delta ID$  The increment between the generated ID number and the last ID number.

Valid joint restraint flags are:

- 0 Free or unrestrained degree of freedom.
- 1 Restrained degree of freedom.
- 2 Restrained degree of freedom. A restraint flag of 2 forces the program to assign the dof a higher number. This option can be used to reduce the bandwidth of the stiffness matrix.

Example: NSUPT = 2

Note

```
0 0 0 0 0 0 1 0 0
1 1 1 1 1 1 1 0 0
```

(1)

(2)

- (1) The rotation about the JCS Z axis of all joints is restrained.
- (2) Joint 1 has all six dofs restrained.

d. Joint Condensation. These cards are used to identify which dof are condensed out. This card is repeated NCOND times and is omitted if NCOND equals zero.

ID ITX ITY ITZ IRX IRY IRZ IGEN $\Delta ID$
---------------------------------------------

ID The joint IDentification number. An ID of zero indicates that all of the joints are affected by this card.

ITX Condensation flag for translation in the JCS X direction.

ITY Condensation flag for translation in the JCS Y direction.

ITZ Condensation flag for translation in the JCS Z direction.

IRX Condensation flag for rotation about the JCS X axis.

IRY Condensation flag for rotation about the JCS Y axis.

IRZ Condensation flag for rotation about the JCS Z axis.

IGEN The number of additional joints, with the same condensation, to be generated from this joint.

$\Delta$ ID The increment between the generated ID number and the last ID number.

Valid condensation flags are:

0 Degree of freedom is not condensed out.

1 Degree of freedom is condensed out. Condensation of a restrained dof is ignored.

Example: NCOND= 1

30 0 0 0 1 1 1 0 0

The rotations of joint 30 are condensed out. If the Z axis rotation had been previously restrained, only the X and Y axis rotations are condensed out.

e. Joint Constraints. These cards are used to identify which dof are constrained.

This card is repeated NCONST times, and omitted if NCONST equals zero.

ITYPE MASTER ISLAVE IGEN $\Delta$ ID
--------------------------------------

ITYPE The type of constraint.

0 Rigid body constraint. A rigid body constraint transfers all six joint dof from the slave to the master joint.

1 XY-planar constraint. An XY-planar constraint transfers the joint's JCS X and Y axes translational dof and the joint's JCS Z axis rotational dof from the slave to the master joint.

MASTER The joint IDentification number of the master joint.

ISLAVE The joint IDentification number of the slave joint.

IGEN The number of additional slave joints, constrained to the same master joint to be generated.



$\Delta ID$  The increment between the generated ID number and the previous ID number.

Note: Both the slave and master joint must have the same joint direction cosine number (ICOS).

Example: NCONST = 1

```
1 10 20 0 0
```

Joint 20 is constrained in the JCS XY-plane to Joint 10.

2. Materials and Hysteresis Model Information. These cards are used to input the material and hysteresis model information. The first card is input once. The second card is repeated NMAT times.

NMAT
TYPE VALUE1 VALUE2 ...

NMAT The number of materials input.

TYPE The material type. Valid types are discussed below. Character variable, enclose in single quotes.

VALUE<sub>i</sub> The input required by a given material type. The values for each TYPE are discussed below. (real or integer)

Notes on material - element compatibility:

- 1) Individual elements may not use all of the information provided by a given material.
- 2) A given material may not be compatible with all of the elements. For example the Takeda hysteresis model may not be used with the elastic prismatic beam element. The compatible materials for each element are specified under the element input.

a. TYPE = '3D-BEAM'. Material data for an elastic 3D-beam.

'3D-BEAM' E G AX AY AZ J IY IZ

E Young's modulus. (force/length<sup>2</sup>)  
G Shear modulus. (force/length<sup>2</sup>)  
AX Cross sectional area. (length<sup>2</sup>)  
AY Y axis shear area. (length<sup>2</sup>)  
AZ Z axis shear area. (length<sup>2</sup>)  
J Torsional moment of inertia. (length<sup>4</sup>)  
IY Moment of inertia, about the Y axis. (length<sup>4</sup>)  
IZ Moment of inertia, about the Z axis. (length<sup>4</sup>)

b. TYPE = 'AXLMOD'. AXLMOD axial hysteresis model for reinforced concrete as shown in Figures 2 and 3.

'AXLMOD' Kc Kt Kt2 Fy  $\alpha$   $\beta$   $\mu f$   $\beta DI$

Ks Compression stiffness of a unit length member. (force/length)  
Kt Pre-yielding tensile stiffness of a unit length member. (force/length)  
Kt2 Post-yielding tensile stiffness of a unit length member. (force/length)  
Fy Yield force. (force)  
 $\alpha$  Unloading coefficient, usually 0.90.  
 $\beta$  Pinching coefficient, usually 0.20.  
 $\mu f$  Failure Ductility.  
 $\beta DI$  Parameter for Ang's damage index discussed in Appendix B (1).

The stiffness terms Kc, Kt, and Kt2 are real variables and may contain a decimal point.

c. TYPE = 'BENDI'. Material data for the B1 hysteresis model. The B1 hysteresis model was developed to model the bending behavior of reinforced concrete shear walls and is shown in Figure 4. The input for the backbone curve is shown in Figure 5.

'BENDI' NSEG NI DY $\beta$ DI
P(1) P(2) ... P(NSEG)
D(1) D(2) ... D(NSEG)

NSEG Number of points on the backbone curve.

NI Number of small amplitude loop reversal points that can be stored by the program at one time, usually 10.

DY Rotation of a unit length member, corresponding the yield point. Used to define the ductility ratio. (radian/length)

$\beta$ DI Parameter for Ang's damage index discussed in Appendix B (1).

P(i) The moment of a point on the backbone curve. (force\*length)

D(i) The rotation of a point on the backbone curve. Where the rotation is based on a unit length member. (radian/length)

d. TYPE = 'SHEARI'. Material data for the S1 hysteresis model. The S1 hysteresis model was developed to model the shear deformation of reinforced concrete shear walls and is shown in Figure 6. The input for the backbone curve is shown in Figure 5.

'SHEAR1' NSEG NI DY $\beta$ DI
P(1) P(2) ... P(NSEG)
D(1) D(2) ... D(NSEG)

- NSEG    Number of points on the backbone curve.
- NI        Number of small amplitude loop reversal points that can be stored by the program at one time, usually 10.
- DY        Shear deformation of a unit length member, corresponding the yield point. Used to define the ductility ratio. (length/length)
- $\beta$ DI       Parameter for Ang's damage index discussed in Appendix B (1).
- P(i)       The shear of a point on the backbone curve. (force)
- D(i)       The shear deformation of a point on the backbone curve, where the shear deformation is based on a unit length member. (length/length)

e. TYPE = 'TAKEDA'. Material data for the TAKEDA hysteresis model. The TAKEDA hysteresis model was developed to model the bending deformations in reinforced concrete members and is shown in Figure 7.

'TAKEDA' PC DC PY DY PU DU $\beta$ DI
---------------------------------------

- PC        Cracking moment. (force\*length)
- DC        Cracking rotation, for a unit length member. (radian/length)
- PY        Yield moment. (force\*length)
- DY        Yield rotation, for a unit length member. (radian/length)
- PU        Ultimate moment. (force\*length)
- DU        Ultimate rotation, for a unit length member. (radian/length)

$\beta$ DI Parameter for Ang's damage index discussed in Appendix B (1).

f. TYPE = 'BILINEAR'. The bilinear hysteresis model sketched in Figure 8.

```
'ELSPLS' E PY SIE  $\mu$ f  $\beta$ DI
```

E Elastic stiffness. (force/length)

PY Yield load. (force)

SIE Inelastic stiffness. (force/length)

$\mu$ f Failure Ductility.

$\beta$ DI Parameter for Ang's damage index discussed in Appendix B (1).

3. Geometric Stiffness Data. This card is used to determine the type of geometric stiffness used in the analysis. This card is input once.

```
KGLOAD KGTYPE KGFORM KGCOND
```

KGLOAD The type of axial force used to calculate the geometric stiffness.

- 0 The geometric stiffness is omitted.
- 1 The axial force is equal to the input force, magnified by the ground acceleration in the global Z direction, if applicable.
- 2 The internal element force of the previous load step is use to generate the geometric stiffness.

KGTYPE The type of geometric stiffness formulation.

- 0 The geometric stiffness is omitted.
- 1 A 'lumped parameter' formulation is used for the element geometric stiffness.

- 2 A 'consistent parameter' formulation is used for the element geometric stiffness. If a consistent parameter formulation for an individual element is not available, the lumped parameter formulation is used. Refer to individual element specifications for applicability.

KGFORM Form of the geometric stiffness used.

- 0 The geometric stiffness is omitted.
- 1 The geometric stiffness is subtracted from the structural stiffness.
- 2 Separate structural stiffness and geometric stiffness matrices are formed.

Refer to individual solution for applicability.

KGCOND A logical flag. If KGCOND=.TRUE., the geometric stiffness matrix is condensed when applicable. Logical variable.

4. Element Data. These cards are used to define the elements. The elements are numbered by the program in the order they are input from 1 to NELMT. The element numbers are used to identify the elements in the output. The first card is input once. The second and third card (if used) are repeated until 1) NELMT elements are input, or 2) a TYPE='END' is encountered. The third card follows each second card with a value of IGEN > 1.

NELMT				
TYPE	NAME	VALUE1	VALUE2 ...	IGEN
ΔVALUE1		ΔVALUE2 ...		

NELMT The number of elements input.

- TYPE The element type. Valid types are discussed below. Character variable, enclose in single quotes.
- NAME A user defined name. Character variable, enclose in single quotes.
- VALUEi The input required by a given element type. The values for each TYPE are discussed below. (real or integer)
- IGEN The number of additional elements to be generated from this element.
- ΔVALUEi The incremental value used to generate subsequent elements.

$$VALUE_{i_{generated}} = VALUE_{i_{previous}} + \Delta VALUE_i$$

- a. TYPE = '3D-BEAM'. This card is used to define the element data for the elastic prismatic 3D-beam shown in Figure 9.

<pre> '3D-BEAM' NAME MAT JOINTI JOINTJ V1 V2 V3 XS XE PKG       IRELT IGEN </pre>
-----------------------------------------------------------------------------------

- NAME A user defined name. Character variable, enclose in single quotes.
- MAT Material number. The material number must correspond to the material type '3D-BEAM'. The terms EAX, GJ, EIY and EIZ from material '3D-BEAM' are used to generate the element stiffness.
- JOINTI Start joint ID number.
- JOINTJ End Joint ID number.
- V1 The projection on the GCS X axis of a vector in the element's local XY-plane. This vector defines the orientation of the element's local Y-axis.
- V2 The projection on the GCS Y axis of a vector in the element's local XY-plane.
- V3 The projection on the GCS Z axis of a vector in the element's local XY-plane.

- XS      The off set distance from the start joint to the beginning of the element. Positive in the direction of the element's local X-axis. (length)
- XE      The off set distance from the end joint to the end of the element. Negative in the direction of the element's local X-axis. (length)
- PKG     Axial load used to calculate the geometric stiffness, if KGLOAD= 1. (force) Positive is compression.
- IRELT   A six digit release code that is used to release the rotational dof at the ends of the element. A nonzero value of the i'th digit signifies a released dof.

DIGIT

- 1      Releases the moment about the element's X axis at the start joint.
  - 2      Releases the moment about the element's Y axis at the start joint.
  - 3      Releases the moment about the element's Z axis at the start joint.
  - 4      Releases the moment about the element's X axis at the end joint.
  - 5      Releases the moment about the element's Y axis at the end joint.
  - 6      Releases the moment about the element's Z axis at the end joint.
- IGEN    Element generation parameter. See discussion under 'Element Data'.

b. TYPE= 'SPRING'. This card is used to define the element data for the one dimensional spring shown in Figure 10.

<pre>'SPRING' NAME MAT JOINTI JOINTJ KTYPE XLEN V1 V2 V3 XS XE IGEN</pre>
---------------------------------------------------------------------------

- NAME    A user defined name. Character variable, enclose in single quotes.
- MAT     Material number.
- JOINTI   Start joint ID number.
- JOINTJ   End joint ID number.
- KTYPE   Type of spring.



- 1 Axial spring.
- 2 Shear spring in the element's local Y axis.
- 3 Shear spring in the element's local Z axis.
- 4 Torsional spring.
- 5 Rotational spring about the element's local Y axis.
- 6 Rotational spring about the element's local Z axis.

**XLEN** Length of the spring used to calculate the stiffness. If XLEN is zero the length between the start and end joints less XS and XE is used to formulate the stiffness. (length)

**V1** The projection on the GCS X axis of a vector in the springs local XY-plane. This vector defines the orientation of the element's local Y-axis.

**V2** The projection on the GCS Y axis of a vector in the springs local XY-plane.

**V3** The projection on the GCS Z axis of a vector in the springs local XY-plane.

**XS** The off set distance from the start joint to the beginning of the spring. Positive in the direction of the element's local X axis. (length)

**XE** The off set distance from the end joint to the end of the spring. Negative in the direction of the element's local X axis. (length)

**IGEN** Element generation parameter. See discussion under 'Element Data'.

**Notes:**

- 1) The material specified for the spring element may consist of any of the following: 3D-BEAM, AXLMOD, BEND1, SHEAR1, TAKEDA, and ELSPLS.
- 2) The spring uses the axial stiffness from the 3D-BEAM material.
- 3) The BEND1 and TAKEDA models are usually based on moment-rotation, (KTYPE=4 to KTYPE=6) but they can be used as translational springs (KTYPE=1 to KTYPE=3) by changing the material input from moment-rotation to force-translation.

- 4) The AXLMOD and SHEAR1 models are usually based on force-translation, and are valid models for KTYPE = 1 to KTYPE = 3.
- 5) The program does not check the user's choice of model.
- 6) If the distance between the start and end joints is zero, the spring is orientated such that the ECS is parallel to the start joints JCS.

c. TYPE = 'SHEAR WALL'. This card is used to define the element data for the reinforced concrete shear wall shown in Figure 14.

'SHEAR WALL' NAME MATB MATS MATA J1 J2 J3 J4 ALPHA PKG IGEN
----------------------------------------------------------------

- NAME A user defined name. Character variable, enclose in single quotes.
- MATB Bending hysteresis model material number.
- MATS Shear hysteresis model material number.
- MATA Axial hysteresis model material number.
- J1 Joint at the upper right hand corner of the element.
- J2 Joint at the upper left hand corner of the element.
- J3 Joint at the lower left hand corner of the element.
- J4 Joint at the lower right hand corner of the element.
- ALPHA Fraction of the length from the top of the element to the internal springs.
- PKG Axial load used to calculate the geometric stiffness, if KGLOAD = 1.  
Positive is compression. (force)
- IGEN Element generation parameter. See discussion under 'Element Data'.

Notes:

- 1) The material specified for the shear wall element may consist of any of the following: 3D-BEAM, AXLMOD, BEND1, SHEAR1, TAKEDA, and ELSPLS.
- 2) The BEND1 model is usually specified for the bending material.

- 3) The SHEAR1 model is usually specified for the shear material.
- 4) The AXLMOD model is usually specified for the axial material.
- 5) The 3D-BEAM material's axial stiffness is used for the spring's stiffness if the 3D-BEAM material is specified.

Example:

Note

5	(1)
'3D-BEAM' 'AI' 1 10 20 0. 0. 1. 0. 0. 0. 100000 2	(2, 3)
0 10 10 0. 0. 0. 0. 0. 0. 000000	(3)
'SPRING' 'SI' 2 10 11 1 0. 0. 0. 1. 0. 0. 0	(4)
'SHEAR WALL' 'WI' 3 4 5 20 10 1 2 1. 35. 0	(5)

- (1) Five elements are to be input.
- (2) A 3D-beam is input between joints 10 and 20.
- (3) Two more 3D-beams are generated from the first beam.
- (4) An axial spring is input between joints 10 and 11.
- (5) A shear wall element is input between joints 20, 10, 1 and 2.

5. Mass. These cards are used to input lumped masses at the joints. The first card is input once. The second card is repeated INMASS times, or until a joint ID  $\leq 0$  is encountered. If INMASS is less than one, or FMASS is zero, omit the second card.

INMASS FMASS MCOND
ID PX PY PX RXX RYY RZZ RXY RXZ RYZ IGEN ΔID

INMASS The number of mass cards to be read.

FMASS Mass flag.

- 0 The mass matrix is omitted.
- 1 The mass matrix due to concentrated joint masses is formed.

MCOND A logical flag. If MCOND=.TRUE., the mass matrix is condensed when applicable. Logical variable.

ID Identification number of the joint.

PX Translational mass in the joint's JCS X direction. (mass)

PY Translational mass in the joint's JCS Y direction. (mass)

PZ Translational mass in the joint's JCS Z direction. (mass)

RXX Rotational mass moment of inertia about the joint's JCS X axis.  
(mass\*length<sup>2</sup>)

RYY Rotational mass moment of inertia about the joint's JCS Y axis.  
(mass\*length<sup>2</sup>)

RZZ Rotational mass moment of inertia about the joint's JCS Z axis.  
(mass\*length<sup>2</sup>)

RXY Rotational mass product of inertia about the joint's JCS XY axis.  
(mass\*length<sup>2</sup>)

RXZ Rotational mass product of inertia about the joint's JCS XZ axis.  
(mass\*length<sup>2</sup>)

RYZ Rotational mass product of inertia about the joint's JCS YZ axis.  
(mass\*length<sup>2</sup>)

IGEN Number of joints with identical mass, to be generated.

ΔID Increment of joint ID number for generated values.

Example: INMASS=1, FMASS=1,

10 8. 8. 8. 0 0 0 0 0 0 0

Joint 10 has a translational mass of 8.0 in the X, Y and Z directions.

6. Damping. This card is used to input proportional damping data.

ALPHA BETA
------------

ALPHA Proportional damping coefficient for mass.

BETA Proportional damping coefficient for stiffness.

## B. SOL01 - ELASTIC STATIC SOLUTION

The following solution is an elastic solution with multiple load cases. The following cards are input once.

'SOL01'
TITLE
NLOAD MAXELD

SOL01 Signifies solution #1. Character variable, enclose in single quotes.

TITLE User input title, 80 characters maximum. Character variable, enclose in single quotes.

NLOAD Number of load cases.

MAXELD Maximum number of element loads.

Notes:

- 1) Condensation increases the band width of the stiffness matrix for SOL01 without any other benefits. Condensation is not recommended for SOL01.
- 2) A separate geometric stiffness (KGFORM=2) is not used by SOL01. The geometric stiffness may be included by using KGFORM=1.
- 3) If the geometric stiffness is included, the element axial loads must be input, KGLOAD=1.

1. Joint Loads. These cards are used to apply loads to joints. Loads applied to restrained joints are considered as displacements, yielding, support settlement or displacement control solutions. Loads applied to constrained joints are transferred to their 'master' joints. If the 'master' joint is restrained, loads transferred to restrained dof are considered as displacements. Joint loads are additive; applying two loads to the same joint results in the sum of the joint loads being considered. The following card is repeated until the value of DIR is 'END'.

LOAD	ID	IGEN	ΔID	DIR	VALUE
------	----	------	-----	-----	-------

- LOAD    Number of the load case that the load is applied to.
- ID        Joint ID number that the load is applied to.
- IGEN    Number of identical joint loads to be generated.
- ΔID      Increment of joint ID number for generated values.
- DIR      Direction of load, in the joint coordinate system. Valid directions and the units of VALUE are given below. Character variable, enclose in single quotes.
- 'FX'    Applied force in the joint's JCS X direction. (force)
- 'FY'    Applied force in the joint's JCS Y direction. (force)
- 'FZ'    Applied force in the joint's JCS Z direction. (force)
- 'MX'    Applied moment about the joint's JCS X axis. (force\*length)
- 'MY'    Applied moment about the joint's JCS Y axis. (force\*length)
- 'MZ'    Applied moment about the joint's JCS Z axis. (force\*length)
- 'END'    Terminate the input of element loads.
- VALUE    Magnitude of the applied load.

Example:

Note

1 2 2 1 'FZ' -3.00	(1)
2 7 0 0 'MX' 33.5	(2)
0 0 0 0 'END' 0	(3)

- (1) Joints 2, 3, and 4 have an applied force of -3.00 in the Z direction, load case 1.
- (2) Joints 7 has an applied moment of 33.50 in the X direction, load case 2.
- (3) Joint loading input is terminated.

2. Element Loads. These cards are used to apply element loads to the '3D-BEAM' element. The loads are applied to the portion of the beam between points A and B of Figure 9, in the ECS. The loads are transferred by the program to the start and end joints. The following card is only included if MAXELD > 0. The card is repeated MAXELD times, or until the value of TYPE is 'END'.

LOAD IELE IGEN ΔIELE TYPE DIR VALUE1, VALUE2, ...

LOAD Load case number.

IELE Element number.

IGEN Number of similar element loads to be generated.

ΔIELE Increment of element number for generated values.

TYPE Type of load. Valid types are described in detail below. Character variable, enclose in single quotes.

'CONC' Concentrated load applied in direction DIR. VALUE1 is the magnitude of the load (force or force\*length). VALUE2 is the ratio of the distance to the load, divided by the flexible length of the member. The distance is measured from the beginning of the

flexible length at the member's start end. VALUE2 is between 0 and 1. Only two values are input.

'UNIF' Uniform load applied in direction DIR. VALUE1 is the magnitude of the load. Only one value is input. (force/length)

'FEM' Input the fixed end forces on the end of the member. DIR is not used and may be set to any value. VALUE1 to VALUE12 are required.

VALUE1 Fixed end axial force, at point A of Figure 9, in the ECS X direction. (force)

VALUE2 Fixed end shear, at point A of Figure 9, in the ECS Y direction. (force)

VALUE3 Fixed end shear, at point A of Figure 9, in the ECS Z direction. (force)

VALUE4 Fixed end torsion, at point A of Figure 9, about the ECS X axis. (force\*length)

VALUE5 Fixed end moment, at point A of Figure 9, about the ECS Y axis. (force\*length)

VALUE6 Fixed end moment, at point A of Figure 9, about the ECS Z axis. (force\*length)

VALUE7 Fixed end axial force, at point B of Figure 9, in the ECS X direction. (force)

VALUE8 Fixed end shear, at point B of Figure 9, in the ECS Y direction. (force)

VALUE9 Fixed end shear, at point B of Figure 9, in the ECS Z direction. (force)

VALUE10 Fixed end torsion, at point B of Figure 9, about the ECS X axis. (force\*length)



VALUE11 Fixed end moment, at point B of Figure 9, about the  
ECS Y axis. (force\*length)

VALUE12 Fixed end moment, at point B of Figure 9, about the  
ECS Z axis. (force\*length)

'END' Terminate the input of element loads.

DIR Direction of load, in element coordinate system. Valid directions given  
below. Character variable, enclose in single quotes.

'FX' Axial load is applied.

'FY' Force is applied in the local element's Y direction.

'FZ' Force is applied in the local element's Z direction.

'MX' Torque is applied.

'MY' Moment is applied about the local element's Y axis.

'MZ' Moment is applied about the local element's Z axis.

VALUEi Values used to calculate the element loads.

Notes:

- 1) Multiple loads may be put on a single element.
- 2) 'UNIF' 'MY' and 'UNIF' 'MZ' are not available.
- 3) Element load TYPE = 'FEM' is not modified to reflect member end releases.

Example: MAXELD = 1,

```
1 13 0 0 'UNIF' 'FZ' -3.00
```

Element 13 has a uniform load of -3.00 applied in the element's local Z direction, for load case 1.

### C. SOL02 - DYNAMIC SOLUTION BY NUMERICAL INTEGRATION

This is a dynamic solution of the structure subject to ground accelerations. Both elastic and nonlinear behavior can be modeled. The following cards are input once.

'SOL02'
TITLE
INTEG THETA ELASTIC UNBAL
IPRINT IWRITE MAXACC SLMASS
TO ΔT TF GRAV

- SOL02 Signifies solution #2. Character variable, enclose in single quotes.
- TITLE User input title, 80 characters maximum. Character variable, enclose in single quotes.
- INTEG Type of numerical integration used. Valid values of INTEG are given below. Character variable, enclose in single quotes.
- 'LINEAR' The linear acceleration method is used.
- 'AVERAGE' The average acceleration method is used.
- THETA Not used, set THETA = 0.
- ELASTIC A logical flag. If ELASTIC = .TRUE., the structure is assumed to behave elastically. Logical variable.
- UNBAL A logical flag. If UNBAL = .TRUE., the unbalanced loads from the preceding step are added to the current dynamic loads for nonlinear analysis. Logical variable.
- IPRINT Step increment for printed output.
- IWRITE Step increment for data written to output files.
- MAXACC The maximum number of points in each ground acceleration record.

SLMASS A logical flag. If SLMASS = .TRUE., a special mass matrix is input. This matrix is used, with the ground acceleration to generate loads. Logical variable.

TO Initial time at the beginning of the solution. (time)

$\Delta T$  Time step. (time)

TF Final time at the end of the solution. (time)

GRAV Gravitational acceleration constant. (length/sec<sup>2</sup>)

1. Special Loading Mass. The special loading mass matrix discussed in step 1 of Section C in Chapter II is input by these cards. If the special loading mass is input the dynamic joint loads are the ground acceleration times the special loading mass. If the special loading mass is not input, the dynamic joint loads are the ground acceleration times the structural mass. The first card is input once. The second card is repeated INMASS times, or until an ID less than one is encountered. If INMASS is less than one, or FMASS is zero, omit the second card. Omit both cards if SLMASS = .FALSE..

INMASS FMASS
ID PX PY PX RXX RYY RZZ RXY RXZ RYZ IGEN $\Delta$ ID

These cards are identical to the 'Mass' cards in the block STRUCT. Refer to STRUCT for a detailed description.

2. Output Data to Disk Files. These cards control the data that is written to separate disk files. This data is used to print reports and plot data. The card is repeated until the value of TYPE is 'END'.

TYPE NUMB IUNIT IGEN ΔNUMB ΔIUNIT
-----------------------------------

TYPE Type of data to be written to output file. Valid types are given below.  
Character variable, enclose in single quotes.

'DOF' Data is printed for a degree of freedom. The degree of freedom ID number, as assigned by the program, is used.

'JOINT FX' Data is printed for the degree of freedom corresponding to the joint's JCS X translation.

'JOINT FY' Data is printed for the degree of freedom corresponding to the joint's JCS Y translation.

'JOINT FZ' Data is printed for the degree of freedom corresponding to the joint's JCS Z translation.

'JOINT MX' Data is printed for the degree of freedom corresponding to the joint's JCS X rotation.

'JOINT MY' Data is printed for the degree of freedom corresponding to the joint's JCS Y rotation.

'JOINT MZ' Data is printed for the degree of freedom corresponding to the joint's JCS Z rotation.

'ELE' Element data is printed.

'ENERGY' The structures energy balance is printed.

'SUMRCT' The structures summation of reactions is printed.

'GROUND' The ground response is printed.

'END' Terminate the input of element loads.

NUMB Element, dof or joint number. Set NUMB=0 if TYPE='ENERGY'.

IUNIT Output file unit number.

IGEN Number of similar data groups to be printed.

$\Delta$ NUMB Incremental element dof or joint number for generation.

$\Delta$ IUNIT Incremental output file unit number for generation.

Example:

	<u>Note</u>
'DOF' 5 10 0 0 0	(1)
'ELE' 32 11 1 1 1	(2)
'END' 0 0 0 0 0	(3)

(1) Degree of freedom #5 data is written to file 10.

(2) Element 32's data is written to file 11, and element 33's data is written to file 12.

(3) Output requests are terminated.

3. Initial Displacements, Velocities, Accelerations and Loads. This card is used to define initial conditions for dynamic analysis. This card is repeated until OPTION has a value of 'END'.

ID IGEN $\Delta$ ID OPTION V1 V2 V3 V4 V5 V6
----------------------------------------------

ID Joint ID number.

IGEN Number of joints with identical initial conditions.

$\Delta$ ID Increment of the joint ID number for generation.

OPTION Type of initial condition. Valid options are listed below. Character variable, enclose in single quotes.

'DISPL' Initial displacements are given. V1, V2 and V3 are displacements (length), while V4, V5 and V6 are rotations (radians).

'VEL' Initial velocities are given. V1, V2 and V3 are translational velocities (length/time), while V4, V5 and V6 are rotational velocities (radians/time).

'ACC' Initial accelerations are given. V1, V2 and V3 are translational accelerations (length/time<sup>2</sup>), while V4, V5 and V6 are rotational accelerations (radians/time<sup>2</sup>).

'LOA' Initial loads are given. V1, V2 and V3 are loads (force), while V4, V5 and V6 are moments (force\*length).

V1 Initial value of translation or force in the joint's JCS X direction.

V2 Initial value of translation or force in the joint's JCS Y direction.

V3 Initial value of translation or force in the joint's JCS Z direction.

V4 Initial value of rotation or moment about the joint's JCS X axis.

V5 Initial value of rotation or moment about the joint's JCS Y axis.

V6 Initial value of rotation or moment about the joint's JCS Z axis.

Note:

- 1) If the acceleration at time TO is nonzero, initial conditions must be specified to ensure equilibrium.
- 2) The initial acceleration may be set equal to zero by one of the following methods:
  - a) The initial time at the beginning of the solution is equal to the initial time of the acceleration record, (TO = TOG), set A(1) = 0.
  - a) The initial time at the beginning of the solution is less than the initial time of the acceleration record, (TO < TOG), set A(1) ≠ 0.
- 3) If the dynamic solution, SOL02, follows a static solution, SOL01, then the resulting displacements and element forces are automatically included as the initial conditions for the dynamic solution. The results from the static solution may be excluded from the dynamic solution by releasing the memory between solutions.

Example:

```
2 2 1 'ACC' 3.0 0 0 0 0
0 0 0 'END' 0 0 0 0 0
```

Note

(1)

(2)

- (1) Joints 2, 3 and 4 have an initial acceleration of 3.0 in the X direction.

(2) Initial conditions are terminated.

4. Ground Acceleration Record. These cards are used to input the ground acceleration record, and its orientation. The following cards are input once.

NA ASCALE TOG ΔTG PRINT
Vxi Vzj Vxk Vyi Vyj Vyk

NA Number of components of ground acceleration input.  $1 \leq NA \leq 3$

ASCALE Ground acceleration amplitude scale factor.

TOG Time at the first point of the ground acceleration. (time)

ΔTG Time increment for the input ground acceleration. (time)

PRINT A logical flag. If PRINT=.TRUE. then the 3D ground accelerations are printed.

Vxi The GCS X axis projection of a unit vector defining the X' axis of the input ground acceleration.

Vxj The GCS Y axis projection of a unit vector defining the X' axis of the input ground acceleration.

Vxk The GCS Z axis projection of a unit vector defining the X' axis of the input ground acceleration.

Vyi The GCS X axis projection of a unit vector defining the Y' axis of the input ground acceleration.

Vyj The GCS Y axis projection of a unit vector defining the Y' axis of the input ground acceleration.

Vyk The GCS Z axis projection of a unit vector defining the Y' axis of the input ground acceleration.

The following set of cards are repeated NA times. The two FORMAT cards are only used if the value of FMT=.TRUE.. The two ATITLE cards and A() are input on unit=IN.

IN NPTS IDIR FMT ECHO REWIND
FORMAT1
FORMAT2
ATITLE2
ATITLE2
A(1) A(2) A(3) ... ... A(NPTS)

- IN            Input unit number for acceleration record.
- NPTS        Number of acceleration points to be read.  $NPTS \leq MAXACC$
- IDIR        Direction of acceleration being read.
- 1    Ground acceleration is in the X' direction.
  - 2    Ground acceleration is in the Y' direction.
  - 3    Ground acceleration is in the Z' direction.
- FMT        A logical flag. If FMT=.TRUE. then the input acceleration is formatted and the corresponding Fortran format codes, FORMAT1 and FORMAT2, must be input. Logical variable.
- ECHO       A logical Flag. If ECHO=.TRUE. then the input acceleration is printed. Logical variable.



- REWIND A logical Flag. If REWIND = .TRUE. then the acceleration input file is rewound before it is read. This allows the same acceleration input file to be read more than once. IF IN=5 then set REWIND = .FALSE.. Logical variable.
- FORMAT1 Fortran format code capable of reading the two 80-character titles. (Character variable, do not enclose in single quotes)
- FORMAT2 Fortran format code capable of reading the input ground accelerations. (Character variable, do not enclose in single quotes)
- ATITLE1 Ground acceleration title. Read from unit IN. (Character variable, do not enclose in single quotes)
- ATITLE2 Ground acceleration title. Read from unit IN. (Character variable, do not enclose in single quotes)
- A() Input ground acceleration. If FMT = .FALSE., A() must be separated by blank spaces or commas. Otherwise, A( ) is input by the fixed format code FORMAT2. Read from unit IN. (g's)

Example:

2 1.0 0.0 0.01 .FALSE.	(1)
1 0 0 0 1 0	(2)
5 5 1 .TRUE. .FALSE.	(3)
(A/A)	(4)
(8F9.6)	(5)
ELCENTRO- 1940 EQ DATA FORMAT: (8F9.6)	(6)
DT=0.01 SEC + + + E-W DIRECTION + + +	(6)
-0.011848-0.008267-0.004687-0.002477-0.004856	(7)
5 5 2 .FALSE. .FALSE.	(8)
ELCENTRO- 1940 EQ DATA	(9)
DT=0.01 SEC + + + N-S DIRECTION + + +	(9)
0.010966 0.008610	(10)
0.006255	(10)
0.003900 .001545	(10)

- (1) Two ground motions are to be input.
- (2) Vectors defining the X' and Y' axes are input.
- (3) Input the first ground motion in fixed format from unit 5.

- (4) Format code for titles.
- (5) Format code for acceleration data.
- (6) Titles.
- (7) Acceleration data.
- (8) Input the second ground motion in free format from unit 5.
- (9) Titles.
- (10) Acceleration data.

**D. SOL03 - EIGENVALUE SOLUTION**

The following solution is used to calculate the elastic natural frequency and mode shape or the buckling load and mode shape. The following cards are input once.

'SOL03'
TITLE
OPTION IPRINT IPJT

**SOL03** Signifies solution #3. Character variable, enclose in single quotes.

**TITLE** User input title, 80 characters maximum. Character variable, enclose in single quotes.

**OPTION** Choice of natural frequency or buckling load. Character variable, enclose in single quotes.

'FREQ' Solves for the natural frequency and mode shapes of the structure.

'BUCK' Solves for the buckling load and mode shapes of the structure.

**IPRINT** Number of modes to be printed.

**IPJT** Number of modes to be printed with detailed mode shape.

## E. SOL04 - INCREMENTAL STATIC SOLUTION

The following solution is used to calculate the static cyclic response of nonlinear structures. The following cards are input once.

'SOL04'
TITLE
MAXELD IPRINT IWRITE UNBAL

SOL04 Signifies solution #4. Character variable, enclose in single quotes.

TITLE User input title, 80 characters maximum. Character variable, enclose in single quotes.

MAXELD Maximum number of element loads.

IPRINT Step increment for printed output.

IWRITE Step increment for data written to output files.

UNBAL A logical flag. If UNBAL=.TRUE., the unbalanced loads from the preceding step is added to the current load. Logical variable.

Note: The load case for this solution is always input as one.

1. Output Data to Disk Files. These cards control the data that is written to separate disk files. This data is used to print reports, or plot data. These cards are identical to the 'Output Data to Disk File' cards in block SOL02. Refer to SOL02 for a detailed description. The cards are repeated until the value of TYPE is 'END'.

TYPE NUMB IUNIT IGEN ΔNUMB ΔIUNIT
-----------------------------------

2. Joint Loads. These cards are used to apply loads to joints. These cards are identical to the 'Joint Load' cards in block SOL01. Refer to SOL01 for a detailed description. The following card is repeated until the value of DIR is 'END'.

LOAD ID IGEN ΔID DIR VALUE
----------------------------

3. Element Loads. These cards are used to apply element loads to the '3D-BEAM' element. These cards are identical to the 'Element Load' cards in block SOL01. Refer to SOL01 for a detailed description. The following card is only included if MAXELD > 0. The card is repeated MAXELD times, or until the value of TYPE is 'END'.

LOAD IELE IGEN ΔIELE TYPE DIR VALUE1, VALUE2, ...
---------------------------------------------------

4. Load Factors. These cards contain the load factors that are used to generate incremental static loads. Two options are available to limit the size of the load step: 1) the results of each step are scaled such that joint loads and displacements on free dof are less than PMAX and DMAX, and the step is repeated until the value of FACTOR is achieved (loading option A), or 2) each load step is subdivided into N steps (loading option B). The card is repeated until the value of STEP is 'END'.

STEP FACTOR PMAX DMAX N
-------------------------

STEP User input step name, 80 characters maximum. Character variable, enclose in single quotes. If STEP is 'END', the current solution is terminated.

FACTOR Load factor. The applied load at the end of the step is FACTOR \* (applied joint and element loads).

- PMAX Maximum value for a free dof joint load, per load step. (force or force\*length)
- DMAX Maximum value for a free dof joint displacement, per load step. (length or radians)
- N Number of load steps between the previous and current factor. N is only used if both PMAX and DMAX are equal to zero.

Example:

Note

'LOAD'	10.0	25.	.25	0	(1)
'UNLOAD'	0.0	0.	.0	20	(2)
'END'	0	0.	.0	0	(3)

- (1) The structure is loaded to 10 times the joint and element loads. in steps that do not have load increments greater than 25, or displacement increments greater than 0.25.
- (2) The structure is then unloaded with 20 equal size load steps.
- (3) SOLN04 is terminated.

F. BUG - SET BUG OPTIONS

This card is used to set the bug options, which print out the intermediate results listed below. The entire statement is a character variable, and is enclosed in single quotes.

```
'BUG = options'
```

Option Description

- A Print element displacements.  
Print loads applied to degrees of freedom
- B Not used.

- C Print plot data for program SEE to unit 07. SEE is a program that plots the structure on the UMR CALCOMP plotter. A listing of program SEE is given in Appendix C.
- D Print joint, element, and dynamic loading data.
- E Print numerical integration data for linear and average acceleration methods.
- F Print the element's structural and geometric stiffness.  
Print the global mass, structural stiffness, geometric stiffness, loads and displacements.
- G Print the condensed global mass, structural stiffness and geometric stiffness matrices.
- H Print the element transformations, structural and geometric stiffness, etc.
- I Print contents of memory for elements.
- J Print a skyline map for matrices.
- K Print the material data for each load step.
- L Print the energy balance.
- M Print the skyline data for matrices.
- N Print the contents of memory when DUMP is called.

Notes:

- 1) Any number of options may be specified at one time.
- 2) Options specified with the last bug statement are the only options active.

G. READ - READ OUTPUT FILES

This card is used to read and print data written to output files during SOL02 and SOL04. The entire statement is a character variable, and is enclosed in single quotes.

'READ INC=I UNIT=NO'

Where NO is the unit number of the file that contains the data, and I is the increment of the steps printed out. Multiple UNIT=NO statements may exist on each read card.

#### H. NOECHO - INHIBIT INPUT ECHO

This card is used to inhibit the input echo. Character variable, enclose in single quotes.

'NOECHO'

#### I. DUMP - PRINT MEMORY

This card is used to print the addresses of the data in memory. If 'BUG = N' was previously specified, 'DUMP' also prints the nonzero values in the linear array. Character variable, enclose in single quotes.

'DUMP'

#### J. RELEASE - RELEASE MEMORY

This card is used to release or 'free up' memory used for previous solutions. Global displacements, velocities etc. are reset to zero. The entire statement is a character variable, and is enclosed in single quotes.

'RELEASE OPTION'

If OPTION = 'ELEMENT', the element forces, displacements and hysteresis models are also reset to their initial values.

<u>Example:</u>	<u>Note</u>
'STRUCT'	(1)
. Structure input is omitted.	
'SOL01'	(2)
. Solution input is omitted.	
'RELEASE'	(3)
'SOL03'	(4)
. Solution input is omitted.	
'STOP'	(5)

- (1) The structure is defined.
- (2) A static solution is performed.
- (3) The static solution is released. The memory required for load, displacement, stiffness, etc. is released. The element forces are not released because the ELEMENT statement was omitted from the RELEASE card.
- (4) Natural frequencies or buckling loads are determined. For a buckling load solution, the geometric stiffness may be based on the axial load in the elements from SOL01. Releasing the memory after the static solution allows the same memory to be used for SOL03. If the memory had not been released, then the total memory required would be the sum of the memory required for SOL01 and SOL03.
- (5) Terminate the program.

#### K. STOP - TERMINATE EXECUTION



This card is used to terminate execution of the program. The statement is a character variable, and is enclosed in single quotes.

'STOP'

## V. RUNNING PROGRAM INRESB-3D-SUP

This chapter contains the instructions for running program INRESB-3D-SUP in the VM/SP CMS environment on an IBM 4381 computer. The instructions consist of several steps. First a macro library is generated that contains the common blocks. Second, the main program and of the each subroutines are compiled. The text files are stored on a disk in the users account. Third, the program is executed. The first and second steps are only done once to install the program.

### A. GENERATING THE COMMON BLOCK MACRO LIBRARY

The common block macro library, GEM, is generated with the following CMS statements:

```
MACLIB GEN ZCOMN GEM  
MACLIB ADD ZCOMN1 GEM  
MACLIB ADD ZCOMN2 GEM  
MACLIB ADD ZCOMN3 GEM
```

where ZCOMN COPY, ZCOMN1 COPY, ZCOMN2 COPY and ZCOMN3 COPY are four CMS files that contain the common blocks. These files are listed with the program.

### B. COMPILING THE PROGRAM

The program and subroutines are compiled with the following CMS commands:

```
GLOBAL MACLIB GEM  
FORTVS2 INRESB (OPT(2) AUTODBL(DBLPAD4)
```

The GLOBAL MACLIB GEM statement lets the compiler know where to locate the common blocks. The common blocks are put into the program by the Fortran INCLUDE statement, which is in the source code.

The compiler option OPT(2) specifies code optimization to reduce execution time. Vectorization may also be used to reduce execution time if the hardware and software are available.

The accuracy of computers differs according to their word length. Hence the program is written in single precision, and compiler options are used to convert the program to double precision when required. The IBM compiler option AUTODBL(DBLPAD4) automatically converts the program to double precision. The program has integer and real variables that share the same storage location. Thus the compiler option that is used to convert the program to double precision must pad the length of the integer variables, such that integer variables and real variables have the same length. Failure to use the DBLPAD4 compiler option an equivalent compiler option on other systems will lead to unpredictable results.

### C. RUNNING THE PROGRAM

The program is run in the local CMS environment by the following commands:

```
GLOBAL TXTLIB VSF2LINK VSF2FORT CMSLIB IMSLDOUB UFORTLIB
FILEDEF 5 DISK FN FT05 A ( PERM LRECL 80 RECFM F
FILEDEF 6 DISK FN FT06 A ( PERM LRECL 132 RECFM F
FILEDEF 10 DISK FN FT10 A ( PERM LRECL 80 RECFM F
FILEDEF 11 DISK FN FT11 A ( PERM LRECL 80 RECFM F

.

FILEDEF 92 DISK ELCENTRO EW A
FILEDEF 93 DISK ELCENTRO NS A
LOAD INRESB ( CLEAR RESET MAIN START NOMAP
```

The GLOBAL TXTLIB command loads the Fortran libraries needed to run the program. The IMSL library is required to link IMSL subroutine EIGZS. The UFORTLIB library contains the local routines CPUTIM, TIMEON, TIMEIT, TIME and DATE. The input is contained in a files FN FT05 A, ELCENTRO EW A and

ELCENTRO NS A. The output is written to file FN FT06 A and the data files FN FT10 A, FN FT11 A, etc.

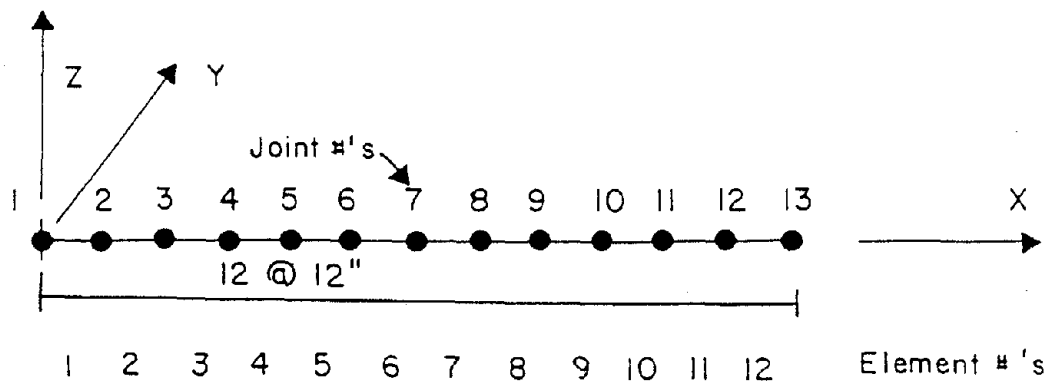
## VI. EXAMPLE PROBLEMS

### A. CANTILEVER BEAM

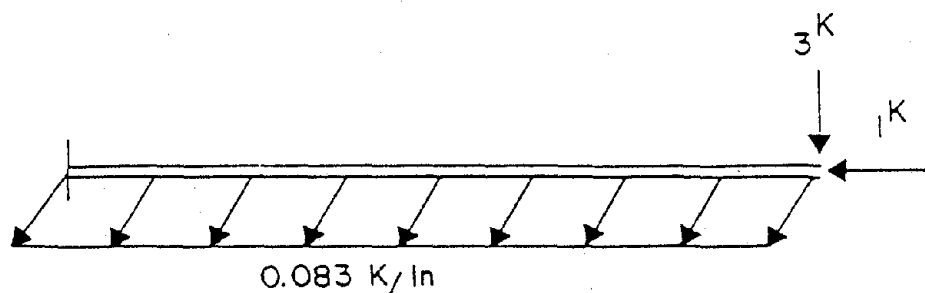
1. Description of Input Information. Thirteen joints and twelve beam segments are used to define the cantilever beam as shown in Figure 22(a). Each joint has a lumped mass of  $1.0 \text{ kip} - \text{sec}^2/\text{in}$ . Joint loads of -3 kips and -1 kip are applied at the end of the cantilever in the global Z and X directions, respectively. A uniform load of .08333 k/in is applied to the cantilever in the global Y direction as shown in Figure 22(b). The internal forces are shown for element 1 in figure 22(c).

The natural frequency is determined for the second solution. Note that the masses are defined at all 13 joints, and only joints 4, 7, 10 and 13 have lateral dof. The dof at joints 2, 3, 5, 6, 8, 9, 11 and 12 are condensed out and the dof at joint 1 are restrained. Thus the masses are condensed with the structural stiffness.

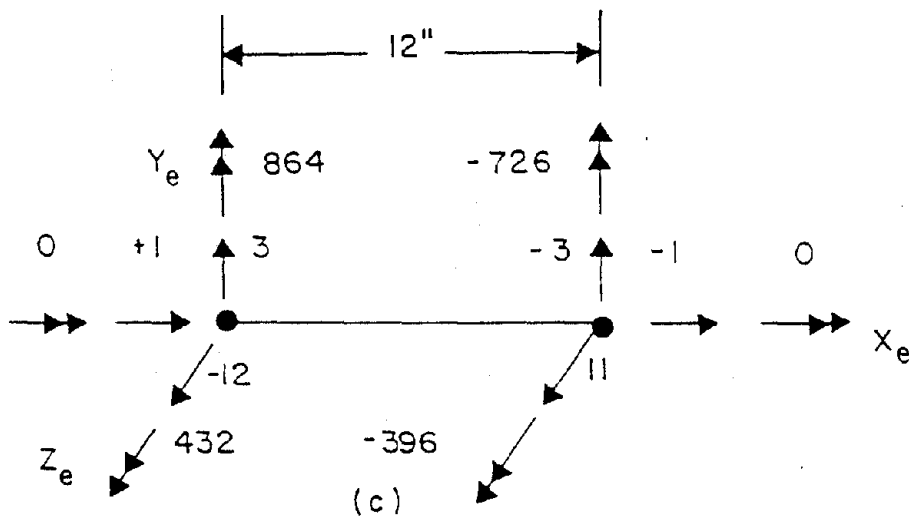
The elastic buckling load is determined for the third solution. The axial element forces from the first solution are used to generate the geometric stiffness. Similar to the second solution, the geometric stiffness is condensed out with the structural stiffness.



(a)



(b)



(c)

Figure 22. Cantilever Beam: (a) Joints, Elements, and Dof, (b) Applied loadings, (c) Member Forces for Element 1

## 2. Input Data.

```

ECHO OF INPUT DATA
LINE .....10.....20.....30.....40.....50.....60.....70.....80
1: 'STRUCTURE DEFINITION'
2: 'EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...'
3: 15 1 1 5 0 12.00
4: 1 0.00 0.00 0.00 1 12
5: 1 1.00 0.00 0.00
6: 1 0 0 0 1 0
7: 1 1 1 1 1 1 0 0
8: 0 1 0 0 1 1 1 0 0
9: 2 1 1 1 0 0 0 1 1
10: 5 1 1 1 0 0 0 1 1
11: 8 1 1 1 0 0 0 1 1
12: 11 1 1 1 0 0 0 1 1
13: 1
14: 'SD-BEAM' 'H12X40' '29000 11600 11.8 0 0 0.95 44.1 310.
15: 2 2 2 .TRUE.
16: 12
17: 'SD-BEAM' 'MEMBER 1' 1 1 2 0 0 1 0 0 0 000000 11
18: 0 1 1 0 0 0 0 0 0 000000 0
19: 4 1 .TRUE.
20: 1 .5 .5 .5 0. 0. 0. 0 0 0 0 0 0
21: 2 1 .1 .1 0. 0. 0. 0 0 0 0 10 1
22: 15 .5 .5 .5 0. 0. 0. 0 0 0 0 0 0
23: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
24: 0 0
25: 'SOL01 SOLUTION'
26: 'STATIC LOADINGS'
27: 1 1
28: 1 15 0 0 'FX' -1.0
29: 1 15 0 0 'FZ' -5.0
30: 0 0 0 0 'END' 0
31: 1 1 1 1 1 'UNIF' 'FZ' 0.085555555
32: 'SOL05 - SOLUTION'
33: 'FREQUENCY ANALYSIS'
34: 'FREQ' 4 0
35: 'SOL05 - SOLUTION'
36: 'STABILITY ANALYSIS'
37: 'BUCK' 4 0
38: 'STOP'
  
```

## 3. Output.

```

STRUCTURE.....: EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...
SOLUTION.....:
TIME: 14:59:52, DATE: 06/07/89

*** PROGRAM FEM ***          DOUBLE PRECISION VERSION
  
```

```

NODE COORDINATES AND DEGREES OF FREEDOM
TOTAL NUMBER OF DEGREES OF FREEDOM..... 78
NUMBER OF DEGREES OF FREEDOM CONDENSED OUT..... 64
NUMBER OF FREE DEGREES OF FREEDOM..... 14
NUMBER OF RESTRAINED DEGREES OF FREEDOM..... 6

   NODE  COSM   X-COORD   Y-COORD   Z-COORD   FX   FY   FZ   MX   MY   MZ
   ----  ----  -
1  1  0.0000E+00  0.0000E+00  0.0000E+00  75-R  74-R  75-R  76-R  77-R  78-R
2  1  12.0000  0.0000E+00  0.0000E+00  1  2  5  4  5  6
3  1  24.0000  0.0000E+00  0.0000E+00  7  8  9  10  11  12
4  1  36.0000  0.0000E+00  0.0000E+00  15  65  66  14  15  16
5  1  48.0000  0.0000E+00  0.0000E+00  17  18  19  20  21  22
6  1  60.0000  0.0000E+00  0.0000E+00  25  24  25  26  27  28
7  1  72.0000  0.0000E+00  0.0000E+00  29  67  68  30  31  32
8  1  84.0000  0.0000E+00  0.0000E+00  33  54  35  36  37  38
9  1  96.0000  0.0000E+00  0.0000E+00  39  40  41  42  43  44
10 1 108.00  0.0000E+00  0.0000E+00  45  69  70  46  47  48
11 1 120.00  0.0000E+00  0.0000E+00  49  50  51  52  53  54
12 1 132.00  0.0000E+00  0.0000E+00  55  56  57  58  59  60
15 1 144.00  0.0000E+00  0.0000E+00  61  71  72  62  63  64

NOTE: R - RESTRAINED DEGREE OF FREEDOM
      C - CONSTRAINED DEGREE OF FREEDOM
  
```

```

DIRECTION COSINES ...
COSK 1) VX: 1.0000 I +0.0000 J +0.0000 K  VY: 0.0000 I +1.0000 J +0.0000 K  VZ: 0.0000 I +0.0000 J +1.0000 K
  
```

```

STRUCTURE.....: EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...
SOLUTION.....:
TIME: 14:59:52, DATE: 06/07/89
  
```

```

S=0 ELASTIC BEAM ELEMENT
=====
MATEL.  E  GAMMA  AX  AY  AZ  IX  IY  IZ
1  2.900E+04  1.160E+04  11.8  0.000E+00  0.000E+00  0.950  44.1  310.
  
```

```

STRUCTURE.....: EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...
SOLUTION.....:
TIME: 14:59:52, DATE: 06/07/89
  
```

```

GEOMETRIC STIFFNESS DATA
=====
KGLLOAD = 2, PREVIOUS LOAD STEP'S AXIAL LOAD IS USED
KGTTYPE = 2, CONSISTENT FORMULATION
KGFFORM = 2, SEPARATE GLOBAL KG IS FORMED

- THE GEOMETRIC STIFFNESS MATRIX IS CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.
  
```

STRUCTURE..... EXAMPLE #1. 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...  
 SOLUTION.....

TIME: 14:39:52, DATE: 06/07/89



ELEMENT DB, 3D BEAM ELEMENT

MEMBER	#	MATL	START	END	REL CD	LENGTH	V-AXIS			START DIST	END DIST	PKG			
1	1	1	1	2		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	2	1	2	3		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	3	1	3	4		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	4	1	4	5		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	5	1	5	6		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	6	1	6	7		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	7	1	7	8		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	8	1	8	9		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	9	1	9	10		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	10	1	10	11		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	11	1	11	12		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00
GENERATED	12	1	12	13		12.00	0.00000	I	+0.00000	J	+1.00000	K	0.0000E+00	0.0000E+00	0.0000E+00

STRUCTURE..... EXAMPLE #1. 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...  
 SOLUTION.....

TIME: 14:39:52, DATE: 06/07/89

LUMPED NODE MASSES

NODE	MX	MY	MZ	RX	RY	RZ	IX	IY	IZ	IGEN	INC
1	0.5000	0.5000	0.5000	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0
2	1.0000	1.0000	1.0000	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	10	1
13	0.5000	0.5000	0.5000	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0

- THE MASS MATRIX IS CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.

PROPORTIONAL DAMPING COEFFICIENTS

ALPHA= 0.00000E+00 BETA= 0.00000E+00

MEMORY UTILIZATION	
IZ=	7465. MEM= 1.495%
ELAPSED CPU TIME 0.41 SEC	
TOTAL CPU TIME 0.41 SEC	

STRUCTURE..... EXAMPLE #1. 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...  
 SOLUTION..... STATIC LOADINGS

TIME: 14:39:52, DATE: 06/07/89  
 TIME: 14:39:52, DATE: 06/07/89

SOLUTION #1. STATIC - ELASTIC ANALYSIS

NUMBER OF LOAD CASES ..... 1  
 GEOMETRIC STIFFNESS IS NOT INCLUDED. USE KGFOR=1 TO INCLUDE GEOMETRIC STIFFNESS.  
 APPLIED JOINT LOADS

LOAD CASE:	1	JOINT:	13	DIRECTION:	FY	DOF(S)	61	MAGNITUDE:	-1.00000
LOAD CASE:	1	JOINT:	13	DIRECTION:	FZ	DOF(S)	72	MAGNITUDE:	-5.00000

ELEMENT LOADS

LOAD IELE	IGEN	IELE	TYPE	DIR	VALUES....	
1	1	11	1	UNDF	FZ	B.533555E-02

STRUCTURE..... EXAMPLE #1. 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...  
 SOLUTION..... STATIC LOADINGS

TIME: 14:39:52, DATE: 06/07/89  
 TIME: 14:39:52, DATE: 06/07/89

GCS DISPLACEMENTS, LOADING # 1

NODE	DX	DY	DZ	RX	RY	RZ
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
2	-5.506721E-05	-5.599578E-02	-5.563757E-05	0.000000E+00	5.526140E-04	-7.450152E-05
5	-7.015442E-05	-0.175849	-1.507052E-02	0.000000E+00	1.057175E-05	-1.566176E-02
4	-1.052016E-04	-0.369574	-2.854572E-02	0.000000E+00	1.515682E-05	-1.874756E-02
5	-1.402688E-04	-0.619733	-4.926676E-02	0.000000E+00	1.922156E-05	-2.281196E-02
6	-1.755361E-04	-0.913441	-7.448276E-02	0.000000E+00	2.282556E-05	-2.594109E-02
7	-2.104053E-04	-1.24057	-0.105795	0.000000E+00	2.594883E-05	-2.857458E-02
8	-2.454705E-04	-1.59172	-0.156568	0.000000E+00	2.859177E-05	-3.008210E-02
9	-2.805577E-04	-1.96008	-0.172225	0.000000E+00	3.075417E-05	-3.122685E-02
10	-3.156049E-04	-2.35957	-0.210186	0.000000E+00	3.245604E-05	-3.192118E-02
11	-3.506721E-04	-2.72484	-0.249878	0.000000E+00	3.363757E-05	-3.227774E-02
12	-3.857395E-04	-3.11313	-0.290723	0.000000E+00	3.435818E-05	-3.240910E-02
13	-4.208065E-04	-3.50221	-0.332145	0.000000E+00	3.459844E-05	-3.242787E-02

STRUCTURE..... EXAMPLE #1. 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF...  
 SOLUTION..... STATIC LOADINGS

TIME: 14:39:52, DATE: 06/07/89  
 TIME: 14:39:52, DATE: 06/07/89

GCS RESTRAINT REACTIONS, LOADING # 1

NODE	FX	FY	FZ	MX	MY	MZ
1	1.000000	12.00000	3.000000	0.000000E+00	-452.0000	864.0000
SUMMATION	1.000000	12.00000	3.000000	0.000000E+00	-452.0000	864.0000



STRUCTURE..... EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF... TIME: 14:59:52, DATE: 06/07/89  
 SOLUTION..... STATIC LOADINGS TIME: 14:59:52, DATE: 06/07/89

SD BEAM FORCES...								
ELEMENT	LOAD	NODE	AXIAL	FV	FZ	TORSION	MV	MZ
1	FORCE	1	1.00000	3.00000	-12.0000	0.00000E+00	864.000	432.000
	FORCE	2	-1.00000	-5.00000	11.0000	0.00000E+00	-726.000	-396.000
2	FORCE	2	1.00000	5.00000	-11.0000	0.00000E+00	726.000	396.000
	FORCE	3	-1.00000	-5.00000	10.0000	0.00000E+00	-600.000	-560.000
3	FORCE	3	1.00000	5.00000	-10.0000	0.00000E+00	600.000	560.000
	FORCE	4	-1.00000	-5.00000	9.00000	0.00000E+00	-486.000	-524.000
4	FORCE	4	1.00000	5.00000	-9.00000	0.00000E+00	486.000	524.000
	FORCE	5	-1.00000	-5.00000	8.00000	0.00000E+00	-584.000	-288.000
5	FORCE	5	1.00000	5.00000	-8.00000	0.00000E+00	584.000	288.000
	FORCE	6	-1.00000	-5.00000	7.00000	0.00000E+00	-294.000	-252.000
6	FORCE	6	1.00000	5.00000	-7.00000	0.00000E+00	294.000	252.000
	FORCE	7	-1.00000	-5.00000	6.00000	0.00000E+00	-216.000	-216.000
7	FORCE	7	1.00000	5.00000	-6.00000	0.00000E+00	216.000	216.000
	FORCE	8	-1.00000	-5.00000	5.00000	0.00000E+00	-150.000	-180.000
8	FORCE	8	1.00000	5.00000	-5.00000	0.00000E+00	150.000	180.000
	FORCE	9	-1.00000	-5.00000	4.00000	0.00000E+00	-96.0000	-144.000
9	FORCE	9	1.00000	5.00000	-4.00000	0.00000E+00	96.0000	144.000
	FORCE	10	-1.00000	-5.00000	3.00000	0.00000E+00	-54.0000	-108.000
10	FORCE	10	1.00000	5.00000	-3.00000	0.00000E+00	54.0000	108.000
	FORCE	11	-1.00000	-5.00000	2.00000	0.00000E+00	-24.0000	-72.0000
11	FORCE	11	1.00000	5.00000	-2.00000	0.00000E+00	24.0000	72.0000
	FORCE	12	-1.00000	-5.00000	1.00000	0.00000E+00	-8.00000	-56.0000
12	FORCE	12	1.00000	5.00000	-1.00000	0.00000E+00	6.00000	36.0000
	FORCE	15	-1.00000	-5.00000	1.746298E-12	0.00000E+00	1.95224E-11	1.09159E-11

```

-----*
*--- MEMORY UTILIZATION -----*
*--- IZ= 7870, MEM= 1.574% ---*
*-----*
*--- ELAPSED CPU TIME 0.15 SEC ---*
*--- TOTAL CPU TIME 0.53 SEC ---*
-----*

```

STRUCTURE..... EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF... TIME: 14:59:52, DATE: 06/07/89  
 SOLUTION..... FREQUENCY ANALYSIS TIME: 14:59:53, DATE: 06/07/89

SOLUTION #5, DETERMINE EIGENVALUES AND EIGENVECTORS

```

=====
OPTION:.....NATURAL FREQUENCIES
NUMBER OF EIGENVALUES:..... 4
PERFORMANCE INDEX: 0.290678468488079483
MODE:      1      2      3      4
FREQ (RAD/SEC): 0.66219      1.7557      4.1268      10.941
FREQUENCY (HZ): 0.10539      0.27942      0.65680      1.7414
PERIOD (SEC): 9.4685      3.5788      1.5225      0.57426
EIGENVECTORS:
DOF( 65) 9.71210E-02 2.50500E-15 -0.41885 1.76607E-15
DOF( 66) -1.49621E-15 9.71210E-02 5.15534E-16 -0.41885
DOF( 67) 0.53911 7.26854E-15 -0.72162 2.68976E-16
DOF( 68) -5.50069E-15 0.53911 7.41779E-16 -0.72162
DOF( 69) 0.65732 1.09734E-14 -0.14744 -1.67126E-15
DOF( 70) -1.03996E-14 0.65732 1.78485E-15 -0.14744
DOF( 71) 1.0000 1.23337E-14 1.0000 1.94012E-15
DOF( 72) -1.53597E-14 1.0000 5.16971E-15 1.0000

```

```

-----*
*--- MEMORY UTILIZATION -----*
*--- IZ= 8092, MEM= 1.618% ---*
*-----*
*--- ELAPSED CPU TIME 0.16 SEC ---*
*--- TOTAL CPU TIME 0.69 SEC ---*
-----*

```

STRUCTURE..... EXAMPLE #1, 12 ELEMENT BEAM VIBRATION AND BUCKLING LOAD, 4 DOF... TIME: 14:59:52, DATE: 06/07/89  
 SOLUTION..... STABILITY ANALYSIS TIME: 14:59:53, DATE: 06/07/89

SOLUTION #5, DETERMINE EIGENVALUES AND EIGENVECTORS

```

=====
OPTION:.....ELASTIC BUCKLING LOAD
NUMBER OF EIGENVALUES:..... 4
PERFORMANCE INDEX: 0.269008294972055390
MODE:      1      2      3      4
EIGENVALUE: 152.18      1069.8      1574.4      5950.6
EIGENVECTORS:
DOF( 65) 7.61205E-02 -3.32096E-16 0.52087 0.80996
DOF( 66) -8.51674E-17 7.61205E-02 2.60076E-16 -5.95682E-17
DOF( 67) 0.29289 -8.64958E-16 0.88733 1.0000
DOF( 68) -1.86999E-17 0.29289 9.45507E-16 -9.47499E-17
DOF( 69) 0.61732 -8.54068E-16 1.0000 6.45903E-02
DOF( 70) -1.49916E-16 0.61732 1.80181E-15 -1.19718E-16
DOF( 71) 1.0000 -1.56099E-16 0.51978 0.58579
DOF( 72) -5.96887E-16 1.0000 2.87797E-15 -9.17196E-17

```

```

-----*
*--- MEMORY UTILIZATION -----*
*--- IZ= 8514, MEM= 1.665% ---*
*-----*
*--- ELAPSED CPU TIME 0.17 SEC ---*
*--- TOTAL CPU TIME 0.86 SEC ---*
-----*

```

Notes:

(1) Vector in the beam's local XY-plane,  $\vec{V} = V1i + V2j + V3k$

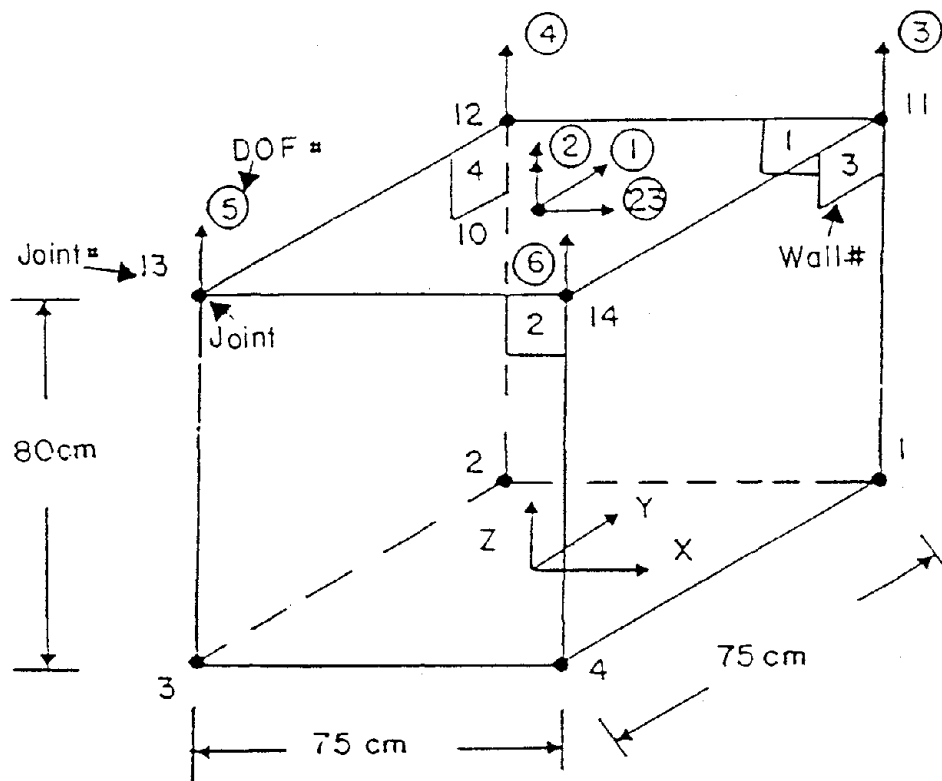
(2) IMSL performance index for routine EIGZS. When  $PI < 1$ , the performance of the eigensolution is excellent, and when  $PI > 100$ , the performance of the eigensolution is poor.

B. ONE STORY R/C BOX TYPE BUILDING

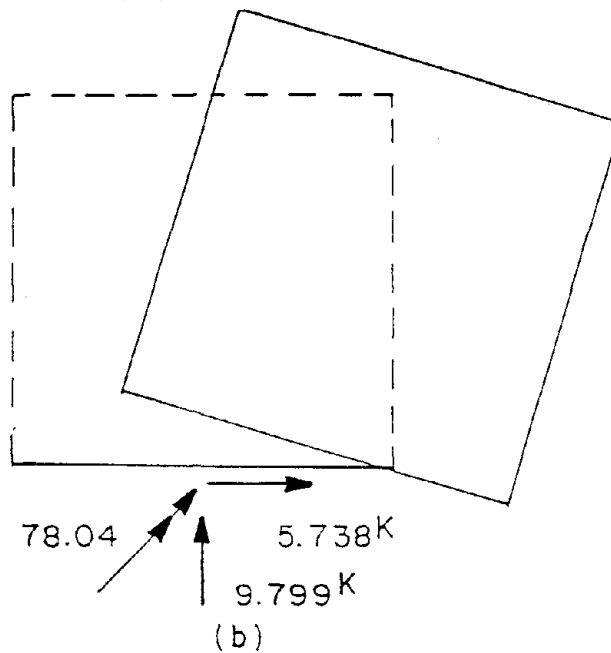
1. Description of Input Information.

The one story R/C box type building consists of four shear walls and a rigid roof diaphragm as shown in Figure 23. Nine joints are used to define the three dimensional structural model. At the base, joints 1 through 4 define the corners of the box. Joints 11 through 14 define the corners of the box at the roof. Joint 10 is at the mass center of the roof. The JCS for all of the joints is parallel to the GCS. The three dimensional structural model consists of four shear wall elements, numbered 1 through 4. The wall's center line dimensions are used for the structural model, thus each of the shear wall elements is 75 cm wide, and 80 cm tall. P- $\Delta$  effects are neglected.

Each joint has 6 degrees of freedom. At the base of the box, joints 1 through 4, all six degrees of freedom are restrained. The slab at the top of the box is assumed to be a rigid diaphragm. A planar constraint is used to transfer the translations in the X and Y axes and the rotation about the Z axis from joints 11 through 14, at the corners of the box, to joint 10, at the mass center. The planar constraint at the roof reduces the number of degrees of freedom at joints 11 through 14, leaving rotational dof about the X and Y axes which are restrained and translational dof in the Z axis which is free to displace. None of the elements are connected to joint 10. Thus joint 10 does not have any stiffness until joints 11 through 14 are constrained to it. As a 'master' joint,



(a)



(b)

Figure 23. One Story R/C Box Type Building: (a) Building, (b) Forces and Deformation of Wall #1 at Load Step 50

joint 10 has translational stiffness in the X and Y axes, and rotational stiffness about the Z axis. Loading consist of the imposed displacement of joint 10 in the X direction. Thus the X translational dof of joint 10 is restrained. The Z translational dof and the rotations about the X and Y axes are also restrained, because these dof do not have any stiffness. The Y translational dof and the Z rotational dof of joint 10, are free to displace. The dof are numbered in accordance with the global degree of freedom (Gdof) numbering scheme (17), as shown in Table I. All of the rotations about the X and Y axes are restrained with a restraint flag of 2.

## 2. Input Data.

```

ECHO OF INPUT DATA
LINE .....10.....20.....30.....40.....50.....60.....70.....80
1:  *STRUCTURE DEFINITION*
2:  *UNIV. OF TOKYO BOX B6 3-D MODEL, 4/6/89 *
3:  9 1 5 0 1 1.
4:  1 57.5 57.5 0. 1 0
5:  2 -57.5 57.5 0. 1 0
6:  3 -57.5 -57.5 0. 1 0
7:  4 57.5 -57.5 0. 1 0
8:  10 0 0 80. 1 0
9:  11 57.5 57.5 80. 1 0
10: 12 -57.5 57.5 80. 1 0
11: 13 -57.5 -57.5 80. 1 0
12: 14 57.5 -57.5 80. 1 0
13: 1 0 0 0 1 0
14: 0 0 0 0 2 2 0 0
15: 1 1 1 1 1 1 1 5 1
16: 10 1 0 1 2 2 0 0 0
17: 1 10 11 3 1
18: 5
19: *ANLMOD * 172800 155520 172.8 14.06 .40 .2 15 .2
20: *BEND1 B01* 9 10 5.075819E-5 .2
21: 80.0000 100.0000 160.0000 280.0000 360.0000
22: 391.0000 420.0000 440.0000 460.0000
23: 1.409580E-06 2.297770E-06 5.720770E-06 1.592260E-05 2.401540E-05
24: 5.073319E-05 5.967050E-05 4.950700E-05 5.073318E-04
25: *SHEAR1 B01* 10 10 2.72587E-5 .2
26: -.00000 5.00000 8.00000 12.0000 16.0000
27: 19.0000 19.5500 21.0000 22.0000 22.1000
28: 1.245750E-04 1.958900E-04 4.987020E-04 1.020270E-05 1.705120E-05
29: 2.552620E-05 2.725875E-05 5.440410E-05 4.277610E-05 2.725875E-02
30: 0 0 0 .FALSE.
31: *
32: *SHEAR WALL* *NORTH* 2 3 1 11 12 2 1 1.00 0.0 0 0
33: *SHEAR WALL* *SOUTH* 2 3 1 14 15 3 4 1.00 0.0 0 0
34: *SHEAR WALL* *EAST* 2 3 1 11 14 4 1 1.00 0.0 0 0
35: *SHEAR WALL* *WEST* 2 3 1 12 15 5 2 1.00 0.0 0 0
36: 0 0 .FALSE.
37: 0 0
38: *SOLO4 *
39: *MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION *
40: 0 99999 1 .TRUE.
41: *ELE* 1 21 5 1 1
42: *JOINT FX* 10 31 0 0 0
43: *JOINT FY* 10 32 0 0 0
44: *JOINT FZ* 11 41 0 0 0
45: *JOINT F2* 12 42 0 0 0
46: *JOINT F2* 15 45 0 0 0
47: *JOINT F2* 14 44 0 0 0
48: *EMBRN* 00 37 0 0 0
49: *SUMRST * 00 38 0 0 0
50: *END* 0 0 0 0 0 0
51: 1 10 0 0 *FX* 0.1
52: 0 0 0 0 *END* 0.

```

Table I. DEGREES OF FREEDOM FOR UT BOX B6

Joint #	Condensed DOF			Free DOF			Restrained DOF *			Restrained DOF **									
	<u>TX</u>	<u>TY</u>	<u>TZ</u>	<u>RX</u>	<u>RY</u>	<u>RZ</u>	<u>TX</u>	<u>TY</u>	<u>TZ</u>	<u>RX</u>	<u>RY</u>	<u>RZ</u>	<u>TX</u>	<u>TY</u>	<u>TZ</u>	<u>RX</u>	<u>RY</u>	<u>RZ</u>	
1																			
2							7	8	9										25 26
3							11	12	13										27 28
4							15	16	17										29 30
10							19	20	21										31 32
11										2									33 34
12										2c									35 36
13										2c									37 38
14										2c									39 40
										2c									41 42

Notes:

- 1) TX, TY and TZ signify translation in the joints X, Y and Z axes respectively.
  - 2) RX, RY and RZ signify rotation about the joints X, Y and Z axes respectively.
  - 3) The constrained dof of 'slave' joints are represented by #c, where # is the dof number of the 'master' joint.
- \* Restraint flag = 1 on the joint restraint input card.  
 \*\* Restraint flag = 2 on the joint restraint input card.

ECHO OF INPUT DATA

```

LINE .....10.....20.....30.....40.....50.....60.....70.....80
55: *LOAD- 1* 0.01 0 .0 1
54: *LOAD- 1* 0.46 0 .0 4 6
55: *LOAD- 1* 0.4599 0 .0 2
56: *LOAD- 2* -0.46 0 .0 9 2
57: *LOAD- 2* -0.4599 0 .0 2
58: *LOAD- 3* 0.7000 0 .0 10 6
59: *LOAD- 3* 1.70 0 .0 2
60: *LOAD- 3* 1.6999 0 .0 2
61: *LOAD- 4* -0.8200 0 .0 35
62: *LOAD- 4* -1.82 0 .0 10 2
63: *LOAD- 4* -1.8199 0 .0 2
64: *LOAD- 5* 0.7000 0 .0 55
65: *LOAD- 5* 1.70 0 .0 10 2
66: *LOAD- 5* 1.6999 0 .0 2
67: *LOAD- 6* -0.5600 0 .0 32
68: *LOAD- 6* -1.56 0 .0 10 6
69: *LOAD- 6* -1.5599 0 .0 2
70: *LOAD- 7* 2.8000 0 .0 53
71: *LOAD- 7* 3.80 0 .0 10 6
72: *LOAD- 7* 3.7999 0 .0 2
73: *LOAD- 8* -5.0000 0 .0 78
74: *LOAD- 8* -4.00 0 .0 10 0
75: *LOAD- 8* -5.9999 0 .0 2
76: *LOAD- 9* 2.9000 0 .0 79
77: *LOAD- 9* 3.90 0 .0 10 0
78: *LOAD- 9* 3.8999 0 .0 2
79: *LOAD-10* -2.9000 0 .0 78
80: *LOAD-10* -3.90 0 .0 10 0
81: *LOAD-10* -5.8999 0 .0 2
82: *LOAD-11* 5.2200 0 .0 81
83: *LOAD-11* 4.22 0 .0 10 2
84: *LOAD-11* 4.2199 0 .0 2
85: *LOAD-12* -2.9000 0 .0 81
86: *LOAD-12* -5.90 0 .0 10 2
87: *LOAD-12* -5.8999 0 .0 2
88: *LOAD-13* .0000 0 .0 119
89: *LOAD-13* 7.0600 0 .0 119
90: *LOAD-15* 3.06 0 .0 10 6
91: *LOAD-15* 8.0599 0 .0 2
92: *LOAD-14* -7.1800 0 .0 162
93: *LOAD-14* -8.18 0 .0 10 4
94: *LOAD-14* -8.1799 0 .0 2
95: *LOAD-15* 7.0000 0 .0 161
96: *LOAD-15* 8.00 0 .0 10 8
97: *LOAD-15* 7.9999 0 .0 2
98: *LOAD-16* -7.1800 0 .0 161
99: *LOAD-16* -8.18 0 .0 10 8
100: *LOAD-16* -8.1799 0 .0 2
101: *LOAD-17* 14.6000 0 .0 537
102: *LOAD-17* 15.60 0 .0 10 8
103: *LOAD-17* 15.5999 0 .0 2
104: *LOAD-18* 9.7000 0 .0 50
105: *LOAD-18* 10.70 0 .0 10 0
106: *LOAD-18* 10.69999 0 .0 2
107: *LOAD-19* 19.4000 0 .0 97
108: *LOAD-19* 20.40 0 .0 10 0
109: *END* 0 0 0 0
110: *READ DIM=50 UNIT=21 UNIT=57 *
111: *STOP*

```

3. Output.

STRUCTURE.....UNIV. OF TOKYO BOX 86 3-D MODEL. 4/6/89  
SOLUTION.....

TIME: 16:59:04, DATE: 05/31/89

\*\*\* PROGRAM FEM \*\*\* DOUBLE PRECISION VERSION

NODE CONSTRAINTS

```

XV-PLANE CONSTRAINT, MASTER: 10 SLAVE: 11
XV-PLANE CONSTRAINT, MASTER: 10 SLAVE: 12
XV-PLANE CONSTRAINT, MASTER: 10 SLAVE: 13
XV-PLANE CONSTRAINT, MASTER: 10 SLAVE: 14

```

NODE COORDINATES AND DEGREES OF FREEDOM

```

TOTAL NUMBER OF DEGREES OF FREEDOM..... 42
NUMBER OF DEGREES OF FREEDOM CONDENSED OUT..... 0
NUMBER OF FREE DEGREES OF FREEDOM..... 6
NUMBER OF RESTRAINED DEGREES OF FREEDOM..... 56

```

NODE	CDS#	X-COORD	Y-COORD	Z-COORD	FX	FY	FZ	MX	MY	MZ
1	1	57.500	57.500	0.00000E+00	7-R	8-R	9-R	25-R	26-R	10-R
2	1	-57.500	57.500	0.00000E+00	11-R	12-R	15-R	27-R	28-R	14-R
5	1	-57.500	-57.500	0.00000E+00	15-R	16-R	17-R	29-R	30-R	18-R
4	1	57.500	-57.500	0.00000E+00	19-R	20-R	21-R	31-R	32-R	22-R
10	1	0.00000E+00	0.00000E+00	80.000	23-R	1	24-R	33-R	34-R	2
11	1	57.500	57.500	80.000	25-C	1-C	5	35-R	36-R	2-C
12	1	-57.500	57.500	80.000	25-C	1-C	4	37-R	38-R	2-C
13	1	-57.500	-57.500	80.000	25-C	1-C	5	39-R	40-R	2-C
14	1	57.500	-57.500	80.000	25-C	1-C	6	41-R	42-R	2-C

NOTE: R - RESTRAINED DEGREE OF FREEDOM  
C - CONSTRAINED DEGREE OF FREEDOM

DIRECTION COSINES ...

COSK 1) VK: 1.00000 I +0.00000 J +0.00000 K VV: 0.00000 I +1.00000 J +0.00000 K VZ: 0.00000 I +0.00000 J +1.00000 K

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION.....

TIME: 16:59:04, DATE: 05/31/89

AKLHOD HYSTERESIS MODEL - FOR UNIT LENGTH MEMBER

MAT.	SC	ST1	ST2	PV	ALPHA	BETA	MAX DUCT.	BETA-DI
1	172800.	155520.	172.800	14.0600	0.400000	0.200000	15.0000	0.200000

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION.....

TIME: 16:59:04, DATE: 05/31/89

BEND1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER

BACKBONE CURVE POINTS - MATL	NI	DV	BETA	MOMENT	ROTATION
2	10	0.307582E-04	0.200000	80.0000	0.140958E-05
				100.0000	0.229777E-05
				160.0000	0.572077E-05
				280.0000	0.139226E-04
				360.0000	0.290134E-04
				591.0000	0.307582E-04
				420.0000	0.596705E-04
				440.0000	0.495070E-04
				460.0000	0.307582E-05

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION.....

TIME: 16:59:04, DATE: 05/31/89

SHEAR1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER

BACKBONE CURVE POINTS - MATL	NI	DV	BETA	STRESS	STRAIN
5	10	0.272587E-02	0.200000	4.00000	0.124575E-05
				5.00000	0.195890E-05
				8.00000	0.498702E-05
				12.0000	0.102027E-02
				16.0000	0.170512E-02
				19.0000	0.253262E-02
				19.5500	0.272587E-02
				21.0000	0.344041E-02
				22.0000	0.427761E-02
				22.1000	0.272587E-01

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION.....

TIME: 16:59:04, DATE: 05/31/89

ELEMENT 05, R/C SHEAR WALL ELEMENT

	ELEM	BEND	SHEAR	AXIAL	JOINT	JOINT	JOINT	JOINT	LENGTH	WIDTH	ALPHA	PKG	
	#	MATL	MATL	MATL	#1	#2	#3	#4					
NORTH	1	2	5	5	1	11	12	2	1	80.00	75.00	1.000	0.0000E+00
SOUTH	2	2	5	5	1	14	15	5	4	80.00	75.00	1.000	0.0000E+00
EAST	3	2	5	5	1	11	14	4	1	80.00	75.00	1.000	0.0000E+00
WEST	4	2	5	5	1	12	15	5	2	80.00	75.00	1.000	0.0000E+00

ZERO MASS MATRIX

PROPORTIONAL DAMPING COEFFICIENTS

ALPHA= 0.00000E+00 BETA= 0.00000E+00

-----  
\*--- MEMORY UTILIZATION .....  
\*--- IZ= 2625, MEM= 0.525%  
\*---  
\*--- ELAPSED CPU TIME 0.20 SEC  
\*--- TOTAL CPU TIME 0.20 SEC  
-----

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION  
SOLUTION #9, STATIC NONLINEAR SOLUTION

TIME: 16:59:04, DATE: 05/31/89

TIME: 16:59:05, DATE: 05/31/89

INTERVAL FOR PRINTING DATA.....99999  
INTERVAL FOR WRITING DATA TO FILE..... 1

UNBALANCED JOINT FORCES ARE ADDED TO THE NEXT CYCLE

DATA WRITTEN TO FILES

-----  
ELEMENT # 1 IS WRITTEN TO UNIT # 21  
ELEMENT # 2 IS WRITTEN TO UNIT # 22  
ELEMENT # 3 IS WRITTEN TO UNIT # 23  
ELEMENT # 4 IS WRITTEN TO UNIT # 24  
DEGREE OF FREEDOM # 23 IS WRITTEN TO UNIT # 31 JOINT: 10 DIRECTION: FX  
DEGREE OF FREEDOM # 1 IS WRITTEN TO UNIT # 32 JOINT: 10 DIRECTION: FV  
DEGREE OF FREEDOM # 5 IS WRITTEN TO UNIT # 41 JOINT: 11 DIRECTION: FZ  
DEGREE OF FREEDOM # 4 IS WRITTEN TO UNIT # 42 JOINT: 12 DIRECTION: FZ  
DEGREE OF FREEDOM # 5 IS WRITTEN TO UNIT # 43 JOINT: 13 DIRECTION: FZ  
DEGREE OF FREEDOM # 6 IS WRITTEN TO UNIT # 44 JOINT: 14 DIRECTION: FZ  
ENERGY BALANCE IS WRITTEN TO UNIT # 57  
SUMMATION OF REACTIONS IS WRITTEN TO UNIT # 58  
APPLIED JOINT LOADS  
-----

LOAD CASE: 1 JOINT: 10 DIRECTION: FX DEF(S) 25

MAGNITUDE: 0.100000 ...JOINT DISPLACEMENT...

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89

TIME: 16:59:05, DATE: 05/31/89

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
TIME: 16:59:05, DATE: 05/31/89

LOADING # 0 MAXIMUM DISPLACEMENTS

GCS DISPLACEMENTS

NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

NODE	DX	DY	DZ	RX	RY	RZ
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
2	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
5	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
4	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
10	2.04000	2.224492E+16	0.000000E+00	0.000000E+00	0.000000E+00	-8.109588E-18
11	2.04000	-8.166050E-17	0.542589	0.000000E+00	0.000000E+00	-8.109588E-18
12	2.04000	5.265588E-16	1.60591	0.000000E+00	0.000000E+00	-8.109588E-18
13	2.04000	5.265588E-16	1.60591	0.000000E+00	0.000000E+00	-8.109588E-18
14	2.04000	-8.166050E-17	0.542589	0.000000E+00	0.000000E+00	-8.109588E-18

STRUCTURE..... UNIV. OF TOKYO BOX B6 3-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
TIME: 16:59:05, DATE: 05/31/89

LOADING # 0 MAXIMUM REACTIONS

MAXIMUM GCS RESTRAINT REACTIONS

NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

NODE	FX	FY	FZ	MX	MY	MZ
1	-21.34217	1.7242261E-14	22.76498	0.000000E+00	0.000000E+00	0.000000E+00
2	0.000000E+00	1.5276904E-14	-22.76498	0.000000E+00	0.000000E+00	0.000000E+00
5	0.000000E+00	0.000000E+00	-22.76498	0.000000E+00	0.000000E+00	0.000000E+00
4	-21.54217	0.000000E+00	22.76498	0.000000E+00	0.000000E+00	0.000000E+00
10	42.68454	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
11	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
12	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
13	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
14	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00

MAX OF ALL.....  
GCS SUMM. 0.5872458E-12 0.1449694E-15 0.1250051E-12 0.1875883E-11 -0.5029754E-10 0.5069645E-11

MAXIMUM RESULTANT OF REACTIONS, FORCE= 5.8734E-13 MOMENT= 5.0559E-11

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
TIME: 16:59:05, DATE: 05/31/89

LOADING # 0 PEAK ELEMENT FORCES

R/C	SHEAR	MOMENT	ROTATION	SHEAR	SHEAR DISPL.	AXIAL	AXIAL DISPL.				
1	2	11	12	2	1	457.261	2.177222E-02	21.5422	0.298222	15.7879	0.787452
2	2	14	15	5	4	457.261	2.177222E-02	21.5422	0.298222	15.7879	0.787452
5	2	11	14	4	1	2.102525E-12	2.965674E-18	-4.502961E-14	-1.072083E-16	-49.1242	-2.906605E-02
4	2	12	15	3	2	4.276459E-12	6.028264E-18	-4.765052E-14	-1.685513E-16	-49.4505	-2.067143E-02

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
TIME: 16:59:05, DATE: 05/31/89

LOADING # 0 PEAK DUCTILITIES AND EXCURSION RATIOS

ELEM#	BENDING COMPONENT					SHEAR COMPONENT					AXIAL COMPONENT							
	DEFN 1	DEFN 2	DEFN 3	DEFN 4	DEFN 5	DEFN 1	DEFN 2	DEFN 3	DEFN 4	DEFN 5	DEFN 1	DEFN 2	DEFN 3	DEFN 4	DEFN 5			
1	6.60	15.95	8.09	25.06	9.53	22.28	1.25	0.22	2.24	8.42	1.54	2.57	108.88	125.22	18.54	38.11	109.95	178.32
2	6.60	15.95	8.09	25.06	9.53	22.28	1.25	0.22	2.24	8.42	1.54	2.57	108.88	125.22	18.54	38.11	109.95	178.32
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	75.02	207.45	21.90	55.65	124.04	261.10
4	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	221.76	381.64	29.14	88.48	274.62	548.05

STRUCTURE..... UNIV. OF TOKYO BOX B6 5-D MODEL, 4/6/89  
SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
TIME: 16:59:05, DATE: 05/31/89

LOADING # 0 DAMAGE INDEX

ELEM#	BENDING COMPONENT			SHEAR COMPONENT			AXIAL COMPONENT		
	DAMAGE	ESE	PSE	DAMAGE	ESE	PSE	DAMAGE	ESE	PSE
1	1.24058	1.04057E-02	0.21545	0.17395	2.54124E-02	9.91175E-02	8.94944	4.69800E-05	0.16121
2	1.24058	1.04057E-02	0.21545	0.17395	2.54124E-02	9.91175E-02	8.94944	4.69800E-05	0.16121
3	0.00000	1.71267E-32	1.27541E-57	0.00000	7.85050E-33	5.40540E-47	8.53245	1.75789E-02	0.51756
4	0.00000	1.10166E-51	5.95951E-58	0.00000	7.12661E-32	2.18955E-46	21.16058	7.71512E-05	0.60788

STRUCTURE DAMAGE INDEX= 9.8144

MEMORY UTILIZATION .....  
I2= 55%, MEM= 0.67%  
ELAPSED CPU TIME 68.79 SEC  
TOTAL CPU TIME 68.99 SEC



STRUCTURE..... UNIV. OF TOKYO BOX 86 3-D MODEL, 4/6/89  
 SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:39:04, DATE: 05/31/89  
 TIME: 16:39:05, DATE: 05/31/89

ELEMENT # 1 IS READ FROM UNIT # 21

STEP	TIME	MOMENT	ROTATION	SHEAR	SHEAR DISPL.	AXIAL	AXIAL DISPL.	ESE	PSE
0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00
50	0.0000E+00	78.040	5.8440E-04	5.7380	6.7240E-02	9.7990	5.1800E-05	0.1248	0.6599
100	0.0000E+00	-90.850	-5.2100E-04	-4.4310	-6.2710E-02	8.7640	4.7260E-05	8.945E-02	0.9725
150	0.0000E+00	37.330	1.8440E-04	1.8420	4.2240E-02	7.1710	3.8880E-05	2.4250E-02	1.180
200	0.0000E+00	-6.3970	-1.2710E-05	2.0950	2.1570E-02	5.1970	5.0740E-05	1.9500E-02	1.218
250	0.0000E+00	309.20	2.1440E-05	11.770	0.14740	11.140	6.7440E-02	0.7804	5.250
300	0.0000E+00	-150.90	-3.2070E-04	-7.5910	-4.1270E-02	-1.8860	4.2660E-02	0.2520	5.255
350	0.0000E+00	-244.40	-1.8550E-05	-5.5830	-0.10510	6.2570	6.4940E-02	0.2977	4.171
400	0.0000E+00	180.30	1.1060E-03	7.3290	9.6690E-02	2.1770	6.2110E-02	0.2812	4.245
450	0.0000E+00	164.50	1.2350E-05	1.4810	6.4540E-02	1.9250	6.1810E-02	8.4890E-02	4.590
500	0.0000E+00	-268.40	-1.7670E-05	-11.050	-0.15120	5.7010	6.6500E-02	0.6470	4.819
550	0.0000E+00	-85.990	-7.3570E-04	0.54090	-1.4690E-02	1.7670	6.1620E-02	2.3570E-02	5.026
600	0.0000E+00	566.00	2.3920E-05	16.390	0.18070	11.220	7.2860E-02	1.594	5.467
650	0.0000E+00	56.250	6.8040E-04	-1.2200	-1.0410E-02	1.4710	7.0650E-02	1.5660E-02	5.740
700	0.0000E+00	-590.80	-2.6080E-05	-16.470	-0.18140	10.280	8.1650E-02	1.457	6.199
750	0.0000E+00	-225.50	-1.7610E-05	-5.9880	-8.5290E-02	3.5970	7.3300E-02	0.2101	6.194
800	0.0000E+00	-81.560	-6.9120E-05	0.65440	-6.9640E-05	1.3500	7.0490E-02	2.1670E-02	6.158
850	0.0000E+00	159.00	1.1870E-05	6.4910	8.8950E-02	1.5450	7.0740E-02	0.2220	6.262
900	0.0000E+00	407.80	5.5170E-05	18.640	0.19920	14.290	0.11190	1.874	7.184
950	0.0000E+00	445.30	7.3580E-05	19.520	0.21740	14.600	0.25540	2.281	10.88
1000	0.0000E+00	44.490	4.1800E-05	-0.87610	1.2020E-05	-0.42040	0.21290	9.8182E-05	10.90
1050	0.0000E+00	-257.20	-2.3280E-04	-8.760	-0.11610	-2.8910	0.17520	0.4456	11.28
1100	0.0000E+00	-441.30	-5.2840E-05	-15.390	-0.18240	6.1790	0.19060	1.577	12.97
1150	0.0000E+00	-202.80	-5.9450E-05	-5.3110	-9.7210E-02	2.8940	0.25820	0.2057	14.81
1200	0.0000E+00	65.920	-2.0040E-05	2.8410	5.8900E-02	0.45670	0.25160	4.4950E-02	14.87
1250	0.0000E+00	266.40	5.2190E-05	8.1040	0.11250	0.41200	0.25080	0.4866	15.58
1300	0.0000E+00	587.30	7.1640E-05	15.670	0.19860	11.620	0.25260	1.551	17.09
1350	0.0000E+00	8.3050	3.7610E-05	-0.91350	-5.8330E-04	0.40900	0.25040	3.4650E-05	16.90
1400	0.0000E+00	-177.80	-1.0140E-05	-5.7600	-9.0200E-02	0.46670	0.25060	0.2312	17.52
1450	0.0000E+00	-568.50	-9.0150E-05	-15.190	-0.16150	5.2380	0.24910	1.157	18.48
1500	0.0000E+00	-254.90	-6.2510E-05	-5.1920	-0.11510	4.5940	0.25990	0.3111	19.27
1550	0.0000E+00	6.1280	-5.6130E-05	1.2440	1.1810E-02	0.47590	0.25160	6.0750E-05	19.20
1600	0.0000E+00	153.50	-2.7750E-04	4.5980	8.2940E-02	0.44560	0.25150	0.1401	19.48
1650	0.0000E+00	277.50	3.4900E-05	8.2850	0.11950	0.41150	0.25070	0.5265	20.10
1700	0.0000E+00	407.70	6.9000E-05	15.150	0.18470	7.0480	0.24560	1.470	21.14
1750	0.0000E+00	746.40	1.0510E-02	19.940	0.23350	14.890	0.23220	2.466	24.46
1800	0.0000E+00	50.20	1.4490E-02	20.440	0.25520	15.210	0.22180	2.485	28.66
1850	0.0000E+00	105.20	1.5570E-02	2.1420	0.10860	0.82440	0.53180	6.1450E-02	30.56
1900	0.0000E+00	168.90	1.3470E-02	10.400	0.16260	3.6890	0.50580	0.5529	30.47
1950	0.0000E+00	445.50	1.7690E-02	20.730	0.27390	15.460	0.63490	2.815	33.42

STRUCTURE..... UNIV. OF TOKYO BOX 86 3-D MODEL, 4/6/89  
 SOLUTION..... MONOTONIC PSEUDO-STATIC EQ LOADING GLOBAL X DIRECTION

TIME: 16:59:04, DATE: 05/31/89  
 TIME: 16:59:06, DATE: 05/31/89

ENERGY DATA IS READ FROM UNIT # 37

STEP	TIME	INPUT	ELASTIC STRAIN	KINETIC	PLASTIC STRAIN	DAMPING	RELATIVE ERROR %
0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000
50	0.0000E+00	1.9944	0.54182	0.0000E+00	1.4400	0.0000E+00	0.6302
100	0.0000E+00	2.9921	0.35454	0.0000E+00	2.6277	0.0000E+00	0.5326
150	0.0000E+00	3.4619	9.7265E-02	0.0000E+00	5.2557	0.0000E+00	0.5155
200	0.0000E+00	3.9899	7.9254E-02	0.0000E+00	5.8610	0.0000E+00	0.4979
250	0.0000E+00	11.516	1.4006	0.0000E+00	9.5818	0.0000E+00	0.2047
300	0.0000E+00	11.242	0.45243	0.0000E+00	10.565	0.0000E+00	0.2242
350	0.0000E+00	15.518	0.70458	0.0000E+00	14.594	0.0000E+00	0.1510
400	0.0000E+00	16.425	0.76168	0.0000E+00	15.658	0.0000E+00	0.1455
450	0.0000E+00	17.763	0.17827	0.0000E+00	17.555	0.0000E+00	0.1645
500	0.0000E+00	20.963	1.7867	0.0000E+00	19.149	0.0000E+00	0.1314
550	0.0000E+00	20.602	7.14255E-02	0.0000E+00	20.507	0.0000E+00	0.1126
600	0.0000E+00	26.616	5.7755	0.0000E+00	22.821	0.0000E+00	0.0751
650	0.0000E+00	24.471	6.57818E-02	0.0000E+00	24.581	0.0000E+00	0.1055
700	0.0000E+00	50.957	3.8690	0.0000E+00	27.045	0.0000E+00	0.0885
750	0.0000E+00	27.891	0.46309	0.0000E+00	27.413	0.0000E+00	0.0915
800	0.0000E+00	27.530	6.7752E-02	0.0000E+00	27.454	0.0000E+00	0.0988
850	0.0000E+00	29.105	0.60536	0.0000E+00	28.475	0.0000E+00	0.0880
900	0.0000E+00	26.886	4.8586	0.0000E+00	32.002	0.0000E+00	0.0482
950	0.0000E+00	49.408	5.7962	0.0000E+00	45.587	0.0000E+00	0.0509
1000	0.0000E+00	44.206	5.86909E-02	0.0000E+00	44.151	0.0000E+00	0.0821
1050	0.0000E+00	48.383	1.2071	0.0000E+00	47.141	0.0000E+00	0.0734
1100	0.0000E+00	59.472	4.3640	0.0000E+00	55.072	0.0000E+00	0.0610
1150	0.0000E+00	62.208	0.44825	0.0000E+00	61.715	0.0000E+00	0.0715
1200	0.0000E+00	62.587	0.15829	0.0000E+00	62.402	0.0000E+00	0.0755
1250	0.0000E+00	67.751	1.2427	0.0000E+00	66.441	0.0000E+00	0.0698
1300	0.0000E+00	77.577	4.2955	0.0000E+00	73.040	0.0000E+00	0.0959
1350	0.0000E+00	75.576	1.95520E-02	0.0000E+00	73.306	0.0000E+00	0.0689
1400	0.0000E+00	74.419	0.61070	0.0000E+00	75.758	0.0000E+00	0.0645
1450	0.0000E+00	84.845	3.2168	0.0000E+00	81.579	0.0000E+00	0.0579
1500	0.0000E+00	85.918	0.75645	0.0000E+00	85.157	0.0000E+00	0.0521
1550	0.0000E+00	85.272	2.88542E-02	0.0000E+00	85.196	0.0000E+00	0.0544
1600	0.0000E+00	87.184	0.58190	0.0000E+00	86.756	0.0000E+00	0.0552
1650	0.0000E+00	91.572	1.3388	0.0000E+00	90.187	0.0000E+00	0.0506
1700	0.0000E+00	99.491	4.5948	0.0000E+00	94.856	0.0000E+00	0.0413
1750	0.0000E+00	112.44	6.6295	0.0000E+00	105.77	0.0000E+00	0.0394
1800	0.0000E+00	126.09	7.1768	0.0000E+00	118.87	0.0000E+00	0.0351
1850	0.0000E+00	125.42	0.15484	0.0000E+00	125.25	0.0000E+00	0.0429
1900	0.0000E+00	127.89	2.0508	0.0000E+00	125.79	0.0000E+00	0.0386
1950	0.0000E+00	145.50	7.5282	0.0000E+00	135.69	0.0000E+00	0.0552

MAXIMUM 158.10 8.1861 0.0000E+00 149.84 0.0000E+00

GROSS RE: 0.06467

```

----- MEMORY UTILIZATION -----
----- IZ= 337%, MEM= 0.675X -----
----- ELAPSED CPU TIME 3.42 SEC -----
----- TOTAL CPU TIME 72.41 SEC -----

```

Notes:

- (1) The results for an individual step are written to the output file every 99999th step. The choice of a large increment (99999) suppresses the output for individual steps.
- (2) The ductility and excursion ratio's are defined in Appendix I.
- (3) The damage index is defined in Appendix II.

C. TWO STORY UNSYMMETRIC BUILDING WITH ISOLATED SHEAR WALLS

1. Description of Input Information. The two story unsymmetric building with isolated shear walls is shown in Figures 24 and 25. This 'L' shaped, two-story building has four 30' wide shear walls. All of the lateral loads are resisted by the shear walls. Some of the gravity loads in the building are carried by a separate vertical load resisting system, with the shear walls carrying the remainder of the gravity loads.

The model used for the unsymmetric building has 8 shear wall elements, 16 vertical degrees of freedom, 2 translational degrees of freedom at each level and one rotational degree of freedom at each level as shown in Figure 24. All 16 of the vertical degrees of freedom are condensed out, leaving the 2 translational and one rotational degrees of freedom at each level, Gdof 17 through 22, for the dynamic analysis. The separate vertical load resisting system is not included in the model. The geometric stiffness of the unsymmetric building reflects the gravity loads on the structure.

For the first solution the natural frequency and mode shapes of the structure are calculated. For the second solution, the nonlinear response to the first 10 seconds of the two component 1940 El Centro earthquake is calculated. The north south

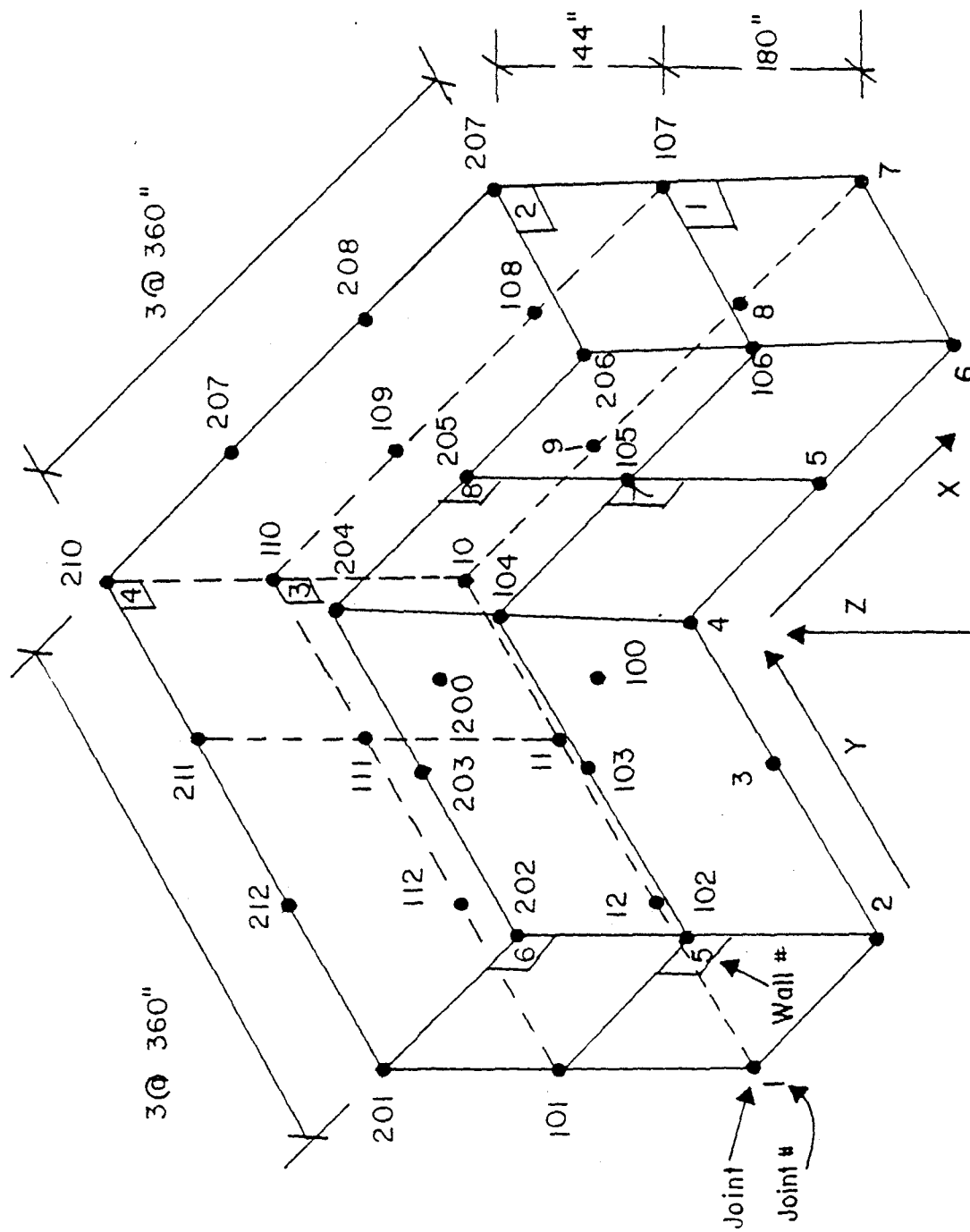


Figure 24. Two-story Unsymmetric Building: Dimensions, Joints and Walls

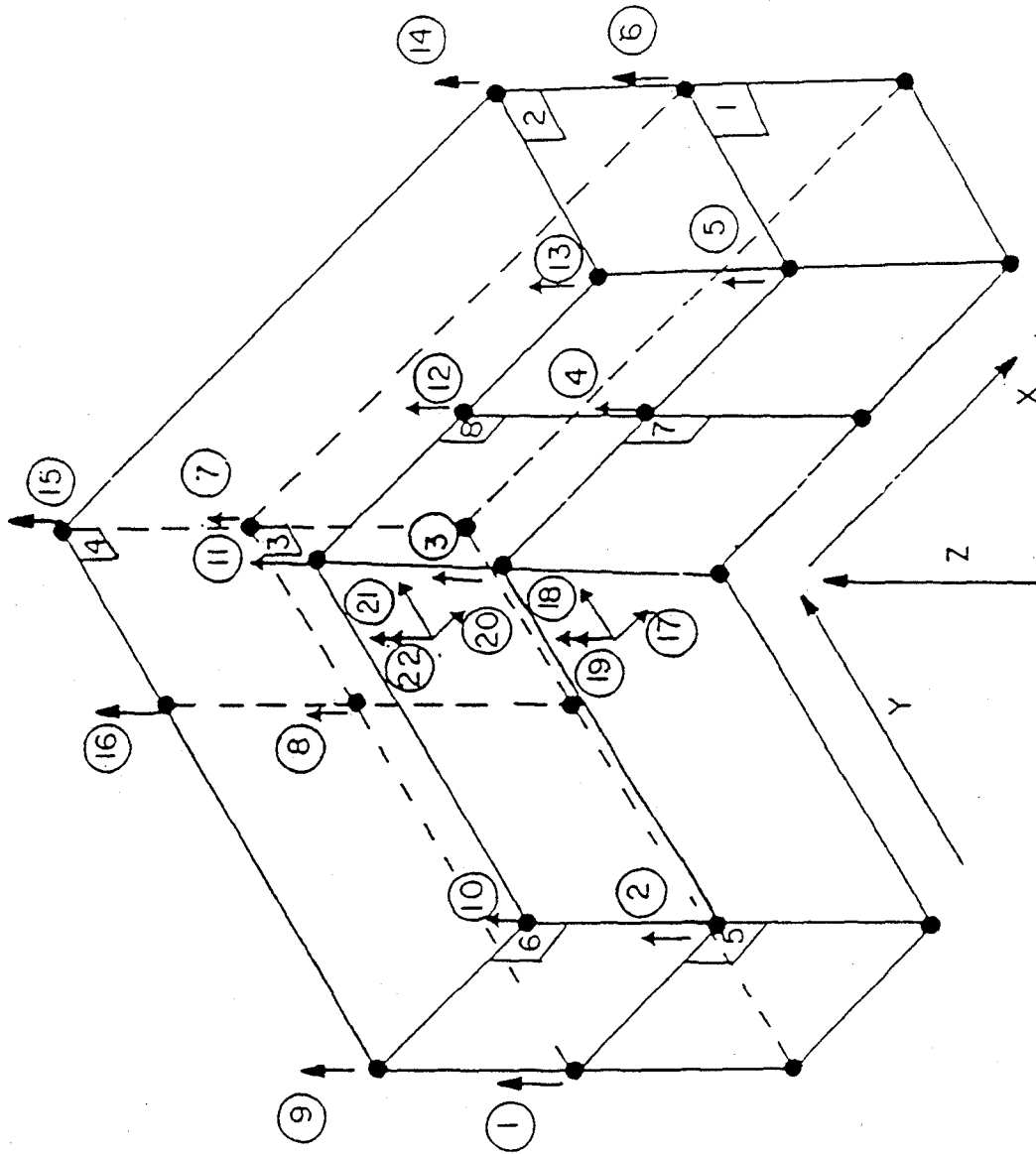


Figure 25. Two-story Unsymmetric building: Degrees of Freedom

component of the El Centro earthquake is stored in the file accessed by unit 92, while the east west component is stored in the file accessed by unit 93. For the third solution the natural frequency and mode shapes of the damaged structure are calculated.

## 2. Input Data.

```

ECHO OF INPUT DATA
LINE .....10.....20.....30.....40.....50.....60.....70.....80
1: 'STRUCTURE DEFINITION'
2: 'BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG'
3: 58 1 12 1 2 12.
4: 1 0 0 0 1 0
5: 2 50 0 0 1 0
6: 5 50 50 0 1 0
7: 4 50 60 0 1 0
8: 5 60 60 0 1 0
9: 6 90 60 0 1 0
10: 7 90 90 0 1 0
11: 8 60 90 0 1 0
12: 9 50 90 0 1 0
13: 10 0 90 0 1 0
14: 11 0 60 0 1 0
15: 12 0 50 0 1 0
16: 100 54.7598 55.2602 15 1 0
17: 101 0 0 15 1 0
18: 102 50 0 15 1 0
19: 105 50 50 15 1 0
20: 104 50 60 15 1 0
21: 105 60 60 15 1 0
22: 106 90 60 15 1 0
23: 107 90 90 15 1 0
24: 108 60 90 15 1 0
25: 109 50 90 15 1 0
26: 110 0 90 15 1 0
27: 111 0 60 15 1 0
28: 112 0 50 15 1 0
29: 200 54.4811 55.5191 27 1 0
30: 201 0 0 27 1 0
31: 202 50 0 27 1 0
32: 203 50 50 27 1 0
33: 204 50 60 27 1 0
34: 205 60 60 27 1 0
35: 206 90 60 27 1 0
36: 207 90 90 27 1 0
37: 208 60 90 27 1 0
38: 209 50 90 27 1 0
39: 210 0 90 27 1 0
40: 211 0 60 27 1 0
41: 212 0 50 27 1 0
42: 1 0 0 0 1 0
43: 1 1 1 1 1 1 11 1
44: 0 0 0 0 2 2 0 0 0
45: 100 0 0 2 0 0 0 0 0
46: 105 0 0 2 0 0 0 0 0
47: 108 0 0 2 0 0 0 0 0
48: 109 0 0 2 0 0 0 0 0
49: 112 0 0 2 0 0 0 0 0
50: 200 0 0 2 0 0 0 0 0
51: 205 0 0 2 0 0 0 0 0
52: 208 0 0 2 0 0 0 0 0
53: 209 0 0 2 0 0 0 0 0
54: 212 0 0 2 0 0 0 0 0
55: 0 0 0 1 0 0 0 0 0
56: 1 100 101 11 1

```

ECHO OF INPUT DATA

```

LINE .....10.....20.....30.....40.....50.....60.....70.....80
57: 1 200 201 11 1
58: 5
59: *ANLMOD * 7.68E6 6.91E6 7.68E3 257.6 .9 .2 15 .2
60: *BEND1 BOT* 9 10 3.55885E-6 .2
61: 44100.0 46550.0 56644.0 66150.0 68600.0
62: 71050.0 75500.0 75950.0 77179.3
63: 9.111390E-07 1.250030E-06 3.558854E-06 7.339490E-06 1.065460E-05
64: 1.641140E-05 2.357860E-05 3.125210E-05 3.558853E-05
65: *BEND1 TOP* 10 10 3.32151E-6 .2
66: 57440.0 38880.0 51840.0 52450.4 60480.0
67: 61920.0 64800.0 67680.0 70560.0 75306.5
68: 6.782970E-07 8.315580E-07 3.210960E-06 3.521510E-06 5.859730E-06
69: 6.857940E-06 1.025450E-05 1.602140E-05 2.589400E-05 3.521510E-05
70: *SHEAR1 BOT* 10 10 2.90442E-4 .2
71: 140.000 160.000 210.000 251.200 270.000
72: 280.000 290.000 300.000 310.000 360.5
73: 5.650959E-05 7.255400E-05 2.177690E-04 2.904420E-04 4.957469E-04
74: 6.590021E-04 8.475210E-04 1.096060E-03 1.534810E-03 2.904420E-03
75: *SHEAR1 TOP* 10 10 4.85123E-4 .2
76: 250.000 260.000 340.000 364.100 450.000
77: 440.000 460.000 480.000 500.000 559.2
78: 1.146500E-04 1.411250E-04 3.81614E-04 4.85123E-04 8.824540E-04
79: 1.005020E-03 1.572420E-03 1.885950E-03 2.587450E-03 4.851236E-03
80: 1 1 2 .FALSE.
81: 3
82: *SHEAR WALL* 'NS F' 2 4 1 107 106 6 7 1.00 250.5 0 0
83: *SHEAR WALL* 'NS S' 5 5 1 207 206 106 107 1.00 71.1 0 0
84: *SHEAR WALL* 'NS F' 2 4 1 110 111 11 10 1.00 250.5 0 0
85: *SHEAR WALL* 'NS S' 5 5 1 210 211 111 110 1.00 71.1 0 0
86: *SHEAR WALL* 'EW F' 2 4 1 102 101 1 2 1.00 250.5 0 0
87: *SHEAR WALL* 'EW S' 5 5 1 202 201 101 102 1.00 71.1 0 0
88: *SHEAR WALL* 'EW F' 2 4 1 105 104 4 5 1.00 250.5 0 0
89: *SHEAR WALL* 'EW S' 5 5 1 205 204 104 105 1.00 71.1 0 0
90: 24 1 .FALSE.
91: 101 .067547 .067547 .067547 0 0 0 0 0 0 0
92: 102 .067547 .067547 .067547 0 0 0 0 0 0 0
93: 106 .067547 .067547 .067547 0 0 0 0 0 0 0
94: 107 .067547 .067547 .067547 0 0 0 0 0 0 0
95: 110 .074017 .074017 .074017 0 0 0 0 0 0 0
96: 201 .148486 .148486 .148486 0 0 0 0 0 0 0
97: 202 .148486 .148486 .148486 0 0 0 0 0 0 0
98: 206 .148486 .148486 .148486 0 0 0 0 0 0 0
99: 207 .148486 .148486 .148486 0 0 0 0 0 0 0
100: 210 .148486 .148486 .148486 0 0 0 0 0 0 0
101: 103 .051242 .051242 .0 0 0 0 0 0 0 0
102: 108 .051242 .051242 .0 0 0 0 0 0 0 0
103: 109 .057712 .057712 .0 0 0 0 0 0 0 0
104: 112 .051242 .051242 .0 0 0 0 0 0 0 0
105: 205 .129270 .129270 .0 0 0 0 0 0 0 0
106: 208 .129270 .129270 .0 0 0 0 0 0 0 0
107: 209 .129270 .129270 .0 0 0 0 0 0 0 0
108: 212 .129270 .129270 .0 0 0 0 0 0 0 0
109: 105 .079175 .079175 .079157 0 0 0 0 0 0 0
110: 111 .085663 .085663 .085663 0 0 0 0 0 0 0
111: 205 .192158 .192158 .192158 0 0 0 0 0 0 0
112: 211 .192158 .192158 .192158 0 0 0 0 0 0 0

```

ECHO OF INPUT DATA

```

LINE .....10.....20.....30.....40.....50.....60.....70.....80
113: 104 .097508 .097508 .097508 0 0 0 0 0 0 0
114: 204 .255831 .255831 .255831 0 0 0 0 0 0 0
115: 1.4845 .000455339
116: *SOL05 - SOLUTION*
117: *NATURAL FREQUENCIES AND MODE SHAPES*
118: *FREQUENCY* 6 0
119: *SOL02 - SOLUTION*
120: *NONLINEAR RESPONSE TO (1940 ELCCENTRO NS & EW)*1.75*
121: *LINEAR* 0 .FALSE. .TRUE.
122: 99999 40 2400 .FALSE.
123: 0.00 .00025 10. 386.4
124: *ELEM* 1 21 7 1 1
125: *JOINT FM* 100 51 1 100 5
126: *JOINT FV* 100 52 1 100 3
127: *JOINT WZ* 100 33 1 100 3
128: *ENERGY* 00 57 0 0 0
129: *DUMRCT* 00 58 0 0 0
130: *END* 0 0 0 0 0
131: 0 0 0 *END* 0 0 0 0 0
132: 2 1.75 .00 .01 .FALSE.
133: 1 0 0 0 1 0 V1, V2
134: 92 2400 2 .TRUE. .FALSE. .TRUE.
135: (A/A)
136: (F9.6)/(8F9.6))
137: 93 2400 1 .TRUE. .FALSE. .TRUE.
138: (A/A)
139: (F9.6)/(8F9.6))
140: *READ [INC:1000 UNIT=57 *
141: *SOL05 - SOLUTION*
142: *NATURAL FREQUENCIES AND MODE SHAPES*
143: *FREQUENCY* 6 0
144: *STOP*

```

### 3. Output.

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

\*\*\* PROGRAM FEM \*\*\* DOUBLE PRECISION VERSION

#### NODE CONSTRAINTS

XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 101
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 102
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 103
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 104
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 105
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 106
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 107
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 108
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 109
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 110
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 111
XV-PLANE	CONSTRAINT, MASTER: 100 SLAVE: 112
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 201
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 202
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 203
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 204
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 205
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 206
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 207
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 208
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 209
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 210
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 211
XV-PLANE	CONSTRAINT, MASTER: 200 SLAVE: 212

#### NODE COORDINATES AND DEGREES OF FREEDOM

TOTAL NUMBER OF DEGREES OF FREEDOM..... 156  
NUMBER OF DEGREES OF FREEDOM CONDENSED OUT..... 16  
NUMBER OF FREE DEGREES OF FREEDOM..... 6  
NUMBER OF RESTRAINED DEGREES OF FREEDOM..... 154

NODE	COS#	X-COORD	Y-COORD	Z-COORD	FX	FY	FZ	MX	MY	MZ
1	1	0.00000E+00	0.00000E+00	0.00000E+00	25-R	24-R	25-R	71-R	72-R	26-R
2	1	560.00	0.00000E+00	0.00000E+00	27-R	28-R	29-R	73-R	74-R	30-R
3	1	560.00	560.00	0.00000E+00	51-R	52-R	53-R	75-R	76-R	54-R
4	1	560.00	720.00	0.00000E+00	55-R	56-R	57-R	77-R	78-R	58-R
5	1	720.00	720.00	0.00000E+00	59-R	60-R	61-R	79-R	80-R	62-R
6	1	1080.0	720.00	0.00000E+00	63-R	64-R	65-R	81-R	82-R	66-R
7	1	1080.0	1080.0	0.00000E+00	67-R	68-R	69-R	83-R	84-R	50-R
8	1	720.00	1080.0	0.00000E+00	51-R	52-R	53-R	85-R	86-R	54-R
9	1	560.00	1080.0	0.00000E+00	55-R	56-R	57-R	87-R	88-R	58-R
10	1	0.00000E+00	1080.0	0.00000E+00	59-R	60-R	61-R	89-R	90-R	62-R
11	1	0.00000E+00	720.00	0.00000E+00	63-R	64-R	65-R	91-R	92-R	66-R
12	1	0.00000E+00	560.00	0.00000E+00	67-R	68-R	69-R	93-R	94-R	70-R
100	1	416.88	663.12	180.00	17	18	95-R	96-R	97-R	19
101	1	0.00000E+00	0.00000E+00	180.00	17-C	18-C	1	98-R	99-R	19-C
102	1	560.00	0.00000E+00	180.00	17-C	18-C	2	100-R	101-R	19-C
103	1	560.00	560.00	180.00	17-C	18-C	102-R	103-R	104-R	19-C
104	1	560.00	720.00	180.00	17-C	18-C	3	105-R	106-R	19-C
105	1	720.00	720.00	180.00	17-C	18-C	4	107-R	108-R	19-C
106	1	1080.0	720.00	180.00	17-C	18-C	5	109-R	110-R	19-C
107	1	1080.0	1080.0	180.00	17-C	18-C	6	111-R	112-R	19-C
108	1	720.00	1080.0	180.00	17-C	18-C	113-R	114-R	115-R	19-C
109	1	560.00	1080.0	180.00	17-C	18-C	116-R	117-R	118-R	19-C
110	1	0.00000E+00	1080.0	180.00	17-C	18-C	7	119-R	120-R	19-C
111	1	0.00000E+00	720.00	180.00	17-C	18-C	8	121-R	122-R	19-C
112	1	0.00000E+00	560.00	180.00	17-C	18-C	123-R	124-R	125-R	19-C
200	1	+15.77	666.25	524.00	20	21	126-R	127-R	128-R	22
201	1	0.00000E+00	0.00000E+00	524.00	20-C	21-C	9	129-R	130-R	22-C
202	1	560.00	0.00000E+00	524.00	20-C	21-C	10	131-R	132-R	22-C
203	1	560.00	560.00	524.00	20-C	21-C	153-R	134-R	135-R	22-C
204	1	560.00	720.00	524.00	20-C	21-C	11	136-R	137-R	22-C
205	1	720.00	720.00	524.00	20-C	21-C	12	138-R	139-R	22-C
206	1	1080.0	720.00	524.00	20-C	21-C	13	140-R	141-R	22-C
207	1	1080.0	1080.0	524.00	20-C	21-C	14	142-R	143-R	22-C
208	1	720.00	1080.0	524.00	20-C	21-C	144-R	145-R	146-R	22-C
209	1	560.00	1080.0	524.00	20-C	21-C	147-R	148-R	149-R	22-C
210	1	0.00000E+00	1080.0	524.00	20-C	21-C	15	150-R	151-R	22-C
211	1	0.00000E+00	720.00	524.00	20-C	21-C	16	152-R	153-R	22-C
212	1	0.00000E+00	560.00	524.00	20-C	21-C	154-R	155-R	156-R	22-C

NOTE: R - RESTRAINED DEGREE OF FREEDOM  
C - CONSTRAINED DEGREE OF FREEDOM

#### DIRECTION COSINES ...

COS# 1> VX: 1.00000 I +0.00000 J +0.00000 K W: 0.00000 I +1.00000 J +0.00000 K VZ: 0.00000 I +0.00000 J +1.00000 K

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

#### AXIUMMO HYSTERESIS MODEL- FOR UNIT LENGTH MEMBER

MAT.	SC	ST1	ST2	PY	ALPHA	BETA	MAX DUCT.	BETA-01
1	0.768000E+07	0.691000E+07	7680.00	237.600	0.900000	0.200000	15.0000	0.200000

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

BEND1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER

BACKBONE CURVE POINTS - MATL NI				DV	BETA	MOMENT	ROTATION
2	10	0.555885E-05	0.200000			44100.0	0.911159E-06
						46550.0	0.125003E-05
						56644.0	0.355885E-05
						66150.0	0.723949E-05
						68600.0	0.106546E-04
						71050.0	0.164114E-04
						73500.0	0.255786E-04
						75950.0	0.512521E-04
						77179.3	0.555885E-04
3	10	0.532151E-05	0.200000			57440.0	0.678297E-06
						58880.0	0.851528E-06
						51840.0	0.321096E-05
						52450.4	0.532151E-05
						60480.0	0.585973E-05
						61920.0	0.683784E-05
						64800.0	0.110254E-04
						67680.0	0.164021E-04
						70560.0	0.258940E-04
						73306.3	0.332151E-04

2

3

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

SHEAR1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER

BACKBONE CURVE POINTS - MATL NI				DV	BETA	STRESS	STRAIN
4	10	0.290442E-05	0.200000			140.000	0.565094E-04
						160.000	0.725540E-04
						210.000	0.217769E-05
						251.200	0.290442E-05
						270.000	0.493747E-05
						280.000	0.639002E-05
						290.000	0.847521E-05
						500.000	0.109606E-02
						510.000	0.133481E-02
						560.500	0.290442E-02
5	10	0.485124E-05	0.200000			250.000	0.114650E-05
						260.000	0.141123E-05
						540.000	0.581614E-05
						564.100	0.485124E-05
						450.000	0.882454E-05
						440.000	0.100502E-02
						460.000	0.157242E-02
						480.000	0.188593E-02
						500.000	0.258745E-02
						539.200	0.485124E-02

2

3

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

GEOMETRIC STIFFNESS DATA

KGLOAD = 1, LOAD= F(INPUT)\*(1.00+ACCEL)  
 F(INPUT) IS POSITIVE IN COMPRESSION  
 ACCEL IS POSITIVE GLOBAL Z-AXIS ACCELERATION  
 KGTYPE = 1, LUMPED FORMULATION  
 KGFORM = 2, SEPERATE GLOBAL KG IS FORMED

- THE GEOMETRIC STIFFNESS MATRIX IS NOT CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG SOLUTION.....

TIME: 17:01:22, DATE: 05/31/89

ELEMENT 05, R/C SHEAR WALL ELEMENT

	ELEM	BEND				SHEAR				AXIAL				JOINT #1	JOINT #2	JOINT #3	JOINT #4	LENGTH	WIDTH	ALPHA	PKG
		#	MATL	MATL	MATL	#1	#2	#3	#4	#1	#2	#3	#4								
NS F	1	2	4	1	107	106	6	7	180.0	560.0	1.000	250.5									
NS S	2	5	5	1	207	206	106	107	144.0	560.0	1.000	71.10									
NS F	3	2	4	1	110	111	11	10	180.0	560.0	1.000	250.5									
NS S	4	5	5	1	210	211	111	110	144.0	560.0	1.000	71.10									
EM F	5	2	4	1	102	101	1	2	180.0	560.0	1.000	250.5									
EM S	6	5	5	1	202	201	101	102	144.0	560.0	1.000	71.10									
EM F	7	2	4	1	105	104	4	5	180.0	560.0	1.000	250.5									
EM S	8	5	5	1	205	204	104	105	144.0	560.0	1.000	71.10									



STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
 SOLUTION.....

TIME: 17:01:22, DATE: 05/51/89

LUMPED NODE MASSES

NODE	MX	MY	MZ	RXX	RYX	RZZ	RXY	RKZ	RYZ	IGEN	INC
101	6.7547E-02	6.7547E-02	6.7547E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
102	6.7547E-02	6.7547E-02	6.7547E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
106	6.7547E-02	6.7547E-02	6.7547E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
107	6.7547E-02	6.7547E-02	6.7547E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
110	7.4017E-02	7.4017E-02	7.4017E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
201	0.1485	0.1485	0.1485	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
202	0.1485	0.1485	0.1485	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
206	0.1485	0.1485	0.1485	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
207	0.1485	0.1485	0.1485	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
210	0.1485	0.1485	0.1485	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
105	5.1242E-02	5.1242E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
108	5.1242E-02	5.1242E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
109	5.7712E-02	5.7712E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
112	5.1242E-02	5.1242E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
203	0.1295	0.1295	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
208	0.1295	0.1295	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
209	0.1295	0.1295	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
212	0.1295	0.1295	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
105	7.9175E-02	7.9175E-02	7.9175E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
111	8.5665E-02	8.5665E-02	8.5665E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
205	0.1922	0.1922	0.1922	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
211	0.1922	0.1922	0.1922	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
104	9.7508E-02	9.7508E-02	9.7508E-02	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0
204	0.2358	0.2358	0.2358	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0	0

- THE MASS MATRIX IS NOT CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.

PROPORTIONAL DAMPING COEFFICIENTS

ALPHA= 1.0E+5      BETA= 6.5589E-04

```

-----*
--- MEMORY UTILIZATION -----*
--- IZ= 7727, MEM= 1.545% ---*
-----*
--- ELAPSED CPU TIME 0.46 SEC ---*
--- TOTAL CPU TIME 0.46 SEC ---*
-----*

```

STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
 SOLUTION..... NATURAL FREQUENCIES AND MODE SHAPES

TIME: 17:01:22, DATE: 05/51/89  
 TIME: 17:01:25, DATE: 05/51/89

SOLUTION #5, DETERMINE EIGENVALUES AND EIGENVECTORS

OPTION:.....NATURAL FREQUENCIES

NUMBER OF EIGENVALUES:..... 6

PERFORMANCE INDEX: 0.60747465781552744E-02

NODE:	1	2	5	4	5	6
FREQ (RAD/SEC):	55.480	40.526	60.262	192.82	254.55	546.54
FREQUENCY (HZ):	9.3286	6.4498	9.5910	30.689	37.326	55.154
PERIOD (SEC):	0.18767	0.15504	0.10426	5.25851E-02	2.67908E-02	1.81512E-02
EIGENVECTORS:						
DOF( 17)	0.51200	-0.20888	0.51856	1.0000	-0.1158	1.0000
DOF( 18)	0.20820	0.51555	0.21111	0.0965	1.0000	0.11860
DOF( 19)	-5.36055E-04	-6.20854E-08	2.07477E-05	-1.05752E-05	7.09672E-07	5.8179E-05
DOF( 20)	1.0000	-0.10681	1.0000	-0.22480	9.19646E-02	-0.21311
DOF( 21)	0.10855	1.0000	0.10021	-9.29952E-02	-0.22541	-8.81609E-02
DOF( 22)	-1.04515E-05	1.10425E-08	4.05471E-05	2.47461E-04	1.59911E-06	-8.75256E-04

```

-----*
--- MEMORY UTILIZATION -----*
--- IZ= 7967, MEM= 1.593% ---*
-----*
--- ELAPSED CPU TIME 0.09 SEC ---*
--- TOTAL CPU TIME 0.55 SEC ---*
-----*

```

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:23, DATE: 05/31/89

SOLUTION #2, LINEAR ACCELERATION METHOD OF NUMERICAL INTEGRATION

INITIAL TIME ..... 0.000000E+00  
TIME STEP ..... 2.500000E-04  
FINAL TIME ..... 10.0000  
ACCELERATION DUE TO GRAVITY ..... 386.400  
STEP INTERVAL FOR PRINTING ..... 99999

DATA WRITTEN TO FILES

ELEMENT # 1 IS WRITTEN TO UNIT # 21  
ELEMENT # 2 IS WRITTEN TO UNIT # 22  
ELEMENT # 3 IS WRITTEN TO UNIT # 23  
ELEMENT # 4 IS WRITTEN TO UNIT # 24  
ELEMENT # 5 IS WRITTEN TO UNIT # 25  
ELEMENT # 6 IS WRITTEN TO UNIT # 26  
ELEMENT # 7 IS WRITTEN TO UNIT # 27  
ELEMENT # 8 IS WRITTEN TO UNIT # 28  
DEGREE OF FREEDOM # 17 IS WRITTEN TO UNIT # 51 JOINT: 100 DIRECTION: FX  
DEGREE OF FREEDOM # 20 IS WRITTEN TO UNIT # 54 JOINT: 200 DIRECTION: FX  
DEGREE OF FREEDOM # 18 IS WRITTEN TO UNIT # 52 JOINT: 100 DIRECTION: FY  
DEGREE OF FREEDOM # 21 IS WRITTEN TO UNIT # 55 JOINT: 200 DIRECTION: FY  
DEGREE OF FREEDOM # 19 IS WRITTEN TO UNIT # 53 JOINT: 100 DIRECTION: MZ  
DEGREE OF FREEDOM # 22 IS WRITTEN TO UNIT # 56 JOINT: 200 DIRECTION: MZ  
ENERGY BALANCE IS WRITTEN TO UNIT # 57  
SUMMATION OF REACTIONS IS WRITTEN TO UNIT # 38

GROUND ACCELERATION RECORD

INPUTING TRANSLATIONAL ACCELERATION RECORD # 1, FROM UNIT: 92  
ELCENTRO- 1940 EQ DATA FORMAT: (8F9.6)  
DT=0.01 SEC \*\*\* E-W DIRECTION \*\*\* 2400 DATA  
THE RECORD CONTAINS 2400 POINTS, BEGINNING AT TIME: 0.000000E+00 WITH A TIME INCREMENT OF: 1.000000E-02  
DIRECTION OF ACCELERATION: 0.00000 I +1.00000 J +0.00000 K

INPUT ACCELERATION	MAXIMUM	AT TIME	MINIMUM	AT TIME	AVERAGE	STANDARD DEV.	RMS
	0.21490	1.8700	-0.16138	11.050	-2.49E-05	5.46E-02	5.46E-02

GROUND ACCELERATION RECORD

INPUTING TRANSLATIONAL ACCELERATION RECORD # 2, FROM UNIT: 95  
ELCENTRO- 1940 EQ DATA  
DT=0.01 SEC \*\*\* N-S DIRECTION \*\*\* 2400 DATA  
THE RECORD CONTAINS 2400 POINTS, BEGINNING AT TIME: 0.000000E+00 WITH A TIME INCREMENT OF: 1.000000E-02  
DIRECTION OF ACCELERATION: 1.00000 I +0.00000 J +0.00000 K

INPUT ACCELERATION	MAXIMUM	AT TIME	MINIMUM	AT TIME	AVERAGE	STANDARD DEV.	RMS
	0.29242	2.2200	-0.31450	2.0000	1.05550E-04	6.85682E-02	6.8550E-02
X-AXIS ACCELERATION	0.51174	2.2200	-0.55005	2.0000	1.84712E-04	0.11999	0.11997
Y-AXIS ACCELERATION	0.27607	1.8700	-0.28242	11.050	-7.45648E-05	9.56358E-02	9.56159E-02
Z-AXIS ACCELERATION	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:23, DATE: 05/31/89

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:23, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

GLOBAL MAXIMUM DISPLACEMENTS

NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

NODE	UX	UY	UZ	RX	RY	RZ
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
2	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
3	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
4	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
5	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
6	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
7	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
8	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
9	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
10	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
11	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
12	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
100	0.904662	0.557587	0.000000E+00	0.000000E+00	0.000000E+00	-8.952485E-04
101	0.511729	0.929962	0.506021	0.000000E+00	0.000000E+00	-8.952485E-04
102	0.511729	0.608595	-0.506021	0.000000E+00	0.000000E+00	-8.952485E-04
103	0.632398	0.608595	0.000000E+00	0.000000E+00	0.000000E+00	-8.952485E-04
104	0.954668	0.608595	0.849100	0.000000E+00	0.000000E+00	-8.952485E-04
105	0.954668	0.286823	-0.849100	0.000000E+00	0.000000E+00	-8.952485E-04
106	0.954668	-5.474606E-02	0.444751	0.000000E+00	0.000000E+00	-8.952485E-04
107	1.27444	-5.474606E-02	-0.444751	0.000000E+00	0.000000E+00	-8.952485E-04
108	1.27444	0.286823	0.000000E+00	0.000000E+00	0.000000E+00	-8.952485E-04
109	1.27444	0.608595	0.000000E+00	0.000000E+00	0.000000E+00	-8.952485E-04
110	1.27444	0.929962	-0.828259	0.000000E+00	0.000000E+00	-8.952485E-04
111	0.954668	0.929962	0.828259	0.000000E+00	0.000000E+00	-8.952485E-04
112	0.632398	0.929962	0.000000E+00	0.000000E+00	0.000000E+00	-8.952485E-04
200	1.58562	0.979505	0.000000E+00	0.000000E+00	0.000000E+00	-1.557565E-05
201	0.545927	1.62378	0.520378	0.000000E+00	0.000000E+00	-1.557565E-05
202	0.545927	1.06306	-0.520378	0.000000E+00	0.000000E+00	-1.557565E-05
203	1.10665	1.06306	0.000000E+00	0.000000E+00	0.000000E+00	-1.557565E-05
204	1.66737	1.06306	0.863567	0.000000E+00	0.000000E+00	-1.557565E-05
205	1.66737	0.502356	-0.863567	0.000000E+00	0.000000E+00	-1.557565E-05
206	1.66737	-5.858670E-02	0.477672	0.000000E+00	0.000000E+00	-1.557565E-05
207	2.22809	-5.858670E-02	-0.477672	0.000000E+00	0.000000E+00	-1.557565E-05
208	2.22809	0.502356	0.000000E+00	0.000000E+00	0.000000E+00	-1.557565E-05
209	2.22809	1.06306	0.000000E+00	0.000000E+00	0.000000E+00	-1.557565E-05
210	2.22809	1.62378	-0.850990	0.000000E+00	0.000000E+00	-1.557565E-05
211	1.66737	1.62378	0.850990	0.000000E+00	0.000000E+00	-1.557565E-05
212	1.10665	1.62378	0.000000E+00	0.000000E+00	0.000000E+00	-1.557565E-05

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION.....: NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/51/89  
TIME: 17:01:25, DATE: 05/51/89

MAXIMUM VALUES FOR ALL STEPS  
=====

GCS MAXIMUM VELOCITIES

NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

NODE	DX	DY	DZ	RX	RY	RZ
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
2	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
3	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
4	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
5	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
6	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
7	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
8	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
9	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
10	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
11	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
12	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
100	-10.4175	5.58568	0.000000E+00	0.000000E+00	0.000000E+00	9.567673E-05
101	+0.07280	1.59715	-5.57271	0.000000E+00	0.000000E+00	9.567673E-05
102	+0.07280	5.04149	5.57271	0.000000E+00	0.000000E+00	9.567673E-05
103	-7.51716	5.04149	0.000000E+00	0.000000E+00	0.000000E+00	9.567673E-05
104	-10.9615	5.04149	-9.61586	0.000000E+00	0.000000E+00	9.567673E-05
105	-10.9615	8.48586	9.61586	0.000000E+00	0.000000E+00	9.567673E-05
106	-10.9615	11.9502	6.16408	0.000000E+00	0.000000E+00	9.567673E-05
107	-14.4059	11.9502	-6.16408	0.000000E+00	0.000000E+00	9.567673E-05
108	-14.4059	8.48586	0.000000E+00	0.000000E+00	0.000000E+00	9.567673E-05
109	-14.4059	5.04149	0.000000E+00	0.000000E+00	0.000000E+00	9.567673E-05
110	-14.4059	1.59715	-7.21577	0.000000E+00	0.000000E+00	9.567673E-05
111	-10.9615	1.59715	7.21577	0.000000E+00	0.000000E+00	9.567673E-05
112	-7.51716	1.59715	0.000000E+00	0.000000E+00	0.000000E+00	9.567673E-05
200	-17.6712	9.62714	0.000000E+00	0.000000E+00	0.000000E+00	1.659585E-02
201	-6.71189	2.75606	-5.45632	0.000000E+00	0.000000E+00	1.659585E-02
202	-6.71189	8.72985	5.45632	0.000000E+00	0.000000E+00	1.659585E-02
203	-12.8857	8.72985	0.000000E+00	0.000000E+00	0.000000E+00	1.659585E-02
204	-18.6594	8.72985	-9.84467	0.000000E+00	0.000000E+00	1.659585E-02
205	-18.6594	14.7056	9.84467	0.000000E+00	0.000000E+00	1.659585E-02
206	-18.6594	20.6779	6.45004	0.000000E+00	0.000000E+00	1.659585E-02
207	-24.8332	20.6779	-6.45004	0.000000E+00	0.000000E+00	1.659585E-02
208	-24.8332	14.7056	0.000000E+00	0.000000E+00	0.000000E+00	1.659585E-02
209	-24.8332	8.72985	0.000000E+00	0.000000E+00	0.000000E+00	1.659585E-02
210	-24.8332	2.75606	-7.59595	0.000000E+00	0.000000E+00	1.659585E-02
211	-18.6594	2.75606	7.59595	0.000000E+00	0.000000E+00	1.659585E-02
212	-12.8857	2.75606	0.000000E+00	0.000000E+00	0.000000E+00	1.659585E-02

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION.....: NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/51/89  
TIME: 17:01:25, DATE: 05/51/89

MAXIMUM VALUES FOR ALL STEPS  
=====

GCS MAXIMUM ACCELERATIONS

NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

NODE	DX	DY	DZ	RX	RY	RZ
1	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
2	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
3	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
4	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
5	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
6	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
7	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
8	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
9	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
10	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
11	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
12	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00	0.000000E+00
100	242.857	131.458	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
101	99.5459	221.539	-219.546	0.000000E+00	0.000000E+00	-0.520782
102	99.5459	145.749	219.546	0.000000E+00	0.000000E+00	-0.520782
103	177.556	145.749	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
104	255.127	145.749	277.762	0.000000E+00	0.000000E+00	-0.520782
105	255.127	95.981	-277.762	0.000000E+00	0.000000E+00	-0.520782
106	255.127	11.8325	-225.358	0.000000E+00	0.000000E+00	-0.520782
107	332.918	-11.8325	225.358	0.000000E+00	0.000000E+00	-0.520782
108	332.918	45.9681	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
109	332.918	145.749	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
110	332.918	221.539	-245.012	0.000000E+00	0.000000E+00	-0.520782
111	255.127	221.539	245.012	0.000000E+00	0.000000E+00	-0.520782
112	177.556	221.539	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
200	422.660	226.354	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
201	208.946	559.085	190.171	0.000000E+00	0.000000E+00	-0.520782
202	208.946	245.605	-190.171	0.000000E+00	0.000000E+00	-0.520782
203	324.427	245.605	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
204	459.909	245.605	254.265	0.000000E+00	0.000000E+00	-0.520782
205	459.909	128.122	-254.265	0.000000E+00	0.000000E+00	-0.520782
206	459.909	12.4400	212.052	0.000000E+00	0.000000E+00	-0.520782
207	555.590	12.4400	-212.052	0.000000E+00	0.000000E+00	-0.520782
208	555.590	128.122	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
209	555.590	245.605	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782
210	555.590	559.085	-178.809	0.000000E+00	0.000000E+00	-0.520782
211	459.909	559.085	178.809	0.000000E+00	0.000000E+00	-0.520782
212	324.427	559.085	0.000000E+00	0.000000E+00	0.000000E+00	-0.520782

STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:25, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

MAXIMUM GCS RESTRAINT REACTIONS NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY

Table with 7 columns: NODE, FX, FY, FZ, MX, MY, MZ. It lists maximum reaction values for nodes 1 through 212. The values are mostly zero, with some non-zero values for nodes 1, 2, 4, 5, 6, 7, 8, 9, 10, 11, 12, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, and 212.

MAX OF ALL GCS SUMM. -505.9169 450.8115 0.9258572E-11 -125848.8 -144080.5 -118525.9

MAXIMUM RESULTANT OF REACTIONS, FORCE= 595.5 MOMENT= 4.4158E+05

STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:25, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

Table with 12 columns: R/C SHEAR WALL FORCES..., MAXIMUM LOADS AND DISPL AT MAXIMUM LOADS, NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY. Columns include ELEMENT, LOAD, INT-1, INT-2, INT-3, INT-4, MOMENT, ROTATION, SHEAR, SHEAR DISPL., AXIAL, and AXIAL DISPL. It lists data for elements 1 through 8.

STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:25, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

Table with 15 columns: R/C SHEAR WALL DUCTILITY AND ENCURSION RATIOS. Columns include ELEM#, BENDING COMPONENT (DEFN 1-5), and SHEAR COMPONENT (DEFN 1-5). It lists ductility and excursion ratios for elements 1 through 8.

STRUCTURE..... BUILDING 82, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
TIME: 17:01:25, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

Table with 15 columns: DAMAGE. Columns include ELEM#, DAMAGE, and AXIAL COMPONENT (DEFN 1-5). It lists damage values for elements 1 through 8.

STRUCTURE DAMAGE INDEX= 1.1570

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
 SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
 TIME: 17:01:25, DATE: 05/31/89

MAXIMUM VALUES FOR ALL STEPS

PEAK ENERGY VALUES  
 MAX INPUT ENERGY..... 5738.1  
 MAX ELASTIC STRAIN ENERGY..... 123.55  
 MAX PLASTIC STRAIN ENERGY..... 4094.8  
 MAX KINETIC ENERGY..... 16.405  
 MAX DAMPING ENERGY..... 1589.5

-----  
 \*--- MEMORY UTILIZATION ..... \*  
 \*--- IZ= 21725, MEM= 4.545% \*  
 \*--- ELAPSED CPU TIME 4857.27 SEC \*  
 \*--- TOTAL CPU TIME 4857.82 SEC \*  
 -----

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
 SOLUTION..... NONLINEAR RESPONSE TO (1940 ELCENTRO NS & EW)\*1.75

TIME: 17:01:22, DATE: 05/31/89  
 TIME: 17:01:25, DATE: 05/31/89

ENERGY DATA IS READ FROM UNIT # 57

STEP	TIME	INPUT	ELASTIC STRAIN	KINETIC	PLASTIC STRAIN	DAMPING	RELATIVE ERROR %
0	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000E+00	0.0000
1000	0.25000	4.5152	0.14857	4.1255	1.15270E-15	5.1585E-02	0.1789
2000	0.50000	8.4457	0.89772	7.2519	2.1655E-14	0.39316	-0.9104
5000	0.75000	67.570	0.41480	64.964	5.82791E-14	2.2551	-0.0943
4000	1.0000	82.079	5.2810	72.921	0.28674	5.8929	-0.5695
5000	1.2500	55.644	9.1222	33.398	2.5+31	11.318	-0.9294
6000	1.5000	1630.4	2.9165	1590.5	28.722	17.081	-0.5292
7000	1.7500	822.59	52.765	413.01	134.46	37.684	-2.7817
8000	2.0000	2122.8	72.172	1589.0	395.99	88.145	-1.0617
9000	2.2500	5010.9	27.990	1679.8	1080.6	254.15	-1.0520
10000	2.5000	2715.1	42.772	857.35	1462.6	405.25	-1.2098
11000	2.7500	2497.6	65.092	440.18	1590.5	440.47	-1.5654
12000	3.0000	2465.7	1.9506	457.62	1587.1	470.19	-1.2446
13000	3.2500	2236.6	10.444	156.28	1609.3	485.90	-1.1525
14000	3.5000	2291.5	10.121	97.955	1680.1	524.86	-0.9449
15000	3.7500	2815.9	0.35257	505.17	1765.4	559.47	-0.5146
16000	4.0000	2496.7	21.962	65.126	1851.5	587.32	-0.2808
17000	4.2500	2505.5	18.620	24.772	1865.8	608.07	-0.3980
18000	4.5000	3772.0	17.808	940.84	2115.6	716.58	-0.4977
19000	4.7500	5458.3	40.459	61.955	2550.9	835.32	-0.3201
20000	5.0000	4484.5	48.382	661.32	2848.8	955.57	-0.6595
21000	5.2500	4702.7	99.820	402.15	3176.1	1066.6	-0.8923
22000	5.5000	4851.2	19.270	440.66	3299.4	1121.6	-0.6109
23000	5.7500	4822.7	32.391	225.58	3396.6	1178.8	-0.1812
24000	6.0000	4702.6	9.5645	36.558	3462.0	1202.5	-0.1665
25000	6.2500	4716.5	12.595	6.2502	3485.2	1218.4	-0.0850
26000	6.5000	4758.6	1.5705	41.416	3490.8	1229.4	-0.0968
27000	6.7500	4737.0	5.5428	3.7085	3499.1	1233.6	-0.1055
28000	7.0000	4790.7	3.7615	21.742	3515.5	1254.0	-0.0488
29000	7.2500	4959.9	21.108	58.435	3562.2	1289.2	-0.1028
30000	7.5000	4996.6	2.1952	39.318	3634.1	1324.5	-0.0699
31000	7.7500	5145.6	8.7271	74.698	3699.8	1364.8	-0.0469
32000	8.0000	5315.8	0.87374	234.78	3716.2	1372.5	-0.1986
33000	8.2500	5186.1	2.1959	95.194	3728.7	1381.7	-0.3798
34000	8.5000	5157.0	11.902	13.215	3763.0	1395.4	-0.5156
35000	8.7500	5287.5	6.9645	110.48	3779.1	1420.7	-0.5668
36000	9.0000	5447.9	8.2668	271.16	3811.0	1444.5	-0.4749
37000	9.2500	5585.3	21.391	64.100	4000.6	1525.0	-0.4669
38000	9.5000	5485.3	1.9463	109.43	4037.1	1552.9	-0.2859
39000	9.7500	5675.1	7.2102	56.192	4064.8	1575.3	-0.1477

MAXIMUM 5738.0 122.87 2260.7 4092.5 1589.2  
 GROSS RE: 0.4489%

-----  
 \*--- MEMORY UTILIZATION ..... \*  
 \*--- IZ= 21725, MEM= 4.545% \*  
 \*--- ELAPSED CPU TIME 0.81 SEC \*  
 \*--- TOTAL CPU TIME 4858.63 SEC \*  
 -----

STRUCTURE..... BUILDING B2, L SHAPED TWO STORY BOX STRUCTURE, WITH KG  
 SOLUTION..... NATURAL FREQUENCIES AND MODE SHAPES

TIME: 17:01:22, DATE: 05/31/89  
 TIME: 18:44:16, DATE: 05/31/89

SOLUTION #5, DETERMINE EIGENVALUES AND EIGENVECTORS

OPTION:.....NATURAL FREQUENCIES

NUMBER OF EIGENVALUES:..... 6  
 PERFORMANCE INDEX: 0.127945951615354664E-02

MODE:	1	2	3	4	5	6
FREQ (RAD/SEC):	12.324	20.547	24.322	146.06	180.46	252.41
FREQUENCY (HZ):	1.9614	3.2701	3.8726	23.246	28.722	40.172
PERIOD (SEC):	0.50984	0.30580	0.25823	4.30176E-02	3.48168E-02	2.48927E-02

EIGENVECTORS:

D0FC	17)	7.65997E-02	0.95409	0.56612	0.52999	1.0000	1.0000
D0FC	18)	0.57560	-0.28112	0.25051	1.0000	-0.71089	0.57858
D0FC	19)	-5.47059E-04	-7.32726E-04	1.27154E-05	-1.09132E-05	-5.84490E-04	3.47856E-05
D0FC	20)	0.14275	1.0000	1.0000	-0.13689	-0.24581	-0.24554
D0FC	21)	1.0000	-0.47729	0.43305	-0.25301	0.17774	-0.15995
D0FC	22)	-9.49768E-04	-1.29555E-05	2.17037E-05	2.85772E-04	1.49215E-04	-8.98719E-04

-----  
 \*--- MEMORY UTILIZATION ..... \*  
 \*--- IZ= 21965, MEM= 4.395% \*  
 \*--- ELAPSED CPU TIME 0.16 SEC \*  
 \*--- TOTAL CPU TIME 4858.79 SEC \*  
 -----

Notes:

- (1) The Gdof are printed for the six dof of each joint. The suffix -C denotes a constrained, 'slave' dof. The suffix -R denotes a restrained dof.
- (2) First floor walls with a moment to shear ratio of 246".
- (3) Second floor walls with a moment to shear ratio of 144".

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## APPENDIX A

### DUCTILITY AND EXCURSION RATIO

Three definitions of ductility are considered in this study. The first and most common definition is the displacement definition as shown in Figure 26. Let the displacement ductility be defined as

$$\mu_1 = \frac{|\Delta_{\max}|}{\Delta_y} \quad (8)$$

when  $\Delta_{\max}$  represents the maximum displacement, rotation or strain in the structure or element, and  $\Delta_y$  is the yield displacement, rotation or strain. The ductility for the elastic 3D prismatic beam element is not calculated. For the reinforced concrete shear wall element the ductility is calculated for the bending, shear and axial components of deformation. The type of the spring element determines if its ductility is calculated for axial, shear, torsional or rotational deformation.

Cheng, et al, (14, 9) have proposed several energy based ductility definitions. Both the variable strain energy and the constant strain energy formulations are used in this study. The variable strain energy definition of the ductility is shown in Figure 27 and defined as

$$\mu_2 = 1 + \frac{\text{PSE}}{\text{ESE}} \quad (9)$$

where PSE corresponds to the plastic strain energy for the current half cycle. The constant strain energy definition of the ductility is shown in Figure 28 and defined as

$$\mu_3 = 1 + \frac{\text{PSE}}{\text{CSE}} \quad (10)$$

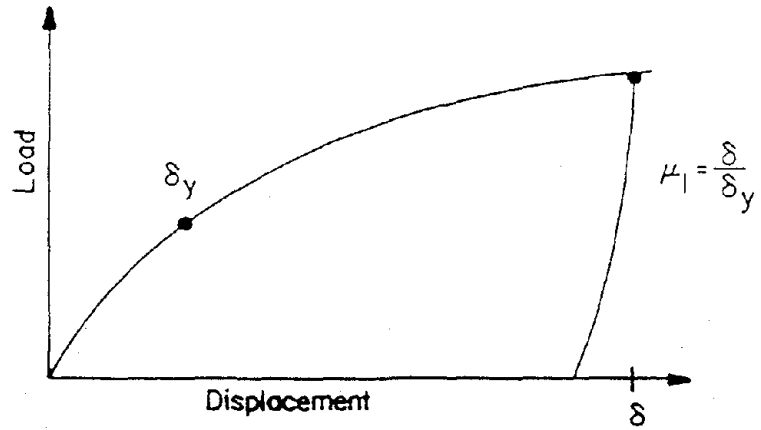


Figure 26. Displacement Definition of Ductility

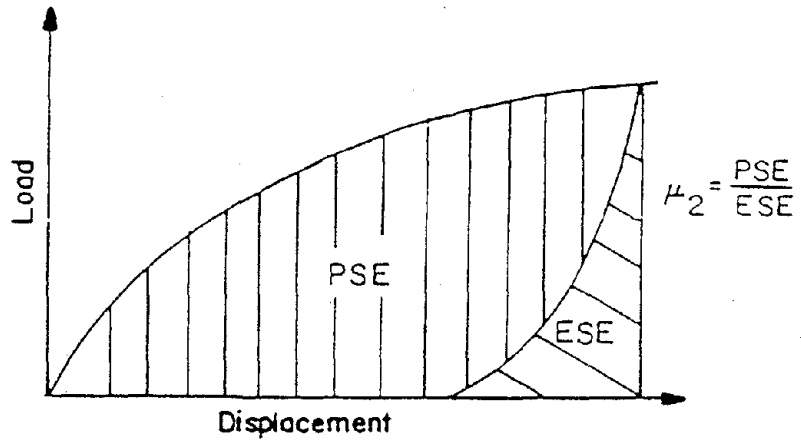


Figure 27. Variable Strain Energy Definition of Ductility

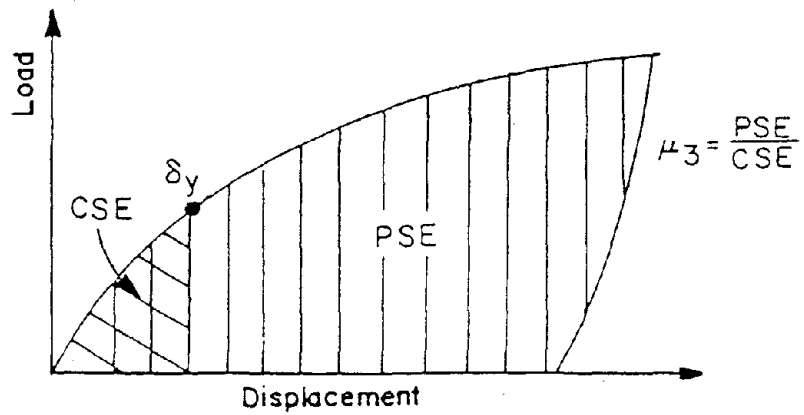


Figure 28. Constant Strain Energy Definition of Ductility

where CSE is the constant strain energy corresponding to displacement at yield.

For each ductility ratio, a corresponding excursion ratio exist, where the excursion ratio is given by

$$\varepsilon = \sum (\mu - 1) \quad (11)$$

and the summation is carried out for each half cycle.

## APPENDIX B

### DAMAGE INDEX

The damage index is a parameter developed by Ang, et al, to assess the damage in a structure (18, 19, 1). A damage index greater than 1.0 indicates total damage or collapse. The damage index is defined as

$$DI = \frac{\Delta_{\max}}{\Delta_{\text{ult}}} + \frac{\beta}{F_y \Delta_{\text{ult}}} \int_0^t d(\text{PSE}) \quad (12)$$

where  $\Delta_{\max}$  is the maximum displacement,  $\Delta_{\text{ult}}$  is the failure displacement under monotonic loading,  $F_y$  is the yield force, and  $\beta$  is a hysteretic energy coefficient. For R/C shear walls, Sheu (20) determined  $\beta = 0.20$ , based on NCKU walls SW1a through SW6.

The damage index for the elastic 3D prismatic beam element is not calculated. For the reinforced concrete shear wall element the damage index is calculated independently for the bending, shear and axial components of deformation. The type of the spring element determines if its damage index is calculated for axial, shear, torsional or rotational deformation. The damage index for each of the shear wall element's components and the spring element are printed in the output. The damage index for the entire structure is then calculated by taking a weighted average of each individual component's damage index, where the total strain energy,  $SE_i$ , for each component is used as the weighting factor. Thus

$$DI = \frac{\sum SE_i DI_i}{\sum SE_i} \quad (13)$$

where the summation is carried out for all the members. A sample calculation of the damage index is included in Section B.1 of Chapter VI.

# APPENDIX C

## LISTING OF PROGRAM INRESB-3D-SUP

### A. COMMON BLOCKS

#### FILE: ZCOMN COPY

```

----- BEGIN COMMON ----- ZC000010
INCLUDE (ZCOMN1)              ZC000020
INCLUDE (ZCOMN2)              ZC000050
----- END COMMON ----- ZC000090
    
```

#### FILE: ZCOMN1 COPY

```

----- BEGIN BLOCK - ZCOMN1 ----- ZC000010
CHARACTER*112 TITLE(2)       ZC000020
CHARACTER*40 STEPID          ZC000050
LOGICAL BUG, NCOND, KCOND, DOUBLE, NENK, MEKKG, ELSTIC, ABORT ZC000090
INTEGER FMASS, FDAMP, CPUREM, CPUELA ZC000050
DOUBLE PRECISION EIE, ESE, PSE, EKE, EDO, EDUMMY ZC000060
COMMON /ZDATA/ TITLE, BUG, IBUG, NAMEOF, NDC(25), STEPID, GRAV ZC000070
COMMON /ZDATA/ IZ, IZREL, CPUREM, CPUELA, ILCPU, INCPU, ZC000080
& NENK, KNAME, MEKKG, NCOND, KCOND, DOUBLE, ELSTIC, ABORT, ZC000090
& NNODE, NDOF, NCOND, NFREE, NREST, NNODES, NCOOS, ZC000100
& NMAI, NEMLT, NMASS, ZC000110
& NLOAD, NSOLN, ZC000120
& NAMELD, NELD, ZC000150
C IZID, IZIDOF, IZICORD, IZCOS, IZCONST, IZJFLG, IZJCOS, ZC000140
& IZMAT, IZELE, ZC000150
& IZIELD, IZELD, ZC000160
& IZKE, IZLN, IZSTIF, IZHO, IZKEKG, IZLMKG, ZC000170
& IZLNASS, IZLNEMS, IZNDAT, IZDAMP, IZKDOT, IZKG, IZMKG, ZC000180
& IZLOAD, IZDISP, IZVEL, IZACC, ZC000190
& IZDOLA, IZDISP, IZVEL, IZDACC, ZC000200
& IZAGTK, IZAGTY, IZAGTZ, ZC000220
& IZDUMP, IZPUB, IZAN, IZAR, ZC000250
C FMASS, FDAMP, TUNIT, ZC000240
& EIE, ESE, PSE, EKE, EDO, EDUMMY, ZC000250
& SUMRC(6), GROUND(9), INC, ZC000270
& EDUMMY(500) ZC000280
----- END BLOCK - ZCOMN1 ----- ZC000500
    
```

#### FILE: ZCOMN2 COPY

```

----- BEGIN BLOCK - ZCOMN2 ----- C ZC000010
PARAMETER (MAXZ=500000, MAXDZ=MAXZ/2) C ZC000020
COMMON /ZDATA/ ZCOMN2 ZC000070
DIMENSION NZ(MAXZ), DZ(MAXZ/2) ZC000090
DOUBLE PRECISION DZ ZC000100
EQUIVALENCE (Z(1), NZ(1), DZ(1)) C ZC000110
----- END BLOCK - ZCOMN2 ----- C ZC000120
    
```

#### FILE: ZCOMN3 COPY

```

----- BEGIN BLOCK - ZCOMN3 ----- ZC000010
DATA LZDATA/500/ ZC000020
----- VARIABLES IN COMMON ----- ZC000050
C TITLE = USER INPUT TITLES DESCRIBING STRUCTURE AND SOLUTION ZC000060
C IZ = NEXT AVAILABLE LOCATION IN LINEAR ARRAY Z ZC000090
C IZREL = VALUE OF IZ IF STORAGE FOR A SOLUTION IS RELEASED ZC000060
C BUG = FLAG, IF TRUE, DETAILED OUTPUT IS PRINTED FOR DEBUGGING ZC000070
C NCOND = FLAG, IF TRUE, MASS HAS 'NOT' BEEN CONDENSED OUT ZC000080
C NNODE = NUMBER OF NODES ZC000090
C NDOF = TOTAL NUMBER OF DEGREES OF FREEDOM ZC000100
C NCOND = NUMBER OF DOF TO BE CONDENSED OUT ZC000120
C NFREE = NUMBER OF FREE DOF ZC000150
C NREST = NUMBER OF RESTRAINED DOF ZC000140
C MAXNOD = MAXIMUM NUMBER OF NODES INPUT ZC000150
C NMAI = NUMBER OF MATERIAL PROPERTIES ZC000160
C NEMLT = NUMBER OF ELEMENTS ZC000170
C NLOAD = NUMBER OF LOADING CASES ZC000180
C NSOLN = SOLUTION NUMBER ZC000190
C NAMEOF = MAXIMUM NUMBER OF ELEMENT DOF ZC000200
C NDI = MAIN DIAGONAL ADDRESSES FOR AN UPPER TRIANGULAR STIFFNESS ZC000210
C NCOOS = NUMBER OF JOINT DIRECTION COSINES ZC000250
C NAMELD = MAXIMUM NUMBER OF ELEMENT LOADS ZC000240
C NELD = NUMBER OF ELEMENT LOADS ZC000250
C ..... ALL VARIABLES BEGINNING WITH IZ ARE THE ABSOLUTE ADDRESS ZC000270
..... IN THE LINEAR ARRAY FOR THE ____ DATA. ZC000280
C IZID = EXTERNAL JOINT NUMBERS ZC000290
C IZIDOF = DEGREE OF FREEDOM MATRIX FOR JOINT DOF'S ZC000500
C IZICORD = MATRIX OF JOINT COORD'S ZC000510
C IZCOS = MATRIX OF JOINT DIRECTION COSINES ZC000520
C IZCONST = MATRIX OF JOINT CONSTRAINT COEFF ZC000550
C IZMAT = MATERIAL DATA ZC000550
C IZELE = ELEMENT DATA ZC000560
C IZJFLG = MATRIX OF JOINT DOF FLAGS (RELEASE CONSTRAIN CONDENSE ELEM.) ZC000570
C IZJCOS = MATRIX OF JOINT COSINE ID NUMBERS ZC000580
    
```

```

C IZIE = ADDRESS OF ELEMENT STIFFNESS ZC000590
C IZLN = ADDRESS OF ELEMENT GLOBAL TO LOCAL MAPPING MATRIX ZC000600
C IZKEKG = ADDRESS OF ELEMENT GEOMETRIC STIFFNESS ZC000610
C IZLMKG = ADDRESS OF ELEMENT KG GLOBAL TO LOCAL MAPPING MATRIX ZC000620
C IZSTIF = GLOBAL STIFFNESS ZC000650
C IZLOAD = ADDRESS OF MAIN DIAGONAL STIFFNESS TERMS ZC000640
C IZDISP = DISPLACEMENT ZC000650
C IZIELD = INTEGER ELEMENT LOAD DATA ZC000670
C IZIELD = REAL ELEMENT LOAD DATA ZC000680
C IZLOAD = TOTAL LOAD ZC000690
C IZDISP = TOTAL DISPLACEMENT ZC000510
C IZVEL = TOTAL VELOCITY ZC000520
C IZACC = TOTAL ACCELERATION ZC000550
C IZDOLA = INCREMENTAL LOAD ZC000560
C IZDOSP = INCREMENTAL DISPLACEMENT ZC000570
C IZDVEL = INCREMENTAL VELOCITY ZC000580
C IZDACC = INCREMENTAL ACCELERATION ZC000590
C IZAGTK = TRANSLATIONAL GROUND ACCELERATION - X DIRECTION ZC000610
C IZAGTY = TRANSLATIONAL GROUND ACCELERATION - Y DIRECTION ZC000620
C IZAGTZ = TRANSLATIONAL GROUND ACCELERATION - Z DIRECTION ZC000630
C IZPUB = UNBALANCED FORCE VECTOR ZC000640
C IZR = TEMPORARY VECTOR ZC000660
C IZR = TEMPORARY VECTOR ZC000670
C FDAMP = DAMPING TYPE ZC000690
C FMASS = MASS TYPE ZC000700
C TUNIT = UNIT # FOR PRINTING DATA TO AN OUTPUT FILE ZC000710
----- END COMMON BLOCK - ZCOMN ----- ZC000750
    
```

### B. PROGRAM INRESB-3D-SUP

#### FILE: INRESB FORTRAN

```

===== CFEM00010
C CFEM00020
C PROGRAM INRESB CFEM00050
C CFEM00090
C===== CFEM00050
C NOTE: USE IBM FORTV52 COMPILER OPTION AUTOOBL(DBLPAD) CFEM00060
C TO COMPILE THIS PROGRAM IN DOUBLE PRECISION CFEM00070
C===== CFEM00090
C NOTE: USE IBM FORTV52 COMPILER OPTION OPT(2) CFEM0100
C TO OPTIMIZE THE CODE FOR FASTER EXECUTION CFEM0110
C===== CFEM0120
CHARACTER*80 OPTION, INPUT, BLANK CFEM0140
CHARACTER*80 TIME, DATEI CFEM0150
CHARACTER*1 CHR(0:25), NAME CFEM0160
LOGICAL TEST, BTEST, HEAD, AXIAL CFEM0170
INCLUDE (ZCOMN1) CFEM0180
INCLUDE (ZCOMN2) CFEM0190
DATA CHR/'A','B','C','D','E','F','G','H','I','J','K','L','M', CFEM0200
& 'N','O','P','Q','R','S','T','U','V','W','X','Y','Z' CFEM0210
C CFEM0220
C===== CFEM0250
C===== CFEM0260
CPUREM=0 CFEM0270
CPUELA=0 CALL CPUTIM, CPUREM, CPUELA CFEM0280
ITLCPUS=CPUREM CFEM0500
C===== CFEM0510
C===== CFEM0520
C===== CFEM0550
C===== CFEM0560
ICPU=0 CFEM0570
C===== CFEM0580
C===== CFEM0590
C===== CFEM0600
C===== CFEM0610
C===== CFEM0620
C===== CFEM0630
C===== CFEM0640
C===== CFEM0650
C===== CFEM0660
C===== CFEM0670
C===== CFEM0680
C===== CFEM0690
C===== CFEM0700
C===== CFEM0710
C===== CFEM0720
C===== CFEM0730
C===== CFEM0740
C===== CFEM0750
C===== CFEM0760
C===== CFEM0770
C===== CFEM0780
C===== CFEM0790
C===== CFEM0800
C===== CFEM0810
C===== CFEM0820
C===== CFEM0830
C===== CFEM0840
C===== CFEM0850
C===== CFEM0860
C===== CFEM0870
C===== CFEM0880
C===== CFEM0890
C===== CFEM0900
C===== CFEM0910
C===== CFEM0920
C===== CFEM0930
C===== CFEM0940
C===== CFEM0950
C===== CFEM0960
C===== CFEM0970
C===== CFEM0980
C===== CFEM0990
C===== CFEM1000
    
```

```

DOUBLE=.FALSE.
IBUG=0
MAXDEF=24
MOKI=.FALSE.
DO 1 I=2,(NAMEDEF+1)
1 MOKI=MOKI-1+(I-1)
IZ=0

20 READS,* ,END=1000) OPTION
RATIZ=100.*REAL(IZ)/REAL(MANZ)

C=====
C== DEFINE THE STRUCTURE ==
C=====
IF (INDEX(OPTION,'STR').NE.0) THEN
  ABORT=.FALSE.
  CALL COMPT(I,LZDATA)
  GRAV=586.4
  READ (5,* ,END=1000) TITLE(1)
  CALL TIME(TIME1)
  CALL DATE(DATE1)
  WRITE (TITLE(1),80),45) TIME1,DATE1
  RATIZ=100.*REAL(IZ)/REAL(MANZ)
  WRITE (1,52) 'BUILDING STRUCTURAL MODEL -----'
  &
  &
  WRITE (1,51) TITLE(1X:1:70)
  ABORT=.FALSE.
  CALL STRUCT
  IZREL=IZ
  RATIZ=100.*REAL(IZ)/REAL(MANZ)
  CALL TIMEIT(CPU)
  TCPU=CPU+TCPU
  WRITE (6,55) IZ,RATIZ,CPU,TCPU

C=====
C== DUMP THE MEMORY ==
C=====
ELSE IF (INDEX(OPTION,'SOL').NE.0) THEN
  READ (5,* ,END=1000) TITLE(2)
  CALL TIME(TIME1)
  CALL DATE(DATE1)
  WRITE (TITLE(2),80),45) TIME1,DATE1
  WRITE (1,52) 'SOLVING STRUCTURAL MODEL -----'
  &
  &
  WRITE (1,51) TITLE(1X:1:70)
  WRITE (1,51) TITLE(2X:1:70)
  ABORT=.FALSE.
  CALL SOLN(OPTION)
  RATIZ=100.*REAL(IZ)/REAL(MANZ)
  CALL TIMEIT(CPU)
  TCPU=CPU+TCPU
  WRITE (6,55) IZ,RATIZ,CPU,TCPU

C=====
C== DUMP THE MEMORY ==
C=====
ELSE IF (INDEX(OPTION,'DUMP').NE.0) THEN
  WRITE (1,52) 'DUMPING MEMORY -----'
  &
  &
  WRITE (1,51) TITLE(1X:1:70)
  WRITE (1,51) TITLE(2X:1:70)
  CALL COMPMZ(NZ,DZ)
  RATIZ=100.*REAL(IZ)/REAL(MANZ)
  CALL TIMEIT(CPU)
  TCPU=CPU+TCPU
  WRITE (6,55) IZ,RATIZ,CPU,TCPU

C=====
C== STOP... END OF PROGRAM ==
C=====
ELSE IF (INDEX(OPTION,'STOP').NE.0) THEN
  WRITE (1,52) 'NORMAL STOP -----'
  &
  &
  STOP

C=====
C== READ RESULTS FROM INPUT FILE ==
C=====
ELSE IF (INDEX(OPTION,'READ').NE.0) THEN
  CALL GETINT(OPTION,'UNIT',LIMT,0.,TRUE,...TRUE)
  CALL GETINT(OPTION,'DNC',DNC,1.,TRUE,...FALSE)
  IF (LIMT.NE.0) THEN
    WRITE (1,52)
    &
    &
    'READING DATA FROM FILE -----',IZ,RATIZ
    IOPT=
    CALL COMDAT(IOPT,INRTE,TO,DT)
    GO TO 140
  ENDIF
  ENDIF
  RATIZ=100.*REAL(IZ)/REAL(MANZ)
  CALL TIMEIT(CPU)
  TCPU=CPU+TCPU
  WRITE (6,55) IZ,RATIZ,CPU,TCPU

C=====
C== SET BUG OPTION ==
C=====
ELSE IF (TEST(OPTION,'BUG',.FALSE.)) THEN
  CALL GETCHK(OPTION,'BUG',INPUT,.TRUE,...FALSE)
  IBUG=0
  WRITE (OPTION,160) INPUT(1:70)
  DO 150 I=0,25
    IF (TEST(INPUT,CHK(I),.FALSE.)) THEN
      IBUG=IBUG+1
    ENDIF
  ENDIF
  CONTINUE
  150 FORMAT ('BUG'/'A')
  160 WRITE (1,52) 'SET BUG OPTION: -----'
  &
  &
  WRITE (1,51) OPTION(1:70)
  WRITE (6,51) 'SET BUG OPTION: '
  WRITE (6,51) OPTION(1:70)

C=====
C== SET BUG OPTION ==
C=====
ELSE IF (INDEX(OPTION,'BUG').NE.0) THEN
  WRITE (1,51) 'SET BUG OPTION: '//OPTION(1:54)
  BUG=.TRUE
  IF (INDEX(OPTION,'NOBUG').NE.0) BUG=.FALSE.

C=====
C== RELEASE MEMORY FROM LAST SOLUTION ==
C=====
ELSE IF (INDEX(OPTION,'RELEASE').NE.0) THEN

```

```

FEM00660 WRITE (6,52)
FEM00660 WRITE (1,52) 'RELEASING MEMORY -----'
FEM00670 WRITE (6,52) 'RELEASING MEMORY -----'
FEM00680 IF (INDEX(OPTION,'ELEMENT').NE.0) THEN
FEM00690 WRITE (6,52) 'RESETTING ELEMENT FORCES -----'
FEM00700 WRITE (6,52)
FEM00710 DO 170 IELNO=1,NELMT
FEM00720 LSTTYP=0
FEM00730 HEAD=.FALSE.
FEM00740 CALL ELEM LIB
FEM00750 &
FEM00760 & IELNO,IELDOP,KDOOF,PGEOM,2 ,AXIAL,IZDOSP,IZDOLA,MSTOR)
FEM00770 ELSE
FEM00780 WRITE (6,52)
FEM00790 ENDOF
FEM00800 IZ=IZREL
FEM00810 IZACC=0
FEM00820 IZDACC=0
FEM00830 IZDOSP=0
FEM00840 IZDISP=0
FEM00850 IZDOLA=0
FEM00860 IZVEL=0
FEM00870 IZFL=0
FEM00880 IZLOAD=0
FEM00890 IZVEL=0
FEM00900 RATIZ=100.*REAL(IZ)/REAL(MANZ)
FEM00910 CALL TIMEIT(CPU)
FEM00920 TCPU=CPU+TCPU
FEM00930 WRITE (6,55) IZ,RATIZ,CPU,TCPU
FEM00940
FEM00950 C=====
FEM00960 C== DUMMY STATEMENTS DURING ABORT ==
FEM00970 C=====
FEM00980 ELSE IF (ABORT) THEN
FEM00990 GO TO 20
FEM01000
FEM01010 C=====
FEM01020 C== INVALID OPTION ==
FEM01030 C=====
FEM01040 ELSE
FEM01050 IF (TEST(OPTION,'MECHO',.FALSE.)) GO TO 20
FEM01060 IF (OPTION.EQ.BLANK) GO TO 20
FEM01070 WRITE (6,50) OPTION
FEM01080 WRITE (1,51) 'INVALID OPTION: '//OPTION(1:54)
FEM01090 ENDOF
FEM01100 GO TO 20
FEM01110
FEM01120 C=====
FEM01130 C== 45 FORMAT: TIME: 'A', DATE: 'A' ==
FEM01140 50 FORMAT (AL,' STRUCTURE: ','A',)
FEM01150 & IX,' SOLUTION:.....','A,/)
FEM01160 51 FORMAT (IX,A)
FEM01170 52 FORMAT (IX,' ',A5,' ',IZ,' IZ', MEM='F6.5,')
FEM01180 55 FORMAT (//
FEM01190 & IX,' ',55,' ',**//
FEM01200 & IX,' ',IZ,' IZ', MEM='F6.5,')
FEM01210 & IX,' ',55,' ',**//
FEM01220 & IX,' ',ELAPSED CPU TIME ',F8.2,' SEC -----'
FEM01230 & IX,' ',TOTAL CPU TIME ',F8.2,' SEC -----'
FEM01240 & IX,' ',55,' ',**//
FEM01250 50 FORMAT ('I INVALID OPTION: ','A)
FEM01260 510 FORMAT ('ZNRKX',I6,' ',IX,IP,G20.10,,G20.10)
FEM01270 1000 STOP
FEM01280 ENDOF
FEM01290 C=====
FEM01300 SUBROUTINE AVEACC(IOPT,BUG,DT,TO,TF,T,THETA,NEWKDY,
FEM01310 & LI,L2,L5,L6,L6,INDMAS,IND,INDS,INDKG,NDOF,NFREE,
FEM01320 & KGLDAD,KGFORM,
FEM01330 & A ,V ,D ,P ,
FEM01340 & DA ,DV ,DD ,DP ,MOK,
FEM01350 & MASS ,MOMASS,DAMP ,STIFF ,MD ,
FEM01360 & KG ,MOKG ,ACC ,GRAV ,
FEM01370 & S ,MDS ,Q ,R ,PBAR ,
FEM01380 & FOAMP,FMASS,CO,C1,C2,C3,C4,C5,C6,ALPHA,BETA,C10,C11,ABORT)
FEM01390 INTEGER FOAMP,FMASS
FEM01400 REAL MASS,KG
FEM01410 LOGICAL BUG,NEWKDY,ABORT
FEM01420 LOGICAL BIEST
FEM01430 DIMENSION A(NDOF),V(NDOF),D(NDOF),D(NDOF),DV(NDOF),DD(NDOF)
FEM01440 DIMENSION P(NDOF),DP(NDOF),MOK(2*NDOF)
FEM01450 DIMENSION PBAR(5,1),QLS(1),R(5,1)
FEM01460 DIMENSION MOMASS(NDOF+1),MASS(INDMAS)
FEM01470 DIMENSION MOKG(NDOF+1) ,KG(INDKG)
FEM01480 DIMENSION MOK(NDOF+1) ,STIFF(DMD)
FEM01490 DIMENSION MDS(NDOF+1) ,SK(INDS) ,DAMP(5)
FEM01500
FEM01510 C=====
FEM01520 C== DETERMINE THE RESPONSE AT TIME DT*2 ==
FEM01530 C=====
FEM01540 THETA=2.0
FEM01550 CALL ILMACC(IOPT,BUG,THOOT,TO,TF,T,THETA,NEWKDY,
FEM01560 & LI,L2,L5,L6,L6,INDMAS,IND,INDS,INDKG,NDOF,NFREE,
FEM01570 & KGLDAD,KGFORM,
FEM01580 & A ,V ,D ,P ,
FEM01590 & DA ,DV ,DD ,DP ,MOK,
FEM01600 & MASS ,MOMASS,DAMP ,STIFF ,MD ,
FEM01610 & KG ,MOKG ,ACC ,GRAV ,
FEM01620 & S ,MDS ,Q ,R ,PBAR ,
FEM01630 & FOAMP,FMASS,CO,C1,C2,C3,C4,C5,C6,ALPHA,BETA,C10,C11,ABORT)
FEM01640
FEM01650 C=====
FEM01660 IF (IOPT.NE.2) RETURN
FEM01670 C=====
FEM01680 C== DETERMINE ACCELERATION, VELOCITY AND DISPLACEMENT AT TIME DT ==
FEM01690 C=====
FEM01700 DA = INCREMENTAL ACCELERATION BETWEEN TIMES T AND T+DT
FEM01710 DV = INCREMENTAL VELOCITY BETWEEN TIMES T AND T+DT
FEM01720 DD = INCREMENTAL DISPLACEMENT BETWEEN TIMES T AND T+DT
FEM01730
FEM01740 DO 270 I=1,5,4
FEM01750 DSP2DT=DD(I)
FEM01760 VEL2DT=DV(I)
FEM01770 ACC2DT=DA(I)
FEM01780 IF (BUG) WRITE (6,271) I,DSP2DT,VEL2DT,ACC2DT
FEM01790 DA(I)=ACC2DT/2.00
FEM01800 DV(I)=(DA(I)+ACC2DT)*DT/4.
FEM01810 DD(I)=DV(I)*DT+(6.00*DA(I)+ACC2DT)*DT*DT/12.
FEM01820 271 FORMAT (' D'/'I6,' AT T+ZDT, DSP',IP,G14.6,' VEL',G14.6,
FEM01830 & ACC',G14.6)
FEM01840
FEM01850 C=====
FEM01860 C== RETURN ==
FEM01870 RETURN
FEM01880
FEM01890 C=====
FEM01900 C== END ==
FEM01910 END
FEM01920
FEM01930 C=====
FEM01940 =====BNL00020

```





```

10          VZ(I)=VZ(I)/AVZ
C          ENDIF
          RETURN
          END
-----
C - DIRECTION OF LOADING -----
C P = CURRENT LOAD
C PL = LAST LOAD
C D = CURRENT DISPLACEMENT
C DIR = CURRENT DIRECTION
C DIR=1, POSITIVE LOADING
C DIR=2, POSITIVE UNLOADING
C DIR=3, NEGATIVE LOADING
C DIR=4, NEGATIVE UNLOADING
C DIRL = LAST DIRECTION
C VEL = PRODUCT OF LAST AND CURRENT VELOCITIES
SUBROUTINE DIRECT(DIR,DIRL,P,PL,VEL)
IMPLICIT REAL(A-H,O-Z)
IMPLICIT INTEGER(I-N)
INTEGER DIR,DIRL
LOGICAL BTEST
IF (P.GT.0) THEN
  IF (P.GT.PL .AND. PL.GT.0) THEN
    DIRL=1
  ELSE IF (P.GT.PL .AND. PL.LT.0) THEN
    DIRL=4
  ELSE IF (P.LT.0) THEN
    DIRL=2
  ELSE
    DIRL=DIR
  ENDIF
ELSE IF (P.LT.0) THEN
  IF (P.LT.PL .AND. PL.LT.0) THEN
    DIRL=1
  ELSE IF (P.LT.PL .AND. PL.GT.0) THEN
    DIRL=2
  ELSE IF (P.GT.0) THEN
    DIRL=4
  ELSE
    DIRL=DIR
  ENDIF
IF (PL.LT.0) THEN
  DIRL=2
ELSE IF (PL.GT.0) THEN
  DIRL=4
ELSE
  DIRL=DIR
ENDIF
IF (DIRL.EQ.1 .OR. DIRL.EQ.0) THEN
  IF (VEL.GT.0) THEN
    DIR=1
  ELSE
    DIR=2
  ENDIF
ELSE IF (DIRL.EQ.2) THEN
  IF (VEL.GT.0) THEN
    DIR=3
  ELSE IF (P.LT.0) THEN
    DIR=4
  ELSE IF (DIRL.EQ.4) THEN
    IF (VEL.GT.0) THEN
      DIR=4
    ELSE
      DIR=1
    ENDIF
  ELSE
    DIR=5
  ENDIF
ENDIF
WRITE (6,5)
5   FORMAT('X','ROR IN SUBROUTINE DIRECT, DIRL=ME, 1,2,3,OR 4')
WRITE (6,10) DIR,DIRL,P,PL,VEL
ENDIF
IF (DIR.EQ.0) DIR=1
C   WRITE (6,10) DIR,DIRL,P,PL,VEL
10  FORMAT('X','** IN DIRECT ',1X,
& ' DIR=' ,1X, ' DIRL=' ,1X, ' P=' ,F8.5, ' PL=' ,F8.5, ' VEL=' ,F10.5)
RETURN
END
-----
SUBROUTINE DMPDAT(IOP7,IMRITE,TO,DT)
LOGICAL TEST,OPEN,FALSE,ANIAL
LOGICAL BTEST,FIRST
CHARACTER*40 OPTION
CHARACTER*80 NAME,DIR=2
CHARACTER*112 TITL(2)
CHARACTER*12 INAME
DIMENSION RINPUT(100)
DOUBLE PRECISION TEI,TSE,DSE
SAVE FIRST
INCLUDE (ZCONM)
C   GO TO (100,200,300,400),IOP7
C
C-----
C= READ DATA ID TO BE SAVED, AND INITIALIZE FILES ===
C-----
100 FIRST = .TRUE.
I2DIMP=I2
I2=I2+1
CRO00260 NWRITE=0
CRO00270 WRITE (6,109)
CRO00280 109 FORMAT (/,5X,' DATA WRITTEN TO FILES '//
CRO00290 & ' SX, '=====')
CRO00300 101 READ (5,*) OPTION,IDOF,IUNIT,IGEN,IIDOF,IUNIT
102 CONTINUE
C-----
C-----SET UP DOF DATA
IF (TEST(OPTION,'DOF',.FALSE.)) THEN
  WRITE (6,110) 'DEGREE OF FREEDOM',IDOF,IUNIT
C-----
C----- CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (.OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C-----
C----- INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
N2(I2)=1
N2(I2+1)=IIDOF
N2(I2+2)=IUNIT
I2=I2+3
WRITE (IUNIT,120) TITL(1)(1:80),TITL(1)(81:)
WRITE (IUNIT,120) TITL(2)(1:80),TITL(2)(81:)
WRITE (IUNIT,150) 1,IDOF,DWRITE,TO,DT
C-----
C----- SET UP JOINT
ELSE IF (TEST(OPTION,'JOINT',.FALSE.)) THEN
  JOINT=IDOF
  JOINTI=QUICK(IIDOF,N2(I2ID),NMODE)-1
  IF (TEST(OPTION,'FK',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI)
    DIR='FK'
  ELSE IF (TEST(OPTION,'FV',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI+MAXMOD*1)
    DIR='FV'
  ELSE IF (TEST(OPTION,'FZ',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI+MAXMOD*2)
    DIR='FZ'
  ELSE IF (TEST(OPTION,'RV',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI+MAXMOD*3)
    DIR='RV'
  ELSE IF (TEST(OPTION,'RW',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI+MAXMOD*4)
    DIR='RW'
  ELSE IF (TEST(OPTION,'MZ',.FALSE.)) THEN
    IDOF=N2(I2IDOF+JOINTI+MAXMOD*5)
    DIR='MZ'
  ENDIF
  WRITE (6,110) 'DEGREE OF FREEDOM',IDOF,IUNIT,JOINT,DIR
C-----
C----- CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (.OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C-----
C----- INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
N2(I2)=1
N2(I2+1)=IIDOF
N2(I2+2)=IUNIT
I2=I2+3
WRITE (IUNIT,120) TITL(1)(1:80),TITL(1)(81:)
WRITE (IUNIT,120) TITL(2)(1:80),TITL(2)(81:)
WRITE (IUNIT,150) 1,IDOF,IWRITE,TO,DT,JOINT,DIR
C-----
C----- SET UP ELEMENT
ELSE IF (TEST(OPTION,'ELE',.FALSE.)) THEN
  WRITE (6,110) 'ELEMENT',IDOF,IUNIT
C-----
C----- CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (.OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C-----
C----- INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
N2(I2)=2
N2(I2+1)=IIDOF
N2(I2+2)=IUNIT
I2=I2+3
WRITE (IUNIT,120) TITL(1)(1:80),TITL(1)(81:)
WRITE (IUNIT,120) TITL(2)(1:80),TITL(2)(81:)
WRITE (IUNIT,150) 2,IDOF,IWRITE,TO,DT,IELTYP,'ELEMENT'
C-----
C----- SET UP ENERGY
ELSE IF (TEST(OPTION,'ENERGY',.FALSE.)) THEN
  WRITE (6,111) 'ENERGY BALANCE',IUNIT
C-----
C----- CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (.OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C-----
C----- INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
N2(I2)=5
N2(I2+1)=IIDOF
N2(I2+2)=IUNIT
I2=I2+3
WRITE (IUNIT,120) TITL(1)(1:80),TITL(1)(81:)
WRITE (IUNIT,120) TITL(2)(1:80),TITL(2)(81:)
WRITE (IUNIT,150) 5,IDOF,IWRITE,TO,DT,0,'ENERGY'
C-----
C----- SET UP SUM OF REACTIONS
ELSE IF (TEST(OPTION,'SUMRC',.FALSE.)) THEN
  WRITE (6,111) 'SUM OF REACTIONS',IUNIT

```

```

WRITE (6,111) 'SUMMATION OF REACTIONS',IUNIT
C
C CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C
C INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
NZ(I2)=4
NZ(I2+1)=0
NZ(I2+2)=IUNIT
I2=I2+5
WRITE (IUNIT,I20) TITLE(1X:80),TITLE(1X:81:)
WRITE (IUNIT,I20) TITLE(2X:1:80),TITLE(2X:81:)
WRITE (IUNIT,I50) 4,IDOF,WRITE,TO,DT,0,'SUMRCT'
C
C SET UP SUM OF REACTIONS
ELSE IF (TEST(OPTION,'GROUND',FALSE)) THEN
  WRITE (6,111) 'GROUND MOTION',IUNIT
C
C CHECK FILE STATUS
INQUIRE (UNIT=IUNIT,OPENED=OPEN)
IF (OPEN) THEN
  WRITE (6,105)
ELSE
  OPEN (UNIT=IUNIT)
ENDIF
C
C INITIALIZE DATA AND FILE
NWRITE=NWRITE+1
NZ(I2)=5
NZ(I2+1)=0
NZ(I2+2)=IUNIT
I2=I2+5
WRITE (IUNIT,I20) TITLE(1X:80),TITLE(1X:81:)
WRITE (IUNIT,I20) TITLE(2X:1:80),TITLE(2X:81:)
WRITE (IUNIT,I50) 5,IDOF,WRITE,TO,DT,0,'GROUND'
C
ELSE IF (TEST(OPTION,'END',FALSE)) THEN
  NZ(I2DUMP)=NWRITE
  RETURN
ELSE
  WRITE (6,140) OPTION
  GO TO 101
ENDIF
C
C..... GENERATE LOADS
IF (IGEN.NE.0) THEN
  IGEN=IGEN+1
  IDOF=IDOF + IDOF
  IUNIT=IUNIT + IUNIT
  GO TO 102
ENDIF
GO TO 101
C
C 105 FORMAT (SM,'FILE IS ALREADY OPENED, WRITE IS ABORTED',10X)**
110 FORMAT (SM,A,' * IS, IS WRITTEN TO UNIT #,IS.,',JOINT,'.IS,
&
& DIRECTION: ',A)
111 FORMAT (SM,A,' IS WRITTEN TO UNIT #,IS )
120 FORMAT (A)
130 FORMAT (S10,IP,2G15.5,OP,IX,16,A)
140 FORMAT (SM,'INVALID INPUT: ',A,', INPUT IS SKIPPED...')
C
C=====
C= WRITE DATA TO FILES ===
C=====
C
200 NUMB=NZ(I2DUMP)
DO 250 I=1,NUMB
  II=I2DUMP+S*(I-1)+1
  ITYPE=NZ(I2)
  IDOF=NZ(I2+1)
  IUNIT=NZ(I2+2)
  IF (ITYPE.EQ.1) THEN
    J=IDOF-1
    IF (IZVEL.EQ.0 .OR. IZACC.EQ.0) THEN
      WRITE (IUNIT,210) Z(I2LOAD+J),Z(I2DISP+J),0,0
    ELSE
      WRITE (IUNIT,210) Z(I2LOAD+J),Z(I2DISP+J),
&
& Z(I2VEL+J),Z(I2ACC+J)
    ENDIF
  ELSE IF (ITYPE.EQ.2) THEN
    I7=
    IELNO=IDOF
    LASTVP=0
    FALSE=.FALSE.
    CALL ELEMIB
    &
    & (I7, LASTVP, FIRST, IREL, FIRST, NAME, ESE, EPSE, DAMAGE,
&
& IELNO, IELDOF, KGDOF, PSEOM, RINPUT, ANIAL, IZDOSP, IZDOLA, NSTOR)
  ELSE IF (ITYPE.EQ.3) THEN
    DIFP=EIE-ESE-EKE-PSE-EDD
    IF (EIE.NE.0) THEN
      RE=DIFP/EIE * 100
    ELSE
      IF (DIFP.NE.0) RE=100.00
      IF (DIFP.EQ.0) RE= 0.00
    ENDIF
    WRITE (IUNIT,210) EIE, ESE, EKE, PSE, EDD, RE
  ELSE IF (ITYPE.EQ.4) THEN
    WRITE (IUNIT,210) SUMRCT
  ELSE IF (ITYPE.EQ.5) THEN
    WRITE (IUNIT,210) GROUND
  ENDIF
250 CONTINUE
210 FORMAT (IP,2G15.5)
FIRST=.FALSE.
RETURN
C
C=====
C= CLOSE DATA FILES ===
C=====
C
300 NUMB=NZ(I2DUMP)
DO 350 I=1,NUMB
  II=I2DUMP+S*(I-1)+1
  IUNIT=NZ(I2+2)
  CLOSE(UNIT=IUNIT)
350 CONTINUE
RETURN
C
DMP01490
DMP01500
DMP01510
DMP01520
DMP01530
DMP01540
DMP01550
DMP01560
DMP01570
DMP01580
DMP01590
DMP01600
DMP01610
DMP01620
DMP01630
DMP01640
DMP01650
DMP01660
DMP01670
DMP01680
DMP01690
DMP01700
DMP01710
DMP01720
DMP01730
DMP01740
DMP01750
DMP01760
DMP01770
DMP01780
DMP01790
DMP01800
DMP01810
DMP01820
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DMP01950
DMP01960
DMP01970
DMP01980
DMP01990
DMP02000
DMP02010
DMP02020
DMP02030
DMP02040
DMP02050
DMP02060
DMP02070
DMP02080
DMP02090
DMP02100
DMP02110
DMP02120
DMP02130
DMP02140
DMP02150
DMP02160
DMP02170
DMP02180
DMP02190
DMP02200
DMP02210
DMP02220
DMP02230
DMP02240
DMP02250
DMP02260
DMP02270
DMP02280
DMP02290
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DMP02890
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DMP02950
DMP02960
DMP02970
DMP02980
DMP02990
DMP03000
DMP03010
DMP03020
DMP03030
DMP03040
DMP03050
DMP03060
DMP03070
DMP03080
DMP03090
DMP03100
DMP03110
DMP03120
DMP03130
DMP03140
DMP03150
DMP03160
DMP03170
DMP03180
DMP03190
DMP03200
DMP03210
DMP03220
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DMP03250
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DMP03950
DMP03960
DMP03970
DMP03980
DMP03990
C=====
C= READ DATA FROM FILE AND WRITE TO F106 ===
C=====
C
400 OPEN (UNIT=IUNIT)
  REINDX UNIT=IUNIT
  READ (IUNIT,I20,END=499) TITLE(1X:80),TITLE(1X:81:)
  READ (IUNIT,I20,END=499) TITLE(2X:1:80),TITLE(2X:81:)
  WRITE (6,405) TITLE(1),TITLE(2)
  405 FORMAT ('1 STRUCTURE.....: ',A,/,
&
& ' SOLUTION.....: ',A,/)
  READ (IUNIT,I51,END=499) ITYPE,IDOF,WRITE,TO,DT,ITEMP,INAME
  I51 FORMAT (S10,OP,2G15.5,OP,IX,16,A)
C
C DOF DATA
IF (ITYPE.EQ.1) THEN
  WRITE (6,450) IDOF,IUNIT,ITEMP,INAME
  ISTEP=IWRITE
  410 READ (IUNIT,*,END=440) RLOAD,DISP,VEL,ACC
  ISTEP=ISTEP+IWRITE
  T=TO-DT*ISTEP
  IF (MOD(ISTEP,INC).EQ.0)
    &
    & WRITE (6,460) ISTEP,T,RLOAD,DISP,VEL,ACC
  GO TO 410
ELSE IF (ITYPE.EQ.2) THEN
  IELNO=IDOF
  IELTYP=ITEMP
  WRITE (6,445) IELNO,IUNIT
C
C GET ELEMENT TYPE AND COMPARE WITH INPUT TYPE.....
IF (I2ELE.GT.0) THEN
  IC=NZ(I2ELE+IELNO)
ELSE
  IC=-1
ENDIF
IF (IC.GT.0 .AND. IC.LE.MAXZ) THEN
  IELTPO = NZ(IC)
ELSE
  IELTPO = -100
ENDIF
C
C CREATE DUMMY ELEMENT DIRECTORY IF INPUT TYPE IS DIFF
I2ELET=I2ELE
IF (IELTYP.NE.IELTPO) THEN
  CALL CSTROR,IELNO+2,0)
  I2ELE = I2+2
  NZ(I2ELE+IELNO) = I2ELE+IELNO+1
  NZ(I2ELE+IELNO+1)=IELTYP
ENDIF
IS=8
LASTVP=0
FALSE=.FALSE.
CALL ELEMIB
&
& (I7, LASTVP, FIRST, IREL, FIRST, NAME, ESE, EPSE, DAMAGE,
&
& IELNO, IELDOF, KGDOF, PSEOM, RINPUT, ANIAL, IZDOSP, IZDOLA, NSTOR)
C
C RESTORE OLD ELEMENT DIRECTORY
I2ELE=I2ELET
ELSE IF (ITYPE.EQ.5) THEN
  I7=0
  TSE=0.00
  DSE=0.00
  ESEM=0
  ESEM=0
  EKEEM=0
  PSEEM=0
  EDOM=0
  WRITE (6,455) IUNIT
  ISTEP=IWRITE
  450 READ (IUNIT,*,END=451) EIE, ESE,EKE, PSE, EDD, RE
  I7=I7+1
  TSE=TSE+ESE+EKE+PSE+EDD
  DSE=DSE+ABS(EIE-ESE-EKE-PSE-EDD)
  ESEM=AMMUL(SGNL(EIE),EIE),ESEM)
  ESEM=AMMUL(SGNL(ESE),ESEM)
  EKEEM=AMMUL(SGNL(EKE),EKEM)
  PSEEM=AMMUL(SGNL(PSE),PSEEM)
  EDOM=AMMUL(SGNL(EDD),EDDM)
  ISTEP=ISTEP+IWRITE
  T=TO-DT*ISTEP
  IF (MOD(ISTEP,INC).EQ.0)
    &
    & WRITE (6,459) ISTEP,T, EIE, ESE,EKE, PSE, EDD, RE
  GO TO 450
451 RE =200*PSE/(TSE+TSE)
  WRITE (6,458) ESEM,ESEM,PSEM,EDDM,RE
  GO TO 440
ELSE IF (ITYPE.EQ.4) THEN
  ISTEP=IWRITE
  455 READ (IUNIT,*,END=440) SUMRCT
  ISTEP=ISTEP+IWRITE
  T=TO-DT*ISTEP
  IF (MOD(ISTEP,INC).EQ.0)
    &
    & WRITE (6,460) ISTEP,T, SUMRCT
  GO TO 455
ELSE IF (ITYPE.EQ.5) THEN
  WRITE (6,457) IUNIT
  ISTEP=IWRITE
  456 READ (IUNIT,*,END=440) GROUND
  ISTEP=ISTEP+IWRITE
  T=TO-DT*ISTEP
  IF (MOD(ISTEP,INC).EQ.0)
    &
    & WRITE (6,461) ISTEP,T, GROUND
  GO TO 456
ENDIF
440 CLOSE (UNIT=IUNIT)
RETURN
C
499 CLOSE (UNIT=IUNIT)
WRITE (6,500) IUNIT
500 FORMAT (///10X,'PREMATURE END OF FILE, UNIT:',IS/,
&
& ' 10X,'READ COMMAND IS ABORTED'///)
RETURN
C
445 FORMAT (SM,'ELEMENT #,IS, IS READ FROM UNIT #,IS)
450 FORMAT (SM,'DEGREE OF FREEDOM #,IS, IS READ FROM UNIT #,IS,
&
& SM,'JOINT #,IS, DIRECTION: ',A2//
&
& SM,'STEP', TIME, LOAD
&
& SM,'DISPLACEMENT', VELOCITY, ACCELERATION)
455 FORMAT (SM,'ENERGY DATA IS READ FROM UNIT #,IS//
&
& SM,'STEP', TIME, INPUT
&
& SM,'ELASTIC STRAIN', KINETIC, PLASTIC STRAIN',
&
& SM,'CAMPINED', RELATIVE ERROR Z')

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456 FORMAT (5X,'SUMMATION OF REACTIONS ARE READ FROM UNIT #',I5//
& 6X,'STEP', TIME, FK
& 7X,'FV', FZ, NK
& 8X,'VY', NZ
457 FORMAT (5X,'GROUND MOTION IS READ FROM UNIT #',I5//
& 2X,'
& 1X,'ACCELERATION'
& 1X,'VELOCITY'
& 1X,'DISPLACEMENT'
& 2X,'STEP', TIME
& 3X,'GLOBAL X', GLOBAL Y, GLOBAL Z
& 3X,'GLOBAL X', GLOBAL Y, GLOBAL Z
& 3X,'GLOBAL X', GLOBAL Y, GLOBAL Z
458 FORMAT(25X,90X,'/10X,' MAXIMUM ',IP,5G15.5, /
& /25X,'GROSS RE: ',OP,F15.4,'X')
459 FORMAT(10,IP,6G15.5,OP,F15.4)
460 FORMAT(10,IP,7G15.5)
461 FORMAT(16,IP,10G12.4)
C
END
C
DUCTILITIES AND EXCURSION RATIOS
C
SUBROUTINE DNE(IOPT,U,E,DV,D,ESE,PSE,PSEOLD,CSE)
DIMENSION UC(5),EC(6),UC(5)
C
VARIABLES
C
UC(1) = DUCTILITY (I)
C
EC(1) = EXCURSION RATIO (I)
C
EC(1:5) = DUCTILITY (I) FOR THE CURRENT HALF CYCLE
C
DV = VEILD DISPLACEMENT
C
D = CURRENT DISPL
C
YSE = TOTAL STRAIN ENERGY
C
PSE = PLASTIC STRAIN ENERGY
C
ESE = ELASTIC STRAIN ENERGY
C
CSE = CONSTANT STRAIN ENERGY AT YIELD....
C
UC = CURRENT DUCTILITY
C
IF (IOPT.EQ.1) THEN
..... CALCULATE CURRENT DUCTILITIES .....
PSE=PSE-PSEOLD
IF (DV.NE.0) UC(1)=D/DV
IF (ESE.NE.0) UC(2)=(PSE/DSE + 1)
IF (CSE.NE.0) UC(3)=(PSE/CSE + 1)
UC(4)=MAX(UC(1),UC(2))
UC(5)=MAX(UC(2),UC(3))
UC(6)=MAX(UC(4),UC(5))
ELSE
..... CALCULATE EXCURSION RATIOS .....
DO 20 I=1,5
J=I+1
IF (EC(J).GT.1) EC(I) = EC(I) + EC(J) - 1
20 ENDF
RETURN
END
C
SUBROUTINE DYOLOC(OPT,BUG,N,NDOF,MAIN,T,TL,ACCEL,Z,TO,OT,GRAV,
& NAXO,NDICE,COSINE,DOF,JTFLG,JTICS,NCOS,
& TX,TY,TZ,MASS,MO,DMD,A,MC,P,GA,GAT)
DIMENSION COSINE(3,3),NDICE(5),IDOF(NAXO,6)
DIMENSION JTFLG(NAXO),JTICS(NAXO)
DIMENSION TX(N),TY(N),TZ(N),AK(N),PK(NDF)
DIMENSION VC(5),VZ(5),VX(5),MDC(NDF+1),GAC(5),GAT(5)
REAL MASS(20),MDC(NDF,5)
CHARACTER*80 FORMAT(2),ATTITLE(2)
LOGICAL FMT,ECHO,BUG,PRINT,REHND
LOGICAL BTST
ACCELZ=0
C
GO TO (100,200) IOPT
C
C=====
C INPUT ACCELERATIONS ===
C=====
100 CONTINUE
C----- ZERO GLOBAL BASE ACCELERATIONS
DO 101 I=1,N
TK(I)=0
TV(I)=0
TZ(I)=0
101
C----- INPUT NUMBER OF ACCEL, AMP, FACTOR SCALE, AND TIME INCREMENT
READ (5,*) NA,ASCALE,TO,DT,PRINT
C----- INPUT DIRECTION VECTORS V1 AND V2
READ (5,*) V1,V2
IF (BUG) WRITE (6,29) 'INPUT- V1:',V1,' V2:',V2
C----- CALCULATE VS = V1 X V2
CALL CROSS(VS,V1,V2,0)
IF (BUG) WRITE (6,29) 'VS=V1XV2: V1:',V1,' V2:',V2,' VS:',VS
C----- CALCULATE VZ = VS X V1, AND NORMALIZE ALL VECTORS...
CALL CROSS(VZ,VS,V1,1)
IF (BUG) WRITE (6,29) 'VZ=VSXV1: V1:',V1,' V2:',V2,' VS:',VS
C
IF (BUG) WRITE (6,29) 'V1:',V1,' V2:',V2,' VS:',VS
29 FORMAT(5X,5,'A,5S,F9.5,' I',SP,F9.5,' J',F9.5,' K ',SS)
C----- INPUT INDIVIDUAL ACCELEROGRAMS
DO 50 I=1,NA
READ (5,*) IN,NPTS,DIRR,FMT,ECHO,REHND
NPTS=MIN(NPTS,N)
IF (REHND.AND. IN.NE.5) REHND (IN)
C
IF (FMT) THEN
READ (5,91) FORMAT(1),FORMAT(2)
READ (IN,FORMAT(1)) ATITLE(1),ATTITLE(2)
ELSE
READ (IN,91) ATTITLE(1),ATTITLE(2)
ENDIF
C
IF (DIRR.EQ.1 .AND. DIRR.LE.5) THEN
WRITE (6,10) I,IN,ATTITLE(1),ATTITLE(2),NPTS,TO,DT
10 FORMAT (/5X,' GROUND ACCELERATION RECORD ' /
& 5X,' ===== ' /
& 5X,' INPUTTING TRANSLATIONAL ACCELERATION RECORD #',
& 12,' FROM UNIT: ',I4,'/5X,/,5X,A/
& 5X,' THE RECORD CONTAINS ',I6,' POINTS, ',
& 8 ' BEGINING AT TIME: ',IP,616.6,
& WITH A TIME INCREMENT OF: ',IP,616.6)
DYL00700
DYL00710
DYL00720
DYL00730
DYL00740
DYL00750
DYL00760
DYL00770
DYL00780
DYL00790
DYL00800
DYL00810
DYL00820
DYL00830
DYL00840
DYL00850
DYL00860
DYL00870
DYL00880
DYL00890
DYL00900
DYL00910
DYL00920
DYL00930
DYL00940
DYL00950
DYL00960
DYL00970
DYL00980
DYL00990
DYL01000
DYL01010
DYL01020
DYL01030
DYL01040
DYL01050
DYL01060
DYL01070
DYL01080
DYL01090
DYL01100
DYL01110
DYL01120
DYL01130
DYL01140
DYL01150
DYL01160
DYL01170
DYL01180
DYL01190
DYL01200
DYL01210
DYL01220
DYL01230
DYL01240
DYL01250
DYL01260
DYL01270
DYL01280
DYL01290
DYL01300
DYL01310
DYL01320
DYL01330
DYL01340
DYL01350
DYL01360
DYL01370
DYL01380
DYL01390
DYL01400
DYL01410
DYL01420
DYL01430
DYL01440
DYL01450
DYL01460
DYL01470
DYL01480
DYL01490
DYL01500
DYL01510
DYL01520
DYL01530
DYL01540
DYL01550
DYL01560
DYL01570
DYL01580
DYL01590
DYL01600
DYL01610
DYL01620
DYL01630
DYL01640
DYL01650
DYL01660
DYL01670
DYL01680
DYL01690
DYL01700
DYL01710
DYL01720
DYL01730
DYL01740
DYL01750
DYL01760
DYL01770
DYL01780
DYL01790
DYL01800
DYL01810
DYL01820
DYL01830
DYL01840
DYL01850
DYL01860
DYL01870
DYL01880
DYL01890
DYL01900
DYL01910
DYL01920
DYL01930
C=====
C----- CALCULATE MASS * COSINE MATRIX FOR EACH DOF...
C----- LOOP FOR DIRECTION - JDIR
DO 90 JDIR=1,5
C----- ZERO MC MATRIX AND TEMP COSINE MATRIX FOR JDIR
DO 40 I=1,NDOF
MCCI,JDIR=0
ACT=0
C----- CONSTRUCT COSINE MATRIX FOR JDIR
OMIT ALL DOF THAT ARE CONSTRAINED TO A MASTER DOF...
DO 50 NNODE=1,NMODE
ICOS=JICOS(NODE)
DO 50 K=1,3
IF (.NOT. BTST(JTFLG(NODE),K+1)) THEN
II=IDOF(NODE,K)
ACII=ACT*ICOS(JDIR,K,ICOS)
ENDIF
50 CONTINUE
C----- MULTIPLY MASS * COSINE MATRIX FOR JDIR
STORE IN MCCI,JDIR
DO 60 J=1,NDOF
MDC(MDK(J),J)=1
DO 60 I=1,J-1
MCCI,JDIR=MCCI,JDIR + MASS*(MDI-I) * ACJ
60 DO 70 I=2,NDOF
MDC(MDK(I),I)=1
MDC(MDK(I-1),MDC(I))=1
DO 70 J=1,I-1
MCCI,JDIR=MCCI,JDIR + MASS*(MDI-J) * ACJ
70
90 CONTINUE
C
IF (BUG) CALL MMATRC(MC,NDOF,3,'MASS*COSINE')
91 FORMAT (A)
92 FORMAT(5X,'DIRECTION OF ACCELERATION: ',
& 5X,SS,F9.5,' I',SP,F9.5,' J',F9.5,' K ',SS)
93 FORMAT (1X,IP,10G12.4)
94 FORMAT (/5X,' INPUT ACCELERATION: ',
& 8 ' (g)'s)
& / (1X,IP,10G12.4)
C=====
```

```

C= INITIAL GROUND ACCELERATION ==
=====
IF (T.GE.TO .AND. T.LE.NPOT) THEN
  I=(T-TO)/DT +1
  R=(T-TO-T)/DT
  GAT(1)=TK(I)*R
  GAT(2)=TK(I)*R
  GAT(3)=TZ(I)*R
  IF (J.LE.N .AND. R.NE.1) THEN
    GAT(1)=GAT(1) + (1-R)*TK(J)
    GAT(2)=GAT(2) + (1-R)*TK(J)
    GAT(3)=GAT(3) + (1-R)*TZ(J)
  ENDIF
ELSE
  GAT(1)=0
  GAT(2)=0
  GAT(3)=0
ENDIF
GAT(1)=GAT(1)*GRAV
GAT(2)=GAT(2)*GRAV
GAT(3)=GAT(3)*GRAV
IF (BUG) WRITE (6,9279) T,TL,ACCELZ,GAT(1),GAT(2),GAT(3)
RETURN

C
=====
C= DETERMIN INCREMENTAL ACCELERATIONS ==
=====
DO 201 CONTINUE
C----- DETERMINE THE INCREMENTAL ACCELERATION BETWEEN TIME T AND TL
201 GAK(I)=0
  I=1
  DT=TO-T
C..... CURRENT ACCELERATION
  IF (T.GE.TO .AND. T.LE.NPOT) THEN
    I=(T-TO)/DT +1
    R=(T-TO-T)/DT
    GAK(1)=TK(I)*R
    GAK(2)=TK(I)*R
    GAK(3)=TZ(I)*R
    IF (J.LE.N .AND. R.NE.1) THEN
      GAK(1)=GAK(1) + (1-R)*TK(J)
      GAK(2)=GAK(2) + (1-R)*TK(J)
      GAK(3)=GAK(3) + (1-R)*TZ(J)
    ENDIF
    TKL=TK(I)
    TKJ=TK(J)
  ENDIF
C..... PREVIOUS ACCELERATION
  IF (TL.GE.TO .AND. TL.LE.NPOT) THEN
    I=(TL-TO)/DT +1
    J=1
    R=(TL-TO-TL)/DT
    GAK(1)=GAK(1)*R+TKL*(1-R)
    GAK(2)=GAK(2)*R+TKL*(1-R)
    GAK(3)=GAK(3)*R+TZL*(1-R)
    IF (J.LE.N .AND. R.NE.1) THEN
      GAK(1)=GAK(1) + (1-R)*TK(J)
      GAK(2)=GAK(2) + (1-R)*TK(J)
      GAK(3)=GAK(3) + (1-R)*TZ(J)
    ENDIF
    TKL=TK(I)
    TKJ=TK(J)
  ENDIF
C----- MULTIPLY B BY GRAV.
  DO 215 K=1,5
    215 GAK(K)=GAK(K)*GRAV
C----- CALC. ACCELERATION VECTOR = -MASS * COSINE * GROUND ACCELERATION
  DO 220 I=1,NDOF
    220 PK(I)=PK(I) - NK(I,K)*GAK(K)
C-----
  IF (BUG) WRITE (6,9279) T,TL,ACCELZ,GAK(1),GAK(2),GAK(3)
  9279 FORMAT(' DVLG= ',I,IP,G12.4,' TL= ',G12.4,' ACCELZ= ',G12.4,'
    & ' DVLG= ',X,IP,G12.4,' V= ',G12.4,' Z= ',G12.4)
  IF (BUG) CALL WMATRK(P,NDOF,1,'INCREMENTAL LOAD')
  RETURN
9280 FORMAT('SK,20K,' MAXIMUM AT TIME ',IX,
    & ' MINIMUM AT TIME AVERAGE STANDARD DEV.,IX,
    & ' RMS ')
9290 FORMAT('SK,A,IP,G15.5)
C-----
END
=====
SUBROUTINE ELELIB
  & IOPT,LISTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,DAMAGE,
  & TELNO,TELDOF,KDOF,PGEOM,RINPUT,AXIAL,IDISP,ILOAD,MSOR)
  LOGICAL ESE,ERR,FIRST,PRINT,HEAD,AXIAL,BTEST
  CHARACTER*90 NAME
  DIMENSION RINPUT(100)
C-----
  INCLUDE (ZCOMM)
  IOPT=IOPT
  IN = IZ
  IC = NZ(IZELE+TELNO)
  IZELE= IZELE
  IZELNO= IELNO
  IELTYP = NZ(IC)
  IF (LISTYP.EQ.IELTYP) THEN
    FIRST=.FALSE.
  ELSE
    FIRST=.TRUE.
    IF (HEAD) WRITE (6,506) TITLE(1),TITLE(2)
505 FORMAT('1 STRUCTURE.....',A,
    & ' SOLUTION.....',A,/)
  ENDIF
  MSOR=0
C-----
  IF (IELTYP.EQ.1) THEN
    IZLN=IC+9
    IZKE=IC+149+NZ(IC+133)
    IZLMG=IC+121
    IF (IOPT.NE.5) CALL ELE01
    & IOPT,UNIT,INC, FIRST, PRINT
    & NDOF,MLoad,MAKNOD,MAKODE,NCOS
    & NZ(IZID),NZ(IZIDOF),Z(IZCORD),Z(IZCOS),NZ(IZJCOS)
    & Z(IZCNST),Z(IZDISP),Z(IZLOAD),IREL,BUG
  ELSE
    IZLN=IC+155
    IELDOF=NZ(IC+1)
    IZLMG=IC+121
    IZKEG=IZKE+NZ(IC+120)
    KDOF = NZ(IC+119)
  ENDIF
  IF (IELTYP.EQ.2) THEN
    AXIAL=.FALSE.
    IZKE=IC+55+NZ(IC+12)
    IZLN=IC+40
  ELSE
    CALL ELE02
    & IOPT,UNIT,MAKNOD,MAKODE,NCOS
    & NZ(IZID),NZ(IZIDOF),Z(IZCORD),Z(IZCOS),NZ(IZJCOS)
    & Z(IZCNST),Z(IZDISP),Z(IZDVEL),Z(IZFUB),
    & IREL,BUG,IBUG,ACCEL,NZ(IZKDOT+1),
    & GRAV,PGEOM,ELSTIC,NAME,STEPID
    & TELNO,RINPUT,AXIAL,ESE,EPSE,INC
    & NZ(IC),NZ(IC+1),NZ(IC+2),NZ(IC+3),NZ(IC+4),
    & NZ(IC+5),NZ(IC+6),NZ(IC+7),NZ(IC+8),NZ(IC+9),
    & NZ(IC+10),NZ(IC+11),NZ(IC+12),NZ(IC+13),NZ(IC+14),
    & NZ(IC+15),NZ(IC+16),NZ(IC+17),NZ(IC+18),NZ(IC+19),
    & NZ(IC+20),NZ(IC+21),NZ(IC+22),NZ(IC+23),NZ(IC+24),
    & NZ(IC+25),NZ(IC+26),NZ(IC+27),NZ(IC+28),NZ(IC+29),
    & NZ(IC+30),NZ(IC+31),NZ(IC+32),NZ(IC+33),NZ(IC+34),
    & NZ(IC+35),NZ(IC+36),NZ(IC+37),NZ(IC+38),NZ(IC+39),
    & NZ(IC+40),NZ(IC+41),NZ(IC+42),NZ(IC+43),NZ(IC+44),
    & NZ(IC+45),NZ(IC+46),NZ(IC+47),NZ(IC+48),NZ(IC+49),
    & NZ(IC+50),NZ(IC+51),NZ(IC+52),NZ(IC+53),
    & NZ(IC+54),NZ(IC+55),NZ(IC+56),NZ(IC+57),
    & NZ(IC+58),NZ(IC+59),NZ(IC+60),NZ(IC+61),
    & NZ(IC+62),NZ(IC+63),NZ(IC+64),NZ(IC+65),
    & NZ(IC+66),NZ(IC+67),NZ(IC+68),NZ(IC+69),
    & NZ(IC+70),NZ(IC+71),NZ(IC+72),NZ(IC+73),
    & NZ(IC+74),NZ(IC+75),NZ(IC+76),NZ(IC+77),
    & NZ(IC+78),NZ(IC+79),NZ(IC+80),NZ(IC+81),
    & NZ(IC+82),NZ(IC+83),NZ(IC+84),NZ(IC+85),
    & NZ(IC+86),NZ(IC+87),NZ(IC+88),NZ(IC+89),
    & NZ(IC+90),NZ(IC+91),NZ(IC+92),NZ(IC+93),
    & NZ(IC+94),NZ(IC+95),NZ(IC+96),NZ(IC+97),
    & NZ(IC+98),NZ(IC+99),NZ(IC+100)
  ENDIF
  MSOR = NZ(IC+5)
  IELDOF=NZ(IC+1)
  IZLMG=0
  IZKEG=0
  KDOF = 0
  ELSE IF (IELTYP.EQ.5) THEN
    CALL ELE05
    & IOPT,UNIT,MAKNOD,MAKODE,NCOS
    & NZ(IZID),NZ(IZIDOF),Z(IZCORD),Z(IZCOS),NZ(IZJCOS)
    & Z(IZCNST),Z(IZDISP),Z(IZDVEL),Z(IZLOAD),Z(IZFUB)
    & IREL,BUG,IBUG,ACCEL,NZ(IZKDOT+1),
    & GRAV,PGEOM,ELSTIC,NAME,STEPID
    & TELNO,RINPUT,AXIAL,ESE,EPSE,INC
    & NZ(IC),NZ(IC+1),NZ(IC+2),NZ(IC+3),NZ(IC+4),
    & NZ(IC+5),NZ(IC+6),NZ(IC+7),NZ(IC+8),NZ(IC+9),
    & NZ(IC+10),NZ(IC+11),NZ(IC+12),NZ(IC+13),NZ(IC+14),
    & NZ(IC+15),NZ(IC+16),NZ(IC+17),NZ(IC+18),NZ(IC+19),
    & NZ(IC+20),NZ(IC+21),NZ(IC+22),NZ(IC+23),NZ(IC+24),
    & NZ(IC+25),NZ(IC+26),NZ(IC+27),NZ(IC+28),NZ(IC+29),
    & NZ(IC+30),NZ(IC+31),NZ(IC+32),NZ(IC+33),NZ(IC+34),
    & NZ(IC+35),NZ(IC+36),NZ(IC+37),NZ(IC+38),NZ(IC+39),
    & NZ(IC+40),NZ(IC+41),NZ(IC+42),NZ(IC+43),NZ(IC+44),
    & NZ(IC+45),NZ(IC+46),NZ(IC+47),NZ(IC+48),NZ(IC+49),
    & NZ(IC+50),NZ(IC+51),NZ(IC+52),NZ(IC+53),
    & NZ(IC+54),NZ(IC+55),NZ(IC+56),NZ(IC+57),
    & NZ(IC+58),NZ(IC+59),NZ(IC+60),NZ(IC+61),
    & NZ(IC+62),NZ(IC+63),NZ(IC+64),NZ(IC+65),
    & NZ(IC+66),NZ(IC+67),NZ(IC+68),NZ(IC+69),
    & NZ(IC+70),NZ(IC+71),NZ(IC+72),NZ(IC+73),
    & NZ(IC+74),NZ(IC+75),NZ(IC+76),NZ(IC+77),
    & NZ(IC+78),NZ(IC+79),NZ(IC+80),NZ(IC+81),
    & NZ(IC+82),NZ(IC+83),NZ(IC+84),NZ(IC+85),
    & NZ(IC+86),NZ(IC+87),NZ(IC+88),NZ(IC+89),
    & NZ(IC+90),NZ(IC+91),NZ(IC+92),NZ(IC+93),
    & NZ(IC+94),NZ(IC+95),NZ(IC+96),NZ(IC+97),
    & NZ(IC+98),NZ(IC+99),NZ(IC+100)
  ENDIF
  MSOR = NZ(IC+5)
  IELDOF=NZ(IC+1)
  IZLMG=54
  IZLMG=IC+58
  IZKEG=IC+167+NZ(IC+5) + NZ(IC+55)-1
  KDOF = NZ(IC+159)
  ELSE
    WRITE (6,10) IELNO
    ERR=.TRUE.
  10 FORMAT(' ELEMENT ',I6,' IS NOT AVAILABLE')
  ENDIF
  LISTYP=IELTYP
  IOPT=IOPT
  RETURN
END
=====
SUBROUTINE ELE04G,BK,NF,NELM,MAKELD,NELD,NDOF,MLoad,FORCE,IELD,
  & ELD,IDISP,ILOAD,NAME,TITLE,HEAD)
C-----
C NOTE ON ARGUMENTS: THE LOAD MATRIX FORCE IS PASSED FROM THE CALLING
C ROUTINE. FORCE IS EQUIVALENT TO THE Z MATRIX BY THE CALLING ROUTINE
C IE, Z(ILOAD)=FORCE(I,1), WHERE ILOAD IS THE OFFSET IN THE Z MATRIX.
C BOTH THE CALLING ROUTINE AND SUBROUTINE ELE_LIB USE THE Z MATRIX
C-----
  DIMENSION FORCE(NDOF,MLoad),IELD(5,MAKELD),ELDK(2,MAKELD)
  DIMENSION RINPUT(100)
  LOGICAL FIRST,HEAD,FALSE
  LOGICAL AXIAL,BUG
  LOGICAL BTEST
  CHARACTER*(*) TITLE(2)
  CHARACTER*(*) NAME
  CHARACTER*20 TYPE,DIRI
  CHARACTER*40 DIR
  CHARACTER*1 CK(6)
  FIRST=.TRUE.
  5 FORMAT('1 STRUCTURE.....',A,
    & ' SOLUTION.....',A,/)
  6 FORMAT('1 ELEMENT LOADS ',
    & ' *****')
  & IX,' LOAD TELE IGEN DIELE TYPE DIR VALUES....')
C-----
C= INPUT LOADING DATA ==
=====
N=0
  10 N=N+1
  IF (N.GT.MAKELD) GO TO 100
  20 READ (5,*) (IELD(I,N),I=1,4),TYPE,DIRI,ELDK(I,N)
  DIR=TYPE/DIRI
  IF (INDEX(DIR,'END').NE.0) GO TO 100
  NELD=N
  IF (FIRST) THEN
    IF (HEAD) WRITE (6,5) TITLE(1),TITLE(2)
    WRITE (6,6)
    FIRST=.FALSE.
  ENDIF
C-----
C----- PROCESS LOAD GROUPS AND READ ADDITIONAL INFO...
  IF (INDEX(DIR,'CONC').NE.0) THEN
    KOE=100
  ENDIF

```

```
J=2
BACKSPACE(5)
READ (5,*) (IELDX(N),I=1,4),TYPE,DIRI,(ELDX(N),I=1,4)
DIR=TYPE//DIRI
CALL CKRNK(ELDX(2),N),0,1,'DISTANCE')
ELSE IF (INDEX(DIR,'UNIF').NE.0) THEN
J=1
KODE=200
ELSE IF (INDEX(DIR,'VARR').NE.0) THEN
KODE=300
J=4
BACKSPACE(5)
READ (5,*) (IELDX(N),I=1,4),TYPE,DIRI,(ELDX(N),I=1,4)
DIR=TYPE//DIRI
CALL CKRNK(ELDX(5),N),0,1,'DISTANCE')
CALL CKRNK(ELDX(4),N),0,1,'DISTANCE')
ELSE IF (INDEX(DIR,'FEM').NE.0) THEN
KODE=400
J=12
BACKSPACE(5)
READ (5,*) (IELDX(N),I=1,4),TYPE,DIRI,(ELDX(N),I=1,4)
DIR=TYPE//DIRI
ELSE
WRITE(6,50) 'INVALID LOAD TYPE'
GO TO 20
ENDIF
IF (INDEX(DIR,'FX').NE.0) THEN
KODE=KODE+1
ELSE IF (INDEX(DIR,'FY').NE.0) THEN
KODE=KODE+2
ELSE IF (INDEX(DIR,'FZ').NE.0) THEN
KODE=KODE+3
ELSE IF (INDEX(DIR,'MX').NE.0) THEN
KODE=KODE+4
ELSE IF (INDEX(DIR,'MY').NE.0) THEN
KODE=KODE+5
ELSE IF (INDEX(DIR,'MZ').NE.0) THEN
KODE=KODE+6
ELSE IF (KODE.NE.400) THEN
WRITE(6,50) 'INVALID LOAD DIRECTION'
GO TO 20
ENDIF
IELDX(N)=KODE
WRITE(6,40) (IELDX(N),I=1,4),DIR,(ELDX(N),I=1,4)
GO TO 10
C
50 FORMAT ('A. --- LOAD IS SKIPPED')
1X,15,1X,A20,1P,6D14.6,/(4X,6D14.6)
40 FORMAT (1X,15,1X,A20,1P,6D14.6,/(4X,6D14.6)
C
RETURN IF NO ELEMENT LOADS WERE INPUT
100 IF (FIRST) RETURN
C
LOOP TO GENERATE MEMBER LOADS FOR EACH ELEMENT
IOP1=6
DO 101 IELNO=1,MELNT
FALSB=FALSE
101 CALL ELELBI
& IOP1,LSITYP,FALSB,IREL,FALSB,NAME,EESE,EPSE,DAMAGE,
& IELNO,IELDOF,KDOOF,PGEOM,RINPUT,AKIAL,IOISP,ILOAD,HSTOR)
C
PRINT LOADS AT EACH DOF
IF (BUG) THEN
NS=NDOF+5
DO 120 I=1,MLOAD
IF (MLOAD) WRITE (6,5) TITLE(1),TITLE(2)
WRITE (6,130) I
DO 120 I=1,NS,5
IS=MIN(I,NS)
DO 110 J=1,IS
K=J-1
CKX(K)=*
110 IF (.GT.NF) CKX(K)=**
WRITE (6,140) J,FORCE(J,L),CKX(J-1),J,I,IS
120 CONTINUE
ENDIF
150 FORMAT (' GLOBAL JOINT FORCES DUE TO ELEMENT LOADS ',5X,
' LOADING #',15,10X,
' NOTE: * DENOTES SUPPORT DISPLACEMENT')
&
& '*****'//
& 5X,5C,DOF,7X,LOAD,')//
140 FORMAT (5X,5COP,15,1P,6D14.6,A)
RETURN
END
C
SUBROUTINE ELE01
& IOP1,IMUNIT,INC,FIRST,PRINT
& NDOF,MLOAD,MANNO,MANNO,MANNO,NCOS,
& ID,IOOP,COORD,COSINE,JTCOS,
& CONST,DISPL,FORCE,IREL,BUG,
& IBUG,ACCEL,KGDATA,GRAV,PGEOM,
& HAMELD,HELD,IELD,NAME,
& STEPID,AKIAL,IELNO,RINPUT,
& EESE,EPSE,DAMAGE,
& IELTYP,IELDOF,PKG,IM,J,
& AI,AJ,C,S212,S22,S23,
& S22,RT,RT,FT,
& LM,CTS,CTE,BS,BE,
& D,NODEI,NODEJ,JOINTI,JOINTJ,
& REL,LENGTH,KDOOF,LKG,LKMG,
& ISE,ENGDAT,FMAX,MAT,SE,
& STIFF,
& FEM)
C
IMPLICIT REAL(A-H,O-Z)
LOGICAL ERR,FIRST,PRINT,BUG,FEMFLG,FALSB,AKIAL,BTEST
CHARACTER*80 NAME
CHARACTER*6 STEPID
CHARACTER*6 IREL
DIMENSION KGDATA(3)
DIMENSION IDOF(MANNO,6),COORD(MANNO,6),COSINE(3,MANNO)
DIMENSION CONST(MANNO,6),IX(MANNO)
DIMENSION ASAT(12,12),SAT(12,12),STIFF(156)
DIMENSION AC(12,12),SK(12,12),LAK(12),LAKG(12),FMAX(12)
DIMENSION CTS(3,3),CTE(3,3),COSLOC(5,5),VK(5),VCS(5),VZ(5)
DIMENSION BSC(3,3),BEC(3,3),SEC(15),ENGDAT(2)
DIMENSION RR(12),DISP(NDOF,MLOAD),F(12),RT(12),FT(12),FURCH(NDOF)
DIMENSION FORCE(NDOF,MLOAD),IELDX,HAMELD,ELDX(12,HAMELD)
DIMENSION ASAC(12,12),RINPUT(100),FEM(12,MLOAD),GFEM(12)
```

```
ELE00490 DIMENSION DUCT(3),EXDR(6)
ELE00500 DIMENSION V(12),VL(12)
ELE00510 REAL LX,LY,LZ,KI1Z,KJ1Z,KL1Z,KI1V,KJ1V,KL1V,KI1T,KJ1T,KL1T,VJ
ELE00520 REAL IX,IY,IZ,KI1Z,KJ1Z,KL1Z,KI1V,KJ1V,KL1V,KI1T,KJ1T,KL1T,VJ
ELE00530 INTEGER REL,REL
ELE00540 DIMENSION MUX(15)
ELE00550 DATA MUX(1,2,3,4,7,11,16,22,29,37,46,56,67,79)
ELE00560
ELE00570 C
ELE00580 C VARIABLES:
ELE00590
ELE00600 C----- GLOBAL VARIABLES
ELE00610 C IOP1 = 1, INITIALIZE BEAM COLUMN ELEMENT
ELE00620 C C = 2, CALCULATE GEOMETRIC STIFFNESS
ELE00630 C = 5, FORM STIFFNESS
ELE00640 C = 4, CALCULATE INCREMENTAL FORCES
ELE00650 C = 5, CALCULATE TOTAL FORCES AND ENERGIES
ELE00660 C IUNIT = OUTPUT FILE UNIT # FOR PRINTING OUTPUT
ELE00670 C ERR = ERR OR FLAG, IF AN ERR OR HAS OCCURRED, ERR=.TRUE.
ELE00680 C FIRST = FLAG, FIRST=.TRUE., PRINT HEADERS
ELE00690 C PRINT = FLAG, PRINT=.TRUE., PRINT DATA
ELE00700 C NDOF = # OF GLOBAL DOF
ELE00710 C MLOAD = # OF LOAD COMBINATIONS
ELE00720 C MANNO = # ROW DIMENSION OF NODE ARRAY
ELE00730 C NMODE = # OF NODES
ELE00740 C ID = ARRAY OF EXTERNAL NODE NUMBERS
ELE00750 C IDOF = ARRAY OF DEGREES OF FREEDOM
ELE00760 C COORD = ARRAY OF COORDINATES
ELE00770 C COSINE = ARRAY OF DIRECTION COSINES OF NODES
ELE00780 C CONST = ARRAY OF CONSTRAINT TRANSFORMATIONS
ELE00790 C DISPL = GLOBAL DISPLACEMENT MATRIX
ELE00800 C IZMAT = LOCATION OF MATERIAL DATA IN GLOBAL STORAGE VECTOR
ELE00810 C NAME = ELEMENT NAME
ELE00820 C IELNO = ELEMENT NUMBER
ELE00830 C RINPUT = INPUT DATA
ELE00840 C STIFF = OUTPUT ELEMENT STIFFNESS (UPPER TRIANGULAR FORM)
ELE00850 C LM = OUTPUT LOCAL TO GLOBAL STIFFNESS MAPPING MATRIX
ELE00860 C----- ELEMENT VARIABLES
ELE00870 C H,Q,A,I,AJ,C,BI,BJ,S22,S26,S212,S23,S25,S211,D
ELE00880 C = INDIVIDUAL TERMS IN THE ELEMENT STIFFNESS (S) MATRIX
ELE00890 C PKG = INPUT LOAD FOR FORMING GEOMETRIC STIFFNESS MATRIX...
ELE00900 C R = INCREMENTAL DISPLACEMENTS
ELE00910 C RT = TOTAL DISPLACEMENTS
ELE00920 C F = INCREMENTAL FORCES
ELE00930 C FT = TOTAL FORCES
ELE00940 C LM = LOCAL TO GLOBAL STIFFNESS MAPPING MATRIX
ELE00950 C CTE = LOCAL TO GLOBAL ROTATION MATRIX START
ELE00960 C BE = LOCAL TO GLOBAL ROTATED ECCENTRICITY/CONSTRAINT MATRIX END
ELE00970 C BS = LOCAL TO GLOBAL ROTATED ECCENTRICITY/CONSTRAINT MATRIX START
ELE00980 C BE = LOCAL TO GLOBAL ROTATED ECCENTRICITY/CONSTRAINT MATRIX END
ELE00990 C STIFF = ELEMENT STIFFNESS
ELE1000 C IELTYP = ELEMENT TYPE = ID
ELE10010 C X = EXTERNAL JOINT NUMBER, END I
ELE10020 C NODEJ = EXTERNAL JOINT NUMBER, END J
ELE10030 C JOINTI = INTERNAL JOINT NUMBER, END I
ELE10040 C JOINTJ = INTERNAL JOINT NUMBER, END J
ELE10050 C----- TEMPORARY VARIABLES
ELE10060 C VX = VECTOR DEFINING THE ELEMENT X AXIS
ELE10070 C VY = VECTOR DEFINING THE ELEMENT Y AXIS
ELE10080 C COSLOC = LOCAL COSINE MATRIX
ELE10090 C A = GLOBAL TO LOCAL FORCE TRANSFORMATION MATRIX
ELE10100 C S = ELEMENT STIFFNESS AT LOCAL COORD, AT ENDS OF FLEXIBLE PART
ELE10110 C SAT = PRODUCT OF S*A
ELE10120 C ASAT = PRODUCT OF A*SAT
ELE10130
ELE10140
ELE10150 C----- CHOOSE OPTION
ELE10160 IF (IOP1.LT.1 .OR. IOP1.GT.14)
ELE10170 & WRITE (6,*) 'INVALID OPTION IN ELE-01, IOP1=',IOP1
ELE10180
ELE10190 GO TO (100,200,500,400,500,600,700,800,900,1000,1100,1200,
ELE10200 & 1500,1+00),IOP1
ELE10210
ELE10220 C
ELE10230 C 100 CONTINUE
ELE10240
ELE10250 C----- ZERO STRAIN ENERGY
ELE10260 ENGDAT(1) = 0
ELE10270 ENGDAT(2) = 0
ELE10280
ELE10290 C
ELE10300 IF (BTEST(BUG,7) ) THEN
ELE10310 WRITE (6,*) NAME
ELE10320 CALL AMATRK(RINPUT,10,1,'RINPUT')
ELE10330
ELE10340 ENDF
ELE10350 C
ELE10360 C----- INTERPERATE INPUT DATA
ELE10370 IELTYP=1
ELE10380 NODEI = RINPUT( 1)
ELE10390 NODEJ = RINPUT( 2)
ELE10400 VK(1) = RINPUT( 3)
ELE10410 VK(2) = RINPUT( 5)
ELE10420 VK(3) = RINPUT( 6)
ELE10430 XS = RINPUT( 7)
ELE10440 ME = RINPUT( 8)
ELE10450 PKG = RINPUT( 9)
ELE10460 RELT = RINPUT(10)
ELE10470
ELE10480 C
ELE10490 GET INTERNAL NODE # ASSOCIATED WITH EXTERNAL NODE #'S
ELE10500 JOINTI=QUICK(NODEI,IM,NMODE)
ELE10510 JOINTJ=QUICK(NODEJ,IM,NMODE)
ELE10520
ELE10530 C----- PRINT DATA FOR PLOTTING
ELE10540 IF (BTEST(BUG,2)) THEN
ELE10550 WRITE(7,10) G,(COORD(JOINTJ,I),I=1,5),(COORD(JOINTI,J),J=1,5)
ELE10560 10 FORMAT (15,1P,6D12.4)
ELE10570 ENDF
ELE10580
ELE10590 C
ELE10600 C GET GLOBAL TO LOCAL TRANSFORMATION MATRIX
ELE10610
ELE10620 C----- DEFINE VECTOR X, LENGTH
ELE10630 VK(1)=COORD(JOINTJ,1)-COORD(JOINTI,1)
ELE10640 VK(2)=COORD(JOINTJ,2)-COORD(JOINTI,2)
ELE10650 VK(3)=COORD(JOINTJ,3)-COORD(JOINTI,3)
ELE10660 LENGTH=SQRT(VK(1)**2+VK(2)**2+VK(3)**2)+NS-ME
ELE10670 IF (LENGTH.LE.0) THEN
ELE10680 WRITE(6,101) IELNO,JOINTI,JOINTJ,LENGTH
ELE10690 101 FORMAT(1X,2X,'**'),ER, 'ROR - LENGTH IS LE 0',/
ELE10700 & 5X,'IELNO=',15,5X,'JOINTI=',15,5X,'JOINTJ=',15,
ELE10710 & 5X,'LENGTH',1P,6D14.6/
ELE10720 & 5X,'REVISE INPUT.....'//
ELE10730 LENGTH=1.0
ELE10740 ENDF
ELE10750 IF (BTEST(BUG,7) ) THEN
```

```

WRITE (6,*) 'JOINTS',JOINTI,JOINTJ
WRITE (6,*) 'VK',VK
WRITE (6,*) 'VW',VW
WRITE (6,*) 'LENGTH',LENGTH
ENDIF
C----- GET LOCAL TO GLOBAL TRANSFORMATION MATRICIES CT AND B
ICE=JTCOSK(JOINTI)
ICE=JTCOSK(JOINTJ)
CALL ROTMZY(VK,VW,COSINE(1,1,ICE),CTS,XS,0.0,0.0,BS,
& CONST(JOINTI,1),MAXMOD)
CALL ROTMZY(VK,VW,COSINE(1,1,ICE),CTE,XE,0.0,0.0,BE,
& CONST(JOINTJ,1),MAXMOD)
IF ( BTEST(18UG.7) ) THEN
CALL MMATRK CTS , 5, 5, 'CTS ' )
CALL MMATRK CTE , 5, 5, 'CTE ' )
ENDIF
C
C----- GET GLOBAL CONSTRAINT MATRIX BS, BE
C
C
IF ( BTEST(18UG.7) ) THEN
CALL MMATRK BS, 5, 5, 'BS ' )
CALL MMATRK BE, 5, 5, 'BE ' )
ENDIF
C
C----- ZERO MATRICIES
DO 40 I=1,12
FMATK(I)=0
F(I)=0
FT(I)=0
R(I)=0
RT(I)=0
DO 40 J=1,12
& K(I,J)=0
40 K(I,J)=0
C
C----- ASSEMBLE TRANSFORMATION MATRIX A
DO 50 I=1,5
DO 50 J=1,5
& A(I,J)=0
& A(I+5,J+5)=CTSCI(J)
& A(I+6,J+6)=CTE(I,J)
& A(I+9,J+9)=CTE(I,J)
& A(I+5,J)=BS(I,J)
& A(I+9,J)=BE(I,J)
50 IF ( C BTEST(18UG.7) ) CALL MMATRK A , 12,12, ' A ' )
C
C----- GET MATERIAL PROPERTIES
FALSE=.FALSE.
LSTYP=0
CALL MATLIB
& ( 2 ,LSTYP, FALSE ,IREL, FALSE, NAME, EISE, EPSE, DUCT, ENCR,
& FT , F , RT , R , V , VL , LELEN, LMAT ,
& MAT , MATYP, SE, IELMO, DAMAGE )
C
IF (MATTYP.NE.1) THEN
WRITE (6,190) IELMO,MATTYP,MODEI,MODEJ
190 FORMAT ( ' ELEMENT: ',I6, ' INCOMPATIBLE MATERIAL PROP. #',I5,
& ' START JOINT: ',I5, ' END JOINT: ',I5, /
& ' THE ELEMENT IS REJECTED AND ER, 'ROR CHECKING CONTINUES' )
ERR=.TRUE.
GO TO 191
ENDIF
C
EAM =SEC( 1 )
GAV =SEC( 2 )
CAZ =SEC( 3 )
GIX =SEC( 4 )
EIV =SEC( 5 )
EIZ =SEC( 6 )
C
C----- DETERMINE THE MEMBER RELEASE CODES
C
REL1 IS AN INPUT MEMBER RELEASE CODE
REL IS THE INTERNAL MEMBER RELEASE CODE
& BIT 5 AXIAL TRUE = AXIAL DEFORMATION CONSIDERED
& BIT 6 MY AT END I
& BIT 4 MY AT END I ----> TRUE=RELEASE
& BIT 5 MZ AT END I
& BIT 2 MY AT END J
& BIT 1 MY AT END J
& BIT 0 MZ AT END J
C
IF (BTEST(18UG.7)) WRITE (6,*) 'REL1',REL1
REL=0
& IRELC=0
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,0)
& IRELC(6:6)=2
ENDIF
& REL=REL/10
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,1)
& IRELC(5:5)=4
ENDIF
& REL=REL/10
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,2)
& IRELC(4:4)=8
ENDIF
& REL=REL/10
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,3)
& IRELC(5:5)=2
ENDIF
& REL=REL/10
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,4)
& IRELC(2:2)=4
ENDIF
& REL=REL/10
IF (MOCK(REL,10),NE.0) THEN
& REL=IBSET(REL,5)
& IRELC(1:1)=8
ENDIF
ENDIF
C----- SET STIFFNESS COEFFICIENTS...
C----- SET CONSISTENT MASS GEOMETRIC STIFFNESS COEFFICIENTS...
A2=0
B2=0
C2=0
D2=0
E2=0
ELE01650 FZ=1.0 / LENGTH
ELE01660 C----- BOTH ENDS RELEASED, Z-AXIS
ELE01670 IF (BTEST(REL,0) .AND. BTEST(REL,5)) THEN
ELE01680 KIZ=0
ELE01690 KJZ=0
ELE01700 KIZ=0
ELE01710 C----- START END RELEASED, Z-AXIS
ELE01720 ELSE IF (BTEST(REL,5)) THEN
ELE01730 KIZ=0
ELE01740 KJZ=5
ELE01750 KJZ=0
ELE01760 BZ= 0.20 * LENGTH
ELE01770 EZ= 0.20
ELE01780 FZ= 1.20 / LENGTH
ELE01790 C----- END END RELEASED, Z-AXIS
ELE01800 ELSE IF (BTEST(REL,0)) THEN
ELE01810 KIZ=5
ELE01820 KJZ=0
ELE01830 KJZ=0
ELE01840 AZ= 0.20 * LENGTH
ELE01850 DZ= 0.20
ELE01860 FZ= 1.20 / LENGTH
ELE01870 C----- BOTH ENDS RELEASED, Z-AXIS
ELE01880 ELSE
ELE01890 KIZ=4
ELE01900 KJZ=4
ELE01910 KJZ=2
ELE01920 AZ= 2 * LENGTH / 15.
ELE01930 BZ= AZ
ELE01940 CZ= LENGTH / 50.
ELE01950 DZ= 0.10
ELE01960 EZ= 0.10
ELE01970 FZ= 1.2 / LENGTH
ELE01980 ENDF
ELE01990 C
ELE02000 AV=0
ELE02010 BV=0
ELE02020 CV=0
ELE02030 DV=0
ELE02040 EV=0
ELE02050 FV=1.0 / LENGTH
ELE02060 C----- BOTH ENDS RELEASED, Y-AXIS
ELE02070 IF (BTEST(REL,1) .AND. BTEST(REL,4)) THEN
ELE02080 KIV=0
ELE02090 KJV=0
ELE02100 KIV=0
ELE02110 KJV=0
ELE02120 BV= 0.20 * LENGTH
ELE02130 EV= 0.20
ELE02140 FV= 1.20 / LENGTH
ELE02150 C----- END END RELEASED, Y-AXIS
ELE02160 ELSE IF (BTEST(REL,1)) THEN
ELE02170 KIV=5
ELE02180 KJV=0
ELE02190 KJV=0
ELE02200 AV= 0.20 * LENGTH
ELE02210 DV= 0.20
ELE02220 FV= 1.20 / LENGTH
ELE02230 C----- BOTH ENDS RELEASED, Y-AXIS
ELE02240 ELSE
ELE02250 KIV=4
ELE02260 KJV=4
ELE02270 KJV=2
ELE02280 AV= 2 * LENGTH / 15.
ELE02290 BV= AV
ELE02300 CV= LENGTH / 50.
ELE02310 DV= 0.10
ELE02320 EV= 0.10
ELE02330 FV= 1.2 / LENGTH
ELE02340 ENDF
ELE02350 C
ELE02360 IF (BTEST(REL,2) .AND. BTEST(REL,5)) THEN
ELE02370 KTI=0
ELE02380 KTI=0
ELE02390 ELSE IF (BTEST(REL,5)) THEN
ELE02400 KTI=0
ELE02410 KTI=1
ELE02420 ELSE IF (BTEST(REL,2)) THEN
ELE02430 KTI=1
ELE02440 KTI=0
ELE02450 ELSE
ELE02460 KTI=1
ELE02470 KTI=1
ELE02480 ENDF
ELE02490 C
ELE02500 IF ( BTEST(18UG.7) ) WRITE (6,*) 'IRELC',IRELC,'REL',REL
C
C----- ASSEMBLE LOCAL STIFFNESS MATRIX
M=EA/KLENGTH
Q=EI/LLENGTH
& A1=KIZ*EIZ/LENGTH
& A2=KJZ*EIZ/LENGTH
& C=KIZ*EI/LENGTH
& B1=KIV*EIV/LENGTH
& B2=KJV*EIV/LENGTH
& D=KIV*EI/LENGTH
& S22=(A1+2*C+AJ)/(LENGTH**2)
& S26=(A1+C)/(LENGTH)
& S212=(C+AJ)/(LENGTH)
& S33=(B1+2*D+BJ)/(LENGTH**2)
& S35=(B1+D)/(LENGTH)
& S311=(D+BJ)/(LENGTH)
& SK(1,1)=M
& SK(1,7)=-M
& SK(2,2)=S22
& SK(2,6)=S26
& SK(2,8)=-S22
& SK(2,12)=S212
& SK(5,5)=S33
& SK(5,9)=-S35
& SK(5,9)=-S35
& SK(5,11)=-S311
& SK(4,4)=Q * KTI
& SK(10,1)=-Q
& SK(5,5)=BT
& SK(5,9)=S35
& SK(5,11)=D
& SK(6,6)=A1
ELE05060
ELE05070
ELE05080
ELE05090
ELE05100
ELE05110
ELE05120
ELE05130
ELE05140
ELE05150
ELE05160
ELE05170
ELE05180
ELE05190
ELE05200
ELE05210
ELE05220
ELE05230
ELE05240
ELE05250
ELE05260
ELE05270
ELE05280
ELE05290
ELE05300
ELE05310
ELE05320
ELE05330
ELE05340
ELE05350
ELE05360
ELE05370
ELE05380
ELE05390
ELE05400
ELE05410
ELE05420
ELE05430
ELE05440
ELE05450
ELE05460
ELE05470
ELE05480
ELE05490
ELE05500
ELE05510
ELE05520
ELE05530
ELE05540
ELE05550
ELE05560
ELE05570
ELE05580
ELE05590
ELE05600
ELE05610
ELE05620
ELE05630
ELE05640
ELE05650
ELE05660
ELE05670
ELE05680
ELE05690
ELE05700
ELE05710
ELE05720
ELE05730
ELE05740
ELE05750
ELE05760
ELE05770
ELE05780
ELE05790
ELE05800
ELE05810
ELE05820
ELE05830
ELE05840
ELE05850
ELE05860
ELE05870
ELE05880
ELE05890
ELE05900
ELE05910
ELE05920
ELE05930
ELE05940
ELE05950
ELE05960
ELE05970
ELE05980
ELE05990
ELE06000
ELE06010
ELE06020
ELE06030
ELE06040
ELE06050
ELE06060
ELE06070
ELE06080
ELE06090
ELE06100
ELE06110
ELE06120
ELE06130
ELE06140
ELE06150
ELE06160
ELE06170
ELE06180
ELE06190
ELE06200
ELE06210
ELE06220
ELE06230
ELE06240
ELE06250
ELE06260
ELE06270
ELE06280
ELE06290
ELE06300

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C THE STIFFNESS IS STORED IN STIFF. THE MAPPING MATRIX IN LM
C THESE HAVE THE GLOBAL ADDRESSES IZKE AND IZLM...
C
C RETURN
C----- DETERMINE INCREMENTAL FORCES -----
400 CONTINUE
IF (PRINT.AND.FIRST) WRITE (6,491) STEPID
C
C CALL SML0A TO DETERMINE THE FIXED END FORCES
IF (MAXELD.GT.0) THEN
CALL SML0A(IELNO,FENPLG,LENGTH,REL,MAXELD,NELD,NLOAD,
& FEN,IELD,ELD)
ELSE
FENPLG=.FALSE.
ENDIF
C
C----- LOOP FOR EACH LOAD
DO 450 I=1,NLOAD
C
C----- TRANSFORM FRAME DISPL INTO LOCAL DISPL
DO 410 I=1,5
RCI =0.
RCI(5)=0.
RCI(6)=0.
RCI(9)=0.
DO 410 J=1,5
D1=DISPL(I,DOF,JOINTI,J) *LOAD
D2=DISPL(I,DOF,JOINTI,J+5) *LOAD
D3=DISPL(I,DOF,JOINTI,J) *LOAD
D4=DISPL(I,DOF,JOINTI,J+5) *LOAD
RCI(1)=RCI(1)+CTSC(J,I)*D1 + HSC(J,I)*D2
RCI(2)=RCI(2)+CTSC(J,I)*D2
RCI(3)=RCI(3)+CTSC(J,I)*D3 + BEC(J,I)*D4
RCI(4)=RCI(4)+CTSC(J,I)*D4
410
C----- INCREMENTAL FORCES
FC(1)= H*RC(1)-RC(7)
FC(2)= S22*RC(2)-RC(8) + S26*RC(6) + S212*RC(12)
FC(3)= S33*RC(3)-RC(9) + S35*RC(5) + S311*RC(11)
FC(4)= Q*RC(4)-RC(10)
FC(5)= S35*RC(5)-RC(9) + B1*RC(5) + D*RC(11)
FC(6)= S26*RC(2)-RC(8) + A1*RC(6) + C*RC(12)
C
FC(7)= -M*RC(1)-RC(7)
FC(8)= S22*RC(2)-RC(8) + S26*RC(6) + S212*RC(12)
FC(9)= S33*RC(3)-RC(9) + S35*RC(5) + S311*RC(11)
FC(10)= -Q*RC(4)-RC(10)
FC(11)= S311*RC(5)-RC(9) + D*RC(5) + B1*RC(11)
FC(12)= S212*RC(2)-RC(8) + C*RC(6) + A1*RC(12)
C
C----- SUBTRACT OF FIXED END FORCES
IF (FENPLG) THEN
DO 420 I=1,12
420 FC(I)=FC(I)-FEN(I,LOAD)
ENDIF
C
C----- DETERMINE MAXIMUM VALUES FOR MULTIPLE LOAD CASES
IF (NLOAD.GT.1) THEN
DO 425 I=1,12
425 IF ( ABSFC(I) ) .GT. ABS(FMAX(I)) FMAX(I)=FC(I)
ENDIF
C
C----- PRINT FORCES
IF (BTEST(IBUG,0).AND.PRINT)
& WRITE (6,495) IELNO,LOAD,NODEJ,(RC(J),J=1,6),
& NODEJ,(RC(J),J=7,12)
IF ( PRINT) WRITE (6,492) IELNO,LOAD,NODEJ,(FC(J),J=1,6),
& NODEJ,(FC(J),J=7,12)
C
450 CONTINUE
C
C----- CALCULATE MEMBER FORCE ON JOINT, AND ADD TO UNBALANCED FORCES
THIS IS USED TO CALC UNBALANCED FORCES.
DO 440 I=1,5
I1=IDOF(JOINTI,I)
I2=IDOF(JOINTI,I+5)
J1=IDOF(JOINTI,I)
J2=IDOF(JOINTI,I+5)
DO 440 J=1,5
FUB(I1)=FUB(I1)+CTSC(I,J)*FC(J) +FTC(J)
FUB(I2)=FUB(I2)+BSC(I,J)*FC(J) +FTC(J)
FUB(I1)=FUB(I1)+CTSC(I,J)*FC(J+6)+FTC(J+6)
FUB(I2)=FUB(I2)+BSC(I,J)*FC(J+6)+FTC(J+6)
440
491 FORMAT (' SD BEAM FORCES...', 'SK, /'
& ' ELEMENT LOAD, NODE', 'X, 'AXIAL', 'LX, 'FY', 'LX, 'FZ',
& 'LX, 'TORSION', 'LX, 'MY', 'LX, 'M2')
492 FORMAT (' /10, 15, 2X, 'FORCE', 16, 1P, 6G15.6,
& /15X, '2X, 'FORCE', 16, 6G15.6)
495 FORMAT (' /110, 15, 2X, 'DISPL', 16, 1P, 6G15.6,
& /15X, '2X, 'DISPL', 16, 6G15.6)
RETURN
C----- DETERMINE TOTAL FORCES
500 CONTINUE
IF (PRINT.AND.FIRST) WRITE (6,491) STEPID
C
C----- TOTAL FORCES AND DISPLACEMENTS
DO 510 I=1,12
FTC(I)=FTC(I)+FC(I)
RT(I)=RT(I)+RC(I)
510
520 FORMAT (' /1, 15, ' RT', 1P, G12.4, ' FT', G12.4,
& /15X, '1P, G12.4, ' FT', G12.4)
LOAD=1
IF (BTEST(IBUG,0).AND.PRINT)
& WRITE (6,495) IELNO,LOAD,NODEJ,(RT(J),J=1,6),
& NODEJ,(RT(J),J=7,12)
IF ( PRINT) WRITE (6,492) IELNO,LOAD,NODEJ,(FTC(J),J=1,6),
& NODEJ,(FTC(J),J=7,12)
C
RETURN
C----- DETERMINE FIXED END FORCES, AND ADD TO FORCES
400 IF (MAXELD.LE.0) RETURN
C
C----- CALL SML0A TO DETERMINE THE FIXED END FORCES
CALL SML0A(IELNO,FENPLG,LENGTH,REL,MAXELD,NELD,NLOAD,
& FEN,IELD,ELD)
FENPLG=FENPLG
IF (.NOT. FENPLG) RETURN
C
C----- ADD FIXED END FORCES TO LOAD MATRIX
ELE06780 DO 620 I=1,NLOAD
ELE06790 DO 610 I=1,5
ELE06800 GFEM(I)=0
ELE06810 GFEM(I+5)=0
ELE06820 GFEM(I+6)=0
ELE06830 GFEM(I+9)=0
ELE06840 DO 610 J=1,5
ELE06850 D1=GFEM(J,LOAD)
ELE06860 D2=GFEM(J+5,LOAD)
ELE06870 D3=GFEM(J+6,LOAD)
ELE06880 D4=GFEM(J+9,LOAD)
ELE06890 GFEM(I)=GFEM(I)+CTSC(I,J)*D1
ELE06900 GFEM(I+5)=GFEM(I+5)+BSC(I,J)*D1 + CTSC(I,J)*D2
ELE06910 GFEM(I+6)=GFEM(I+6)+CTSC(I,J)*D3
ELE06920 GFEM(I+9)=GFEM(I+9)+BEC(I,J)*D3 + CTSC(I,J)*D4
610
IF (BTEST(IBUG,7)) THEN
WRITE(6,*) 'IELNO',IELNO
CALL MMATRX(FEM, 1, 12, 'LOCAL FIXED END FORCES')
CALL MMATRX(GFEM, 1, 12, 'GLOBAL FIXED END FORCES')
ENDIF
C
DO 620 J=1,6
J1=IDOF(JOINTI,J)
J2=IDOF(JOINTI,J)
FORCE(J1,LOAD)=FORCE(J1,LOAD)+GFEM(J)
620 FORCE(J2,LOAD)=FORCE(J2,LOAD)+GFEM(J+6)
IF (BTEST(IBUG,7)) THEN
CALL MMATRX(FORCE, NDOF, NLOAD, 'GLOBAL LOAD MATRIX')
ENDIF
C
RETURN
C----- WRITE MEMBER FORCES TO OUTPUT FILE -----
700 CONTINUE
WRITE (IUNIT,710) NODEJ,(FTC(J),J=1,6),NODEJ,(FTC(J),J=7,12)
710 FORMAT ('16, 1P, 6G12.5)
C
RETURN
C----- READ AND PRINT MEMBER FORCES FROM OUTPUT FILE -----
800 CONTINUE
BACKSPACE(IUNIT)
READ (IUNIT, *) ITYPE,IELNO,INWRITE,TO,DT
WRITE (6,805)
ISTEP=-IWRITE
810 READ (IUNIT,815,END=850)
& NODEJ,(FTC(J),J=1,6),NODEJ,(FTC(J),J=7,12)
815 FORMAT ('16, 6G12.5)
ISTEP=ISTEP-IWRITE
IF (MOD(ISTEP,INC).EQ.0)
& WRITE (6,820) ISTEP,I,NODEJ,(FTC(J),J=1,6),
& NODEJ,(FTC(J),J=7,12)
GO TO 810
C
805 FORMAT (' SD BEAM FORCES...',
& ' STEP TIME, NODE', 'X, 'AXIAL', 'LX, 'FY', 'LX, 'FZ',
& 'LX, 'TORSION', 'LX, 'MY', 'LX, 'M2')
820 FORMAT (' /110, 1P, G15.5, 0P, 16, 1P, 6G15.6,
& /25X, '16, 6G15.6)
C
830 RETURN
C----- DETERMINE THE LENGTH OF THE MATERIAL DATA
900 CONTINUE
MVSZ=1
ISE=0
C
MAT = RINPUT(1)
CALL MATLIS
& ( O, LSTTYP, .FALSE, IREL, .FALSE, NAME, EESE, EPSE, DUCT, ENCR,
& FT, F, RT, R, V, VL, LELEM, LMAT,
& MAT, MATTYP, SE, IELNO, DAMAGE)
ISE=ISE+LELEM
RETURN
C----- DETERMINE THE TOTAL STRAIN ENERGY
1000 CONTINUE
EES=0
EPSE=0
C
DO 1010 I=1,12
1010 EES=EES + (FTC(I)+FC(I))*RC(I)+RTC(I)*2.
C
ENGDAT(1) = EES
ENGDAT(2) = 0
C
RETURN
C----- DUCTILITIES AND EXCURSION RATIOS
NO D & E RATIOS FOR ELASTIC ELEMENT
1100 RETURN
C
C----- PRINT MAXIMUM ELEMENT LOADS
1200 CONTINUE
LOAD=0
IF (FIRST) WRITE (6,491) ' MAXIMUM VALUES FOR ALL STEPS '
& ' NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY!'
WRITE (6,492) IELNO,LOAD2,NODEJ,(FMAX(I),I=1,6),
& NODEJ,(FMAX(I),I=7,12)
C
RETURN
C----- RESET ELEMENT FORCES
1500 CONTINUE
ZERO MATRICES
DO 1540 I=1,12
FMAX(I)=0
F(I)=0
FTC(I)=0
R(I)=0
1540 RTC(I)=0
WRITE (6,1530) IELNO
1530 FORMAT (' SD BEAM..... ELEMENT #', I6,
& ' INTERNAL FORCES AND HYSTERESIS MODELS ARE RESET TO ZERO')
LSTTYP=0
CALL MATLIS
& ( 2, LSTTYP, .FALSE, IREL, .FALSE, NAME, EESE, EPSE, DUCT, ENCR,

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      & FT ,F ,RT ,R ,V ,VL ,LELE ,LMAT , ELEM9290
      & MAT ,MATTYP,SE,IELNO,DAMAGE) ELEM9500
C RETURN ELEM9510
C----- DAMAGE INDEX ELEM9520
C 1400 DAMAGE = 0. ELEM9530
C RETURN ELEM9540
C ENO ELEM9550
C----- SUBROUTINE ELEM9560
      & IOPT ,IUNIT ,MENEK ,FIRST ,PRINT , ELEM9560
      & IDOF ,MLOAD ,MAMNO ,ANODE ,NCOS , ELEM9570
      & IDOF ,MLOAD ,MAMNO ,ANODE ,NCOS , ELEM9580
      & CONST ,DISPL ,VELOC ,FORCE ,FUB , ELEM9590
      & IREL ,BUG ,IBUG ,ACCEL ,KGDATA , ELEM9600
      & GRAV ,PGEOM ,ELSTIC ,NAME ,STEPID , ELEM9610
      & IELNO ,RINPUT ,EISE ,EPSE ,INC , ELEM9620
      & DAMAGE ,IELNO ,NODEI ,NODEJ ,JOINTI , ELEM9630
      & IELTYP ,R ,RT ,FT , ELEM9640
      & V ,VT ,ISE ,H ,LENGTH , ELEM9650
      & MAT ,A ,LM ,KTYPE ,FMAX , ELEM9660
      & SE ,STIFF ) ELEM9670
C IMPLICIT REAL(A-H,O-Z) ELEM9680
LOGICAL ERR,FIRST,PRINT,BUG,FALSE,MENEK,ELSTIC ELEM9690
LOGICAL BTEST ELEM9700
CHARACTER*80 NAME ELEM9710
CHARACTER*(*) TYPEID ELEM9720
CHARACTER*(*) TYPEID ELEM9730
DIMENSION IDOF(MAMNO,6),COORD(MAMNO,6),COSINE(3,3,NCOS) ELEM9740
DIMENSION CONST(MAMNO,6), ID(MAMNO), JTCOS(MAMNO) ELEM9750
DIMENSION SAT(2,12),STIFF(78) ELEM9760
DIMENSION AC(2,2),S(2,2),LWK(12),FMAX(2) ELEM9770
DIMENSION CTSC(5,5),CTE(5,5),VK(5),VCS(5),VZ(5) ELEM9780
DIMENSION BS(5,5),BE(5,5),SECTISE ELEM9790
DIMENSION DISPL(NODE,MLOAD),FUB(NDOF) ELEM9800
DIMENSION VELOC(NDOF) ELEM9810
DIMENSION FORCE(NDOF,MLOAD) ELEM9820
DIMENSION RINPUT(100),MORR(6),DUCT(5),EXCR(6) ELEM9830
REAL IX,IV,IJ,KITZ,KIJ,KIJZ,KIIZ,KIIZV,KIJV,KTI,TVJ ELEM9840
INTEGER REL,RELT ELEM9850
DIMENSION MDX(15) ELEM9860
DATA MDX(1,2,4,7,11,16,22,29,37,46,56,67,79) ELEM9870
DATA TYPE/' AXIAL',' SHEAR-V',' SHEAR-Z', ELEM9880
& TORSION',' BENDING-Y',' BENDING-Z'/' ELEM9890
C----- VARIABLES: ELEM9900
C----- GLOBAL VARIABLES ELEM9910
C IOPT = 1, INITIALIZE BEAM COLUMN ELEMENT ELEM9920
C IUNIT = 2, CALCULATE GEOMETRIC STIFFNESS ELEM9930
C IDOF = 5, FORM STIFFNESS ELEM9940
C ID = 4, CALCULATE INCREMENTAL FORCES ELEM9950
C IUNIT = 5, CALCULATE TOTAL FORCES AND ENERGIES ELEM9960
C IUNIT = 6, OUTPUT FIX UNIT # FOR PRINTING OUTPUT ELEM9970
C ERR = FLAG, IF AN ERR OR HAS OCCURED, ERR=.TRUE. ELEM9980
C FIRST = FLAG, FIRST=.TRUE., PRINT HEADERS ELEM9990
C PRINT = FLAG, PRINT=.TRUE., PRINT DATA ELEM1000
C NDOF = # OF GLOBAL DOF ELEM1010
C MLOAD = # OF LOAD COMBINATIONS ELEM1020
C MAMNO = # ROM DIMENSION OF NODE ARRAY ELEM1030
C INODE = # OF NODES ELEM1040
C ID = ARRAY OF EXTERNAL NODE NUMBERS ELEM1050
C IDOF = ARRAY OF DEGREES OF FREEDOM ELEM1060
C COORD = ARRAY OF COORDINATES ELEM1070
C COSINE = ARRAY OF DIRECTION COSINES OF NODES ELEM1080
C CONST = ARRAY OF CONSTRAINT TRANSFORMATIONS ELEM1090
C DISPL = GLOBAL DISPLACEMENT MATRIX ELEM1100
C Z = REAL GLOBAL STORAG VECTOR ELEM1110
C NZ = INTEGER GLOBAL STORAG VECTOR ELEM1120
C IZMAT = LOCATION OF MATERIAL DATA IN GLOBAL STORAGE VECTOR ELEM1130
C NAME = ELEMENT NAME ELEM1140
C IELNO = ELEMENT NUMBER ELEM1150
C RINPUT = INPUT DATA ELEM1160
C STIFF = OUTPUT ELEMENT STIFFNESS (UPPER TRIANGULAR FORM) ELEM1170
C LN = OUTPUT LOCAL TO GLOBAL STIFFNESS MAPPING MATRIX ELEM1180
C----- ELEMENT VARIABLES ELEM1190
C H,Q,AI,AJ,C,BI,BJ,S22,S26,S212,S55,S5S,SS11,D ELEM1200
C = INDIVIDUAL TERMS IN THE ELEMENT STIFFNESS (S) MATRIX ELEM1210
C PKG = INPUT LOAD FOR FORMING GEOMETRIC STIFFNESS MATRIX... ELEM1220
C R = INCREMENTAL DISPLACEMENTS ELEM1230
C RT = TOTAL DISPLACEMENTS ELEM1240
C F = INCREMENTAL FORCES ELEM1250
C FT = TOTAL FORCES ELEM1260
C LM = LOCAL TO GLOBAL STIFFNESS MAPPING MATRIX ELEM1270
C CTS = LOCAL TO GLOBAL ROTATION MATRIX START ELEM1280
C CTE = LOCAL TO GLOBAL ROTATION MATRIX END ELEM1290
C BS = LOCAL TO GLOBAL ROTATED ECCENTRICITY/CONSTRAINT MATRIX START ELEM1300
C BE = LOCAL TO GLOBAL ROTATED ECCENTRICITY/CONSTRAINT MATRIX END ELEM1310
C STIFF = ELEMENT STIFFNESS ELEM1320
C IELTYP = ELEMENT TYPE = 10 ELEM1330
C NODEI = EXTERNAL JOINT NUMBER, END I ELEM1340
C NODEJ = EXTERNAL JOINT NUMBER, END J ELEM1350
C JOINTI = INTERNAL JOINT NUMBER, END I ELEM1360
C JOINTJ = INTERNAL JOINT NUMBER, END J ELEM1370
C----- TEMPORARY VARIABLES ELEM1380
C VX = VECTOR DEFINING THE ELEMENT X AXIS ELEM1390
C VV = VECTOR DEFINING THE ELEMENT Y AXIS ELEM1400
C COSLOC = LOCAL COSINE MATRIX ELEM1410
C A = GLOBAL TO LOCAL FORCE TRANSFORMATION MATRIX ELEM1420
C S = ELEMENT STIFFNESS AT LOCAL COORD, AT ENDS OF FLEXIBLE PART ELEM1430
C SAT = PRODUCT OF S*A ELEM1440
C ASAT = PRODUCT OF A*SAT ELEM1450
C----- CHOOSE OPTION ELEM1460
C IF (IOPT.LT.1 .OR. IOPT.GT.14) ELEM1470
& WRITE (6,*) 'INVALID OPTION IN ELE-02, IOPT=',IOPT ELEM1480
GO TO (100,200,300,400,500,600,700,800,900,1000,1100,1200, ELEM1490
& 1300,1400),IOPT ELEM1500
C 100 CONTINUE ELEM1510
C----- INTERPRETATE INPUT DATA ELEM1520
IELTYP = 2 ELEM1530
      MAT = RINPUT( 1) ELEM1540
      NODEI = RINPUT( 2) ELEM1550
      NODEJ = RINPUT( 3) ELEM1560
      KTYPE = RINPUT( 4) ELEM1570
      XLEN = RINPUT( 5) ELEM1580
      VK(1) = RINPUT( 6) ELEM1590
      VK(2) = RINPUT( 7) ELEM1600
      VK(3) = RINPUT( 8) ELEM1610
      XS = RINPUT( 9) ELEM1620
      XE = RINPUT(10) ELEM1630
C----- GET INTERNAL NODE # ASSOCIATED WITH EXTERNAL NODE #'S ELEM1640
      JOINTI=IQUICK(NODEI,ID,NODE) ELEM1650
      JOINTJ=IQUICK(NODEJ,ID,NODE) ELEM1660
C IF (KTYPE.LT.1 .OR. KTYPE.GT.6) THEN ELEM1670
      WRITE(6,102) IELNO,NODEI,NODEJ,KTYPE ELEM1680
102 FORMAT('X,20','*','ER','ROR - INVALID ID KTYPE',/ ELEM1690
& SX,'IELNO=',IS,SX,'JOINTI=',IS,SX,'JOINTJ=',IS, ELEM1700
& SX,'KTYPE=',IS,/ ELEM1710
& SX,'REVISE INPUT 1 LE KTYPE LE 6 .....?') ELEM1720
      LENGTH=L.0 ELEM1730
      ENDF ELEM1740
C GET GLOBAL TO LOCAL TRANSFORMATION MATRIX ELEM1750
C----- DEFINE VECTOR X, LENGTH ELEM1760
      VK(1)=COORD(JOINTI,1)-COORD(JOINTI,1) ELEM1770
      VK(2)=COORD(JOINTI,2)-COORD(JOINTI,2) ELEM1780
      VK(3)=COORD(JOINTI,3)-COORD(JOINTI,3) ELEM1790
      LENGTH=SQRT(VK(1)**2+VK(2)**2+VK(3)**2)-XS-XE ELEM1800
      IF (LENGTH.EQ.0) THEN ELEM1810
        DO 105 I=1,3 ELEM1820
          VK(I)=COSINE(1,II,JTCOS(JOINTI)) ELEM1830
          VK(II)=COSINE(2,II,JTCOS(JOINTI)) ELEM1840
          LENGTH=L.0 ELEM1850
        ELSE ELEM1860
          LENGTH=LENGTH-XS-XE ELEM1870
        ENDF ELEM1880
      IF (XLEN.NE.0) THEN ELEM1890
        LENGTH=XLEN ELEM1900
        XS=0 ELEM1910
        XE=0 ELEM1920
      ENDF ELEM1930
      IF (LENGTH.LE.0) THEN ELEM1940
        WRITE(6,101) IELNO,JOINTI,JOINTJ,LENGTH ELEM1950
101 FORMAT('X,20','*','ER','ROR - LENGTH IS LE 0',/ ELEM1960
& SX,'LENGTH',IP,G15.6/ ELEM1970
& SX,'REVISE INPUT.....?') ELEM1980
        LENGTH=L.0 ELEM1990
      ENDF ELEM2000
      IF (BTEST(BUG,7)) THEN ELEM2010
        WRITE (6,*) 'JOINTS',JOINTI,JOINTJ ELEM2020
        WRITE (6,*) 'VK',VK ELEM2030
        WRITE (6,*) 'VX',VX ELEM2040
        WRITE (6,*) 'LENGTH',LENGTH ELEM2050
      ENDF ELEM2060
C----- GET LOCAL TO GLOBAL TRANSFORMATION MATRICES CT AND B ELEM2070
      ICOS=JTCOS(JOINTI) ELEM2080
      ICS=JTCOS(JOINTJ) ELEM2090
      CALL ROTMZY(VX,VV,COSINE(1,1,ICOS),CTS,XS,JO,0,BS, ELEM2100
& CONST(JOINTI,1),MAMNO) ELEM2110
      CALL ROTMZY(VX,VV,COSINE(1,1,ICS),CTE,XE,JO,0,BE, ELEM2120
& CONST(JOINTJ,1),MAMNO) ELEM2130
      IF (BTEST(BUG,7)) THEN ELEM2140
        CALL MMATRX CTS , 3, 5,'CTS ' ELEM2150
        CALL MMATRX CTE , 3, 5,'CTE ' ELEM2160
      ENDF ELEM2170
C----- GET GLOBAL CONSTRAINT MATRIX BS, BE ELEM2180
      IF (BTEST(BUG,7)) THEN ELEM2190
        CALL MMATRX(BS, 3, 5,'BS ' ELEM2200
        CALL MMATRX(BE, 3, 5,'BE ' ELEM2210
      ENDF ELEM2220
C----- ZERO MATRICES ELEM2230
      F=0 ELEM2240
      FT=0 ELEM2250
      R=0 ELEM2260
      V=0 ELEM2270
      VT=0 ELEM2280
      FMAX(1)=0 ELEM2290
      FMAX(2)=0 ELEM2300
C----- ASSEMBLE TRANSFORMATION MATRIX A ELEM2310
C NOTE: A IS DIMENSIONED AS A 12X2 MATRIX, BUT ONLY THE FIRST IELDOF ELEM2320
      ROM'S CONTAIN INFORMATION, THE BALANCE OF THE MATRIX IS ELEM2330
      UNDEFINED. THE GLOBAL DOF CORRESPONDING TO THE ROM'S OF A ELEM2340
      ARE STORED IN VECTOR LM. AGAIN, ONLY THE FIRST IELDOF ROM'S ELEM2350
      OF LM ARE DEFINED. ELEM2360
      IELDOF=0 ELEM2370
      DO 50 I=1,12 ELEM2380
        REMOVE DOF'S THAT ARE CONSTRAINED TO THE SAME DOF... ELEM2390
        J= I ELEM2400
        IF (I.GT.6) J= I-6 ELEM2410
        IF ( IELDOF(J),EQ.IDOF(JOINTI,J) ) GO TO 50 ELEM2420
        IF (I.LE.6) THEN ELEM2430
          LMT=IDOF(JOINTI,I) ELEM2440
        ELSE ELEM2450
          LMT=IDOF(JOINTI,J) ELEM2460
        ENDF ELEM2470
        A1=0 ELEM2480
        A2=0 ELEM2490
        IF (I.LE.5) THEN ELEM2500
          IF (KTYPE.LE.5) A1=CTS(I,KTYPE) ELEM2510
        ELSE IF (I.LE.6) THEN ELEM2520
          IF (KTYPE.LE.5) THEN ELEM2530
            A1=BS(I-5,KTYPE) ELEM2540
          ELSE A1=CTS(I-5,KTYPE-5) ELEM2550
        ENDF ELEM2560
        IF (I.LE.9) THEN ELEM2570
          IF (KTYPE.LE.5) A2=CTE(I-6,KTYPE) ELEM2580
        ELSE ELEM2590
          IF (KTYPE.LE.3) THEN ELEM2600
            A2=BE(I-9,KTYPE) ELEM2610
          ELSE ELEM2620

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A2=CTE(I-9,KTYPE-5)
ENDIF
ENOFIF
IF (AL.EQ.0 .AND. A2.EQ.0) GO TO 50
IELDOF=IELDOF+1
ACIELDOF,1)=A1
ACIELDOF,2)=A2
LWIELDOF=LWIT
C
50 CONTINUE
IF ( BTEST(IBUG,7) ) CALL HNRX2( A , IELDOF,2, ' A ' ,12)
C
C----- GET SPRING STIFFNESS
FALSE=.FALSE.
LSTYP=0
CALL MATLIB
& ( 2 ,LSTYP ,FALSE ,IREL ,FALSE,NAME,ESE,EPSE, DUCT,EXCR,
& FT ,F ,RT ,R ,O ,O ,LELEM ,LMAT ,
& MAT ,MATTYP,SE,IELNO,DAMAGE)
C
111 FORMAT (OP,' ZNTRX2',I6,' ',I15,IP,Q20.10)
C----- H IS THE SPRING STIFFNESS
C
H = SE(1)
HM= SE(1)/LENGTH
SK,1)=HM
SK,2)=HM
SK,1)=HM
SK,2)=HM
C
C----- CALCULATE SAT
DO 50 J=1,IELDOF
DO 50 K=1,2
SAT(I,J)=SAT(I,J)+SK(I,K)*AK(J,K)
60
C----- CALCULATE ASAT AND CONVERT TO HALF STORAGE NODE BY COLUMNS
C
1 5 6 10 15 21 28 36 45 56 68 NUMBER INDICATES
2 5 9 14 20 27 35 44 54 65 77 LOCATION OF DATA
3 8 13 19 26 34 43 53 64 76 IN ARRAY STIFF
4 7 12 18 25 33 42 52 63 75
5 11 17 24 32 41 51 62 74
6 16 23 31 40 50 61 73
7 22 30 39 49 60 72
8 29 38 48 59 71
9 37 47 58 70
10 46 57 69
11 56 68
12 67
L=0
DO 70 J=1,IELDOF
DO 70 I=J,1,-1
L=L+1
STIFF(L)=0
DO 70 K=1,2
STIFF(L)=STIFF(L)+AK(I,K)*SAT(K,J)
70
C
IF ( BTEST(IBUG,7) ) THEN
WRITE (6,*) 'IELODF', IELDOF, 'LN =', (LWK(I),I=1, IELDOF)
CALL LMATRX(STIFF,NO, IELDOF, (L+1), 'SPRING STIFFNESS')
ENDIF
C
C----- RELEASE UNUSED STORAGE
180 IREL=78-L
C
PRINT COLUMN DATA
IF (FIRST .OR. BTEST(IBUG,7) .OR. BTEST(IBUG,8) ) WRITE (6,192)
191 WRITE(6,195) NAME, IELNO, MAT, NODEI, NODEJ, TYPE(KTYPE), LENGTH,
& VV(1), VV(2), VV(3), XS, -XE
192 FORMAT(// ELEMENT 02, ONE (LOCAL) DOF SPRING ELEMENT//
& T22,'B' MATL START END, 'TYPE', 'LN', 'LENGTH', 'SK,
& '12', ' ', 'START DIST END DIST')
195 FORMAT(1X, A15, I6, 2X, A9, SK, IP, G12, 4, OP,
& F9.5, ' ', SP, F9.5, ' ', F9.5, ' ', IP, SS, G12.4)
& RETURN
C----- DETERMINE GEOMETRIC STIFF
200 RETURN
C
C THE GEOMETRIC STIFFNESS MATRIX IS NOT AVAILABLE FOR THIS ELEMENT
C----- DETERMINE STIFFNESS
300 CONTINUE
C
H CONTAINS THE SPRING STIFFNESS, WHICH HAS DETERMINED IN THE
LAST CALL TO MAT LIB
C
IF H=SE(1) THEN THE STIFFNESS HAS NOT CHANGED, RETURN
C
IF (N.EQ.SE(1)) RETURN
C
H = SE(1)
HM= SE(1)/LENGTH
SK,1)=HM
SK,2)=HM
SK,1)=HM
SK,2)=HM
C
C----- CALCULATE SAT
DO 360 J=1,IELDOF
DO 360 K=1,2
SAT(I,J)=SAT(I,J)+SK(I,K)*AK(J,K)
360
C----- CALCULATE ASAT, STORE IN UPPER TRIANGULAR MATRIX
L=0
DO 370 J=1,IELDOF
DO 370 I=J,1,-1
L=L+1
STIFF(L)=0
DO 370 K=1,2
STIFF(L)=STIFF(L)+AK(I,K)*SAT(K,J)
370
C
IF ( BTEST(IBUG,7) ) THEN
WRITE (6,*) 'IELODF', IELDOF, 'LN =', (LWK(I),I=1, IELDOF)
CALL LMATRX(STIFF,NO, IELDOF, (L+1), 'SPRING STIFFNESS')
ENDIF
C
RETURN
C----- DETERMINE INCREMENTAL FORCES
400 CONTINUE

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ELEM2590 IF (PRINT.AND.FIRST) WRITE (6,491) STEPID
ELEM2600 C
ELEM2610 C----- LOOP FOR EACH LOAD
ELEM2620 DO 450 LOAD=1,NLOAD
ELEM2630 C
ELEM2640 C----- TRANSFORM FRAME DISPL INTO LOCAL DISPL
ELEM2650 C... LOCAL DISPL ARE AT THE END OF THE SPRING, THIS
ELEM2660 C... POSITIVE IS TENSION AND NEGATIVE IS COMPRESSION
ELEM2670 R=0
ELEM2680 V=0
ELEM2690 DO 410 I=1,IELDOF
ELEM2700 J=LWK(I)
ELEM2710 A11= ACI,1)
ELEM2720 A12= ACI,2)
ELEM2730 DISP= DISPL(J,LOAD)
ELEM2740 VEL= VELOC(J)
ELEM2750
ELEM2760 R= R + (ACI,2)-ACI,1)) * DISPL(J,LOAD)
ELEM2770 V= V + (ACI,2)-ACI,1)) * VELOC(J)
ELEM2780
ELEM2790 C
ELEM2800 C----- INCREMENTAL FORCES
ELEM2810 F= H*R/LENGTH
ELEM2820 C
ELEM2830 C----- CHECK STIFFNESS AND CALCULATE UNBALANCED FORCES
ELEM2840 C THIS IS PERFORMED ONLY FOR INELASTIC ANALYSIS
ELEM2850 P =FT-F
ELEM2860 V=VT-V
ELEM2870 IF (.NOT. ELSTIC) THEN
ELEM2880 -- SET UP TEMPORARY - TOTAL LOADS, DISPL'S AND VELOC
ELEM2890 PL=FT
ELEM2900 DL=(RT+R)/LENGTH
ELEM2910 DL=RT /LENGTH
ELEM2920 VL=VT-V
ELEM2930 C
ELEM2940 -- TRANSFER PERMANENT HYSTERESIS DATA TO TEMPORARY STORAGE...
ELEM2950 ISE2=ISE/2
ELEM2960 DO 415 I=1,ISE2
ELEM2970 SE(I)=SE(I+ISE2)
ELEM2980 C
ELEM2990 -- CALL HYST MODEL TO GET NEW STIFFNESS AND
ELEM3000 C THE TOTAL FORCE P AT DISPL D.
ELEM3010 MOPT=3
ELEM3020 CALL MATLIB
ELEM3030 & (MOPT,LSTYP ,FALSE ,IREL ,FALSE,NAME,ESE,EPSE, DUCT,EXCR,
ELEM3040 & P ,PL ,D ,DL ,VC ,VL ,LELEM ,LMAT ,
ELEM3050 & MAT ,MATTYP,SE,ISE2+1), IELNO,DAMAGE)
ELEM3060 IF (SE(ISE2)-1).NE.SE(1)) MNAME=.TRUE.
ELEM3070 ENDOF
ELEM3080 C
ELEM3090 C----- SAVE PEAK VALUES FOR MULTIPLE LOAD CASES
ELEM3100 IF (NLOAD.GT.1 .AND. ABS(F).GT.ABS(FMAX(1))) THEN
ELEM3110 FMAX(1)=F
ELEM3120 ENDOF
ELEM3130 C
ELEM3140 C----- PRINT DATA
ELEM3150 HM= H/LENGTH
ELEM3160 IF (PRINT) WRITE (6,492) IELNO,LOAD,TYPE(KTYPE),NODEI,NODEJ,F,R,HM,ELNO,
ELEM3170
ELEM3180
ELEM3190
ELEM3200
ELEM3210
ELEM3220
ELEM3230
ELEM3240
ELEM3250
ELEM3260
ELEM3270
ELEM3280
ELEM3290
ELEM3300
ELEM3310
ELEM3320
ELEM3330
ELEM3340
ELEM3350
ELEM3360
ELEM3370
ELEM3380
ELEM3390
ELEM3400
ELEM3410
ELEM3420
ELEM3430
ELEM3440
ELEM3450
ELEM3460
ELEM3470
ELEM3480
ELEM3490
ELEM3500
ELEM3510
ELEM3520
ELEM3530
ELEM3540
ELEM3550
ELEM3560
ELEM3570
ELEM3580
ELEM3590
ELEM3600
ELEM3610
ELEM3620
ELEM3630
ELEM3640
ELEM3650
ELEM3660
ELEM3670
ELEM3680
ELEM3690
ELEM3700
ELEM3710
ELEM3720
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ELEM3740
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ELEM3780
ELEM3790
ELEM3800
ELEM3810
ELEM3820
ELEM3830
ELEM3840
ELEM3850
ELEM3860
ELEM3870
ELEM3880
ELEM3890
ELEM3900
ELEM3910
ELEM3920
ELEM3930
ELEM3940
ELEM3950
ELEM3960
ELEM3970
ELEM3980
ELEM3990
ELEM4000
ELEM4010
ELEM4020
ELEM4030
ELEM4040
ELEM4050
ELEM4060
ELEM4070
ELEM4080
ELEM4090
ELEM4100
ELEM4110
ELEM4120
ELEM4130
ELEM4140
ELEM4150
ELEM4160
ELEM4170
ELEM4180
ELEM4190
ELEM4200
ELEM4210
ELEM4220
ELEM4230
ELEM4240
ELEM4250
ELEM4260
ELEM4270
ELEM4280
ELEM4290
ELEM4300
ELEM4310
ELEM4320
ELEM4330
ELEM4340
ELEM4350
ELEM4360
ELEM4370
ELEM4380
ELEM4390
ELEM4400
ELEM4410
ELEM4420
ELEM4430
ELEM4440
ELEM4450
ELEM4460
ELEM4470
ELEM4480
ELEM4490
ELEM4500
ELEM4510
ELEM4520
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ELEM4540
ELEM4550
ELEM4560
ELEM4570
ELEM4580
ELEM4590
ELEM4600
ELEM4610
ELEM4620
ELEM4630
ELEM4640
ELEM4650
ELEM4660
ELEM4670
ELEM4680
ELEM4690
ELEM4700
ELEM4710
ELEM4720
ELEM4730
ELEM4740
ELEM4750
ELEM4760
ELEM4770
ELEM4780
ELEM4790
ELEM4800
ELEM4810
ELEM4820
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WRITE (UNIT,710) NODEI,NOJ,KTYPE,FT,RT,H,ESE,EPSE,
& (DUCT(I),EXCR(I),I=1,5)
710 FORMAT (SI6,IP,SG12,4/6G12,4)
C
C----- RETURN
C----- READ AND PRINT MEMBER FORCES FROM OUTPUT FILE
800 CONTINUE
BACKSPACE(UNIT)
READ (UNIT,* ) ITYPE,IELNO,IMWRITE,TO,DT
ISTEP=IMWRITE
C
810 READ (UNIT,815,END=850) NODEI,NOJ,KTYPE,FT,RT,H,ESE,EPSE,
& (HORK(I),I=1,6)
815 FORMAT (SI6,SG12,4/6G12,4)
ISTEP=IMWRITE
I=IO+DT*ISTEP
IF (ISTEP.EQ.0) WRITE (6,805) NODEI,NOJ,KTYPE
IF (MOD(ISTEP,DMC).EQ.0)
& WRITE (6,820) ISTEP,T,FT,RT,H,ESE,EPSE
GO TO 810
C
805 FORMAT (/ ' SPRING FORCES...'/
& SK,'NODEI:',I6,SK,'NOJ:',I6,SK,'SPRING TYPE:',A,/'
& ' STEP TIME '
& ' FORCE ' , ' DISPLACEMENT ' , ' STIFFNESS' ,
& ' ESE ' , ' PSE ' )
C
820 FORMAT (I10,IP,G15,5,6G15,5)
C
850 WRITE (6,840) (HORK(I),I=1,6)
840 FORMAT (/I10,' MAXIMUM DUCTILITIES AND EXCURSION RATIOS'/
& ' I10,' '
& ' I15 'DISPLACEMENT DEFINITION: U1= IP,G12,4,SK,'E1= G12,4/'
& ' I15 'ENERGY DEFINITION #1: U2= IP,G12,4,SK,'E2= G12,4/'
& ' I15 'ENERGY DEFINITION #2: U3= IP,G12,4,SK,'E3= G12,4/'
RETURN
C
C----- DETERMINE THE LENGTH OF THE MATERIAL DATA
900 CONTINUE
MNSV=1
ISE=0
C
MAT = RZMPC(1)
CALL MATLIB
& C < .LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,ESEE ,EPSE , DUCT ,EXCR ,
& FT ,F ,RT ,R ,.0 ,.0 ,.LELEN ,LMAT ,
& MAT ,MATTYP ,SE ,IELNO ,DAMAGE)
ISE=ISE+LELEN
C
C----- DOUBLE THE STORAGE, TO ALLOW FOR TEMPORARY VALUES...
ISE=ISE*2
RETURN
C
C----- DETERMINE THE STRAIN ENERGY
1000 CONTINUE
C
C----- DUCTILITIES AND EXCURSION RATIOS
1100 CONTINUE
C----- OPTIONS 10 AND 11 HAVE THE SAME CODE FOR THIS ELEMENT...
C----- THE ENERGY HAS CALCULATED WITH THE LAST CALL FOR INCREMENTAL FORCE
C----- THE TOTAL FORCES HAVE NOT BEEN CALLED YET, THUS THE ENERGIES RESIDUE
C----- IN THE MATRIX SE BEGINNING AT ADDRESS ISE21.
ISE21=ISE/2 -1
CALL MATLIB
& C < .LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,ESEE ,EPSE , DUCT ,EXCR ,
& FT ,F ,RT ,R ,.0 ,.0 ,.LELEN ,LMAT ,
& MAT ,MATTYP ,SE (ISE21) ,IELNO ,DAMAGE)
IF (ELSTIC) ESEE=(FT+F)*CRT+R)*.50
IF (PRINT.AND.FIRST) WRITE (6,1191)
IF (PRINT) WRITE (6,1192) IELNO,(DUCT(I),EXCR(I),I=1,5)
1191 FORMAT (/ ' SPRING DUCTILITIES AND EXCURSION RATIOS...'/,SK/
& ' ELEMENT',I12,' I - DUCTILITY DEFINITION #1 - I',
& ' I - DUCTILITY DEFINITION #2 - I',
& ' I - DUCTILITY DEFINITION #3 - I',/ I12,
& ' DUCTILITY EXCURSION ',
& ' DUCTILITY EXCURSION ',
& ' DUCTILITY EXCURSION ')
1192 FORMAT (I10,IP,6G15,6)
C
C----- RETURN
C----- MAXIMUM FORCES
1200 CONTINUE
IF (FIRST) WRITE (6,491) 'MAXIMUM LOAD AND DISPL. AT MAXIMUM LOAD'
& ' (NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY)'
WRITE(6,492) IELNO,0,TYPE(KTYPE),NODEI,NODEJ,FMAX(1),FMAX(2)
RETURN
C
C----- RESET INTERNAL FORCES
1300 CONTINUE
C
C----- ZERO MATRICES
F=0
FT=0
R=0
RT=0
V=0
VT=0
FMAX(1)=0
FMAX(2)=0
DO 1510 I=1,ISE
1510 SE(I)=0
WRITE (6,1350) IELNO
1350 FORMAT (' SPRING..... ELEMENT #',I6,
& ' INTERNAL FORCES AND HYSTERESIS MODELS ARE RESET TO ZERO')
CALL MATLIB
& C < .LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,ESEE ,EPSE , DUCT ,EXCR ,
& FT ,F ,RT ,R ,.0 ,.0 ,.LELEN ,LMAT ,
& MAT ,MATTYP ,SE ,IELNO ,DAMAGE)
RETURN
C
C----- DAMAGE INDEX
1400 IF (ELSTIC) RETURN
C
FMAX1=FMAX(1)
FMAX2=FMAX(2)
CALL MATLIB
& C < .LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,ESEE ,EPSE , DUCT ,EXCR ,
& FMAX1,0 ,FMAX2,0 ,.0 ,.0 ,.LELEN ,LMAT ,
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400 CONTINUE
IF (PRINT.AND.FIRST) WRITE (6,491) STEPID
IF (BTSTC(IBUG,7)) THEN
  WRITE (6,401) IELNO
401 FORMAT (1X,50X=' ',SHEAR WALL, ELEMENT#,16,1X,50X=' ')
ENDIF
C
C----- SET UP THE COMPONENT STIFFNESSES
SB= SECISEB)
SS= SECISES)
SA= SECISEA)
IF (BTSTC(IBUG,7)) WRITE (6,402) IELNO,SB,SS,SA
402 FORMAT(' IELNO:',11, ' SB:',1P,12.5, ' SS:',12.5, ' SA:',12.5)
C
C----- LOOP FOR EACH LOAD
DO 450 I=1,NLOAD
C
C----- TRANSFORM FRAME DISPL INTO LOCAL DISPL
DO 410 I=1,5
  RC(I)=0
  VC(I)=0
  DO 410 J=1,IELDOF
    K=LWKJ)
    RC(I)=RC(I)+KJ,I)*DISPL(K,LOAD)
    VC(I)=VC(I)+KJ,I)*VELOC(K)
410
C----- INCREMENTAL FORCES
FC(1)=SB*RC(1)/LENGTH
FC(2)=SS*RC(2)/LENGTH
FC(3)=SA*RC(3)/LENGTH
C
C----- CHECK STIFFNESS AND CALCULATE UNBALANCED FORCES
THIS IS PERFORMED ONLY FOR INELASTIC ANALYSIS
PC(1)=FT(1)+FC(1)
PC(2)=FT(2)+FC(2)
PC(3)=FT(3)+FC(3)
IF (.NOT. ELSTIC) THEN
  -- TRANSFER PERMANENT HYSTERESIS DATA TO TEMPORARY STORAGE...
  ISE2=ISE2/2
  DO 415 I=1,ISE2
    SE(I)=SE(I)+SE(I)
415
C----- BENDING
C----- SET UP TEMPORARY - TOTAL LOADS, DISPL'S AND VELOC
PL=FT(1)
O=RT(1)+RC(1)/LENGTH
DL=RT(1)/LENGTH
VC=VT(1)+VC(1)
C----- CALL HYST MODEL TO GET NEW STIFFNESS AND
THE TOTAL FORCE P AT DISPL. O.
MOPT=5
CALL MATLIB
& (MOPT,LSTTYP,FALSE,IREL,FALSE,NAME,
& ESEB,PSEB,DUCT(1,1),EXCR(1,1),
& PC(1),PL,O,DL,VC,VL,LELEM,LMAT
& MATB,MATTP,SE(ISE2+ISEB),IELNO,DAMAGE)
IF (SE(ISE2+ISEB).NE.SECISEB) NEMK=.TRUE.
C----- SHEAR
C----- SET UP TEMPORARY - TOTAL LOADS, DISPL'S AND VELOC
PL=FT(2)
O=RT(2)+RC(2)/LENGTH
DL=RT(2)/LENGTH
VC=VT(2)+VC(2)
C----- CALL HYST MODEL TO GET NEW STIFFNESS AND
THE TOTAL FORCE P AT DISPL. O.
MOPT=5
CALL MATLIB
& (MOPT,LSTTYP,FALSE,IREL,FALSE,NAME,
& ESES,PSES,DUCT(1,2),EXCR(1,2),
& PC(2),PL,O,DL,VC,VL,LELEM,LMAT
& MATS,MATTP,SE(ISE2+ISES),IELNO,DAMAGE)
IF (SE(ISE2+ISES).NE.SECISES) NEMK=.TRUE.
C----- AXIAL
C----- SET UP TEMPORARY - TOTAL LOADS, DISPL'S AND VELOC
PL=FT(3)
O=RT(3)+RC(3)/LENGTH
DL=RT(3)/LENGTH
VC=VT(3)+VC(3)
C----- CALL HYST MODEL TO GET NEW STIFFNESS AND
THE TOTAL FORCE P AT DISPL. O.
MOPT=5
CALL MATLIB
& (MOPT,LSTTYP,FALSE,IREL,FALSE,NAME,
& ESEA,PSEA,DUCT(1,3),EXCR(1,3),
& PC(3),PL,O,DL,VC,VL,LELEM,LMAT
& MATA,MATTP,SE(ISE2+ISEA),IELNO,DAMAGE)
IF (SE(ISE2+ISEA).NE.SECISEA) NEMK=.TRUE.
ENDIF
C
IF (ELSTIC) THEN
  ESEB=0.50*(FT(1)+FC(1))*RT(1)+RC(1)
  ESES=0.50*(FT(2)+FC(2))*RT(2)+RC(2)
  ESEA=0.50*(FT(3)+FC(3))*RT(3)+RC(3)
  ESE=ESEB+ESES+ESEA
  PSE=0.0
ELSE
  ESE=(ESEB+ESES+ESEA)*LENGTH
  PSE=(PSEB+PSES+PSEA)*LENGTH
ENDIF
C
C----- SAVE MAXIMUM LOADS
IF (NLOAD.GT.1) THEN
  DO 589 I=1,5
    IF (ABS(FC(I)).GT.ABS(FMAX(I))) THEN
      FMAX(I)=FC(I)
      FMAX(I+5)=RC(I)
    ENDIF
589 CONTINUE
ENDIF
C
C----- PRINT DATA
IF (PRINT) WRITE (6,592) IELNO,LOAD,
& IDKJ1,IDXJ2,IDXJ3,IDXJ4,
& (FC(I),RC(I),I=1,5)
592 FORMAT (11O,15,2X,415,1P,6G15.6)
C
C----- CALCULATE THE UNBALANCED MEMBER FORCE ON A JOINT.
IF (LOAD.EQ.1) THEN
  UBN = - ( FC(1)+FT(1)-PC(1) )
  UBS = - ( FC(2)+FT(2)-PC(2) )
  UBA = - ( FC(3)+FT(3)-PC(3) )
  DO 440 I=1,IELDOF
    K=LWKI)
    EFUBK(I)= ACT(1)*UBN + ACT(2)*UBS + ACT(3)*UBA
    FBK(K)= FBK(K) + EFUBK(I)
440
IF (BTSTC(IBUG,7)) THEN
  WRITE (6,495) (I,FC(I),FT(I),PC(I),I=1,5)
  WRITE (6,*) 'UB: M.S.A =',UBN,UBS,UBA
  WRITE (6,496) (I,LWKI),EFUBK(I),I=1,IELDOF)
ENDIF
ENDIF
FC(1)=PC(1)-FT(1)
FC(2)=PC(2)-FT(2)
FC(3)=PC(3)-FT(3)
450 CONTINUE
C
491 FORMAT (' R/C SHEAR WALL FORCES...',5X,AV
& ' ELEMENT LOAD: TYP,
& ' INT-1', ' INT-2', ' INT-5', ' INT-4',
& ' MOMENT', ' ROTATION',
& ' SHEAR', ' SHEAR DISPL.',
& ' AXIAL', ' AXIAL DISPL.' )
492 FORMAT (11O,15,2X,415,1P,6G15.6)
495 FORMAT (' I',11, ' F',1P,12.5, ' FT',12.5, ' P',12.5)
496 FORMAT (' I',15, ' LWKID',16, ' FBKID',1P,12.5)
C
IOPT=IOPT
RETURN
===== DETERMINE TOTAL FORCES, ENERGIES ECT =====
500 CONTINUE
IF (PRINT.AND.FIRST) WRITE (6,491) STEPID
C----- TOTAL FORCES, DISPLACEMENTS AND VELOCITIES
DO 510 I=1,5
  RT(I)=FT(I)+FC(I)
  RC(I)=RT(I)+RC(I)
  VT(I)=VTC(I)+VC(I)
  IF (ABS(FC(I)).GT.ABS(FMAX(I))) THEN
    FMAX(I)=FC(I)
    FMAX(I+5)=RC(I)
  ENDIF
510 CONTINUE
C----- PRINT DATA
IF (PRINT) WRITE (6,492) IELNO,LOAD,
& IDKJ1,IDXJ2,IDXJ3,IDXJ4,
& (FC(I),RT(I),I=1,5)
C----- TRANSFER TEMPORARY HYSTERESIS DATA TO PERMANENT STORAGE...
ISE2=ISE2/2
IF (.NOT.ELSTIC) THEN
  DO 520 I=1,ISE2
    SE(I)=SE(I)+ISE2
520
ENDIF
RETURN
===== DETERMINE FIXED END FORCES. AND ADD TO FORCE =====
600 RETURN
C----- FIXED END FORCES ARE NOT AVAILABLE FOR R/C SHEAR WALL
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===== WRITE MEMBER FORCES TO OUTPUT FILE =====
700 CONTINUE
C
C----- BENDING ENERGY, DUCTILITY AND EXCURSION .....
IF (ELSTIC) THEN
  ESEB=0.50*(FC(1)+RC(1))*RT(1)+RC(1)
  ESES=0.50*(FC(2)+RC(2))*RT(2)+RC(2)
  ESEA=0.50*(FC(3)+RC(3))*RT(3)+RC(3)
  ESE=ESEB+ESES+ESEA
ELSE
  CALL MATLIB
& (4, LSTTYP,FALSE,IREL,FALSE,NAME,
& ESEB,PSEB,DUCT(1,1),EXCR(1,1),
& FT,RT,R,0,0,0,LELEM,LMAT
& MATB,MATTP,SE(ISEB),IELNO,DAMAGE)
C----- SHEAR ENERGY, DUCTILITY AND EXCURSION .....
CALL MATLIB
& (4, LSTTYP,FALSE,IREL,FALSE,NAME,
& ESES,PSES,DUCT(1,2),EXCR(1,2),
& FT,RT,R,0,0,0,LELEM,LMAT
& MATS,MATTP,SE(ISES),IELNO,DAMAGE)
C----- AXIAL ENERGY, DUCTILITY AND EXCURSION .....
CALL MATLIB
& (4, LSTTYP,FALSE,IREL,FALSE,NAME,
& ESEA,PSEA,DUCT(1,3),EXCR(1,3),
& FT,RT,R,0,0,0,LELEM,LMAT
& MATA,MATTP,SE(ISEA),IELNO,DAMAGE)
C
ESE=(ESEB+ESES+ESEA)*LENGTH
PSE=(PSEB+PSES+PSEA)*LENGTH
ENDIF
C
IF (PRINT) WRITE (IUNIT,710) IDKJ1,IDXJ2,IDXJ3,IDXJ4
WRITE (IUNIT,711) (FC(I),RT(I),I=1,5),ESE,PSE
710 FORMAT (415,1P,6E10.5)
711 FORMAT (1P,6E10.5)
C
RETURN
C
===== READ AND PRINT MEMBER FORCES FROM OUTPUT FILE =====
800 CONTINUE
SX=0
SNX=0
SV=0
SNV=0
SN=0
BACKSPACE(IUNIT)
READ (IUNIT,*) ITYPE,IELNO,WRITE,TO,DT
READ (IUNIT,710) NODE1,NODE2,NODE3,NODE4
ISTEP=-IWRITE
AVENV=0
ICOUNT=0
C
810 READ (IUNIT,815,END=850) (FC(I),RC(I),I=1,5),ESE,PSE
815 FORMAT (8E10.5)
ISTEP=ISTEP+IWRITE
IF (ISTEP.EQ.0) WRITE (6,805) NODE1,NODE2,NODE3,NODE4
IF (MOD(ISTEP,INC).EQ.0)
  & WRITE (6,820) ISTEP,1,(FC(I),RC(I),I=1,5),ESE,PSE
  & SX = SX + FC(2)
  & SNX = SNX + FC(2)*FC(2)
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SV = SV + FC1)
ELOC8650 SKV = SKV + FC1)*FC2)
ELOC8660 SN = SN + 1
ELOC8670 IF (FC2).NE.0) THEN
ELOC8680 RATIOV = F1)/FC2)
ELOC8690 AVEVM=AVEVM+RATIOV
ELOC8700 ICOUNT=ICOUNT+1
ELOC8710 ENDF
ELOC8720 GO TO 810
C
850 CONTINUE
AVEVM=AVEVM/ MAX(ICOUNT,1)
WRITE (6,851) AVEVM,ICOUNT
IF (SV.NE.0) THEN
RMSV/SX
ICOUNT=SN
WRITE (6,855) RM,ICOUNT
ENDF
DM = SN*SK - SK*SN
DB = SN*SN - SK*SN
IF (DM.NE.0 .AND. DB.NE.0) THEN
RB = ( SN*SK - SK*SN ) / DB
RM = ( SN*SV - SK*SV ) / DM
ICOUNT=SN
WRITE (6,855) RM,RB,ICOUNT
ENDF
851 FORMAT(/10,'AVERAGE MOMENT/SheAR RATIO'=,1P,G12.4,5X,OP,16,
& ' POINTS WERE USED',
& ' POINTS WITH V=0 ARE EXCLUDED')
852 FORMAT(/10,'REGRESSION MOMENT-SHEAR EQU: ',
& ' M ',1P,G12.4,' V ',1P,G12.4,5X,
& ' OP,16,' POINTS WERE USED')
853 FORMAT(/10,'REGRESSION MOMENT-SHEAR EQU: ',
& ' M ',1P,G12.4,' V ',1P,G12.4,5X,
& ' OP,16,' POINTS WERE USED')
C
805 FORMAT (/ ' R/C SHEAR WALL FORCES...')
& SX,MODE1',16,5X,MODE2',16,5X,MODE3',16,5X,MODE4',16,5X,
& STEP TIME
& MOMENT ROTATION
& SHEAR SHEAR DISPL.
& AXIAL AXIAL DISPL.
& ESE PSE
820 FORMAT (16,1P,G12.4,5X,2G14.5,2G12.4)
835 FORMAT (/10,' MAXIMUM DUCTILITIES AND EXCURSION RATIOS')
&
840 FORMAT (/10,'
& T15,'DISPLACEMENT DEFINATION: U1=',1P,G12.4,5X,'E1',G12.4/
& T15,'ENERGY DEFINATION #1: U2=',1P,G12.4,5X,'E2',G12.4/
& T15,'ENERGY DEFINATION #2: U3=',1P,G12.4,5X,'E3',G12.4/
&
RETURN
C
***** DETERMINE THE LENGTH OF THE MATERIAL DATA
900 CONTINUE
ISE=0
C----- LOOP FOR EACH MATERIAL
DO 910 I=1,5
IF (I.EQ.1) THEN
ISE=ISE+1
ELSE IF (I.EQ.2) THEN
ISE=ISE+1
ELSE IF (I.EQ.3) THEN
ISE=ISE+1
ELSE IF (I.EQ.4) THEN
ISE=ISE+1
ELSE IF (I.EQ.5) THEN
ISE=ISE+1
ENDIF
MATS = RINPUT(I)
CALL MATLIB
& C 0 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
& ESEB ,PSEB ,DUCT(1,1) ,EXCR(1,1) ,
& FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
& MATS ,MATTP ,SEC(ISEB) ,IELNO ,DAMAGE )
&
ISE=ISE + LELEM
910
C----- DOUBLE THE STORAGE, TO ALLOW FOR TEMPORARY VALUES...
ISE=ISE*2
C
RETURN
C
***** DETERMINE THE STRAIN ENERGY
1000 CONTINUE
***** DUCTILITIES AND EXCURSION RATIOS
1100 CONTINUE
C ... NOTE ELEOS WAS LAST CALLED TO CALC INCREMENTAL DISPL.
C THE ENERGIES ASSOCIATED WITH INCR DISPL ARE STORED IN
C THE ADDRESSES: ISEB=ISE/2
C ISE=ISE/2
C ISE=ISE/2
C----- BENDING ENERGY, DUCTILITY AND EXCURSION *****
ISE2=ISE/2
CALL MATLIB
& C 0 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
& ESEB ,PSEB ,DUCT(1,1) ,EXCR(1,1) ,
& FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
& MATS ,MATTP ,SEC(ISEB+ISE2) ,IELNO ,DAMAGE )
C----- SHEAR ENERGY, DUCTILITY AND EXCURSION *****
CALL MATLIB
& C 0 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
& ESEB ,PSEB ,DUCT(1,2) ,EXCR(1,2) ,
& FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
& MATS ,MATTP ,SEC(ISES+ISE2) ,IELNO ,DAMAGE )
C----- AXIAL ENERGY, DUCTILITY AND EXCURSION *****
CALL MATLIB
& C 0 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
& ESEB ,PSEB ,DUCT(1,3) ,EXCR(1,3) ,
& FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
& MATS ,MATTP ,SEC(ISEA+ISE2) ,IELNO ,DAMAGE )
C
IF (ELSTIC) THEN
ESEB=0.50*(FT(1)+FC1)*RT(1)+R(1))
ESES=0.50*(FT(2)+FC2)*RT(2)+R(2))
ESEA=0.50*(FT(3)+FC3)*RT(3)+R(3))
ESE = ESEB+ESES+ESEA
PSE=0.0
ELSE
ESE=(ESEB+ESES+ESEA)*LENGTH
PSE=(PSEB+PSES+PSEA)*LENGTH
ENDIF
C
IF (BTSTC(1BUG,7)) THEN
WRITE (6,*) 'ESEB ESES ESEA ' ,ESEB,ESES,ESEA
WRITE (6,*) 'PSEB PSES PSEA ' ,PSEB,PSES,PSEA
WRITE (6,*) 'ESE PSE LENGTH' ,ESE ,PSE ,LENGTH
ENDF
ELOC8620 IF (PRINT.AND.FIRST) WRITE (6,1191)
ELOC8630 IF (PRINT) WRITE (6,1192)IELNO,((DUCT(I,J),EXCR(I,J),I=1,5),J=1,5)
ELOC8640 1192 FORMAT (1X,IS,18F7.2)
ELOC8650 1191 FORMAT (/ ' R/C SHEAR WALL DUCTILITY AND EXCURSION RATIOS'/6X,
ELOC8660 & ' |----- BENDING COMPONENT -----|',
ELOC8670 & ' |----- SHEAR COMPONENT -----|',
ELOC8680 & ' |----- AXIAL COMPONENT -----|',
ELOC8690 & ' |----- ELEM# -----|',
ELOC8700 & ' |----- DEFN 1 ----- DEFN 2 ----- DEFN 3 -----|',
ELOC8710 & ' |----- DEFN 1 ----- DEFN 2 ----- DEFN 3 -----|',
ELOC8720 & ' |----- DEFN 1 ----- DEFN 2 ----- DEFN 3 -----|',
ELOC8730 & ' |----- DEFN 1 ----- DEFN 2 ----- DEFN 3 -----|',
ELOC8740 & ' |----- DUCT. EXCR. DUCT. EXCR. DUCT. EXCR. -----|',
ELOC8750 & ' |----- DUCT. EXCR. DUCT. EXCR. DUCT. EXCR. -----|',
ELOC8760 & ' |----- DUCT. EXCR. DUCT. EXCR. DUCT. EXCR. -----|',
ELOC8770 RETURN
ELOC8780
ELOC8790 C----- WRITE MAXIMUM AND MINIMUM VALUES
ELOC8800 1200 CONTINUE
ELOC8810 IF (FIRST) WRITE(6,491)'MAXIMUM LOADS AND DISPL AT MAXIMUM LOADS
ELOC8820 & ' // NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY'
ELOC8830 & ' WRITE (6,492) IELNO,LOAD,
ELOC8840 & ' IDX(J),IDJ,IDX(J),IDJ,IDX(J),
ELOC8850 & ' (FMASK(I),FMASK(I+1),I=1,5)
ELOC8860 RETURN
ELOC8870
ELOC8880 C----- RESET INTERNAL FORCES
ELOC8890 1500 CONTINUE
ELOC8900
ELOC8910 C----- ZERO MATRICES
ELOC8920 DO 1510 I=1,ISE
ELOC8930 1510
ELOC8940 DO 1525 I=1,5
ELOC8950 FMASK(I)=0
ELOC8960 FMASK(I+5)=0
ELOC8970 F(I)=0
ELOC8980 F(I)=0
ELOC8990 R(I)=0
ELOC9000 RT(I)=0
ELOC9010 V(I)=0
ELOC9020 V(I)=0
ELOC9030 1525
ELOC9040 WRITE (6,1550) IELNO
ELOC9050 1550 FORMAT (/ ' SHEAR WALL..... ELEMENT #',I6,
ELOC9060 & ' INTERNAL FORCES AND HYSTERESIS MODELS ARE RESET TO ZERO')
ELOC9070
ELOC9080 CALL MATLIB
ELOC9090 & C 2 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9100 & ESEB ,PSEB ,DUCT(1,1) ,EXCR(1,1) ,
ELOC9110 & FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
ELOC9120 & MATS ,MATTP ,SEC(ISEB) ,IELNO ,DAMAGE )
ELOC9130 CALL MATLIB
ELOC9140 & C 2 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9150 & ESES ,PSES ,DUCT(1,2) ,EXCR(1,2) ,
ELOC9160 & FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
ELOC9170 & MATS ,MATTP ,SEC(ISES) ,IELNO ,DAMAGE )
ELOC9180 CALL MATLIB
ELOC9190 & C 2 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9200 & ESEA ,PSEA ,DUCT(1,3) ,EXCR(1,3) ,
ELOC9210 & FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
ELOC9220 & MATS ,MATTP ,SEC(ISEA) ,IELNO ,DAMAGE )
ELOC9230 CALL MATLIB
ELOC9240 & C 2 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9250 & ESEB ,PSEB ,DUCT(1,5) ,EXCR(1,5) ,
ELOC9260 & FT ,F ,RT ,R ,0 ,0 ,0 ,LELEM ,LMAT ,
ELOC9270 & MATS ,MATTP ,SEC(ISEB) ,IELNO ,DAMAGE )
ELOC9280 RETURN
ELOC9290 C----- DAMAGE INDEX
ELOC9300 1400 IF (ELSTIC) RETURN
ELOC9310 FMASK=FMASK(1)
ELOC9320 FMASK=FMASK(2)
ELOC9330 FMASK=FMASK(3)
ELOC9340 FMASK=FMASK(4)
ELOC9350 FMASK=FMASK(5)
ELOC9360 FMASK=FMASK(6)
ELOC9370 C----- BENDING ENERGY, AND DAMAGE INDEX
ELOC9380 CALL MATLIB
ELOC9390 & C 5 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9400 & ESEB ,PSEB ,DUCT(1,1) ,EXCR(1,1) ,
ELOC9410 & FMASK(1) , FMASK(2) , FMASK(3) , FMASK(4) , FMASK(5) ,
ELOC9420 & MATS ,MATTP ,SEC(ISEB) ,IELNO ,DAMAGE )
ELOC9430 C----- BENDING ENERGY, AND DAMAGE INDEX
ELOC9440 CALL MATLIB
ELOC9450 & C 5 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9460 & ESES ,PSES ,DUCT(1,2) ,EXCR(1,2) ,
ELOC9470 & FMASK(1) , FMASK(2) , FMASK(3) , FMASK(4) , FMASK(5) ,
ELOC9480 & MATS ,MATTP ,SEC(ISES) ,IELNO ,DAMG )
ELOC9490 C----- AXIAL ENERGY, AND DAMAGE INDEX
ELOC9500 CALL MATLIB
ELOC9510 & C 5 ,LSTTYP ,FALSE ,IREL ,FALSE ,NAME ,
ELOC9520 & ESEA ,PSEA ,DUCT(1,3) ,EXCR(1,3) ,
ELOC9530 & FMASK(1) , FMASK(2) , FMASK(3) , FMASK(4) , FMASK(5) ,
ELOC9540 & MATS ,MATTP ,SEC(ISEA) ,IELNO ,DAMA )
ELOC9550 C
ELOC9560 ESE=(ESEB+ESES+ESEA)*LENGTH
ELOC9570 PSE=(PSEB+PSES+PSEA)*LENGTH
ELOC9580 DAMGE=(DAMG+ESEB+PSEB)+DAMG*(ESES+PSES)+DAMA*(ESEA+PSEA)*LENGTH
ELOC9590 IF (FIRST) WRITE (6,1420)
ELOC9600 1420 FORMAT (1X,IS,5KOP,F14.5,1P,2G14.5)
ELOC9610 1410 FORMAT (/6X,
ELOC9620 & ' |----- BENDING COMPONENT -----|',
ELOC9630 & ' |----- SHEAR COMPONENT -----|',
ELOC9640 & ' |----- AXIAL COMPONENT -----|',
ELOC9650 & ' |----- ELEM# -----|',
ELOC9660 & ' |----- DAMAGE ----- ESE ----- PSE -----|',
ELOC9670 & ' |----- DAMAGE ----- ESE ----- PSE -----|',
ELOC9680 & ' |----- DAMAGE ----- ESE ----- PSE -----|',
ELOC9690 RETURN
ELOC9700 END
ELOC9710 C----- ENERGY BALANCE
ELOC9720 ENEO0000
ELOC9730 ENEO0050
ELOC9740 ENEO0060
ELOC9750 ENEO0070
ELOC9760 ENEO0080
ELOC9770 ENEO0090
ELOC9780 ENEO0100
ELOC9790 ENEO0110
ELOC9800 ENEO0120
ELOC9810 ENEO0130
ELOC9820 ENEO0140
ELOC9830 ENEO0150
ELOC9840 ENEO0160
ELOC9850 ENEO0170
ELOC9860 ENEO0180
ELOC9870 ENEO0190
ELOC9880 ENEO0200
ELOC9890 ENEO0210
ELOC9900 ENEO0220
ELOC9910 ENEO0230
ELOC9920 ENEO0240
ELOC9930 ENEO0250
ELOC9940 ENEO0260
ELOC9950 ENEO0270
ELOC9960 ENEO0280
ELOC9970 ENEO0290
ELOC9980 ENEO0300
ELOC9990 ENEO0310
ELOC0000 ENEO0320
ELOC0010 ENEO0330
ELOC0020 ENEO0340
ELOC0030 ENEO0350
ELOC0040 ENEO0360
ELOC0050 ENEO0370
ELOC0060 ENEO0380
ELOC0070 ENEO0390
ELOC0080 ENEO0400
ELOC0090 ENEO0410
ELOC0100 ENEO0420
ELOC0110 ENEO0430
ELOC0120 ENEO0440
ELOC0130 ENEO0450
ELOC0140 ENEO0460
ELOC0150 ENEO0470
ELOC0160 ENEO0480
ELOC0170 ENEO0490
ELOC0180 ENEO0500
ELOC0190 ENEO0510
ELOC0200 ENEO0520
ELOC0210 ENEO0530
ELOC0220 ENEO0540
ELOC0230 ENEO0550
ELOC0240 ENEO0560
ELOC0250 ENEO0570
ELOC0260 ENEO0580
ELOC0270 ENEO0590
ELOC0280 ENEO0600
ELOC0290 ENEO0610
ELOC0300 ENEO0620
ELOC0310 ENEO0630
ELOC0320 ENEO0640
ELOC0330 ENEO0650
ELOC0340 ENEO0660
ELOC0350 ENEO0670
ELOC0360 ENEO0680
ELOC0370 ENEO0690
ELOC0380 ENEO0700
ELOC0390 ENEO0710
ELOC0400 ENEO0720
ELOC0410 ENEO0730
ELOC0420 ENEO0740
ELOC0430 ENEO0750
ELOC0440 ENEO0760
ELOC0450 ENEO0770
ELOC0460 ENEO0780
ELOC0470 ENEO0790
ELOC0480 ENEO0800
ELOC0490 ENEO0810
ELOC0500 ENEO0820
ELOC0510 ENEO0830
ELOC0520 ENEO0840
ELOC0530 ENEO0850
ELOC0540 ENEO0860
ELOC0550 ENEO0870
ELOC0560 ENEO0880
ELOC0570 ENEO0890
ELOC0580 ENEO0900
ELOC0590 ENEO0910
ELOC0600 ENEO0920
ELOC0610 ENEO0930
ELOC0620 ENEO0940
ELOC0630 ENEO0950
ELOC0640 ENEO0960
ELOC0650 ENEO0970
ELOC0660 ENEO0980
ELOC0670 ENEO0990
ELOC0680 ENEO1000
ELOC0690 ENEO1010
ELOC0700 ENEO1020
ELOC0710 ENEO1030
ELOC0720 ENEO1040
ELOC0730 ENEO1050
ELOC0740 ENEO1060
ELOC0750 ENEO1070
ELOC0760 ENEO1080
ELOC0770 ENEO1090
ELOC0780 ENEO1100
ELOC0790 ENEO1110
ELOC0800 ENEO1120
ELOC0810 ENEO1130
ELOC0820 ENEO1140
ELOC0830 ENEO1150
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ELOC0850 ENEO1170
ELOC0860 ENEO1180
ELOC0870 ENEO1190
ELOC0880 ENEO1200
ELOC0890 ENEO1210
ELOC0900 ENEO1220
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ELOC0960 ENEO1280
ELOC0970 ENEO1290
ELOC0980 ENEO1300
ELOC0990 ENEO1310
ELOC1000 ENEO1320
ELOC1010 ENEO1330
ELOC1020 ENEO1340
ELOC1030 ENEO1350
ELOC1040 ENEO1360
ELOC1050 ENEO1370
ELOC1060 ENEO1380
ELOC1070 ENEO1390
ELOC1080 ENEO1400
ELOC1090 ENEO1410
ELOC1100 ENEO1420
ELOC1110 ENEO1430
ELOC1120 ENEO1440
ELOC1130 ENEO1450
ELOC1140 ENEO1460
ELOC1150 ENEO1470
ELOC1160 ENEO1480
ELOC1170 ENEO1490
ELOC1180 ENEO1500
ELOC1190 ENEO1510
ELOC1200 ENEO1520
ELOC1210 ENEO1530
ELOC1220 ENEO1540
ELOC1230 ENEO1550
ELOC1240 ENEO1560
ELOC1250 ENEO1570
ELOC1260 ENEO1580
ELOC1270 ENEO1590
ELOC1280 ENEO1600
ELOC1290 ENEO1610
ELOC1300 ENEO1620
ELOC1310 ENEO1630
ELOC1320 ENEO1640
ELOC1330 ENEO1650
ELOC1340 ENEO1660
ELOC1350 ENEO1670
ELOC1360 ENEO1680
ELOC1370 ENEO1690
ELOC1380 ENEO1700
ELOC1390 ENEO1710
ELOC1400 ENEO1720
ELOC1410 ENEO1730
ELOC1420 ENEO1740
ELOC1430 ENEO1750
ELOC1440 ENEO1760
ELOC1450 ENEO1770
ELOC1460 ENEO1780
ELOC1470 ENEO1790
ELOC1480 ENEO1800
ELOC1490 ENEO1810
ELOC1500 ENEO1820
ELOC1510 ENEO1830
ELOC1520 ENEO1840
ELOC1530 ENEO1850
ELOC1540 ENEO1860
ELOC1550 ENEO1870
ELOC1560 ENEO1880
ELOC1570 ENEO1890
ELOC1580 ENEO1900
ELOC1590 ENEO1910
ELOC1600 ENEO1920
ELOC1610 ENEO1930
ELOC1620 ENEO1940
ELOC1630 ENEO1950
ELOC1640 ENEO1960
ELOC1650 ENEO1970
ELOC1660 ENEO1980
ELOC1670 ENEO1990
ELOC1680 ENEO2000
ELOC1690 ENEO2010
ELOC1700 ENEO2020
ELOC1710 ENEO2030
ELOC1720 ENEO2040
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ELOC1760 ENEO2080
ELOC1770 ENEO2090
ELOC1780 ENEO2100
ELOC1790 ENEO2110
ELOC1800 ENEO2120
ELOC1810 ENEO2130
ELOC1820 ENEO2140
ELOC1830 ENEO2150
ELOC1840 ENEO2160
ELOC1850 ENEO2170
ELOC1860 ENEO2180
ELOC1870 ENEO2190
ELOC1880 ENEO2200
ELOC1890 ENEO2210
ELOC1900 ENEO2220
ELOC1910 ENEO2230
ELOC1920 ENEO2240
ELOC1930 ENEO2250
ELOC1940 ENEO2260
ELOC1950 ENEO2270
ELOC1960 ENEO2280
ELOC1970 ENEO2290
ELOC1980 ENEO2300
ELOC1990 ENEO2310
ELOC2000 ENEO2320
ELOC2010 ENEO2330
ELOC2020 ENEO2340
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ELOC2080 ENEO2400
ELOC2090 ENEO2410
ELOC2100 ENEO2420
ELOC2110 ENEO2430
ELOC2120 ENEO2440
ELOC2130 ENEO2450
ELOC2140 ENEO2460
ELOC2150 ENEO2470
ELOC2160 ENEO2480
ELOC2170 ENEO2490
ELOC2180 ENEO2500
ELOC2190 ENEO2510
ELOC2200 ENEO2520
ELOC2210 ENEO2530
ELOC2220 ENEO2540
ELOC2230 ENEO2550
ELOC2240 ENEO2560
ELOC2250 ENEO2570
ELOC2260 ENEO2580
ELOC2270 ENEO2590
ELOC2280 ENEO2600
ELOC2290 ENEO2610
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ELOC2450 ENEO2770
ELOC2460 ENEO2780
ELOC2470 ENEO2790
ELOC2480 ENEO2800
ELOC2490 ENEO2810
ELOC2500 ENEO2820
ELOC2510 ENEO2830
ELOC2520 ENEO2840
ELOC2530 ENEO2850
ELOC2540 ENEO2860
ELOC2550 ENEO2870
ELOC2560 ENEO2880
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ELOC2580 ENEO2900
ELOC2590 ENEO2910
ELOC2600 ENEO2920
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ELOC2630 ENEO2950
ELOC2640 ENEO2960
ELOC2650 ENEO2970
ELOC2660 ENEO2980
ELOC2670 ENEO2990
ELOC2680 ENEO3000
ELOC2690 ENEO3010
ELOC2700 ENEO3020
ELOC2710 ENEO3030
ELOC2720 ENEO3040
ELOC2730 ENEO3050
ELOC2740 ENEO3060
ELOC2750 ENEO3070
ELOC2760 ENEO3080
ELOC2770 ENEO3090
ELOC2780 ENEO3100
ELOC2790 ENEO3110
ELOC2800 ENEO3120
ELOC2810 ENEO3130
ELOC2820 ENEO3140
ELOC2830 ENEO3150
ELOC2840 ENEO3160
ELOC2850 ENEO3170
ELOC2860 ENEO3180
ELOC2870 ENEO3190
ELOC2880 ENEO3200
ELOC2890 ENEO3210
ELOC2900 ENEO3220
ELOC2910 ENEO3230
ELOC2920 ENEO3240
ELOC2930 ENEO3250
ELOC2940 ENEO3260
ELOC2950 ENEO3270
ELOC2960 ENEO3280
ELOC2970 ENEO3290
ELOC2980 ENEO3300
ELOC2990 ENEO3310
ELOC3000 ENEO3320
ELOC3010 ENEO3330
ELOC3020 ENEO3340
ELOC3030 ENEO3350
ELOC3040 ENEO3360
ELOC3050 ENEO3370
ELOC3060 ENEO3380
ELOC3070 ENEO3390
ELOC3080 ENEO3400
ELOC3090 ENEO3410
ELOC3100 ENEO3420
ELOC3110 ENEO3430
ELOC3120 ENEO3440
ELOC3130 ENEO3450
ELOC3140 ENEO3460
ELOC3150 ENEO3470
ELOC3160 ENEO3480
ELOC3170 ENEO3490
ELOC3180 ENEO3500
ELOC3190 ENEO3510
ELOC3200 ENEO3520
ELOC3210 ENEO3530
ELOC3220 ENEO3540
ELOC3230 ENEO3550
ELOC3240 ENEO3560
ELOC3250 ENEO3570
ELOC3260 ENEO3580
ELOC3270 ENEO3590
ELOC3280 ENEO3600
ELOC3290 ENEO3610
ELOC3300 ENEO3620
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ELOC3340 ENEO3660
ELOC3350 ENEO3670
ELOC3360 ENEO3680
ELOC3370 ENEO3690
ELOC3380 ENEO3700
ELOC3390 ENEO3710
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ELOC3440 ENEO3760
ELOC3450 ENEO3770
ELOC3460 ENEO3780
ELOC3470 ENEO3790
ELOC3480 ENEO3800
ELOC3490 ENEO3810
ELOC3500 ENEO3820
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ELOC3540 ENEO3860
ELOC3550 ENEO3870
ELOC3560 ENEO3880
ELOC3570 ENEO3890
ELOC3580 ENEO3900
ELOC3590 ENEO3910
ELOC3600 ENEO3920
ELOC3610 ENEO3930
ELOC3620 ENEO3940
ELOC3630 ENEO3950
ELOC3640 ENEO3960
ELOC3650 ENEO3970
ELOC3660 ENEO3980
ELOC3670 ENEO3990
ELOC3680 ENEO4000
ELOC3690 ENEO4010
ELOC3700 ENEO4020
ELOC3710 ENEO4030
ELOC3720 ENEO4040
ELOC3730 ENEO4050
ELOC3740 ENEO4060
ELOC3750 ENEO4070
ELOC3760 ENEO4080
ELOC3770 ENEO4090
ELOC3780 ENEO4100
ELOC3790 ENEO4110
ELOC3800 ENEO4120
ELOC3810 ENEO4130
ELOC3820 ENEO4140
ELOC3830 ENEO4150
ELOC3840 ENEO4160
ELOC3850 ENEO4170
ELOC3860 ENEO4180
ELOC3870 ENEO4190
ELOC3880 ENEO4200
ELOC3890 ENEO4210
ELOC3900 ENEO4220
ELOC3910 ENEO4230
ELOC3920 ENEO4240
ELOC3930 ENEO4250
ELOC3940 ENEO4260
ELOC3950 ENEO4270
ELOC3960 ENEO4280
ELOC3970 ENEO4290
ELOC3980 ENEO4300
ELOC3990 ENEO4310
ELOC4000 ENEO4320
ELOC4010 ENEO4330
ELOC4020 ENEO4340
ELOC4030 ENEO4350
ELOC4040 ENEO4360
ELOC4050 ENEO4370
ELOC4060 ENEO4380
ELOC4070 ENEO4390
ELOC4080 ENEO4400
ELOC4090 ENEO4410
ELOC4100 ENEO4420
ELOC4110 ENEO4430
ELOC4120 ENEO4440
ELOC4130 ENEO4450
ELOC4140 ENEO4460
ELOC4150 ENEO4470
ELOC4160 ENEO4480
ELOC4170 ENEO4490
ELOC4180 ENEO4500
ELOC4190 ENEO4510
ELOC4200 ENEO4520
ELOC4210 ENEO4530
ELOC4220 ENEO4540
ELOC4230 ENEO4550
ELOC4240 ENEO4560
ELOC4250 ENEO4570
ELOC4260 ENEO4580
ELOC4270 ENEO4590
ELOC4280 ENEO4600
ELOC4290 ENEO4610
ELOC4300 ENEO4620
ELOC4310 ENEO4630
ELOC4320 ENEO4640
ELOC4330 ENEO4650
ELOC4340 ENEO4660
ELOC4350 ENEO4670
ELOC4360 ENEO4680
ELOC4370 ENEO4690
ELOC4380 ENEO4700
ELOC4390 ENEO4710
ELOC4400 ENEO4720
ELOC4410 ENEO4730
ELOC4420 ENEO4740
ELOC4430 ENEO4750
ELOC4440 ENEO4760
ELOC4450 ENEO4770
ELOC4460 ENEO4780
ELOC4470 ENEO4790
ELOC4480 ENEO4800
ELOC4490 ENEO4810
ELOC4500 ENEO4820
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ELOC4580 ENEO4900
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ELOC4650 ENEO4970
ELOC4660 ENEO4980
ELOC4670 ENEO4990
ELOC4680 ENEO5000
ELOC4690 ENEO5010
ELOC4700 ENEO5020
ELOC4710 ENEO5030
ELOC4720 ENEO5040
ELOC4730 ENEO5050
ELOC4740 ENEO5060
ELOC4750 ENEO5070
ELOC4760 ENEO5080
ELOC4770 ENEO5090
ELOC4780 ENEO5100
ELOC4790 ENEO5110
ELOC4800 ENEO5120
ELOC4810 ENEO5130
ELOC4820 ENEO5140
ELOC4830 ENEO5150
ELOC4840 ENEO5160
ELOC4850 ENEO5170
ELOC4860 ENEO5180
ELOC4870 ENEO5190
ELOC4880 ENEO5200
ELOC4890 ENEO5210
ELOC4900 ENEO5220
ELOC4910 ENEO5230
ELOC4920 ENEO5240
ELOC4930 ENEO5250
ELOC4940 ENEO5260
ELOC4950 ENEO5270
ELOC4960 ENEO5280
ELOC4970 ENEO5290
ELOC4980 ENEO5300
ELOC4990 ENEO5310
ELOC5000 ENEO5320
ELOC5010 ENEO5330
ELOC5020 ENEO5340
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ELOC5050 ENEO5370
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ELOC5070 ENEO5390
ELOC5080 ENEO5400
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ELOC5100 ENEO5420
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ELOC5120 ENEO5440
ELOC5130 ENEO5450
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ELOC5160 ENEO5480
ELOC5170 ENEO5490
ELOC5180 ENEO5500
ELOC5190 ENEO5510
ELOC5200 ENEO5520
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ELOC5360 ENEO5680
ELOC5370 ENEO5690
ELOC5380 ENEO5700
ELOC5390 ENEO5710
ELOC5400 ENEO5720
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ELOC5480 ENEO5800
ELOC5490 ENEO5810
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ELOC5660 ENEO5980
ELOC5670 ENEO5990
ELOC5680 ENEO6000
ELOC5690 ENEO6010
ELOC5700 ENEO6020
ELOC5710 ENEO6030
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ELOC5740 ENEO6060
ELOC5750 ENEO6070
ELOC5760 ENEO6080
ELOC5770 ENEO6090
ELOC5780 ENEO6100
ELOC5790 ENEO6110
ELOC5800 ENEO6120
ELOC5810 ENEO6130
ELOC5820 ENEO6140
ELOC5830 ENEO6150
ELOC5840 ENEO6160
ELOC5850 ENEO6170
ELOC5860 ENEO6180
ELOC5870 ENEO6190
ELOC5880 ENEO6200
ELOC5890 ENEO6210
ELOC5900 ENEO6220
ELOC5910 ENEO6230
ELOC5920 ENEO6240
ELOC5930 ENEO6250
ELOC5940 ENEO6260
ELOC5950 ENEO6270
ELOC5960 ENEO6280
ELOC5970 ENEO6290
ELOC5980 ENEO6300
ELOC5990 ENEO6310
ELOC6000 ENEO6320
ELOC6010 ENEO6330
ELOC6020 ENEO6340
ELOC6030 ENEO6350
ELOC6040 ENEO6360
ELOC6050 ENEO6370
ELOC6060 ENEO6380
ELOC6070 ENEO6390
ELOC6080 ENEO6400
ELOC6090 ENEO6410
ELOC6100 ENEO6420
ELOC6110 ENEO6430
ELOC6120 ENEO
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      & Z(IZKE),NO,ZELDOF,MOKIELDOF+1,NZ(IZLN),1.)
C
C----- SUBTRACT GEOMETRIC STIFFNESS
      NZ(IZKDOT+5)=NZ(IZKDOT+5)
C
C IF (NZ(IZKDOT+5).EQ.1) THEN
      FALSE=.FALSE.
      CALL ELEMIB
      & (2,LSTTYP, FALSE, IREL, FALSE, NAME, EESE, EPSE, DAMAGE,
      & IELNO, ZELDOF, KGDOP, PGEOM, Z, AXIAL, IZDISP, IZLOAD, HSTOR)
C
      KGDOP=KGDOP
C
      IF (BUGS?) THEN
      WRITE (ELNO,15) IELNO,(NZ(I+IZLNG-1),I=1,MINKKGDOP,18))
      CALL LNMATRX(Z(IZKEG),NO,KGDOP,MOKKGDOP+1,ELNO)
      ENDDIF
C
      IF (.NOT. AXIAL) GO TO 120
      DETERMINE THE FACTOR FOR KG
      IF (NZ(IZKDOT+1).EQ.1) THEN
      ACCELZ=Z(IZKDOT)
      PGEOM=PGEOM*(1+ACCELZ)
      ENDDIF
C
      SNAP THE SIGN ON PGEOM FOR SUBTRACTION.....
      PGEOM=-PGEOM
C
      CALL FORML(Z(IZSTIF),NZ(IZNO),NOOF,NZ(IZNO+NOOF),
      & Z(IZKEG),NO,KGDOP,MOKKGDOP+1,NZ(IZLNG),PGEOM)
      ENDDIF
C
      120 CONTINUE
      RETURN
C----- ASSEMBLE GEOMETRIC STIFFNESS
      200 CONTINUE
      IF (NZ(IZKDOT+5).NE.2) RETURN
      IST=IZKG
      IEND=IZKG + NZ(IZMKG+NOOF) - 1
C----- ZERO STIFFNESS
      DO 210 I=IST,IEND
      Z(I)=0
      210
C----- LOOP FOR EACH ELEMENT
      DO 220 IELNO=1,NELNT
C----- GET STIFFNESS OF EACH ELEMENT
      FALSE=.FALSE.
      CALL ELEMIB
      & (2,LSTTYP, FALSE, IREL, FALSE, NAME, EESE, EPSE, DAMAGE,
      & IELNO, ZELDOF, KGDOP, PGEOM, Z, AXIAL, IZDISP, IZLOAD, HSTOR)
C
      IF (.NOT. AXIAL) GO TO 220
      IF (BUGS?) THEN
      WRITE (6,*) 'PGEOM=',PGEOM
      WRITE (ELNO,15) IELNO,(NZ(I+IZLNG-1),I=1,MINKKGDOP,18))
      CALL LNMATRX(Z(IZKEG),NO,KGDOP,MOKKGDOP+1,ELNO)
      ENDDIF
C
      CALL FORML(Z(IZKG),NZ(IZNO),NOOF,NZ(IZNO+NOOF),
      & Z(IZKEG),NO,KGDOP,MOKKGDOP+1,NZ(IZLNG),PGEOM)
      220 CONTINUE
      RETURN
      END
C-----
      SUBROUTINE FORML(K,NO,NOOF,IMD,KE,MOK,IELDOF,INOK,LM,FACTOR)
      DIMENSION MOK(NOOF+1),MOK(IELDOF+1),LM(IELDOF)
      REAL K(IMD),KE(INOK)
C-----
C MATRIX STORAGE SCHEME:
C THE STIFFNESS MATRIX (K) IS Banded AND SYMMETRIC.
C THUS ONLY THE SKYLINE ABOVE THE MAIN DIAGONAL NEEDS TO BE STORED.
C THE MATRIX K IS STORED IN A LINEAR ARRAY BY COLUMNS.
C THE VALUE ON THE MAIN DIAGONAL IS STORED IN THE LINEAR ARRAY FIRST.
C RELATIVE ADDRESSES OF THE LINEAR ARRAY ELEMENTS CONTAINING THE
C MAIN DIAGONAL TERMS ARE STORED IN MD.
C THUS: FOR K(I,J)
C IF I LE J (UPPER TRIANGULAR MATRIX)
C IJ=MOK(J)+J-I : RELATIVE ADDRESS IF ELEMENT (I,J)
C K(I,J)=K(IJ)
C ELSE
C K(I,J)=0 : (I,J) IS ABOVE THE SKYLINE
C-----
C EXAMPLE: LET B BE THE 5X5 FULL SYMMETRIC MATRIX BELOW...
      1 | 5 | | | |
      | 2 | 5 | | | |
      K= | | 4 | 7 | 10 |
      | | | 6 | 9 |
      | | | | 8 |
      LOGICAL BTEST
      MD= 1, 2, 4, 6, 8, 13
C
      SAV IZNO=121, IZSTIF=200
      MOK(1)=1 K(1)=1
      MOK(2)=2 K(2)=2
      MOK(3)=4 K(3)=3
      MOK(4)=6 K(4)=4
      MOK(5)=8 K(5)=5
      MOK(6)=15 K(6)=6
      K(7)=7
      K(8)=8
      K(9)=9
      K(10)=10
      K(11)=11
      K(12)=12
C
      THUS, FOR K(5,4) I=5, J=4
      IJ=MOK(J)+J-I = MOK(4)+4-5 = 6+4-5 = 7
      K(I,J)=K(IJ) = K(7) = 7 OK
C
      THUS, FOR K(2,4) I=2, J=4
      IJ=MOK(J)+J-I = MOK(4)+4-2 = 6+4-2 = 8
      MOK(J)+J-I = MOK(4)+1 = 8
      SINCE IJ GE MOK(J)+1
      K(I,J)=0 (I,J) IS ABOVE THE SKYLINE....
C-----
C THE ELEMENT STIFFNESS IS STORED IN A SIMILAR MANNER.
C KE IS THE LINEAR ARRAY CONTAINING THE ELEMENT STIFFNESS
C MOK IS THE ARRAY CONTAINING THE MAIN DIAGONAL ADDRESSES FOR KE
C-----
      MAP ELEMENT STIFFNESS INTO GLOBAL STIFFNESS

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FOR01050 C LI = GLOBAL DOF ASSOCIATED WITH THE I'ITH ROW OF THE MEMBER STIFF.
FOR01060 C LJ = GLOBAL DOF ASSOCIATED WITH THE I'ITH ROW OF THE MEMBER STIFF.
FOR01070 C IJELM = ABSOLUTE ADDRESS OF THE MEMBER STIFFNESS TERM (I,J)
FOR01080 C IJGLOB = ABSOLUTE ADDRESS OF THE GLOBAL STIFFNESS TERM (LI,LJ)
FOR01090 C
FOR01100 C* MAXIJ = MOK(NOOF+1)
FOR01110 C
FOR01120 C DO 50 I=1,IELDOF
FOR01130 C L=L*LI
FOR01140 C* IF (LI.LE.0 .OR. LI.GT.NOOF) GO TO 50
FOR01150 C DO 20 J=1,IELDOF
FOR01160 C LJA=L*LI+J
FOR01170 C* IF (LJ.LE.0 .OR. LJ.GT.NOOF) GO TO 20
FOR01180 C IJELM =MOK(J)+J-I
FOR01190 C IF (KEC(LJELM).EQ.0) GO TO 20
FOR01200 C IF (LI.LE.LJ) THEN
FOR01210 C IJGLOB=MOK(LJ)+LJ-LI
FOR01220 C ELSE
FOR01230 C IJGLOB=MOK(LI)+LI-LJ
FOR01240 C ENDDIF
FOR01250 C* IF (IJGLOB.GE.MAXIJ) THEN
FOR01260 C* WRITE (6,*) 'ER', 'ROR IN MAPPING ELEMENT STIFFNESS FOR',
FOR01270 C* & 'ELEMENT #', IELNO, LI, LJ, IJGLOB, MAXIJ
FOR01280 C* ELSE
FOR01290 C* K(IJGLOB)=K(IJGLOB)+KE(IJELM) * FACTOR
FOR01300 C* ENDDIF
FOR01310 C* 20 CONTINUE
FOR01320 C* 50 CONTINUE
FOR01330 C
FOR01340 C----- NOTE: LINES COMMENTED OUT C* ARE FOR ER_ROR CHECKING. THE VALUES
FOR01350 C IN LN ARE ASSUMED TO BE CORRECT...
FOR01360 C
FOR01370 C RETURN
FOR01380 C END
FOR01390 C-----
FOR01400 C
FOR01410 C SUBROUTINE GETCHR DETERMINE THE VALUE OF THE FIRST CHARACTER
FOR01420 C AFTER AN OPTIONAL (LWORD=.TRUE.) KEYWORD (WORD),
FOR01430 C AND REMOVES THE STRING (WORD)//CHAR IF
FOR01440 C MODIFY=.TRUE.
FOR01450 C
FOR01460 C SUBROUTINE GETCHR(VERB,WORD,CHAR,LWORD,MODIFY)
FOR01470 C CHARACTER(*) VERB,WORD,CHAR
FOR01480 C LOGICAL MODIFY, LWORD, BTEST
FOR01490 C
FOR01500 C 999 CHAR=' '
FOR01510 C IF (LWORD) THEN
FOR01520 C I=START+INDEX(VERB,WORD)
FOR01530 C IF (I=START+1) RETURN
FOR01540 C I=I+1
FOR01550 C I=I+1
FOR01560 C ELSE
FOR01570 C I=1
FOR01580 C I=I+1
FOR01590 C CALL FIRST(VERB)
FOR01600 C ENDDIF
FOR01610 C
FOR01620 C IF (VERB(I).EQ.'**') THEN
FOR01630 C I=I+1
FOR01640 C I=I+1
FOR01650 C I=INDEX(VERB(I),**)+2 + IJ
FOR01660 C IF (VERB(J+2).EQ.'**') THEN
FOR01670 C I=J+3
FOR01680 C GO TO 10
FOR01690 C ENDDIF
FOR01700 C IF (J.EQ.0) THEN
FOR01710 C CHAR=VERB(I)
FOR01720 C GO TO 10
FOR01730 C
FOR01740 C I=INDEX(VERB(I),*) + I - 2
FOR01750 C ENDDIF
FOR01760 C CHAR=VERB(I)
FOR01770 C ENDDIF
FOR01780 C
FOR01790 C 20 I=INDEX(CHAR,****)
FOR01800 C IF (I.J.NE.0) THEN
FOR01810 C CHAR=CHAR(I)//CHAR(I+2:)
FOR01820 C GO TO 20
FOR01830 C ENDDIF
FOR01840 C ELSE
FOR01850 C J=INDEX(VERB(I),*) + I - 2
FOR01860 C IF (J.GE.1) CHAR=VERB(I:J)
FOR01870 C ENDDIF
FOR01880 C
FOR01890 C IF (MODIFY) THEN
FOR01900 C IF (VERB(J+2).EQ.'*') J=J+1
FOR01910 C VERB(I:J)=VERB(J+2)
FOR01920 C CALL FIRST(VERB)
FOR01930 C ENDDIF
FOR01940 C
FOR01950 C RETURN
FOR01960 C END
FOR01970 C-----
FOR01980 C SUBROUTINE GETINT DETERMINE THE VALUE OF THE FIRST INTEGER (INTEG)
FOR01990 C AFTER AN OPTIONAL (LWORD=.TRUE.) KEYWORD (WORD),
FOR02000 C AND REMOVES THE STRING (WORD)//INTEGER IF
FOR02010 C MODIFY=.TRUE. INTEG CAN BE ANY LENGTH REPRESENTABLE GET00080
FOR02020 C BY SINGLE PRECISION.
FOR02030 C
FOR02040 C SUBROUTINE GETINT(VERB,WORD,INTEG,DEFAULT,LWORD,MODIFY)
FOR02050 C CHARACTER(*) VERB,WORD
FOR02060 C CHARACTER*10 NUMB
FOR02070 C LOGICAL MODIFY, LWORD, HIT, BTEST
FOR02080 C INTEGER DEFUL
FOR02090 C DATA NUMB/'0123456789' /
FOR02100 C
FOR02110 C INTEG=DEFAULT
FOR02120 C HIT=.TRUE.
FOR02130 C IF (LWORD) THEN
FOR02140 C I=START+INDEX(VERB,WORD)
FOR02150 C IF (I=START+1) RETURN
FOR02160 C I=I+1
FOR02170 C I=I+1
FOR02180 C I=START+LEN(WORD)
FOR02190 C ELSE
FOR02200 C I=1
FOR02210 C I=I+1
FOR02220 C ENDDIF
FOR02230 C ISIGN = 1
FOR02240 C IF (LI.GT.1) RETURN
FOR02250 C IF (VERB(I).EQ.'-') THEN
FOR02260 C ISIGN = -1
FOR02270 C GO TO 5
FOR02280 C ELSE IF (VERB(I).EQ.'+' .OR. VERB(I).EQ.' ') THEN

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I=I+1
GO TO 5
ENDIF
C
10 IF (LGEK(VERBK(I),0) .AND. LLEK(VERBK(I),9)) THEN
IF (HIT) THEN
HITS=FALSE
C
INTEG=0
ENDIF
DO 20 I=1,10
IF(VERBK(I).EQ.0) THEN
INTEG=INTEG+(J-1)
I=I+1
GO TO 10
ENDIF
20 CONTINUE
ENDIF
C
INTEG=INTEG*ISIGN
C
IF (MODIFV) THEN
IF (VERBK(I).EQ.0) I=I+1
VERBK(ISTART)=VERBK(I)
ENDIF
C
RETURN
END
=====
HYSTO2 =====
SU BRoutine AXLMOD - AXIAL HYSTERESIS MODEL
REFERENCE: ANALYSIS OF THE FULL SCALE SEVEN
STORY R/C TEST STRUCTURE.
C
C
C P = CURRENT LOAD, POSITIVE IS TENSION
C D = CURRENT DISPLACEMENT, POSITIVE IS ELONGATION
C S = STIFFNESS
C KC = VIRGIN COMPRESSION STIFFNESS, EC
C KT1 = PRE-YIELD VIRGIN TENSILE STIFFNESS, 0.9*KC
C KT2 = POST-YIELD VIRGIN TENSILE STIFFNESS, 0.001*KC
C PV = TENSILE YIELD POINT, P*0*FV
C FMAX = MAXIMUM TENSILE FORCE BEFORE UNLOADING
C DMAX = MAXIMUM TENSILE DISPLACEMENT BEFORE UNLOADING
C FX = FORCE AT STIFFNESS CHANGE POINT ON THE UNLOADING CURVE
C DX = DISPL. AT STIFFNESS CHANGE POINT ON THE UNLOADING CURVE
C PI,DI = INTERSECTION OF TWO LINES
C DVT = TENSILE YIELD DISPLACEMENT = PV/KT1
C DVC = COMPRESSION YIELD DISPLACEMENT = PV/KC
C FP = FORCE AT COMPRESSION STIFFNESS CHANGE POINT
C DP = COMPRESSION AT COMPRESSION STIFFNESS CHANGE POINT
C KR = UNLOADING STIFFNESS = KC/(DMAX/DVT)**2
C KS = LOADING STIFFNESS, LINE BETWEEN (FX,DX) AND (FP,DP)
C KY = LOADING STIFFNESS, LINE BETWEEN (FP,DP) AND (-2*PV,-2*DY)
C
C
SUBROUTINE HYSTOK(P,D,PL,DL,V,VL,S,HRLN,KC,KT1,KT2,PV,ALPHA,BETA,
& DVT,DVC,CSE,FMAX,DMAX,FX,DX,FP,DP,KR,KS,KT,NR,LA,PRINT,
& SEQ,ESE,PSE,PSEOLD,UPOS,UNEQ,ENCR,IDR)
C
REAL*4 KC,KT1,KT2,KR,KS,KT,NR
DIMENSION UPOS(5),UNEQ(5),ENCR(6),ESE(5)
INTEGER RULET
LOGICAL LT,PRINT,PGT,PL,PLT
C
8000 IF (PRINT) WRITE (6,3010) P,D,PL,DL,V,VL,S,HRLN,KC,KT1,KT2,PV,
& ALPHA,BETA,DVT,DVC,FMAX,DMAX,FX,DX,FP,DP,KR,KS,KT,NR,LA,
& SEQ,ESE,PSE,PSEOLD,CSE,UPOS,UNEQ,ENCR
3010 FORMAT
& 'AXLMOD= ',G15.5, ' D= ',G15.5, ' PL= ',G15.5, ' DL= ',G15.5, /
& ' AK= ',G15.5, ' VL= ',G15.5, ' S= ',G15.5, ' HRLN= ',G15.5, /
& ' AK= ',G15.5, ' KT1= ',G15.5, ' KT2= ',G15.5, ' PV= ',G15.5, /
& ' AK= ',G15.5, ' DVT= ',G15.5, ' DVC= ',G15.5, /
& ' AK= ',G15.5, ' FMAX= ',G15.5, ' DMAX= ',G15.5, ' FX= ',G15.5, /
& ' AK= ',G15.5, ' DX= ',G15.5, ' FP= ',G15.5, ' DP= ',G15.5, /
& ' AK= ',G15.5, ' KR= ',G15.5, ' KS= ',G15.5, /
& ' AK= ',G15.5, ' KT= ',G15.5, ' NR= ',G15.5, ' AL= ',G15.5, /
& ' AK= ',G15.5, ' SE= ',G15.5, ' SEQ= ',G15.5, /
& ' AK= ',G15.5, ' PSE= ',G15.5, ' PSEOLD= ',G15.5, /
& ' AK= ',G15.5, ' UPOS= ',G15.5, ' UNEQ= ',G15.5, /
& ' AK= ',G15.5, ' ENCR= ',G15.5, ' ESE= ',G15.5, /
& ' AK= ',G15.5, ' ENCR= ',G15.5, ' ESE= ',G15.5, /
C
C..... SET INITIAL STIFFNESS AND RETURN
IF (NRL.EQ.0) THEN
IF (P.LE.0) THEN
NRL=1
HRLN=1.1
S=KC
SEQ=KC
A=P
ELSE
NRL=2
HRLN=2.1
S=KT1
SEQ=KC
A=P
ENDIF
RETURN
ENDIF
C
C..... RETURN IF NO STEP HAS BEEN TAKEN
IF (P.EQ.PL .OR. D.EQ.DL) RETURN
C
C..... SET LOADING FLAGS
PGT=PL.GT.PL
PLT=PL.LT.PL
C
C..... CALC EXCURSION RATIO AT EVERY ZERO CROSSING...
IF (P*PL.LE.0 .AND. PL.GT.0)
& CALL ONE(0,UPOS,ENCR,DVT,D,ESE,PSE,PSEOLD,CSE)
IF (P*PL.LE.0 .AND. PL.LE.0) THEN
ENCR(4)=0
ENCR(5)=0
ENCR(6)=0
ENDIF
C
C..... CALC DUCTILITY IF LOAD GT PAST LOAD
C
C..... DUCTILITY FOR POSITIVE LOADS ONLY
IF (P.GT.0 .AND. PGT)
& CALL ONE(1,UPOS,ENCR,DVT,D,ESE(2),PSE,PSEOLD,CSE)
999 CALL IDRECT(IDR,IDRV,IDRVO,P,PL,V,VL)
IDR=IDR
HYSTO0380 I IF (NRL.EQ.0) NRL=1
HYSTO0390 C
HYSTO0400 C RULE1=NRL
HYSTO0410 GO TO (100,200,300,400,500,600,700,800,900,
& 1000,1100,1200,1300),RULE1
HYSTO0420 C
HYSTO0430 C RULE 1 - LOADING AND UNLOADING ON THE COMPRESSION BRANCH BEFORE YIELD
HYSTO0440 C
HYSTO0450 100 SEQ=KC
HYSTO0460 IF (P.GT.0) GO TO 200
HYSTO0470 S=KC
HYSTO0480 NRL=1
HYSTO0490 HRLN=1.1
HYSTO0500 IF (PLT) A=DMX(10)*P,-2.*PV)
HYSTO0510 IF (PGT) A=0.
HYSTO0520 RETURN
HYSTO0530 C
HYSTO0540 C RULE 2 - TENSION LOADING BEFORE YIELD
HYSTO0550 C
HYSTO0560 200 IF (IDR) 250,250,210
HYSTO0570 210 IF (P.GE,PV) GO TO 600
HYSTO0580 S=KT1
HYSTO0590 NRL=2
HYSTO0600 HRLN=2.1
HYSTO0610 A=P
HYSTO0620 RETURN
HYSTO0630 C
HYSTO0640 250 IF (P.LE.0) GO TO 210
HYSTO0650 FMAX=AMAXI(P,FMAX)
HYSTO0660 DMAX=AMAXI(D,DMAX)
HYSTO0670 FX =FMAX*PV
HYSTO0680 DX =DMAX*PV/KC
HYSTO0690 S=KC
HYSTO0700 NRL=5
HYSTO0710 HRLN=2.2
HYSTO0720 A=P
HYSTO0730 RETURN
HYSTO0740 C
HYSTO0750 C RULE 5 - UNLOADING ON TENSION BEFORE YIELD
HYSTO0760 C
HYSTO0770 500 IF (PGT) GO TO 500
HYSTO0780 IF (P.GT.0) GO TO 550
HYSTO0790 510 IF (KC.NE.KT1) THEN
HYSTO0800 CALL INTSET(DI,PI,D,P,KC,DX,FX,KT1)
HYSTO0810 ELSE
HYSTO0820 PI=P
HYSTO0830 DI=D
HYSTO0840 EMBIT
HYSTO0850 IF (P.LE.PI) GO TO 520
HYSTO0860 S=KC
HYSTO0870 NRL=5
HYSTO0880 HRLN=5.11
HYSTO0890 A=P
HYSTO0900 RETURN
HYSTO0910 520 S=KT1
HYSTO0920 NRL=4
HYSTO0930 HRLN=5.12
HYSTO0940 A=P
HYSTO0950 RETURN
HYSTO0960 550 IF (P.GE,FMAX) GO TO 200
HYSTO0970 S=KC
HYSTO0980 NRL=5
HYSTO0990 HRLN=5.2
HYSTO1000 A=P
HYSTO1010 RETURN
HYSTO1020 C
HYSTO1030 C RULE 4 - LOADING TOWARDS V' FROM FX.
HYSTO1040 C
HYSTO1050 400 IF (IDR) 500,500,410
HYSTO1060 410 IF (ABS(P).GE,PV) GO TO 100
HYSTO1070 S=KT1
HYSTO1080 NRL=4
HYSTO1090 HRLN=4.1
HYSTO1100 A=P
HYSTO1110 RETURN
HYSTO1120 C
HYSTO1130 C RULE 5 - LOADING AND UNLOADING BETWEEN BRANCHES 0-Y AND FX-Y'
HYSTO1140 C
HYSTO1150 500 IF (KC.NE.KT1) THEN
HYSTO1160 CALL INTSET(DITENS,PITENS,D,P,KC,DVT,PV,KT1)
HYSTO1170 CALL INTSET(DICOMP,PICOMP,D,P,KC,DX,FX,KT1)
HYSTO1180 ELSE
HYSTO1190 PITENS=P
HYSTO1200 DITENS=D
HYSTO1210 PICOMP=P
HYSTO1220 DICOMP=D
HYSTO1230 ENDIR
HYSTO1240 IF (P.LE,PICOMP) GO TO 550
HYSTO1250 IF (P.GE,PITENS) GO TO 210
HYSTO1260 S=KC
HYSTO1270 NRL=5
HYSTO1280 HRLN=5.1
HYSTO1290 A=P
HYSTO1300 IF (PLT) A=PICOMP
HYSTO1310 RETURN
HYSTO1320 C
HYSTO1330 C RULE 6 - LOADING AFTER TENSION VEILD
HYSTO1340 C
HYSTO1350 600 IF (IDR) 650,650,610
HYSTO1360 610 S=KT2
HYSTO1370 NRL=6
HYSTO1380 HRLN=6.1
HYSTO1390 A=P
HYSTO1400 C
HYSTO1410 C..... CALC UNLOADING CURVE FOR ENERGY INFO
HYSTO1420 FMAX=AMAXI(P,FMAX)
HYSTO1430 DMAX=AMAXI(D,DMAX)
HYSTO1440 KR=KC*HRLN(1),(DVT/DMAX)**ALPHA)
HYSTO1450 FX =FMAX*PV
HYSTO1460 DX =DMAX*PV/KR
HYSTO1470 KS =(PV*FX)/(DX-DVC)
HYSTO1480 C----- FORCE KR GE KS, TO PREVENT UNSTABLE LOOPS...
HYSTO1490 IF (KS.GT,KR) KR=(FMAX*PV)/(DMAX-DVC)
HYSTO1500 SEQ=KR
HYSTO1510 RETURN
HYSTO1520 650 FMAX=AMAXI(P,FMAX)
HYSTO1530 DMAX=AMAXI(D,DMAX)
HYSTO1540 KR=KC*HRLN(1),(DVT/DMAX)**ALPHA)
HYSTO1550 FX =FMAX*PV
HYSTO1560 DX =DMAX*PV/KR
HYSTO1570 KS =(PV*FX)/(DX-DVC)
HYSTO1580 C----- FORCE KR GE KS, TO PREVENT UNSTABLE LOOPS...
HYSTO1590 IF (KS.GT,KR) THEN
HYSTO1600 KR=(FMAX*PV)/(DMAX-DVC)
HYSTO1610 KS=KR
HYSTO1620
HYSTO1630
HYSTO1640
HYSTO1650
HYSTO1660
HYSTO1670
HYSTO1680
HYSTO1690
HYSTO1700
HYSTO1710
HYSTO1720
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HYSTO1780
HYSTO1790
HYSTO1800
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HYSTO1910
HYSTO1920
HYSTO1930
HYSTO1940
HYSTO1950
HYSTO1960
HYSTO1970
HYSTO1980
HYSTO1990
HYSTO2000
HYSTO2010
HYSTO2020
HYSTO2030
HYSTO2040
HYSTO2050
HYSTO2060
HYSTO2070
HYSTO2080
HYSTO2090
HYSTO2100
HYSTO2110
HYSTO2120
HYSTO2130
HYSTO2140
HYSTO2150
HYSTO2160
HYSTO2170
HYSTO2180
HYSTO2190
HYSTO2200
HYSTO2210
HYSTO2220

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DX=DMAX-PV/KR
ENDIF
DP =DVC + BETA*(DX-DVC)
FP =PV - (DN-OP)*KS
KT =(C2*PV+FP)/(DP-2*DVC)
DQ =DVC + PV/KR
S=KR
NRL=7
NRLN=6.2
A=FX
RETURN
C
C RULE 7 - UNLOADING AFTER YIELD
C
700 SEQ=KR
IF (DIR) 750,750,710
710 IF (P.GE.FMAX) GO TO 600
S=KR
NRL=7
NRLN=7.1
A=FX
RETURN
750 IF (P.LE.FN) GO TO 800
S=KR
NRL=7
NRLN=7.2
A=FX
RETURN
C
C RULE 8 - ON BRANCH BETWEEN DX & DP
C
800 IF (PGTPL) THEN
IF (KR.EQ.KS) GO TO 1200
GO TO 1500
ENDIF
IF (P.LE.FP) GO TO 900
S=KS
NRL=8
NRLN=8.1
A=FP
RETURN
C
C RULE 9 - ON BRANCH FP-V*
C
900 IF (PGTPL) GO TO 1500
IF (P.LE.(-2*PV)) GO TO 1000
S=KT
NRL=9
NRLN=9.1
A=-2*PV
RETURN
C
C RULE 10 - ON THE COMPRESSION CURVE AFTER YIELDING
C
1000 SEQ= 1. / ( 1./KC + (.4./KR - .4./KC)*(PV/FP)**2 )
IF (DIR) 1050,1050,1010
1010 S=KC
NRL=10
NRLN=10.1
A=10*P
RETURN
1050 IF (ABS(P).LE.PV) GO TO 1100
S=KC
NRL=10
NRLN=10.2
A=-PV
RETURN
C
C RULE 11 - UNLOADING BETWEEN V* & Q
C
1100 SEQ=KR
IF (ABS(P).GT.PV) GO TO 1000
IF ( P.GE. 0.) GO TO 1200
S=KR
NRL=11
NRLN=11.1
A=0
IF (PLTPL) A=0
IF (PLTPL) A=-PV
RETURN
C
C RULE 12 - LOADING FROM Q TO H
C
1200 IF (PLTPL) THEN
IF (KS.EQ.KR .AND. P.GT.FP) GO TO 800
GO TO 1500
ENDIF
IF ( P.GE.FMAX) GO TO 600
S=KS
NRL=12
NRLN=12.1
A=FX
RETURN
C
C RULE 13 - LOADING AND UNLOADING INSIDE Q-H-D-P-V*
C
1500 IF (KR.NE.KS) THEN
CALL INTSCT(DITENS,PITENS,D,P,KR,DMAX,FMAX,KS)
CALL INTSCT(DICOMP,PICOMP,D,P,KR,DK,FX,KS )
ELSE
IF (PGTPL) GO TO 1200
PITENS=P
DITENS=0
PICOMP=P
DICOMP=0
ENDIF
C-----IS POINT WITHIN PV*-FP*-PV* ?
IF (PICOMP.LE.FP) THEN
IF (KR.NE.KS) THEN
CALL INTSCT(DICOMP,PICOMP,D,P,KR,DK,DP,FP,KT )
ELSE
IF (PLTPL) GO TO 900
PICOMP=P
DICOMP=0
ENDIF
ENDIF
IF (KR.EQ.KS .AND. PLTPL) GO TO 800
S2=KT
ELSE
S2=KR
ENDIF
IF (PGTPL) THEN
IF (P.GT.PITENS) GO TO 1200
A=PITENS
ENDIF

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HYS02250
HYS02240
HYS02250
HYS02260
HYS02270
HYS02280
HYS02290
HYS02300
HYS02310
HYS02320
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HYS02340
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HYS02970
HYS02980
HYS02990
HYS03000
HYS03010
HYS03020
HYS03030
HYS03040
HYS03050
HYS03060
HYS03070
HYS03080
HYS03090
HYS03100
HYS03110
HYS03120
HYS03130
HYS03140
HYS03150
HYS03160
HYS03170
HYS03180
HYS03190
HYS03200
HYS03210
HYS03220
HYS03230
HYS03240
HYS03250
HYS03260
HYS03270
HYS03280
HYS03290
HYS03300
HYS03310
HYS03320
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HYS03350
HYS03360
HYS03370
HYS03380
HYS03390
HYS03400
HYS03410
HYS03420
HYS03430
HYS03440
HYS03450
HYS03460

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HRLN=15.1
ENDIF
IF (PLTPL) THEN
IF (P.LT.PICOMP) GO TO 800
A=PICOMP
HRLN=15.2
ENDIF
S=MAX(KR,S2)
NRL=15
RETURN
C
END
C=====
C= BENDING HYSTERESIS MODEL..... HYST05 .....
C=====
C INPUT VARIABLES
C P = CURRENT LOAD
C D = CURRENT DISPLACEMENT
C PL = LAST LOAD
C VEL = PRODUCT OF LAST AND CURRENT VELOCITY
C NB = NUMBER OF BACKBONE CURVE POINTS
C NI = MAXIMUM NUMBER OF SECONDARY LOOPS
C PC = CRACKING LOAD
C DC = CRACKING DISPLACEMENT
C PBK(I) = BACKBONE CURVE LOADING POINT J, J=1,NB
C DBK(J) = BACKBONE CURVE DISPLACEMENT POINT J, J=1,NB
C SI = INITIAL STIFFNESS, PC/DC
C
C OUTPUT VARIABLES
C .....AN INITIAL VALUE OF ZERO , OR FALSE
C IS REQUIRED FOR ALL OUTPUT VARIABLES...
C K = STIFFNESS
C RULE = RULE NUMBER, STORED IN THE FORMAT RN.DIR UPON EXIT OF THIS SUB ROUTINE
C A = LOAD LIMIT BEFORE NEXT RULE CHANGE, IN THE CURRENT DIR
C PMG = MAXIMUM PAST LOAD IN THE POSITIVE DIRECTION
C PMN = MAXIMUM PAST LOAD IN THE NEGATIVE DIRECTION
C DMG = MAXIMUM PAST DISPLACEMENT IN THE POSITIVE DIRECTION
C DMN = MAXIMUM PAST DISPLACEMENT IN THE NEGATIVE DIRECTION
C PRI(I) = SECONDARY LOOP LOADING POINT, I
C DRI(I) = SECONDARY LOOP DISPLACEMENT POINT, I
C FRI(I) = SECONDARY LOOP FLAG
C LR = NUMBER OF SECONDARY LOOPS ACTIVE
C ALPHAI = POSITIVE LOAD DEGRADING STIFFNESS FACTOR
C ALPHAI2 = NEGATIVE LOAD DEGRADING STIFFNESS FACTOR
C BACKB = BACKBONE LOADING FLAG
C
C INTERNAL VARIABLES
C J = BACKBONE CURVE POINT # IN THE CURRENT DIRECTION
C JD = TEMPORARY VARIABLE
C I,IT = SECONDARY LOOP NUMBER
C DIR = CURRENT DIRECTION
C DIR=1, POSITIVE LOADING
C DIR=2, POSITIVE UNLOADING
C DIR=3, NEGATIVE LOADING
C DIR=4, NEGATIVE UNLOADING
C DIRL = LAST DIRECTION
C DIRLE = INTEGER VALUE OF LAST #
C IRLULE = INTEGER VALUE OF RULE #
C REVERSL = LOAD REVERSAL FLAG
C PRINT = PRINT FLAG, USED FOR DEBUGGING
C AP = ABSOLUTE VALUE OF THE LOAD, P.
C PM = MAXIMUM PAST LOAD IN THE CURRENT DIRECTION
C DMAX = MAXIMUM PAST DISPLACEMENT IN BOTH DIRECTIONS
C Q1 = ONE QUARTER OF PM, USED BY UNLOADING CURVES
C Q5 = THREE QUARTERS OF PM, USED BY UNLOADING CURVES
C DQ1 = DISPLACEMENT AT Q1 ON UNLOADING BRANCH
C DQ5 = DISPLACEMENT AT Q5 ON UNLOADING BRANCH
C DD1 = INTERMEDIATE DISPLACEMENT INTERCEPT OF UNLOADING BRANCH
C DD2 = INTERMEDIATE DISPLACEMENT INTERCEPT OF UNLOADING BRANCH
C DP = DISPLACEMENT INTERCEPT OF UNLOADING BRANCH
C DP = DIFFERENCE IN LOAD, USED FOR CALCULATING K
C DD = DIFFERENCE IN DISPLACEMENT, USED FOR CALCULATING K
C PK = LOAD INTERCEPT OF LOADING AND BACKBONE CURVE
C DPL = DISPLACEMENT INTERCEPT OF LOADING AND BACKBONE CURVE
C PCS = PC/S
C DCS = DISPLACEMENT AT PCS
C P2,D2 = INTERSECTION OF LOADING AND UNLOADING CURVES
C PI,DI = SMALL LOOP UNLOADING POINTS
C K = MAXIMUM DISPLACEMENT
C KB = STIFFNESS FROM RULE #
C FLAG1 = UPPER SECONDARY LOOP FLAG
C FLAG2 = LOWER SECONDARY LOOP FLAG
C ALPHAA = DEGRADING FACTOR FOR FIRST CYCLE
C ALPHAB = DEGRADING FACTOR FOR SUBSEQUENT CYCLES
C S1 = TEMPORARY STIFFNESS
C S2 = UNLOADING STIFFNESS FROM FS1
C S3 = UNLOADING STIFFNESS FROM FS3
C S02 = STIFFNESS BETWEEN CURRENT AND RELOADING POINT
C S03 = STIFFNESS BETWEEN PA AND DO
C S05 = STIFFNESS BETWEEN PB AND DO
C
C INTERNAL FUNCTIONS
C FD2 = DISPLACEMENT INTERCEPT OF LOADING AND UNLOADING CURVE
C FS1 = UNLOADING STIFFNESS WHEN P>.75 PMAX
C FS2 = UNLOADING STIFFNESS WHEN .75 PMAX > P > .25 PMAX
C FS3 = UNLOADING STIFFNESS WHEN .25 PMAX > P
C FSL = LOADING STIFFNESS WHEN .P < PC/S WITHOUT REVERSAL...
C
C SU BROU_TINES CALLED
C DIRECT = DETERMINES THE VALUES OF DIR AND DIRL
C INTSCT = DETERMINES THE INTERSECTION OF TWO LINES IN POINT-SLOPE FORM
C KNIN = DETERMINES THE STIFFNESS BASED ON DP,DD AND K_DEFAULT
C
C SUBROUTINE HYSTOSK(P,D,PL,OL,VEL,NB,NI,PC,DC,PS,DB,SI,CSE,
& K,RULE,DIR,A,PMG,PMN,DMG,DMN,BACKB,ALPHAI,ALPHA2,
& IR,SRL,SR2,SRS,SRN,PR,DR,FR,PRINT,
& SE,DV,ESE,PSE,PSO,LD,UP,UNEG,EXCR)
C
C IMPLICIT REAL(A-H,K,O-Z)
C IMPLICIT INTEGER(I,J,L-N)
C INTEGER DIR,DIRL
C CHARACTER*4 FRI(1)
C LOGICAL BACKB,REVERSL,PRINT,BTEST
C DIMENSION PBK(1),DBK(1),DRI(1),DRI(1),UP(SK(5)),EXCR(6),ESE(5)
C DATA ALPHAA/1.1297,ALPHAB/1.0297/
C
C FSI(X)= SI *(DC/K)**.29*
C FS2(X)= SI *(0.8544*(DC/K-1) +1)
C FS3(X)= SI *(0.9092*(DC/K-1) +1)

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HYS05470
HYS05480
HYS05490
HYS05500
HYS05510
HYS05520
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HYS05580
HYS05590
HYS05600
HYS05610
HYS05620
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HYS05660
HYS05670
HYS05680
HYS05690
HYS05700
HYS05710
HYS05720
HYS05730
HYS05740
HYS05750
HYS05760
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HYS05790
HYS05800
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HYS05980
HYS05990
HYS06000
HYS06010
HYS06020
HYS06030
HYS06040
HYS06050
HYS06060
HYS06070
HYS06080
HYS06090
HYS06100
HYS06110
HYS06120
HYS06130
HYS06140
HYS06150

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FSL(X)=SI*(DC/X)**.285
FDZ(X)=GM-.05*PM/(FSL(X))
C
1000 IF (PRINT) WRITE (6,1010) P,D,PL,DL,NB,NI,PC,DC,SI,K,
      & RULE,A,PMG,PMH,DNG,DNH,BACKG,IR,DIR,
      & SE,OV,ESL(1),PSE,PSEOLD,UPOS,CSE,UNEG,EXCR,VEL
1010 FORMAT
      & ' BL- P=,GLS.5, D=,GLS.5, PL=,GLS.5, DL=,GLS.5/
      & ' NB=,GLS.5, NI=,GLS.5, PC=,GLS.5, DC=,GLS.5/
      & ' SI=,GLS.5, K=,GLS.5, PM=,GLS.5, AS=,GLS.5/
      & ' PMH=,GLS.5, PMH=,GLS.5, DMH=,GLS.5, DMH=,GLS.5/
      & ' BACKB=,GLS.5, TR=,GLS.5, DIR=,GLS.5, SE=,GLS.5/
      & ' DV=,GLS.5, ESE=,GLS.5, PSE=,GLS.5, PSE=,GLS.5/
      & ' UP1=,GLS.5, UP2=,GLS.5, UPS=,GLS.5, CSE=,GLS.5/
      & ' UN1=,GLS.5, UN2=,GLS.5, UNS=,GLS.5/
      & ' EX1=,GLS.5, EX2=,GLS.5, EXS=,GLS.5/
      & ' EN=,GLS.5, EMS=,GLS.5, EGM=,GLS.5, VEL=,GLS.5/
1020 FORMAT
      & ' BL- I=,GLS.5, PR=,GLS.5, DR=,GLS.5, FR=,A
C
AP=ABSCP
C..... DETERMINE IF ELASTIC
IF (RULE.EQ.0 .AND. AP.LT.PC) THEN
  K=SI
  SE=K
  RETURN
ENDIF
C..... DETERMINE IF MALL IS INACTIVE. IF SO RETURN
IF (RULE.LT.0.0) RETURN
C..... DETERMINE CURRENT DIRECTION
IRULE=INT(RULE)
DIR=DIR
CALL DIRECT(DIR,DIRL,P,PL,VEL)
DIR=DIR
IF (PRINT) WRITE (6,1050) DIR,DIRL
1050 FORMAT
      & ' BL- DIR=,IB , DIRL=,IB )
C..... DETERMINE MAXIMUM AND MINIMUM VALUES
PMG=MAX(P,PMG,DC)
DMG=MAX(D,DNG,PC)
PMH=MIN(P,PMH,-PC)
DMH=MIN(D,DNH,-DC)
DMAX=MAX(DNG,-DMH)
PMAX=MAX(PMG,-PMH)
C..... SET MAXIMUM AND MINIMUM VALUES...
IF (DIR.EQ.1 .OR. DIR.EQ.2) THEN
  PM=PMG
  DM=DNG
ELSE IF (DIR.EQ.3 .OR. DIR.EQ.4) THEN
  PM=PMH
  DM=DMH
ENDIF
C..... CALCULATE EQUIVALENT UNLOADING STIFFNESS FOR ENERGY...
IF (BACKB .OR. RULE.EQ.1.0) THEN
  S1=FSL(DMAX)
  S2=FSL(DMAX)
  S3=FSL(DMAX)
  DO=DM - PM*(DMH-DNG)/(PMH-PMG)
  Q1=PM/4
  Q2=S1*Q1
  Q3=DM - 0.25*PM/S1
  S21=KMIN(DQ3-0.0, Q1, S1)
  S22=Q3 - 0.50*PM/(MAX(S2, S22))
  S23=KMIN(DQ1-0.0, Q1, S1)
  SE=0.5 * PM**2 / (
    & (PM*Q3)*0.5*(DQ3-DQ1)
    & + (Q3+Q1)*0.5*(DQ3-DQ1)
    & + ( Q1**2)*0.5*( Q1)/MAX(S2, S23) )
ENDIF
C..... CHECK TO SEE IF LAST RULE IS STILL IN EFFECT
IF (DIR.EQ.DIRL .AND.
      & (DIR.EQ.1 .AND. P.LT.A) .OR. (DIR.EQ.2 .AND. P.GT.A) .OR.
      & (DIR.EQ.3 .AND. P.GT.A) .OR. (DIR.EQ.4 .AND. P.LT.A)) THEN
  RETURN
ENDIF
C..... CALC EXCURSION RATIO AT EVERY ZERO CROSSING...
IF (P*PL.LE.0) CALL DNE(0,UPOS,EXCR,OV,DLI,ESE,PSE,PSEOLD,CSE)
C..... ERASE SMALL LOOP FLAGS
IF (IR.GT.0) THEN
  IT=IR
  DO 10 I=1,IT
  & IF ((FR(I).EQ.'L' .AND. (P.LE.PRCI) .OR. D.LE.DRCI) ) .OR.
    & (FR(I).EQ.'7' .AND. (P.GE.PRCI) .OR. D.GE.DRCI) ) THEN
    IR=I-1
    GO TO 15
  ENDIF
  10 CONTINUE
  ENDIF
  15 I=IR+1
C..... LOADING RULES ..... RULES 1,6-11
IF (DIR.EQ.1 .OR. DIR.EQ.5) THEN
  C..... LOADING ON BACKBONE
  1 IF (BACKB .OR. RULE.EQ.0.0) THEN
    K=0
    DO 10 J=2,NB
    DO=DK(J)-ABS(D)
    DP=PK(J)-AP
    IF (AP.LT.PK(J) .AND. (DO*DP).GT.0.) THEN
      S=DP/DO
      IF (S.GT.K) THEN
        K=S
        A=SIGK(PK(J),P)
      ENDIF
    ENDIF
  18 CONTINUE
  RULE=1
  BACKB=.TRUE.
  IR=0
  IF (DIR.EQ.1) THEN
    ALPHAL=ALPHAA
  ELSE
    ALPHAZ=ALPHA
  ENDIF
ENDIF
ENDIF
ENDIF
GO TO 1
C..... UNLOADING RULES ..... RULES 2-5

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HYSD1160
HYSD1170
HYSD1180
HYSD1190
HYSD1200
HYSD1210
HYSD1220
HYSD1230
HYSD1240
HYSD1250
HYSD1260
HYSD1270
HYSD1280
HYSD1290
HYSD1300
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HYSD1490
HYSD1500
HYSD1510
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HYSD1600
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HYSD4000

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C ..... INITIALIZE VALUES
BACKB=FALSE
S1=FS1/DMAX
S2=FS2/DMAX
S3=FS3/DMAX
D0=DM - PM*(DMH-DMG)/(PMH-PMG)
Q1=PM/4
Q2=DM - 0.25*PM/S1
S02=KMIN(D05-D0, Q5, S1)
Q41=Q5-0.50*PM/(MAX(S2, S02))
S05=KMIN(Q41-D0, Q1, S1)
SU=0
HY505640 C PR = SECONDARY LOOP LOADING POINT HY500510
HY505650 C OR = SECONDARY LOOP DISPLACEMENT POINT HY500520
HY505660 C FR = SECONDARY LOOP FLAG HY500530
HY505670 C IR = SECONDARY LOOP NUMBER HY500540
HY505680 C BACKB = BACKBONE LOADING FLAG HY500550
HY505690 C SRL = RELOADING STIFFNESS FROM RULE 8 - USED BY RULE 11 HY500560
HY505700 C SR1 = RELOADING STIFFNESS FROM RULE 9 - USED BY RULE 11 HY500570
HY505710 C SR2 = RELOADING STIFFNESS FROM RULE 7 - USED BY RULE 11 HY500580
HY505720 C SRM = RELOADING STIFFNESS FROM RULES 8 & 9 - USED BY RULE 11 HY500590
HY505730 C HY500600
INTERNAL VARIABLES
HY505740 C HY500610
HY505750 C J = BACKBONE CURVE POINT # IN THE CURRENT DIRECTION HY500620
HY505760 C DIR = CURRENT DIRECTION HY500630
HY505770 C DIR=1, POSITIVE LOADING HY500640
HY505780 C DIR=2, POSITIVE UNLOADING HY500650
HY505790 C DIR=3, NEGATIVE LOADING HY500660
HY505800 C DIR=4, NEGATIVE UNLOADING HY500670
HY505810 C DIRL = LAST DIRECTION HY500680
HY505820 C IRULE = INTEGER VALUE OF RULE HY500690
HY505830 C LRULE = INTEGER VALUE OF LAST RULE # HY500700
HY505840 C CRACKD = CRACKED WALL FLAG HY500710
HY505850 C REVERL = LOAD REVERSAL FLAG HY500720
HY505860 C PRINT = PRINT FLAG, USED FOR DEBUGGING HY500730
HY505870 C PC2 = PC/2, USED BY LOADING CURVES HY500740
HY505880 C DC2 = DISPLACEMENT CORRESPONDING TO PC2 ON THE LOADING BRANCH HY500750
HY505890 C S = INTERMEDIATE STIFFNESS HY500760
HY505900 C SR = RELOADING STIFFNESS HY500770
HY505910 C SRP = MINIMUM RELOADING STIFFNESS HY500780
HY505920 C D0 = DISPLACEMENT INTERSEPT OF PEAK DISPLACEMENTS HY500790
HY505930 C D0P = DISPLACEMENT INTERSEPT OF THE UNLOADING BRANCH HY500800
HY505940 C AP = ABSOLUTE VALUE OF CURRENT LOAD P HY500810
HY505950 C PM = MAXIMUM PAST LOAD IN THE CURRENT DIRECTION HY500820
HY505960 C DM = MAXIMUM PAST DISPLACEMENT IN THE CURRENT DIRECTION HY500830
HY505970 C DMAX = MAXIMUM PAST DISPLACEMENT IN EITHER DIRECTION HY500840
HY505980 C PMAX = MAXIMUM PAST LOAD IN EITHER DIRECTION HY500850
HY505990 C PA = PM-PC, USED BY UNLOADING CURVES HY500860
HY506000 C PB = PC/2, USED BY UNLOADING CURVES HY500870
HY506010 C DA = DISPLACEMENT AT PA, USED BY UNLOADING CURVES HY500880
HY506020 C DB = DISPLACEMENT AT PB, USED BY UNLOADING CURVES HY500890
HY506030 C DP = DIFFERENCE IN LOAD, USED FOR CALCULATING K HY500900
HY506040 C DD = DIFFERENCE IN DISPLACEMENT, USED FOR CALCULATING K HY500910
HY506050 C PX = LOAD INTERCEPT OF LOADING AND BACKBONE CURVE HY500920
HY506060 C DX = DISPLACEMENT INTERCEPT OF LOADING AND BACKBONE CURVE HY500930
HY506070 C PZ, DZ = POINT ON THE LOADING CURVE BETWEEN RULES 7 AND 10 HY500940
HY506080 C X = MAXIMUM DISPLACEMENT HY500950
HY506090 C X1 = DISPLACEMENT INTERCEPT FOR RULE 11 HY500960
HY506100 C X2 = 75% PC DISPLACEMENT FOR RULE 11 HY500970
HY506110 C X3 = 25% PC DISPLACEMENT FOR RULE 11 HY500980
HY506120 C LIT = TEMPORARY LABEL FOR SMALL LOOP LOADING AND UNLOADING PTH500990
HY506130 C J0 = J HY501000
HY506140 C ALPHA = DEGRADING STIFFNESS FACTOR HY501010
HY506150 C ALPHAP = DEGRADING STIFFNESS FACTOR USED BY RULE 10 HY501020
HY506160 C S1 = STIFFNESS FROM FUNCTION FS1 HY501030
HY506170 C S2 = STIFFNESS FROM FUNCTION FS2 HY501040
HY506180 C S3 = STIFFNESS FROM FUNCTION FS3 HY501050
HY506190 C S4 = STIFFNESS BETWEEN CURRENT AND RELOADING POINT HY501060
HY506200 C S02 = STIFFNESS BETWEEN PA AND D0 HY501070
HY506210 C S05 = STIFFNESS BETWEEN PB AND D0 HY501080
HY506220 C HY501090
INTERNAL FUNCTIONS
HY506230 C HY501100
HY506240 C F02 = DISPLACEMENT INTERCEPT OF LOADING AND UNLOADING CURVE HY501110
HY506250 C F01 = UNLOADING STIFFNESS WHEN P<PM-PC/2=PA HY501120
HY506260 C F02 = UNLOADING STIFFNESS WHEN P>PM-PC/2=PB HY501130
HY506270 C F03 = UNLOADING STIFFNESS WHEN P>PB HY501140
HY506280 C F04 = LOADING BELOW PC/2, WITH PINDCHNG HY501150
HY506290 C SU BROUTINES CALLED HY501160
HY506300 C DIRECT = DETERMINES THE VALUES OF DIR AND DIRL HY501170
HY506310 C INTSECT = DETERMINES THE INTERSECTION OF TWO LINES IN POINT-SLOPE FORM HY501180
HY506320 C KMIN = DETERMINES THE STIFFNESS BASED ON DP, DD AND K_DEFAULT HY501190
HY506330 C HY501200
SUBROUTINE HY5TON<P,D,PL,DL,VEL,NS,NI,PRINT,
HY506340 C & PC,DC,PS,DS,SI,CSE,DV
HY506350 C & K,RULE,DIR,IR,PMG,PMH
HY506360 C & DMG,DMH,BACKB,SRL,SR2,SR3
HY506370 C & SRM,IR,SE,UPOS,ENCR
HY506380 C & ESE,PSE,PSEOLD,PR,DR,FR
HY506390 C
HY506400 C IMPLICIT REAL(A-H,K,0-2)
HY506410 C IMPLICIT INTEGER(I,J,L-N)
HY506420 C INTEGER DIR,DIRL
HY506430 C LOGICAL BACKB,CRACKD,REVERL,PRINT,TEST
HY506440 C CHARACTER*(*) FR(N)
HY506450 C DIMENSION PSC(NS),DSC(NS),PR(N),DR(N)
HY506460 C DIMENSION UPOS(S),UMEG(S),ENCR(S),ESE(S)
HY506470 C DATA ALPHA/1.0/
HY506480 C
HY506490 C F01(X)= SI *MINK(1.4675*DC/K)**.545,1.)
HY506500 C F02(X)= SI *MINK(0.7761*DC/K)**.5195,1.)
HY506510 C F03(X)= SI *MINK(0.0707*DC/K**1.569,1.)
HY506520 C F04(X)= SI *MINK(ABS(DC/K)**1.02,1.)
HY506530 C F02(X)= SIGMA(DMG,PM)-.05*SIGMA(PMAX,PM)/C*F01(X)
HY506540 C
HY506550 C 1000 IF (PRINT) WRITE (6,1010) P,D,PL,DL,NS,NI,PC,DC,SI,K,RULE,A,
HY506560 C & PMG,PMH,DMG,DMH,SRL,SR2,SR3,SRM,BACKB,IR,PSEOLD,VEL,
HY506570 C & SE,DV,ESE(1),PSE,UPOS,ENCR
HY506580 C
HY506590 C 1010 FORMAT (
HY506600 C A' SI= ',SI,' G15.5,' S2= ',S2,' G15.5,' S3= ',S3,' G15.5,'
HY506610 C A' PL= ',PL,' G15.5,' DS= ',DS,' G15.5,' DL= ',DL,' G15.5,'
HY506620 C A' NI= ',NI,' G15.5,' NI= ',NI,' G15.5,' PC= ',PC,' G15.5,' DC= ',DC,' G15.5,'
HY506630 C A' SR= ',SR,' G15.5,' SR2= ',SR2,' G15.5,' SR3= ',SR3,' G15.5,'
HY506640 C A' SE= ',SE,' G15.5,' DV= ',DV,' G15.5,' ESE= ',ESE,' G15.5,'
HY506650 C A' U1= ',U1,' G15.5,' U2= ',U2,' G15.5,' U3= ',U3,' G15.5,'
HY506660 C A' EX1= ',EX1,' G15.5,' EX2= ',EX2,' G15.5,' EX3= ',EX3,' G15.5,'
HY506670 C A' EX4= ',EX4,' G15.5,' EX5= ',EX5,' G15.5,'
HY506680 C IF (IR.GT.0.AND.PRINT) WRITE (6,1020) (I,PR(I),DR(I),FR(I),I=1,IR)
HY506690 C
HY506700 C 1020 FORMAT
HY506710 C & (' I= ',I,' G15.5,' PR= ',PR,' G15.5,' DR= ',DR,' G15.5,' FR= ',FR,' A )
HY506720 C
HY506730 C AP=ABS(P)
HY506740 C
HY506750 C ..... DETERMINE IF ELASTIC
HY506760 C IF (RULE.EQ.0.AND.AP.LT.PC) THEN
HY506770 C K=SI
HY506780 C SE=K
HY506790 C GO TO 9999
HY506800 C ENDIF
HY506810 C
HY506820 C ..... DETERMINE IF WALL IS INACTIVE, IF SO RETURN
HY506830 C

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IF (RULE.LT.0.0) GO TO 9999
C..... DETERMINE CURRENT DIRECTION
LRULE=INT(RULE)
DIR =DIR
CALL DIRECT(DIR,DIRL,P,PL,VEL)
DIR =DIR
IF (PRINT) WRITE (6,1050) DIR,DIRL
1050 FORMAT(' DIR=',I8,' DIRL=',I8)
C..... DETERMINE MAXIMUM AND MINIMUM VALUES
PMG=MAX(PMG,PC,P)
DMG=MAX(DMG,DC,D)
PMH=MIN(PMH,PC,P)
DMH=MIN(DMH,DC,D)
DMAX=MAX(DMG,-DMH)
PMAX=MAX(PMG,-PMH)
C..... SET MAXIMUM AND MINIMUM VALUES...
IF (DIR.EQ.1 .OR. DIR.EQ.2) THEN
  PHE=PMG
  DME=DMG
ELSE IF (DIR.EQ.5 .OR. DIR.EQ.4) THEN
  PHE=PMH
  DME=DMH
ENDIF
C..... CALCULATE EQUIVALENT UNLOADING STIFFNESS FOR ENERGY...
IF (BACKB .OR. RULE.EQ.0.0) THEN
  SI=F51(DMAX)
  S2=F52(DMAX)
  S3=F53(DMAX)
  D0=DM-PM*(DMG-DMH)/(PMG-PMH)
  PA=PM-SIGK(PC,PM)/SI
  DA=DM-SIGK(PC,PM)/SI
  PB=SIGK (KMIN ABSKPA),(PC/2)),PM)
  S02=KMIN (DA-D0),PA,SI)
  DB=DA-(PA-PB)/MAX(S2,S02)
  S05=KMIN (DB-D0),PB,SI)
  SE=0.5 * PMH * (
    (PMH+PA)+0.5*(DM-DA)
    + (PA+PB)+0.5*(DA-DB)
    + (PB+0.5*( PB)/MAX(S2,S05) )
  )
ENDIF
C..... CHECK TO SEE IF LAST RULE IS STILL IN EFFECT
IF (DIR.EQ.DIRL .AND.
  & ((DIR.EQ.1 .AND. P.LT.A) .OR. (DIR.EQ.2 .AND. P.GT.A) .OR.
  & (DIR.EQ.5 .AND. P.GT.A) .OR. (DIR.EQ.4 .AND. P.LT.A)) ) THEN
  RETURN
ENDIF
C..... CALC ENCURSION RATIO AT EVERY ZERO CROSSING...
IF (PMPL.LE.0) CALL ONE(O,UPRS,EXRR, DV,DLI,ESE,PSE,PSEOLD,CSE)
C..... ERASE SMALL LOOP FLAGS
IF (IR.GT.0) THEN
  IT=IR
  DO 10 I=1,IT
    IF ((FRCI).EQ.'L' .AND. (P.LE.PRCI) .OR. D.LE.DRCI) ) .OR.
    & (FRCI).EQ.'7' .AND. (P.GE.PRCI) .OR. D.GE.DRCI) ) THEN
      IR=I-1
      GO TO 15
    ENDIF
  10 CONTINUE
ENDIF
15 IS=IR-1
C..... IF (DIR.EQ.1 .OR. DIR.EQ.3) THEN
C..... LOADING RULES ..... RULES 1.5-11
PC2=SIGK(PC/2),PM)
C..... LOADING ON BACKBONE
50 IF (BACKB .OR. RULE.EQ.0.0) THEN
  K=0
  DO 40 J=2,NS
    DO=OSK(J)-ABSK(D)
    DP=PSK(J)-AP
    IF (AP.LT.PSK(J) .AND. (DO*DP).GT.0.) THEN
      S0P=DO
      IF (S.GT.K .AND. S.LE.SI) THEN
        K=S
        A=SIGK(PSK(J),P)
      ENDIF
    ENDIF
  40 CONTINUE
  RULE=1
  BACKB=.TRUE.
  IR=0
C..... LOADING AFTER UNLOADING
ELSE
  CRACKD=(ABS(DM).GT.DC)
  REVRSL=((DIR.EQ.1 .AND. DIRL.EQ.4) .OR. LRULE.EQ.8
  & .OR. (DIR.EQ.5 .AND. DIRL.EQ.2) .OR. LRULE.EQ.9
  & .OR. LRULE.EQ.5 .OR. LRULE.EQ.11)
  IF (CRACKD) THEN
    P2=.95*SIGK(PMAX,PM)
    D2=F02(DMAX)
  ELSE
    P2=PM
    D2=DM
  ENDIF
  SK=KMIN(D2-0),(P2-P),SI)
  I=I-1
20 RELOADING INSIDE SMALL LOOPS
C..... IF (I.GT.0) THEN
  & IF (.NOT.(FRCI).EQ.'7' .AND. DIR.EQ.1) .OR.
  & (FRCI).EQ.'L' .AND. DIR.EQ.5) ) GO TO 20MVS02690
  & IF (SR1.LE.0 .OR. SR2.LE.0 .OR. SRS.LE.0 .OR.
  & SRM.LE.0) THEN
    I=1
    GO TO 20
  ENDIF
  IF (AP.LT.ABS(PC2) .AND. S.GT.SRM) THEN
    REVRSL=.FALSE.
    I=1
    GO TO 20
  ENDIF
  IF (ABS(PRCI).LE.PC/4) THEN
    K=KMIN(D-ORCI),(P-PRCI),SI)
    A=PRCI
    RULE=11.5+I/1000.
  ENDIF
ENDIF

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HVS01600
HVS01610
HVS01620
HVS01630
HVS01640
HVS01650
HVS01660
HVS01670
HVS01680
HVS01690
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HVS02820
HVS02830
HVS02840

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ELSE IF (ABS(PRCI).LE.3*PC/4) THEN
  X2=D2-(P2-1.5*PC2)/SR3
  X1=X2-PC2/SR2
  X0=X2-PC2/2-P/SR2
  IF (AP.LT.PC/4 .AND. ((DIR.EQ.1 .AND. X.LT.X1).OR.
  (DIR.EQ.5 .AND. X.GT.X1)) ) THEN
    K=KMIN(X1-0),(PC2/2-P),SI)
    A=SIGK(PC/4),PM)
    RULE=11.2+I/1000.
  ELSE
    K=KMIN(DRCI-0),(PRCI-P),SI)
    A=PRCI
    RULE=11.5+I/1000.
  ENDIF
  ELSE
  X2=DRCI-(PRCI)-1.5*PC2)/SRM
  X1=X2-PC2/SR2
  X0=X2-PC2/2-P/SR2
  IF (AP.LT.PC/4 .AND. ((DIR.EQ.1 .AND. X.LT.X1).OR.
  (DIR.EQ.5 .AND. X.GT.X1)) ) THEN
    K=KMIN(X1-0),(PC2/2-P),SI)
    A=SIGK(PC/4),PM)
    RULE=11.4+I/1000.
  ELSE
    X0=X2-1.5*PC2-P/SRS
    IF (AP.LT.5*PC/4 .AND.
    ((DIR.EQ.1 .AND. X.LT.X2)
    .OR. (DIR.EQ.5 .AND. X.GT.X2)) ) THEN
      K=KMIN(X2-0),(1.5*PC2-P),SI)
      A=SIGK(5*PC/4),PM)
      RULE=11.5+I/1000.
    ELSE
      SRS=SRM
      K=KMIN(DRCI-0),(PRCI-P),SI)
      A=PRCI
      RULE=11.6+I/1000.
    ENDIF
  ENDIF
C..... INITIAL RELOADING BELOW PC/2 W/O REVERSAL
RULE 6
ELSE IF (AP.LT.ABS(PC2) .AND. .NOT.REVRSL) THEN
  K=F51(DMAX)
  A=PC2
  RULE=6
C..... RELOADING TO P2
RULE 7
ELSE IF (AP.LT.ABS(PC2) .AND.
  & (.NOT.REVRSL .OR. AP.GE.PC*0.75) ) THEN
  K=S
  A=P2
  RULE=7
C..... RELOADING BELOW PC WITH REVERSAL
RULES 8 & 9
ELSE IF (AP.LT.PC*0.75) ) THEN
  SR=SR(DMAX)
  SI=F51(DMAX)
  S2=F52(DMAX)
  S3=F53(DMAX)
  PA=SIGK(PMAX,PM)-SIGK(PC,PM)
  DA=SIGK(DMAX,PM)-SIGK(PC,PM)/SI
  PB=SIGK (KMIN ABSKPA),(PC/2)),PM)
  DB=DA-(PA-PB)/S2
  DOP=DM-PB/S2
  DO=DM-PM*(DMG-DMH)/(PMG-PMH)
  IF (DIR.EQ.1) DOP=MAX(DOP,DO)
  IF (DIR.EQ.5) DOP=MIN(DOP,DO)
  DC2=DOP/PC2/SI
  SRM=KMIN(DC2-D2),(PC2-P2),SI)
  IF (S.GT.SRM) THEN
    REVRSL=.FALSE.
    GO TO 20
  ENDIF
  SRP=KMIN(DC2-0),(PC2-P),SI)
  SR1=MAX(SRP,MIN(SR,S3))
  DC2P=D+(PC2-P)/SR1
  SRS=KMIN(D2-DC2P),(P2-PC2),SI)
  SR2=2.00/(1/SR1 + 1/SRS)
  IF (AP.LT.(PC/4) ) THEN
    K=SR1
    A=SIGK(PC/4),PM)
    RULE=8
  ELSE
    K=SR2
    A=SIGK(PC,PM)*0.75
    RULE=9
  ENDIF
C..... LOADING TOWARDS THE BACKBONE CURVE
RULE 10MVS03720
ELSE
  BACKB=.TRUE.
  IF (.NOT. CRACKD) GO TO 50
  IR=0
  ALPHAP=1.0
  IF (ABSK(DM).EQ.ABSK(DMAX)) ALPHAP=ALPHA
  K=KMIN (ALPHAP*SIGK(DMAX,D2)-D2),(SIGK(PMAX,P2)-P2)
  & (SI)
  DO 50 J=2,NS
    IF (PSK(J).LE.ABSK(PMAX)) GO TO 50
    JO=J-1
    DO=OSK(J)-OSK(JO)
    DP=PSK(J)-PSK(JO)
    IF ((DP*DO).LE.0.) GO TO 50
    CALL INTSCT(DM,PN,D,P,K,SIGK(OSK(J),P),
    & (DP/DO) )
    IF (ABS(DX).GE.ISK(JO) .AND. ABS(DX).LE.OSK(J) .AND.
    & ABS(PN).GT.ABS(PMAX) .AND. PMPX.GT.0) THEN
      IF (AP.GE.ABS(PC)) GO TO 50
      K=KMIN(DN-0),(PN-P),SI)
      A=PN
      RULE=10
      GO TO 100
    ENDIF
  50 CONTINUE
  GO TO 50
ENDIF
C..... UNLOADING RULES .....
C..... INITIALIZE VALUES
RULES 2-5MVS04060
BACKB=.FALSE.
HVS04070

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S1=FSL(DMAX)
S2=FSL(DMAX)
S3=FSL(DMAX)
D0=DM-PM*(DMG-DMH)/(PMG-PMH)
PA=PM-SIGK(PC,PM)
DA=DM-SIGK(PC,PM)/S1
PB=SIGK(MINABS(PA),(PC/2)),PM)
S02=KMIN(DA-D0),PA,S1)
D8=DA-(PA-PB)/MAX(S2,S02)
S05=KMIN(D8-D0),PB,S1)
SU=0.

C ..... UNLOADING INSIDE SMALL POSITIVE LOOPS ..... RULE 5
I=IR-1
I=I-1
IF (I.GT.0) THEN
  IF (NOT((DIR.EQ.2 .AND. FRI).EQ.'L') .OR.
    (DIR.EQ.4 .AND. FRI).EQ.'R')) GO TO 70
C ..... UNLOADING ON THE TOP SEGMENT ..... RULE 2
K=MAX(S1,SU)
A=PA
RULE=2
C ..... UNLOADING ON THE MIDDLE SEGMENT ..... RULE 3
ELSE IF (AP.GT.ABS(PB)) THEN
  K=MAX(S2,S02,SU)
  A=PB
  RULE=3
C ..... UNLOADING ON THE BOTTOM SEGMENT ..... RULE 4
ELSE
  K=MAX(S3,S03,SU)
  A=0.
  RULE=4
ENDIF
ENDIF
C ..... SAVE REVERSAL POINTS FOR SMALL LOOPS .....
100 IRL=INT(RULE)
REVRSL=DIRL.EQ.1.OR.IRL.EQ.10.OR.LRULE.EQ.1.OR.LRULE.EQ.10
IF ((DIRL.EQ.1 .AND. DIR.EQ.2 .AND. NOT REVRSL)
  .OR. (DIRL.EQ.4 .AND. DIR.EQ.5)) THEN
  IF (IR.LT.NI) THEN
    IR=IR+1
    PR(IR)=P
    DR(IR)=D
    FR(IR)=F
  ENDIF
ELSE IF ((DIRL.EQ.5 .AND. DIR.EQ.4 .AND. NOT REVRSL)
  .OR. (DIRL.EQ.2 .AND. DIR.EQ.1)) THEN
  IF (IR.LT.NI) THEN
    IR=IR-1
    PR(IR)=P
    DR(IR)=D
    FR(IR)=F
  ENDIF
ENDIF
IF ((I.OS*SI).GT.K .AND. K.GT.0) GO TO 9999
K=D
RULE=RULE
9999 CONTINUE
RETURN
END

```

```

HYSD4080 C UM2 PEAK LOAD IN THE POSITIVE DIRECTION HYSD0560
HYSD4090 C UM5 PEAK DISPLACEMENT IN THE NEGATIVE DIRECTION HYSD0570
HYSD4100 C UM6 PEAK LOAD IN THE NEGATIVE DIRECTION HYSD0580
HYSD4110 C S1 UNLOADING STIFFNESS HYSD0590
HYSD4120 C X0 HYSD0600
HYSD4130 C X0UM HYSD0610
HYSD4140 C U00 HYSD0620
HYSD4150 C U0 HYSD0630
HYSD4160 C U0 HYSD0640
HYSD4170 C X1UM HYSD0650
HYSD4180 C U1 HYSD0660
HYSD4190 C UID HYSD0670
HYSD4200 C X2U0 HYSD0680
HYSD4210 C U2 HYSD0690
HYSD4220 C XSU1 HYSD0700
HYSD4230 C U3 HYSD0710
HYSD4240 C U3 HYSD0720
HYSD4250 C U3 HYSD0730
HYSD4260 C ACHNG LOAD WHERE RULE CHNGS IF LOADING CONTINUES IN CURR DIRECTION HYSD0740
HYSD4270 C PRINT HYSD0750
HYSD4280 C SE ELASTIC UNLOADING CURVE HYSD0760
HYSD4290 C ESE ELASTIC STRAIN ENERGY HYSD0770
HYSD4300 C PSE PLASTIC STRAIN ENERGY HYSD0780
HYSD4310 C PSEOLD PLASTIC STRAIN ENERGY AT LAST ZERO CROSSING HYSD0790
HYSD4320 C UPOS POSITIVE DUCTILITY INFO. HYSD0800
HYSD4330 C UNEG NEGATIVE DUCTILITY INFO. HYSD0810
HYSD4340 C EXCR EXCURSION RATIO INFO. HYSD0820
HYSD4350 C C HYSD0830
HYSD4360 C JI # FOR CURRENT DIRECTION FOR LOADING AND UNLOADING HYSD0840
HYSD4370 C # FOR NEW DIRECTION FOR REVERSAL HYSD0850
HYSD4380 C UPOS POSITIVE DUCTILITY INFO. # = 1 FOR NEGATIVE LOAD HYSD0860
HYSD4390 C IREVS1 SIGN OF LOAD IN NEW DIRECTION HYSD0870
HYSD4400 C ISGN SIGN OF THE CURRENT LOAD FOR LOADING AND UNLOADING HYSD0880
HYSD4410 C SIGN OF THE NEW LOAD FOR REVERSAL HYSD0890
HYSD4420 C HYSD0900
HYSD4430 C HYSD0910
HYSD4440 C HYSD0920
HYSD4450 C HYSD0930
HYSD4460 C HYSD0940
HYSD4470 C HYSD0950
HYSD4480 C HYSD0960
HYSD4490 C HYSD0970
HYSD4500 C HYSD0980
HYSD4510 C HYSD0990
HYSD4520 C HYSD1000
HYSD4530 C HYSD1010
HYSD4540 C HYSD1020
HYSD4550 C HYSD1030
HYSD4560 C HYSD1040
HYSD4570 C HYSD1050
HYSD4580 C HYSD1060
HYSD4590 C HYSD1070
HYSD4600 C HYSD1080
HYSD4610 C HYSD1090
HYSD4620 C HYSD1100
HYSD4630 C HYSD1110
HYSD4640 C HYSD1120
HYSD4650 C HYSD1130
HYSD4660 C HYSD1140
HYSD4670 C HYSD1150
HYSD4680 C HYSD1160
HYSD4690 C HYSD1170
HYSD4700 C HYSD1180
HYSD4710 C HYSD1190
HYSD4720 C HYSD1200
HYSD4730 C HYSD1210
HYSD4740 C HYSD1220
HYSD4750 C HYSD1230
HYSD4760 C HYSD1240
HYSD4770 C HYSD1250
HYSD4780 C HYSD1260
HYSD4790 C HYSD1270
HYSD4800 C HYSD1280
HYSD4810 C HYSD1290
HYSD4820 C HYSD1300
HYSD4830 C HYSD1310
HYSD4840 C HYSD1320
HYSD4850 C HYSD1330
HYSD4860 C HYSD1340
HYSD4870 C HYSD1350
HYSD4880 C HYSD1360
HYSD4890 C HYSD1370
HYSD4900 C HYSD1380
HYSD4910 C HYSD1390
HYSD4920 C HYSD1400
HYSD4930 C HYSD1410
HYSD4940 C HYSD1420
HYSD4950 C HYSD1430
HYSD4960 C HYSD1440
HYSD4970 C HYSD1450
HYSD4980 C HYSD1460
HYSD4990 C HYSD1470
HYSD5000 C HYSD1480
HYSD5010 C HYSD1490
HYSD5020 C HYSD1500
HYSD5030 C HYSD1510
HYSD5040 C HYSD1520
HYSD5050 C HYSD1530
HYSD5060 C HYSD1540
HYSD5070 C HYSD1550
HYSD5080 C HYSD1560
HYSD5090 C HYSD1570
HYSD5100 C HYSD1580
HYSD5110 C HYSD1590

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100 IF (IDR) 130,130,110
110 IF (ABS(PI).GE.PC) GO TO 200
B=PI
A=PC*ISGN
S=OC
SE=S
NRL=1
HRL=1.11
GO TO 2000
150 B=0.
A=PC*IREVSL
IF (PI.NE.0) A=PC*SIGN(1.0,PI)
S=OC
SE=S
NRL=1
HRL=1.2
GO TO 2000
C ===== TAKEDA RULE 2.0 ===== LOADING ON PRIMARY CURVE UP TO YIELD
200 IF (IDR) 250,250,210
210 IF (ABS(PI).GE.PV) GO TO 500
B=PI
A=PV*ISGN
S=CV
SL=PI<PC*ISGN>><DI-OC*ISGN>
SE=S1
NRL=2
HRL=2.11
GO TO 2000
250 B=0.
A=PI
SL=PI<PC*ISGN>><DI-OC*ISGN>
S=S1
SE=S1
NRL=5
HRL=2.2
GO TO 2000
C ===== TAKEDA RULE 3.0 ===== LOADING ON PRIMARY CURVE AFTER YIELD
500 BOTT=MAX(ABS(DI),ABS(U1),ABS(U2))
SL=CV*(DY/BOTT)**0.40
SE=S1
IF (IDR) 350,350,310
310 IF (ABS(PI).GE.PU) GO TO 520
A=PU*ISGN
B=PI
S=VU
NRL=5
HRL=3.11
GO TO 2000
520 A=PU*ISGN
B=PI
S=0.
IF (MAX(UG.NE.0) S=VU
NRL=5
HRL=3.12
GO TO 2000
530 B=0.
A=PI
BOTT=MAX(ABS(DI),ABS(U1),ABS(U2))
SL=CV*(DY/BOTT)**0.40
S=S1
NRL=9
HRL=3.2
GO TO 2000
C ===== TAKEDA RULE 4.0 ===== UNLOADING FROM POINT U1 ON THE PRIMARY CURVE AFTER YEILDING
400 IF (IDR) 450,440,410
410 IF (ABS(PI).GE.ABS(UK(JI,2))) GO TO 420
A=UK(JI,2)
B=PI
S=S1
NRL=9
HRL=4.11
GO TO 2000
420 A=PU*ISGN
B=PI
S=VU
NRL=5
HRL=4.12
GO TO 2000
450 A=PI
B=0.
S=S1
NRL=9
HRL=4.2
GO TO 2000
440 IF (DI.LE.DS) IDR=1
IF (DI.GT.DS) IDR=2
IF (ABS(UK>IDRW,1)).GT.DC) GO TO 450
A=PC*IREVSL
B=0.
S=S1
NRL=15
HRL=4.51
GO TO 2000
450 X=DI
K2U=(0.-UK>IDRW,2)>><(DI-UK>IDRW,1)>
K2V=(0.-PV*ISGN)>><DI-OC*ISGN>
IF (PY.GT.ABS(UK>IDRW,2)) .AND. XDY.GT.X2U) GO TO 460
A=UK>IDRW,2)
B=0.
S2=X2U
S=S2
NRL=9
HRL=4.52
GO TO 2000
460 UK(JI,1)>>DV*ISGN
UK(JI,2)>>PV*ISGN
A=UK(JI,2)
B=0.
S2=X2V
S=S2
NRL=6
HRL=4.55
GO TO 2000
C ===== TAKEDA RULE 5.0 ===== UNLOADING FROM POINT U1 ON THE PRIMARY CURVE BEFORE YEILDING
500 IF (IDR) 550,540,510
510 IF (ABS(PI).GE.ABS(UK(JI,2))) GO TO 200
A=UK(JI,2)
B=PI
S=S1
NRL=5
HRL=5.11
GO TO 2000
550 A=PI
B=0.
S=S1
NRL=5
HRL=5.11
GO TO 2000
540 IF (DI.LE.DS) IDR=2
IF (DI.GT.DS) IDR=1
IF (ABS(UK>IDRW,1)).GT.DC) GO TO 450
A=PC*IREVSL
B=0.
S=S1
NRL=14
HRL=5.51
GO TO 2000
C ===== TAKEDA RULE 6.0 ===== LOADING TOWARDS POINT U1 ON THE PRIMARY CURVE.
600 IF (IDR) 650,650,610
610 IF (ABS(PI).GE.ABS(UK(JI,2))) GO TO 210
A=UK(JI,2)
B=PI
K2U=(PI-UK(JI,2))>><(DI-UK(JI,1))>
S=X2U
NRL=6
HRL=6.11
GO TO 2000
650 U=DI
U=PI
A=PI
B=0.
S=S1
NRL=7
HRL=6.20
GO TO 2000
C ===== TAKEDA RULE 7.0 ===== UNLOADING FROM POINT U1 AFTER RULE 6
700 IF (IDR) 750,740,710
710 IF (ABS(PI).GE.ABS(U)) GO TO 720
A=U
B=PI
S=S1
NRL=7
HRL=7.11
GO TO 2000
720 A=UK(JI,2)
B=PI
K2U=(0.-UK(JI,2))>><(DI-UK(JI,1))>
S=X2U
NRL=6
HRL=7.12
GO TO 2000
750 A=PI
B=0.
S=S1
NRL=7
HRL=7.2
GO TO 2000
740 A=UK(JI,2)
B=0.
K2U=(PI-UK(JI,2))>><(DI-UK(JI,1))>
S=X2U
NRL=8
HRL=7.5
GO TO 2000
C ===== TAKEDA RULE 8.0 ===== LOADING TOWARDS POINT U1 ON THE PRIMARY CURVE
800 IF (IDR) 850,850,810
810 IF (ABS(PI).GE.ABS(UK(JI,2))) GO TO 210
A=UK(JI,2)
B=PI
K2U=(PI-UK(JI,2))>><(DI-UK(JI,1))>
S=X2U
NRL=8
HRL=8.11
GO TO 2000
850 U=PI
U=DI
A=PI
B=0.
S=S1
NRL=9
HRL=8.2
GO TO 2000
C ===== TAKEDA RULE 9.0 ===== UNLOADING FROM POINT U1 AFTER RULE 8
900 IF (IDR) 950,940,910
910 IF (ABS(PI).GE.ABS(U)) GO TO 810
A=U
B=PI
S=S1
NRL=9
HRL=9.11
GO TO 2000
950 A=PI
B=0.
S=S1
NRL=9
HRL=9.2
GO TO 2000
940 A=U
B=0.
K2U=(PI-U)>><(DI-U)>
S=X2U
NRL=10
HRL=9.5
GO TO 2000
C ===== TAKEDA RULE 10.0 ===== LOADING TOWARDS POINT U1
1000 IF (IDR) 1050,1050,1010
1010 IF (ABS(PI).GE.ABS(U)) GO TO 610
A=U
B=PI
K2U=(PI-U)>><(DI-U)>
S=X2U
NRL=10
HRL=10.11
GO TO 2000
1050 U=PI
A=PI
B=0.
S=S1
NRL=11
HRL=10.2
GO TO 2000
C ===== TAKEDA RULE 11.0 ===== UNLOADING FROM POINT U2 AFTER RULE 10
1100 IF (IDR) 1150,1140,1110
1110 IF (ABS(PI).GE.ABS(U)) GO TO 1010

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A=U2
B=PI
S=S1
NRL=11
      HRLN=11.11
GO TO 2000
1150 A=PI
B=0
S=S1
NRL=11
      HRLN=11.2
GO TO 2000
1160 A=U1
B=0
XSU1=(PI-U1)/(DI-UID)
S=XSU1
NRL=12
      HRLN=11.5
GO TO 2000
C ===== TAKEDA RULE 12.0 ===== LOADING TOWARDS POINT U1
1200 IF (IDR) 1250,1250,1210
1210 IF (ABS(PI).GE.ABS(U1)) GO TO 810
A=U1
B=PI
XSU1=(PI-U1)/(DI-UID)
S=XSU1
NRL=12
      HRLN=12.11
GO TO 2000
1250 U=PI
A=PI
B=0
S=S1
NRL=13
      HRLN=12.2
GO TO 2000
C ===== TAKEDA RULE 15.0 ===== UNLOADING FROM POINT US AFTER RULE 12
1300 IF (IDR) 1350,1400,1410
1310 IF (ABS(PI).GE.ABS(U1)) GO TO 1210
A=U1
B=PI
S=S1
NRL=15
      HRLN=15.11
GO TO 2000
1350 A=PI
B=0
S=S1
NRL=15
      HRLN=15.2
GO TO 2000
C ===== TAKEDA RULE 14.0 ===== LOADING IN THE UNCRACKED DIRECTION AFTER
CRACKING IN THE OTHER DIRECTION.
1400 IF (IDR) 1450,1440,1410
1410 IF (ABS(PI).GE. PC ) GO TO 210
A=PC*ISGM
B=0
S=S1
NRL=14
      HRLN=14.11
GO TO 2000
1450 A=PI
B=0
S=S1
NRL=14
      HRLN=14.2
GO TO 2000
1460 A=UMK(JI,2)
B=0
S=S1
NRL=5
      HRLN=14.5
GO TO 2000
C ===== TAKEDA RULE 15.0 ===== LOADING IN THE UNCRACKED DIRECTION AFTER
YIELDING IN THE OTHER DIRECTION.
1500 IF (IDR) 1550,1540,1510
1510 IF (ABS(PI).GE. PC ) GO TO 1520
A=PC*ISGM
B=PI
S=S1
NRL=15
      HRLN=15.11
GO TO 2000
1520 PQ=PC*ISGM
DQ=(PQ-PI)/S1+OI
QV=(PV*ISGM-PQ)/(DV*ISGM-DQ)
A=PQ*ISGM
B=PQ
S=QV
NRL=16
      HRLN=15.12
GO TO 2000
1550 A=PI
B=0
S=S1
NRL=15
      HRLN=15.2
GO TO 2000
1540 IF (ABS(PI).GE. ABS(UMK(JI,2))) GO TO 1550
A=UMK(JI,2)
B=0
S=S1
NRL=4
      HRLN=15.51
GO TO 2000
1550 A=FU*IREVSL
B=0
S=YU
NRL=5
      HRLN=15.52
GO TO 2000
C ===== TAKEDA RULE 16.0 ===== LOADING TOWARDS THE YIELD POINT AFTER
RULE 15.
1600 IF (IDR) 1650,1650,1610
1610 IF (ABS(PI).GE. PV ) GO TO 300
A=PV*ISGM
B=PI
S=QV
NRL=16
      HRLN=16.11
GO TO 2000
1650 UMK(JI,1)=DV
UMK(JI,2)=PV
UO=PI

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HY504080 UO=DI
HY504090 A=PI
HY504100 B=0
HY504110 S=S1
HY504120 S2=QV
HY504130 XO=DI-PI/S2
HY504140 NRO=7
HY504150 HRLN=16.2
HY504160 GO TO 2000
C
HY504180 C ===== CALCULATE MAXIMUM PREVIOUS DEFORMATION
HY504190 2000 UMI=MIN(UMK(1,1),DI)
HY504200 UM2=MIN(UMK(1,2),PI)
HY504210 UM5=MAX(UMK(2,1),DI)
HY504220 UM6=MAX(UMK(2,2),PI)
HY504230 RNRL=NRL
HY504240 IDRO=IDR
HY504250 RF=0.
HY504260 IF (IDR.GE.0) ACHNG=A
HY504270 IF (IDR.LT.0) ACHNG=B
HY504280 RETURN
HY504290 END
HY504300 C =====
HY504310 C HYSTO7
HY504320 C
HY504330 C SU_BROU_TINE_ELSPLS - ELASTO-PLASTIC BILINEAR HYSTERESIS MODEL
HY504340 C
HY504350 C FC = CURRENT LOAD
HY504360 C PEQ = MODIFIED CURRENT LOAD
HY504370 C DC = CURRENT DISPL.
HY504380 C FL = LAST LOAD
HY504390 C DL = LAST DISPL.
HY504400 C PV = VEILD LOAD
HY504410 C PVEQ = MODIFIED VEILD LOAD
HY504420 C S = ELASTIC STIFFNESS
HY504430 C K = CURRENT STIFFNESS (OUTPUT)
HY504440 C RUL = CURRENT RULE NUMBER, USED TO TRACE MODEL (OUTPUT)
HY504450 C RNRL = NEXT RULE NUMBER (OUTPUT)
HY504460 C VI = NOT USED
HY504470 C VL = NOT USED
HY504480 C KIE = INELASTIC STIFFNESS
HY504490 C
HY504500 C SUBROUTINE HYSTO7(FC,DC,FL,DL,K,RULE,PSEOLD,A,B,
HY504510 $ VI,VL,S,PV,KIE,DV,CSE,PRINT,ESE,PSE,KEY,UPOS,UMEG,ENCR)
HY504520 REAL K,KIE
HY504530 LOGICAL PRINT,BTEST
HY504540 DIMENSION UPOS(5),UMEG(5),ENCR(6),ESE(5)
HY504550
HY504560 FC=FC*DC-DL*FL
HY504570 IF (PRINT) WRITE (6,1010) FC,DC,FL,DL,K,RULE,VI,CSE,VL,S,PV,KIE,
HY504580 $ A,B,KEY,ESE(5),PSE,PSEOLD,UPOS,UMEG,ENCR
HY504590 1010 FORMAT (
HY504600 $ EL SPLS-FC=,G15.5, DC=,G15.5, FL=,G15.5, DL=,G15.5,UMEG(5)/HY504610
HY504620 $ EL- K=,G15.5, RULE=,G15.5, VI=,G15.5, CSE=,G15.5,UMEG(5)/HY504630
HY504640 $ EL- VL=,G15.5, S=,G15.5, PV=,G15.5, KIE=,G15.5,UMEG(5)/HY504650
HY504660 $ EL- A=,G15.5, B=,G15.5/
HY504680 $ EL- KEY=,G15.5, ESE=,G15.5, PSE=,G15.5, PSEOLD=,G15.5,UMEG(5)/HY504690
HY504700 $ EL- UP1=,G15.5, UP2=,G15.5, UP3=,G15.5/
HY504720 $ EL- UM1=,G15.5, UM2=,G15.5, UM3=,G15.5/
HY504740 $ EL- EX1=,G15.5, EX2=,G15.5, EX3=,G15.5/
HY504760 $ EL- EX4=,G15.5, EX5=,G15.5, EX6=,G15.5)
HY504770 C
HY504780 C ..... CALC EXCURSION RATIO AT EVERY ZERO CROSSING...
HY504790 IF (FC*DL.LE.0)CALL DNEQ,UPOS,ENCR, DV,DL,ESE,PSE,PSEOLD,CSE)
HY504800 C
HY504810 C ----- ELASTIC REGION
HY504820 IF (RULE.LE.1 .AND. ABS(FC).LT.PV) THEN
HY504830 K=S
HY504840 RUL=1.
HY504850 A= PV
HY504860 B=-PV
HY504870 FC=S*DC
HY504880 CALL STRENG (ESE,PSE,PSEOLD,FC,FL,DC,DL,K,S )
HY504890 KEY=0
HY504900 GO TO 1000
HY504910 ENDIF
HY504920 C ----- INELASTIC REGION
HY504930 DIR=DC-DL
HY504940 IF (DIR.EQ.0) RETURN
HY504950 PEQ=FC-KIE*DC
HY504960 PVEQ=PV*(1-KIE/S)
HY504970 DVEL=VI*VL
HY504980 IF (PRINT) WRITE (6,*) 'REQ,PVEQ,DVEL,VI,VL.'
HY504990 IF (PRINT) WRITE (6,*) 'PEQ,PVEQ,DVEL,VI,VL'
HY505000 C
HY505010 C ----- LOAD AT OR ABOVE POSITIVE YIELD
HY505020 IF (RULE.EQ.1) THEN
HY505030 IF (DIR.GT.0) THEN
HY505040 ... POSITIVE YIELD ...
HY505050 CALL STRENG (ESE,PSE,PSEOLD, PV,FL, DV,DL,S,S )
HY505060 FL=PV
HY505070 DL=DV
HY505080 GO TO 210
HY505090 ELSE
HY505100 ... NEGATIVE YIELD ...
HY505110 CALL STRENG (ESE,PSE,PSEOLD,-PV,FL,-DV,DL,S,S )
HY505120 FL=-PV
HY505130 DL=-DV
HY505140 GO TO 220
HY505150 ENDIF
HY505160 ELSE
HY505170 IF (RULE.EQ.2.10) GO TO 210
HY505180 IF (RULE.EQ.2.20) GO TO 220
HY505190 IF (RULE.EQ.2.30) GO TO 230
HY505200 ENDIF
HY505210 WRITE (6,*) 'INVALID RULE IN HYSTO7-BILINEAR HYSTERESIS MODEL'
HY505220 C
HY505230 C ----- LOAD AT OR ABOVE POSITIVE YIELD, ON BACKBONE CURVE
HY505240 210 IF (DIR.LE.0) GO TO 250
HY505250 K=KIE
HY505260 RUL=2.10
HY505270 FC=PVEQ-OC*KIE
HY505280 B= FC
HY505290 A= FC*10
HY505300 CALL STRENG (ESE,PSE,PSEOLD,FC,FL,DC,DL,K,S )
HY505310 KEY=1
HY505320 IF (DVEL.LT.0) THEN
HY505330 K=S
HY505340 B= FC
HY505350 A= FC
HY505360 ENDIF
HY505370
HY505380
HY505390
HY505400
HY505410
HY505420
HY505430
HY505440
HY505450
HY505460
HY505470
HY505480
HY505490
HY505500
HY505510
HY505520
HY505530
HY505540
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HY506180
HY506190
HY506200

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GO TO 1000
C----- LOAD AT OR BELOW NEGATIVE YIELD, ON BACKBONE CURVE
220 IF (DIR.GE.0) GO TO 230
K=KIE
RULE=2.20
FC=PVEQ-DC*KIE
B=FC
A=FC*10
CALL STRENG (ESE,PSE,PSEOLD,FC,FL,DC,DL,K,S)
KEY=2
IF (DVEL.LT.0) THEN
  K=S
  B=FC
  A=FC
ENDIF
GO TO 1000

C----- LOAD IN LINEAR RANGE BETWEEN BACKBONE CURVES
230 K=S
RULE=2.3
FC=S*(DC-DL) + FL
A=FC + PVEQ - PEQ
B=FC - PVEQ - PEQ
IF (FC.GT.A) THEN
  DA=DC*(A-FC)/S
  CALL STRENG (ESE,PSE,PSEOLD, A,FL,DA,DL,K,S)
  DL=DA
  FL=A
  GO TO 210
ELSE IF (FC.LT.B) THEN
  DB=DC*(B-FC)/S
  CALL STRENG (ESE,PSE,PSEOLD, B,FL,DB,DL,K,S)
  DL=DB
  FL=B
  GO TO 220
ENDIF

C----- CALC D & E'S BASED ON PEAK STRAIN ENERGY
IF (KEY.EQ.1) CALL DMX1,UPOS,EXGR, DV,DL,ESE(2),PSE,PSEOLD,CSE)
IF (KEY.EQ.2) CALL DMX1,UNEQ,EXGR,-DV,DL,ESE(5),PSE,PSEOLD,CSE)

C----- CALC STRAIN ENERGY FOR THIS STEP...
CALL STRENG (ESE,PSE,PSEOLD,FC,FL,DC,DL,K,S)

C----- CALC PLASTIC STRAIN ENERGY AT ZERO CROSSING ...
KEY=5

1000 IF (PRINT) WRITE (6,1011) FC,K,A,B
1011 FORMAT
  &' EL-END-FC=',F8.3, ' K=',F8.3, ' A=',F8.3, ' B=',F8.3,
  IF (PRINT) WRITE (6,1010) FC,DC,FL,DL,K,RALE,VI,VL,S,PV,KIE,
  & A,B,REV,ESE,PSE,PSEOLD,UPOS,UNEQ,EXGR
  RETURN
  END

C----- SUBROUTINE IDRECT (IDR,IDRV,IDRV0,PI,PS,VI,VS)
SUBROUTINE IDRECT (IDR,IDRV,IDRV0,PI,PS,VI,VS)
  LOGICAL A,NA,B,NC,ND,D,ND,E
  LOGICAL STEST
  A = ABS(PI).GE.ABS(PS)
  B = PI*PS.GE.0
  C = PI.EQ.0
  D = VS*VI.GE.0
  NA = .NOT. A
  NB = .NOT. B
  NC = .NOT. C
  ND = .NOT. D
  C----- IF ( A .AND. B .AND. NC .AND. D ) IDR=1
  IF ( NA .AND. B .AND. NC .AND. ND ) IDR=1
  IF ( NA .AND. B .AND. NC .AND. ND ) IDR=1
  IF ( NA .AND. B .AND. NC .AND. D ) IDR=0
  IF ( A .AND. B .AND. NC .AND. D ) IDR=0
  IF ( A .AND. B .AND. NC .AND. ND ) IDR=-1
  IF ( NA .AND. B .AND. NC .AND. D ) IDR=-1
  E = PI .GE. PS
  IDRV=1
  IDRV=2
  IF (E) IDRV=2
  IF (E) IDRV=0
  RETURN
  END

C----- SUBROUTINE INTDUAL(BUG,NOOF,MAXMOD,MODE,TITLE,
  & IDOF,IO,J,FLG,DISP,VEL,ACC,FORCE)
SUBROUTINE INTDUAL(BUG,NOOF,MAXMOD,MODE,TITLE,
  & IDOF,IO,J,FLG,DISP,VEL,ACC,FORCE)
  DIMENSION DISP*(NOOF),VEL*(NOOF),ACC*(NOOF),AK(6),FORCE*(NOOF)
  DIMENSION ID*(MAXMOD),JFLG*(MAXMOD),IDOF*(MAXMOD,6)
  CHARACTER*80 FORMAT(2)
  CHARACTER*(*) TITLE(2)
  CHARACTER*20 OPTION
  LOGICAL BUG,HEAD,TEST,FLAG
  LOGICAL STEST
  C----- INPUT INITIAL DISPL, VELOC AND ACCEL ===
  C----- HEAD=.TRUE.
  C----- INPUT: NODE,IGEN,INC,OPTION,DK,DV,DZ,RX,RV,RZ
  IO READ (5,*) NODE,IGEN,INC,OPTION,(AK I,I=1,6)
  IF (MODE.LE.0) GO TO 500
  IF (HEAD) THEN
    HEAD=.FALSE.
    WRITE (6,5) TITLE(1),TITLE(2)
  ENDIF
  WRITE (6,7) NODE,IGEN,INC,OPTION,(AK I,I=1,6)
  5 FORMAT ('1 STRUCTURE.....',A,
  & ' SOLUTION.....',A,
  & ' INITIAL ACCELERATIONS, VELOCITIES DISPLACEMENTS ',
  & ' AND LOADS ' /
  & ' =====' /
  & ' ',
  & 'X', 'NODE', '2X', 'IGEN', '5X', 'INC', '1X', 'COMPONENT',
  & ' 144', 'TX', '10X', 'TY', '10X', 'TZ',
  & ' 10X', 'RX', '10X', 'RY', '10X', 'RZ')

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7 FORMAT (2X,3I6,1X,A,1P,6G12.4)
C----- DETERMINE IF DISPLACEMENT, VELOCITY, ACCELERATION OR LOAD
IOPT=0
IF (TEST(OPTION,'DISPL',.FALSE.)) THEN
  IOPT=IBSET(IOPT,1)
ELSE IF (TEST(OPTION,'VEL',.FALSE.)) THEN
  IOPT=IBSET(IOPT,2)
ELSE IF (TEST(OPTION,'ACC',.FALSE.)) THEN
  IOPT=IBSET(IOPT,3)
ELSE IF (TEST(OPTION,'LOA',.FALSE.)) THEN
  IOPT=IBSET(IOPT,4)
ELSE IF (TEST(OPTION,'FOR',.FALSE.)) THEN
  IOPT=IBSET(IOPT,5)
ELSE IF (TEST(OPTION,'END',.FALSE.)) THEN
  GO TO 500
ELSE
  WRITE (6,*) 'INVALID OPTION:',OPTION
  GO TO 10
ENDIF

C----- DETERMINE INTERNAL JOINT NUMBER
20 JOINT=IQUICK(NODE,INODE)
IF (JOINT.LE.0) THEN
  WRITE (6,*) 'NODE #',NODE,
  & ' WAS NOT FOUND, CHECK INPUT, INITIAL VALUE IS OMITTED '
  GO TO 10
ENDIF

C----- PUT INITIAL VALUES IN PROPER ARRAYS
DO 30 I=1,6
  IF (AK(I).EQ.0) GO TO 50
  II=IDOF+JOINT-I
  IF (BTST(JFLG,JOINT),I+1) THEN
    WRITE (6,*) 'CONSTRAINED DOF #',I, ' COMPONENT IS SKIPPED'
  ELSE IF (BTST(IOPT,I)) THEN
    DISP(II)=AK(I)
  ELSE IF (BTST(IOPT,2)) THEN
    VEL(II)=AK(I)
  ELSE IF (BTST(IOPT,3)) THEN
    ACC(II)=AK(I)
  ELSE IF (BTST(IOPT,4)) THEN
    FORCE(II)=AK(I)
  ENDIF
30 CONTINUE

C----- GENERATE VALUES AT OTHER NODES
IF (IGEN.GT.0) THEN
  IGEN=IGEN-1
  NODE=NODE+INC
  GO TO 20
ENDIF

C----- LOOP TO READ ADDITIONAL VALUES
GO TO 10

500 CONTINUE

C----- PRINT OUT NON ZERO INITIAL VALUES
FLAG=.TRUE.
DO 520 I=1,NOOF
  IF (DISP(I).NE.0 .OR. VEL(I).NE.0 .OR. ACC(I).NE.0 .OR.
  & FORCE(I).NE.0) THEN
    IF (FLAG) WRITE (6,510)
    WRITE (6,550) I,DISP(I),VEL(I),ACC(I)
    FLAG=.FALSE.
  ENDIF
520 CONTINUE

510 FORMAT ('/X', 'INITIAL, NON-ZERO VALUES'/
  & 'X', 'DOF', '7X', 'FORCE', '10X', 'DISP', '11X', 'VEL', '11X', 'ACC ' /
  & '550 FORMAT (110,4G15.6)

RETURN

C----- INTERSECTION OF TWO LINES IN POINT SLOPE FORM
C----- DEBBUG UNIT(6),SUBCHK,SUBTRACE
C----- END DEBBUG
C----- X = X COORDINATE OF INTERSECTION
C----- Y = Y COORDINATE OF INTERSECTION
C----- K1 = X COORDINATE OF LINE 1
C----- V1 = Y COORDINATE OF LINE 1
C----- S1 = SLOPE OF LINE 1
C----- K2 = X COORDINATE OF LINE 2
C----- V2 = Y COORDINATE OF LINE 2
C----- S2 = SLOPE OF LINE 2

SUBROUTINE INTSCT(X,V,K1,V1,S1,X2,V2,S2)
  IMPLICIT REAL(A-H,O-Z)
  IMPLICIT INTEGER(L-N)
  LOGICAL STEST
  IF (S1.NE.S2) THEN
    R1=V1-S1*K1
    R2=V2-S2*K2
    X=(R1-R2)/(S2-S1)
    Y=(S1*S2-R2*S1)/(S2-S1)
  ELSE
    WRITE (6,10) K1,V1,S1,K2,V2,S2
    10 FORMAT ('/ ***** ER', 'ROR IN INTSCT...', '1X,
  & 'S1=S2, NO SOLN, THUS SET X=Y=0.',
  & ' K1=',IP,G15.5, ' V1=',G15.5, ' S1=',G15.5/
  & ' K2=',IP,G15.5, ' V2=',G15.5, ' S2=',G15.5/)
    X=0
    Y=0
    CALL ERRTRA
  ENDIF
  RETURN
  END

C----- INTEGER FUNCTION IQUICK(TARGET,IO,N)
INTEGER FUNCTION IQUICK(TARGET,IO,N)
  LOGICAL STEST
  IF (IO(1).GT.TARGET .OR. IO(N).LT.TARGET) GO TO 100
  IQUICK=1
  IF (IQUICK.EQ.TARGET) RETURN
  IQUICK=N
  IF (IQUICK.EQ.TARGET) RETURN
  IQUICK=J
  10 J=J/2
  IF (IQUICK.LT.1) IQUICK=1

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INT01100
INT01110
INT01120

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IF (IQUICK.GT.N) IQUICK=N
IF (ID(IQUICK).EQ.TARGET) RETURN
IF (ID(IQUICK).GT.TARGET .AND. J.NE.0) THEN
  IQUICK=IQUICK-J
  GO TO 10
ELSE IF (ID(IQUICK).LT.TARGET .AND. J.NE.0) THEN
  IQUICK=IQUICK+J
  GO TO 10
ENDIF
C
I=MAX(IQUICK-2,1)
J=MIN(I+N)
DO 20 IQUICK=I,J,1
  IF (ID(IQUICK).EQ.TARGET) RETURN
20 CONTINUE
C
DO 30 IQUICK=1,N
  IF (ID(IQUICK).EQ.TARGET) RETURN
30 CONTINUE
C
100 WRITE (6,110) TARGET,IQUICK,IDX(IQUICK)
110 FORMAT (' TARGET=',I6,' NOT FOUND, LAST ID=',I6,' ',I8)
IQUICK=0
RETURN
END
=====
C
SUBROUTINE ISORT(ID,INDEX,N)
  INTEGER ID(N)
  INTEGER INDEX(N)
  LOGICAL FLAG
  LOGICAL BTEST
  DO 10 I=1,N
    INDEX(I)=I
  10 CONTINUE
C
DO 50 I=N,2,-1
  FLAG=.TRUE.
  DO 20 J=I,1
    IF (INDEX(J).LT.INDEX(J-1)) THEN
      K=INDEX(J)
      INDEX(J)=INDEX(J-1)
      INDEX(J-1)=K
      FLAG=.FALSE.
    ENDIF
  20 CONTINUE
  IF (FLAG) RETURN
30 CONTINUE
RETURN
END
=====
SUBROUTINE JOIDSP(IOPT,MANNO,NDOF,NMODE,NLOAD,NCIN,NF,ID,IDOF,
  & CONST,DISP,TITLE,NAME,STEPID,HEAD,NCOS,COSINE,JTCOS,JTFLG)
  DIMENSION IDOF(MANNO,6) ,CONST(MANNO,6),JTFLG(MANNO)
  DIMENSION DISP(NDOF,NLOAD)
  DIMENSION IDX(MANNO)
  DIMENSION DK6,DC6,COSINE(5,5,NCOS),JTCOS(MANNO)
  CHARACTER*(*) TITLE(2),STEPID,NAME
  CHARACTER*15 CDC6
  CHARACTER*40 EQUAL
  LOGICAL HEAD,FLAG,BTEST
  INTEGER DOF
  DATA EQUAL
  & /
=====
C
  NLEN=NMODE*LEN(NAME)+1,60
  NC=1
C
=====
C= LOOP FOR EACH LOAD CASE ==
=====
C
DO 300 L=1,NLOAD
  NOSPLS=0
C
  IF (.NOT.(NCOS.EQ.1 .AND. COSINE(1,1,1).EQ.1 .AND.
    & COSINE(2,1).EQ.1 .AND. COSINE(5,1,1).EQ.1 )
    & .AND. IOPT.EQ.2) GO TO 210
C
=====
C= PRINT GLOBAL DISPLACEMENTS ==
=====
C NOTE: DISP MAY CONTAIN DISPLACEMENTS, VELOCITIES, ACCELERATIONS OR
  EIGENVALUES...
C ALL OF WHICH ARE PRINTED OUT AT EACH NODE...
C
  IF (HEAD) WRITE (6,510) TITLE(1),TITLE(2)
  IF (IOPT.NE.2) WRITE (6,516) NAME,L,STEPID,EQUAL(1:NLEN)
  IF (IOPT.EQ.2) WRITE (6,416) NAME, EQUAL(1:NLEN)
  DO 100 I=1,NMODE
C
    ..... TRANSFER DISPL TO LOCAL VECTOR .....
    DO 210 J=1,6
      L=IDOF(I,J)
      DC(J)=DISP(I,L)
C
    ..... ADD ROTATIONS TO DISP FOR CONSTRAINTS
    ..... IF UNCONSTRAINED, CONST(I,J)=0
    DC(1) = DC(1) + DC(5)*CONST(I,5) + DC(6)*CONST(I,6)
    DC(2) = DC(2) + DC(4)*CONST(I,1) + DC(6)*CONST(I,6)
    DC(3) = DC(3) + DC(4)*CONST(I,2) + DC(5)*CONST(I,4)
C
    ..... TRANSFER TO GLOBAL DISPLACEMENTS .....
    JCOS=JTCOS(I)
    DO 25 I1=1,5
      I2=I1+5
      G(I1)=0
      G(I2)=0
      DO 25 J1=1,5
        J2=J1+5
        G(I1+J1)=G(I1+J1)+COSINE(J1,I1,JCOS)*DC(J1)
        G(I2+J2)=G(I2+J2)+COSINE(J1,I1,JCOS)*DC(J2)
      25 G(I1+J1)=G(I1+J1)+COSINE(J1,I1,JCOS)*DC(J1)
        G(I2+J2)=G(I2+J2)+COSINE(J1,I1,JCOS)*DC(J2)
C
    ..... WRITE DISPL
    DO 50 J=1,6
      WRITE (CDC(J),9) G(J)
      9 FORMAT (1P,G14.6,' ')
      WRITE (6,220) IDX(I),(CDC(K),K=1,6)
      NOSPLS=NOSPLS+1
100 CONTINUE
C
  IF (NCOS.EQ.1 .AND. COSINE(1,1,1).EQ.1 .AND. COSINE(2,1).EQ.1
    & .AND. COSINE(5,1,1).EQ.1) GO TO 500
C

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IQ000170
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IQ010400
C= PRINT JOINT DISPLACEMENTS ==
C NOTE: DISP MAY CONTAIN DISPLACEMENTS, VELOCITIES, ACCELERATIONS OR
  EIGENVALUES...
C ALL OF WHICH ARE PRINTED OUT AT EACH NODE...
210 IF (HEAD .AND. NOSPLS.GT.20) WRITE (6,510) TITLE(1),TITLE(2)
  IF (IOPT.NE.2) WRITE (6,516) NAME,L,STEPID,EQUAL(1:NLEN)
  IF (IOPT.EQ.2) WRITE (6,416) NAME, EQUAL(1:NLEN)
  DO 200 I=1,NMODE
C
  ..... TRANSFER GLOBAL DISPL TO LOCAL VECTOR .....
  DO 219 J=1,6
    L=IDOF(I,J)
    DC(J)=DISP(I,L)
C
  ..... ADD ROTATIONS TO DISP FOR CONSTRAINTS
  ..... IF UNCONSTRAINED, CONST(I,J)=0
  DC(1) = DC(1) + DC(5)*CONST(I,5) + DC(6)*CONST(I,6)
  DC(2) = DC(2) + DC(4)*CONST(I,1) + DC(6)*CONST(I,6)
  DC(3) = DC(3) + DC(4)*CONST(I,2) + DC(5)*CONST(I,4)
C
  ..... WRITE DISPL
  DO 230 J=1,6
    WRITE (CDC(J),9) DC(J)
    9 FORMAT (1P,G14.6,' ')
    L=IDOF(I,J)
    IF (L.GT.NF) CDC(K)=L-15
  250 WRITE (6,221) IDX(I),(CDC(K),K=1,6),JTCOS(I)
200 CONTINUE
  WRITE (6,520)
C
500 CONTINUE
RETURN
C
10 FORMAT (1P,G14.7)
220 FORMAT (5X,I5,6A)
221 FORMAT (5X,I5,6A,110)
510 FORMAT ('1 STRUCTURE.....',A,/,
  & ' SOLUTION.....',A)
515 FORMAT ('//',
  & ' 2X,'GCS',A,/, ' LOADING #',I5,5X,A,/,
  & ' 1X,'=====',A,/,
  & ' 6X,'NODE',7X,'DX',15X,'DY',15X,'DZ',15X,'RX',15X,'RY',15X,'RZ',/,
  & ' 2X,'JCS',A,/, ' LOADING #',I5,5X,A,/,
  & ' 1X,'=====',A,/,
  & ' 6X,'NODE',7X,'DX',15X,'DY',15X,'DZ',15X,'RX',15X,'RY',15X,'RZ',/,
  & ' 5X,'COSINE #',/,
  & ' 2X,'GCS',A,/,
  & ' 1X,'=====',A,/,
  & ' 25X,'NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY',/,
  & ' 6X,'NODE',7X,'DX',15X,'DY',15X,'DZ',15X,'RX',15X,'RY',15X,'RZ',/,
  & ' 5X,'COSINE #',/)
516 FORMAT ('//',
  & ' 2X,'JCS',A,/,
  & ' 1X,'=====',A,/,
  & ' 25X,'NOTE: MAXIMUM VALUES MAY NOT OCCUR SIMULTANEOUSLY',/,
  & ' 6X,'NODE',7X,'DX',15X,'DY',15X,'DZ',15X,'RX',15X,'RY',15X,'RZ',/,
  & ' 5X,'COSINE #',/)
520 FORMAT ('4X,'NOTE: * DENOTES A RESTRAINED DEGREE OF FREEDOM')
C
END
=====
SUBROUTINE JOIDSP(SUB,MANNO,NDOF,NMODE,NLOAD,NF,ID,IDOF,CONST,
  & FORCE,DISP,JTFLG,TITLE,HEAD)
  DIMENSION IDOF(MANNO,6),CONST(MANNO,6),FORCE(NDOF,NLOAD)
  DIMENSION DISP(NDOF,NLOAD)
  CHARACTER*(*) TITLE(2)
  CHARACTER*40 DIR
  CHARACTER*15 CK6
  CHARACTER*25 SUPT
  CHARACTER*14 F(6)
  LOGICAL DISP,FG,FIRST,BUG,HEAD
  LOGICAL BTEST
  LOAD=1
  FIRST=.TRUE.
  DISP,FG=.FALSE.
  5 FORMAT ('1 STRUCTURE.....',A,/,
    & ' SOLUTION.....',A,/)
  6 FORMAT ('* APPLIED JOINT LOADS',/,
    & ' *****',/)
C
C= INPUT LOADING DATA =
C=
10 READ (5,*) LOAD,JOINT,JTCEN,JTINC,DIR,VALUE
  IF (INDEX(DIR,'END').NE.0) GO TO 100
  15 DOF=' '
  IF (FIRST) THEN
    IF (HEAD) WRITE (6,5) TITLE(1),TITLE(2)
    WRITE (6,6)
    FIRST=.FALSE.
  ENDIF
C
C= CHECK FOR A VALID JOINT NUMBER...
  IF (JOINT.LT.IDX(1) .OR. JOINT.GT.IDX(NMODE)) THEN
    WRITE (6,21) LOAD
    GO TO 10
  ENDIF
C
  J=IQUICK(JOINT,IDX,NMODE)
  SUPT=' '
C
C= PUT A LOAD ON A JOINT
C NOTES: - IX, IY, IZ, MX, MY AND Z ARE THE DOF THAT THE LOADS ARE
  APPLIED TO.
  - THE MOMENTS RESULTING FROM FX, FY AND FZ ARE DUE TO
  CONSTRAINTS. IF A NODE IS NOT CONSTRAINED, THEN THE VALUE
  OF CONST IS ZERO...
  - LOADS APPLIED TO RESTRAINED DOF ARE INTERPRETED AS
  SUPPORT DISPLACEMENTS. I.E. SUPPORT SETTLEMENT OR
  DISPLACEMENT CONTROLL...
C
  IF (INDEX(DIR,'FX').NE.0) THEN
    I=IDOF(J,1)
    FORCE(I,LOAD)=FORCE(IX,LOAD)+VALUE
  ELSE IF (INDEX(DIR,'FY').NE.0) THEN
    I=IDOF(J,2)
    FORCE(I,LOAD)=FORCE(IY,LOAD)+VALUE*CONST(J,5)
  ELSE IF (INDEX(DIR,'FZ').NE.0) THEN
    I=IDOF(J,3)
    FORCE(I,LOAD)=FORCE(IZ,LOAD)+VALUE*CONST(J,5)
  ELSE IF (INDEX(DIR,'MX').NE.0) THEN
    I=IDOF(J,4)
    FORCE(I,LOAD)=FORCE(MX,LOAD)+VALUE*CONST(J,5)
  ELSE IF (INDEX(DIR,'MY').NE.0) THEN
    I=IDOF(J,5)
    FORCE(I,LOAD)=FORCE(MY,LOAD)+VALUE*CONST(J,5)
  ELSE IF (INDEX(DIR,'MZ').NE.0) THEN
    I=IDOF(J,6)
    FORCE(I,LOAD)=FORCE(MZ,LOAD)+VALUE*CONST(J,5)
  ENDIF

```

```
FORCE(MZ,LOAD)=FORCE(MZ,LOAD)+VALUE*CONST(J,5)
WRITE (DOF,55) IX,MY,MZ
ELSE
WRITE (DOF,55) IX
ENDIF
IF (.K.GT.NF) THEN
DSPFLG=.TRUE.
SUPT=...JOINT DISPLACEMENT...
ENDIF
ELSE IF (INDEX(DIR,'FV').NE.0) THEN
IY=IDOF(J,2)
FORCE(IY,LOAD)=FORCE(IY,LOAD)+VALUE
IF (.BTEST(JTFLG,J,13)) THEN
MX=IDOF(J,4)
FORCE(MX,LOAD)=FORCE(MX,LOAD)+VALUE*CONST(J,1)
MZ=IDOF(J,6)
FORCE(MZ,LOAD)=FORCE(MZ,LOAD)+VALUE*CONST(J,6)
WRITE (DOF,55) IY,MX,MZ
ELSE
WRITE (DOF,55) IY
ENDIF
IF (.IY.GT.NF) THEN
DSPFLG=.TRUE.
SUPT=...JOINT DISPLACEMENT...
ENDIF
ELSE IF (INDEX(DIR,'FZ').NE.0) THEN
JZ=IDOF(J,3)
FORCE(JZ,LOAD)=FORCE(JZ,LOAD)+VALUE
IF (.BTEST(JTFLG,J,14)) THEN
MX=IDOF(J,4)
FORCE(MX,LOAD)=FORCE(MX,LOAD)+VALUE*CONST(J,2)
MY=IDOF(J,5)
FORCE(MY,LOAD)=FORCE(MY,LOAD)+VALUE*CONST(J,4)
WRITE (DOF,55) JZ,MX,MY
ELSE
WRITE (DOF,55) JZ
ENDIF
IF (.JZ.GT.NF) THEN
DSPFLG=.TRUE.
SUPT=...JOINT DISPLACEMENT...
ENDIF
ELSE IF (INDEX(DIR,'MV').NE.0) THEN
MV=IDOF(J,5)
FORCE(MV,LOAD)=FORCE(MV,LOAD)+VALUE
WRITE (DOF,55) MV
IF (.MV.GT.NF) THEN
DSPFLG=.TRUE.
SUPT=...JOINT DISPLACEMENT...
ENDIF
ELSE IF (INDEX(DIR,'MZ').NE.0) THEN
MZ=IDOF(J,6)
FORCE(MZ,LOAD)=FORCE(MZ,LOAD)+VALUE
WRITE (DOF,55) MZ
IF (.MZ.GT.NF) THEN
DSPFLG=.TRUE.
SUPT=...JOINT DISPLACEMENT...
ENDIF
ELSE
WRITE (6,20) JOINT,DIR,VALUE
ENDIF
WRITE (6,50) LOAD,JOINT,DIR,DOF,VALUE,SUPT
IF (JGEN.GT.0) THEN
JGEN=JGEN-1
JOINT=JOINT+JING
GO TO 15
ENDIF
GO TO 10
C
20 FORMAT (' INVALID JOINT LOAD...',I6,2X,A,2X,IP,G14.6,
& ' --- LOAD IS SKIPPED')
21 FORMAT (' INVALID LOAD CASE ...',I6,
& ' --- LOAD IS SKIPPED')
30 FORMAT (' LOAD CASE:',IS,') JOINT:',I6,') DIRECTION:',A,
& ' DOF(S):',A,') MAGNITUDE:',IP,G14.6,2X,A)
55 FORMAT (IS,')',IS,')',IS)
C
----- RETURN IF NO JOINT LOADS WERE INPUT
100 IF (FIRST) RETURN
C
IF (.NOT.BUG) RETURN
PRINT JOINT LOADS ON EACH DOF
MS=NDOP+5
DO 120 I=1,NLOAD
IF (.HEAD) WRITE (6,5) ) TITLE(1),TITLE(2)
WRITE (6,130) I
DO 120 I=1,MS,5
IS=MINK(I+4),NDOP)
DO 110 J=1,IS
K=J-1
CK(K)=
CCK(K)=
IF (.I.GT.NF) CCK(K)=**
WRITE (6,140) (J,FORCE(J,I),CCK(J-I+1),J,I,IS)
120 CONTINUE
C
130 FORMAT (' APPLIED JOINT LOADS, LOADING #',IS,10X,
& ' NOTE: * DENOTES SUPPORT DISPLACEMENT'//
& ' =====//
& SX,5X) DOF:',I7X,'LOAD:',I7)
140 FORMAT (SX,5X)OP,IS,IP,G14.6,A)
C
DO 220 I=1,NLOAD
IF (.HEAD) WRITE (6,5) ) TITLE(1),TITLE(2)
WRITE (6,200) I
DO 220 I=1,NMODE
DO 210 J=1,6
CCK(J)=
IF (.BTEST(JTFLG,I,J+1)) THEN
FC(J)=*
ELSE
K=IDOF(I,J)
WRITE (FC,J,240) FORCE(K,I)
IF (.K.GT.NF) CCK(J)=**
ENDIF
ENDIF
CONTINUE
WRITE (6,250) ID(I),(FC(J),CCK(J),J=1,6)
```

```
220 CONTINUE
250 FORMAT (' APPLIED JOINT LOADS, LOADING #',IS,10X,
& ' NOTE: * DENOTES SUPPORT DISPLACEMENT'//
& ' =====//
& SX,5X) DOF:',I7X,'FY',I5X,'FV',I5X,'FZ',I5X,'MX',I5X,'MY',I5X,'MZ')//
260 FORMAT (SX,IS,12X)
240 FORMAT (IP,G14.6)
RETURN
END
C
----- CALCULATES STIFFNESS BASED ON DX AND DY -----
KMIN =
C DD = CHANGE IN DISPLACEMENT
C DP = CHANGE IN LOAD
C SI = MAXIMUM AND DEFAULT STIFFNESS
REAL FUNCTION KMIN(DP,DI,SI)
LOGICAL BTEST
IF ((DP*DP).GT. 0.00) THEN
KMIN=MINK(DP/DI,SI)
ELSE
KMIN=SI
ENDIF
RETURN
END
SUBROUTINE LINACCOPT,BUG,DT,TO,TF,T,THETA,NEWKDV,
& L1,L2,L3,L4,L5,L6,INDMAS,IND,INDS,INDKG,NDOP,NFREE,
& KGL,OAD,KFORN,
& A, V, D, P,
& DA, DV, DD, DP, HORK,
& MASS, MDMASS, DAMP, STIFF, MD,
& KG, MORG, ACC, GRAV,
& S, MORG, R, PBAR,
& FDAMP,FMASS,C0,C1,C2,C3,C4,C5,C6,ALPHA,BETA,C10,C11,ABORT)
INTEGER FDAMP,FMASS
REAL MASS,KG
LOGICAL BUG,NEWKDV,BTEST,ABORT
DIMENSION AK(NDOP),VK(NDOP),DK(NDOP),DV(NDOP),DDX(NDOP)
DIMENSION AK(NDOP),VK(NDOP),DK(NDOP),DV(NDOP),DDX(NDOP)
DIMENSION PBAR(1,4),OCL(1,4),RCL(1,4)
DIMENSION MMASK(NDOP+1),MASS(INDMAS)
DIMENSION MDKG(NDOP+1),KG(INDKG)
DIMENSION MDK(NDOP+1),STIFF(IND)
DIMENSION MDK(NDOP+1),SK(INDS),DAMP(S)
C
GO TO (100,200,300) IOPT
C
=====
C= INITIALIZE VALUES =====
100 CONTINUE
ALPHA=DAMP(1)
BETA=DAMP(2)
C0=S,ALPHA/DT + 6./DT**2)
C1=1.0/(1+5.*BETA/DT)
C2=C0*CI
C3=ALPHA-C2*BETA
C4=.DT
C5=DT/2.
C6=0.
C10=S,DT
C11=./(DT**2)
IF (BUG) WRITE (6,101) ALPHA,BETA,C0,C1,C2,C3,C4,C5,C6,C10,C11
101 FORMAT (IP,
& ' LINACCOPT ALPHA:',G12.5,' BETA:',G12.5,' C0:',G12.5,' C1:',G12.5,ALPHA,NDOP,50
& ' LINACCOPT C2:',G12.5,' C3:',G12.5,' C4:',G12.5,' C5:',G12.5,ALPHA,NDOP,40
& ' LINACCOPT C6:',G12.5,' C10:',G12.5,' C11:',G12.5)
C
----- DEVELOP SKYLINE OF DYNAMIC STIFFNESS (S)
C..... MDC(I) = ADDRESS OF DYNAMIC STIFF. MAIN DIAGONAL TERM ROW I
C..... MDI(I) = ADDRESS OF STIFFNESS MAIN DIAGONAL TERM ROW I
C..... MMASK(I) = ADDRESS OF MASS MAIN DIAGONAL TERM ROW I
C..... MDK(I) = ADDRESS OF GEOMETRIC STIFF. MAIN DIAGONAL TERM ROW I
C..... LSTIFF = # OF STIFFNESS TERMS IN COLUMN J
C..... LMASS = # OF MASS TERMS IN COLUMN J
C..... LKG = # OF KG TERMS IN COLUMN J
C..... L = # OF S TERMS IN COLUMN J
C
----- CHECK FOR PROPORTIONAL DAMPING -----
IF (FDAMP.NE.1) THEN
WRITE (6,*) *****
WRITE (6,*) ** PROPORTIONAL DAMPING HAS NOT SPECIFIED **
WRITE (6,*) ** SOLUTION IS ABORTED... **
WRITE (6,*) *****
STOP
ENDIF
RETURN
C
=====
C= SOLVE FOR INCREMENTAL DISPLACEMENTS, VELOCITIES AND ACCELERATIONS =====
200 CONTINUE
IF (BUG) THEN
CALL ERTRA
DO 205 I=1,S,L4
205 WRITE (6,206) I,DX(I),W(I),K(I),PK(I),DP(I)
206 FORMAT (' DOF:',I6,') DISP:',IP,G12.4,') VEL:',G12.4,
& ' ACC:',G12.4,') LOAD:', G12.4,') DP:',G12.4)
ENDIF
C
----- FORM DYNAMIC STIFFNESS
C..... SOME LOCAL VARIABLES
C J = COLUMN NUMBER FOR MASS AND STIFF
C I = ROW NUMBER FOR MASS AND STIFF
C J1 = COLUMN NUMBER FOR S
C I1 = ROW NUMBER FOR S
C IJSTIFF = ADDRESS OF ELEMENT I, J IN MATRIX STIFF
C IJMASS = ADDRESS OF ELEMENT I, J IN MATRIX MASS
C IJKG = ADDRESS OF ELEMENT I, J IN GEOMETRIC STIFFNESS MATRIX
C IJS = ADDRESS OF ELEMENT I, J1 IN MATRIX S
C IJSTIFF = ROW # CONTAINING THE FIRST NONZERO TERM IN COLUMN J OF STIFF
C IJMASS = ROW # CONTAINING THE FIRST NONZERO TERM IN COLUMN J OF MASS
C IJKG = ROW # CONTAINING THE FIRST NONZERO TERM IN COLUMN J OF KG
C IJS = ROW # CONTAINING THE FIRST NONZERO TERM IN COLUMN J OF S
C
----- FORM DYNAMIC STIFFNESS IF NEWKDV IS TRUE -----
IF (NEWKDV) THEN
C
DETERMINE THE FACTOR FOR KG
IF (KGL,OAD.EQ.1) THEN
```

```

      CKG=1.000
      ELSE IF (KLOAD.EQ.2) THEN
        CKG=1.000
      ENDIF
    C
    C----- K(BAR) = STIFFNESS
    DO 225 I=L3,L4
      I1=I-1
      MDJ=MDK(J+1)
      MDJ=MDK(J)
      LSTIFF=J-(MDK(J+1)-MDK(J)-1)
      MDJ1=MDK(J+1)
      MDJ1=MDK(J)
      LS=J1-(MDK(J+1)-MDK(J)-1)+L2
      L=MAX(L1,LSTIFF)
      DO 210 I=L3,L4-1
        I1=I-1
        IJS=(MDK(J1)+J1)-I1
        LSTIFF=(MDK(J1)+J1)-I
        S(IJS)=STIFF(LSTIFF)
      C
      C----- IF (LS.L1.LSTIFF) THEN
      DO 215 I=L3,L4-1
        IJS=(MDK(J1)+J1)-I1
        S(IJS)=0
      ENDIF
    C
    C----- K(BAR) = K(BAR) + C2*MASS
    LMASS=J-(MDMASS(J+1)-MDMASS(J)-1)
    L=MAX(L1,LMASS)
    DO 220 I=L3,L4-1
      I1=I-1
      IJS=(MDK(J1)+J1)-I1
      LMASS=(MDMASS(J1)+J1)-I
      S(IJS)=MASS(I,MASS)*C2 + S(IJS)
    C
    C----- IF (KFORM.EQ.2) THEN
    C
    C----- NOTE: THE GEOMETRIC STIFFNESS WAS DERIVED WITH COMPRESSION
    C----- BEING POSITIVE, KG HAS POSITIVE TERMS ON THE MAIN DIAGONAL
    C----- REPRESENTING COMPRESSION, THUS KG IS SUBTRACTED FROM S
    C----- CKG IS AN INCREASE FOR VERY ACCEL
    C
    C----- K(BAR) = K(BAR) - CKG*GEOMETRIC STIFFNESS
    LKG=J-(MDKG(J+1)-MDKG(J)-1)
    L=MAX(L1,LKG)
    DO 222 I=L3,L4-1
      I1=I-1
      IJS=(MDK(J1)+J1)-I1
      LKG=(MDKG(J1)+J1)-I
      S(IJS)=S(IJS) - KG(I,KG)*CKG
    C
    C----- CONTINUE
    ENDIF
    C
    C----- CALCULATE Q AND R VECTORS
    DO 230 I=L3,L4
      Q(I)=C4*(I) + S*(K(I))
      R(I)= S*(K(I)) + C5*(K(I))
    C
    C----- FORM DYNAMIC LOAD
    C
    C----- INITIALIZE PBAR = OP*THETA
    C----- THETA=1 FOR LINEAR ACCELERATION
    C----- THETA=2 WHEN LINACC IS CALLED BY AVERAGE ACCELERATION
    DO 240 I=L3,L4
      PBAR(I)= Q(I)*THETA
    C
    C----- IF (FDAMP.EQ.1) THEN
    C
    C----- PBAR=PBAR +MASS*( Q(I) + C5*(R(I)) )
    DO 250 J=L3,L4
      MDJ=MDMASS(J)+J
      MDJ=MDMASS(J)+1
      MDJ=MAX(M,L3)
      DO 250 I=M,J
        PBAR(I)=PBAR(I) + MASS(MDJ-I)*( Q(J)+C5*(R(J)) )
      C
      C----- CONTINUE
      DO 255 I=L3,L4
        MDI=MDMASS(I)+I
        MDI=MDMASS(I)+1
        MDI=MAX(M,L3)
        DO 255 J=M,I-1
          PBAR(I)=PBAR(I) + MASS(MDI-J)*( Q(J)+C5*(R(J)) )
        C
        C----- ENDIF
      ENDIF
    C
    C----- IF (BUG) THEN
    DO 241 I=L3,L4
      WRITE (6,242) I,Q(I),R(I),PBAR(I)
    242 FORMAT (' DOF:',I6,' Q:',I6,' R:',I6,' G12.4,'
      & ' PBAR:',I6,' G12.4')
    ENDIF
    C
    C----- SOLVE FOR INCREMENTAL DISPLACEMENT OVER TIME INTERVAL DT
    C----- NOTE: - WORK IS USED FOR TEMPORARY WORK SPACE
    C----- - IF MEMOVS.FALSE, THE DYNAMIC STIFFNESS HAS ALREADY
    C----- BEEN REDUCED TO UPPER TRIANGULAR FORM
    C
    C----- IF (MEMOVS) THEN
    CALL MSOLL(1,BUG,NFREE,INDS,NFREE,1,1,NFREE,MD,S,PBAR,WORK,
      & .FALSE.,DUMMY,1,1,
      & .FALSE.,DUMMY,1,1,ABORT)
    ELSE
    CALL MSOLL(2,BUG,NFREE,INDS,NFREE,1,1,NFREE,MD,S,PBAR,WORK,
      & .FALSE.,DUMMY,1,1,
      & .FALSE.,DUMMY,1,1,ABORT)
    ENDIF
    IF (ABORT) RETURN
    C
    C----- NOTE: - PBAR CONTAINS THE INCREMENTAL DISPLACEMENT BETWEEN
    C----- TIMES T AND T+DT AFTER THE SECOND CALL TO MSOLL
    CALL MSOLL(3,BUG,NFREE,INDS,NFREE,1,1,NFREE,MD,S,PBAR,WORK,
      & .FALSE.,DUMMY,1,1,
      & .FALSE.,DUMMY,1,1,ABORT)
    IF (ABORT) RETURN
    C
    C----- DETERMINE ACCELERATION, VELOCITY AND DISPLACEMENT AT TIME DT
    CA = INCREMENTAL ACCELERATION BETWEEN TIMES T AND T+DT
    CV = INCREMENTAL VELOCITY BETWEEN TIMES T AND T+DT
    CD = INCREMENTAL DISPLACEMENT BETWEEN TIMES T AND T+DT
  
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    LIND1100 IF (BUG) THEN
    LIND1110 WRITE (6,*) 'INCREMENTAL RESULTS FROM LINACC....'
    LIND1120 WRITE (6,320)
    LIND1130 ENDIF
    LIND1140 DO 270 I=L3,L4
    LIND1150 DOKI=C1*( PBAR(I) + BETA*(R(I)) )
    LIND1160 DV(I)=C10*(DOKI) - R(I)
    LIND1170 DAKI=C11*(DOKI) - Q(I)
    LIND1180 IF (BUG) WRITE (6,330) I,DOKI,DV(I),DAKI
    LIND1190 270 CONTINUE
    C
    LIND1200 RETURN
    C
    C----- CALC TOTAL DISPLACEMENTS, VELOCITIES AND ACCELERATIONS ---
    LIND2500 C=
    LIND2510 500 CONTINUE
    LIND2520 520 FORMAT (' DOF:',I6,' DD:',I6,' DV:',I6,' DA:',I6,' P:',I6,'
    LIND2530 & ' IZ:',I6,' O:',I6,' V:',I6,' A:',I6,' P:')
    LIND2540 530 FORMAT (I6,I6,I6,I6,I6,I6)
    C
    LIND2550 RETURN
    LIND2560 END
    LIND2570
    C----- SUBROUTINE MATRIX A, MD, IC, ZND, NAME
    LINDA0010 DIMENSION MD(KI=1), A(MD)
    LINDA0020 LOGICAL BTEST
    LINDA0030 CHARACTER*(*) NAME
    LINDA0040 CHARACTER*20 NUMB,ROMK(6)
    LINDA0050 LOGICAL PT,DMP
    LINDA0060 I(I,J)=MDK(J)+J-I
    C
    LINDA0070 CALL GETINT(NAME,'DUMP',IDUMP,0.,TRUE.,FALSE.)
    LINDA0080 IF (IDUMP.NE.0) THEN
    LINDA0090 DMP=.TRUE.
    ELSE
    LINDA0100 DMP=.FALSE.
    ENDIF
    DO 1 I=L1,6
    LINDA0110 ROMK(I)=?
    I=IC
    LINDA0120 WRITE (6,*) ' '
    LINDA0130 WRITE (6,*) 'PRINTING MATRIX: ',NAME
    DO 50 ICG=1,IC,6
    LINDA0140 IF (ICG.GT.1) WRITE (6,*) ' '
    LINDA0150 K=MINK(ICG+5),IC
    LINDA0160 WRITE (6.10) (J,J=ICG,K)
    DO 20 I=L1,IR
    LINDA0170 I=0
    LINDA0180 PT=.FALSE.
    DO 15 J=ICG,K
    LINDA0190 I=I(I,J)
    LINDA0200 IF (DMP.AND. A(I,J).NE.0)
    LINDA0210 WRITE (IDUMP,*) I,J,A(I,J),NAME
    ENDIF
    LINDA0220 L=L+1
    LINDA0230 15 ROMK(L)=NUMB
    LINDA0240 20 IF (PT) WRITE (6,50) I,(ROMK(L),L=L1,6)
    LINDA0250 50 CONTINUE
    LINDA0260 RETURN
    LINDA0270 10 FORMAT('10.66','...', COLUMN',IS, '...',')
    LINDA0280 16 FORMAT('F20.6')
    LINDA0290 50 FORMAT(' ROM ',IS,6A)
    LINDA0300 END
    C----- SUBROUTINE MASSIN,IMASS,FMASS,MCND,BUG,IBUG,TITLE,MAXZ,MAXDZ,
    LINDM0010 & MAXMD,MCOS,MODE,IZ,IZD,Z,NZ,IZD,
    LINDM0020 & IZDMS,IZMSS,IZLW,IZKE,IZDMS,
    LINDM0030 & MD,FMASS,IZCOS,IZD,IZDMS,IZ,IZLW,IZCOS,NAME,
    LINDM0040 & MCND,NFREE,IZND)
    C
    LINDM0050 LOGICAL BUG,MCND
    LINDM0060 INTEGER FMASS
    LINDM0070 CHARACTER*(*) NAME,TITLE(2)
    LINDM0080 DIMENSION Z(MAXZ),NZ(MAXZ),DZ(MAXDZ),MD(7)
    LINDM0090 LOGICAL BTEST
    LINDM0100 DOUBLE PRECISION DZ
    LINDM0110 DATA MD/1,2,9,7,11,16,22/
    C
    LINDM0120 IF (FMASS.EQ.1) THEN
    C----- INITIALIZE THE DIAGONAL MASS MATRIX
    LINDM0130 MCND=.TRUE.
    LINDM0140 IZDMS=IZ
    LINDM0150 IZ=IZ + MD*F+1
    LINDM0160 CALL SKVLINK(MD,IBUG,TITLE,NZ(IZDMS),
    LINDM0170 & NZ(IZLW),NZ(IZKE),MD,NAME)
    C
    C----- INPUT THE MASS DATA
    LINDM0180 IZMDAT=IZ
    LINDM0190 IZ=IZ + DIMASS*12
    LINDM0200 IZD=NZ(IZDMS+MD*F)
    LINDM0210 IZMSS=IZ
    LINDM0220 CALL MFORMK(1,IMASS,FMASS,Z(IZMSS),NZ(IZDMS),MD,MD,IZ,MD,TITLE,
    LINDM0230 & MODE,MAXMD,MCOS,BUG,IBUG,
    LINDM0240 & NZ(IZD),Z(IZCOS),NZ(IZD),Z(IZDMS),NZ(IZLW),
    LINDM0250 & NZ(IZCOS),Z(IZMDAT),Z(IZ),NZ(IZ+21),Z(IZ+27),
    LINDM0260 & Z(IZ+65),Z(IZ+99))
    C
    C----- RELEASE UNUSED MASS DATA STORAGE
    LINDM0270 IZ=IZ - (IMASS-FMASS)*12
    C
    C----- MODIFY MASS MATRIX FOR CONDENSATION ---
    LINDM0280 C=
    LINDM0290 C=
    LINDM0300 C=
    C----- THE CONDENSATION PROCESS MAY EXPAND THE MASS MATRIX'S
    C----- SKYLINE. THE MAXIMUM SKYLINE OF BOTH THE MASS AND
    C----- THE STIFFNESS MATRIX IS USED.
    LINDM0310 IF (MCND.AND. MCND.GT.0)THEN
    DO 310 I=0,MD*F
    LINDM0320 I=I+NZ(IZD)-I-1-NZ(IZD)+I
    LINDM0330 NSTIFF=I-1-NH+1
    LINDM0340 NZ(IZDMS+I)=MINK(NZ(IZDMS+I),NSTIFF)
    LINDM0350 ENDIF
    C
    C----- DETERMINE THE MASS MATRIX SKYLINE
    CALL SKVLINK(5,MD,IBUG,TITLE,NZ(IZDMS),
    LINDM0360
  
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C SHAT(7)= DVT, AXLMOO PARAMETER MAT00580 V=VL MAT01620
C SHAT(8)= CVC, AXLMOO PARAMETER MAT00590 C----- IS P GREATER THAN LIMITS ? MAT01650
C SHAT(9)= CSE, CONSTANT STRAIN ENERGY MAT00600 ELSE IF ((PL.LE.A .AND. A.LE.P) .OR. (PL.GE.A .AND. A.GE.P)) .AND. MAT01640
C SHAT(10)=BDAM, ULTIMATE DISPLACEMENT MAT00610 & (STIFF.NE.0.000) THEN MAT01650
C SHAT(11)=BDAM, BETA FOR DAMAGE INDEX MAT00620 DL=DL*(A-PL)/STIFF MAT01670
C----- INPUT DATA FOR AXLMOO HYSTERESIS MODEL ----- MAT00640 P1=A MAT01680
C THE FOLLOWING DATA IS INPUT ONCE FOR EACH MODEL ----- MAT00650 CALL STRENG (SEC(27),SEC(50),SEC(51),P1,PL,DL,SEC(1),SEC(14)) MAT01680
C SC = COMPRESSION STIFFNESS MAT00660 DL=DL MAT01700
C ST1 = INITIAL TENSILE STIFFNESS MAT00670 PL=PL MAT01700
C ST2 = POST YIELD TENSILE STIFFNESS MAT00680 IF (ABS(P-PL).GT. 0.005*ABS(P+PL)) THEN MAT01710
C PV = YIELD LOAD MAT00690 PI=PL*(P-PL)*.01 MAT01720
C ALPHA = MODEL COEFFICIENTS MAT00700 DI=DL*(D-DL)*.01 MAT01730
C BETA = MODEL COEFFICIENTS MAT00750 ELSE MAT01740
C----- MAT00750 PI=P MAT01750
C----- MAT00750 DI=D MAT01770
C----- MAT00750 ENDIF MAT01780
C IF (BUG) THEN MAT01790
C WRITE (6,*) 'C----- IS P GREATER THAN LIMITS ? ' MAT01790
C WRITE (6,*) 'PL,DL=',PL,DL MAT01800
C WRITE (6,*) 'PI,DI=',PI,DI MAT01810
C----- MAT00750 ENDIF MAT01820
C CALL HYSTOZ(PI,DI,PL,DL,1,1,SEC(1),SEC(2), MAT01830
C & SHAT(1),SHAT(2),SHAT(3),SHAT(4),SHAT(5),SHAT(6), MAT01840
C & SHAT(7),SHAT(8),SHAT(9),SEC(3),SEC(4),SEC(5),SEC(6),SEC(7),SEC(8),MAT01850
C & SEC(9),SEC(10),SEC(11),SEC(12),SEC(13),BUG, MAT01860
C & SEC(14),SEC(27),SEC(50),SEC(51),SEC(15),SEC(18),SEC(21),IDR ) MAT01880
C----- IS P LESS THAN LIMITS ? MAT01890
C----- MAT01890 GO TO 510 MAT01890
C ELSE IF ((P.LT.PL .AND. PL.LE.A) .OR. (P.GT.PL .AND. PL.GE.A)) THEN MAT01910
C IF (ABS(P-PL).GT. 0.005*ABS(P+PL)) THEN MAT01920
C PI=PL*(P-PL)*.01 MAT01930
C DI=DL*(D-DL)*.01 MAT01940
C----- MAT01940 ELSE MAT01950
C----- MAT01950 PI=P MAT01960
C----- MAT01950 DI=D MAT01970
C----- MAT01950 ENDIF MAT01980
C IF (BUG) THEN MAT02000
C WRITE (6,*) 'C----- IS P LESS THAN LIMITS ? ' MAT02000
C WRITE (6,*) 'PI,DI=',PI,DI MAT02010
C----- MAT02000 ENDIF MAT02020
C CALL HYSTOZ(PI,DI,PL,DL,1,1,SEC(1),SEC(2), MAT02030
C & SHAT(1),SHAT(2),SHAT(3),SHAT(4),SHAT(5),SHAT(6), MAT02040
C & SHAT(7),SHAT(8),SHAT(9),SEC(3),SEC(4),SEC(5),SEC(6),SEC(7),SEC(8),MAT02050
C & SEC(9),SEC(10),SEC(11),SEC(12),SEC(13),BUG, MAT02060
C & SEC(14),SEC(27),SEC(50),SEC(51),SEC(15),SEC(18),SEC(21),IDR ) MAT02070
C----- MAT02070 V=VL MAT02080
C----- MAT02070 GO TO 510 MAT02090
C----- MAT02070 ENDIF MAT02100
C----- MAT02070 C----- SAVE MAXIMUM PEAK POSITIVE DISPL. MAT02120
C----- MAT02070 IF (D.GT.SEC(52)) THEN MAT02150
C----- MAT02070 SEC(52)=D MAT02140
C----- MAT02070 SEC(53)=P MAT02150
C----- MAT02070 ENDIF MAT02160
C----- MAT02070 C IF (BUG) WRITE (6,*) 'STIFF=',STIFF,' A=',SEC(15) MAT02180
C----- MAT02070 MAT02190
C----- MAT02070 C----- TRANSFER ENERGIES FOR BOTH IOPT=5 AND 4. MAT02200
C----- MAT02070 +00 EESE=SEC(27) MAT02210
C----- MAT02070 EPSE=SEC(50) MAT02220
C----- MAT02070 C----- TRANSFER DUCTILITIES AND EXCURSION RATIOS FOR BOTH IOPT=5 AND 4. MAT02240
C----- MAT02070 DO *IO I=1,5 MAT02250
C----- MAT02070 DUCT(I)=MAX(SEC(14+I),SEC(17+I)) MAT02260
C----- MAT02070 EXCR(I)=SEC(20+I) MAT02270
C----- MAT02070 +10 EXCR(I+5)=SEC(20+I+5) MAT02280
C----- MAT02070 MAT02290
C----- MAT02070 RETURN MAT02300
C----- MAT02070 MAT02310
C----- MAT02070 C----- DAMAGE INDEX ----- MAT02320
C----- MAT02070 500 CONTINUE MAT02350
C----- MAT02070 EESE=SEC(27) MAT02350
C----- MAT02070 EPSE=SEC(50) MAT02350
C----- MAT02070 BDAM=SHAT(11) MAT02360
C----- MAT02070 P=SEC(53) MAT02370
C----- MAT02070 P=SEC(53) MAT02380
C----- MAT02070 DAMAGE=ABS(D)/SHAT(10) + BDAM / ( SHAT(4)*SHAT(10) ) * EPSE MAT02390
C----- MAT02070 MAT02400
C----- MAT02070 9999 CONTINUE MAT02410
C----- MAT02070 C RETURN MAT02420
C----- MAT02070 END MAT02440
C----- MAT02070 C----- SUBROUTINE MATOS ----- MAT00010
C----- MAT02070 & IOPT,I,ELNO,ERR,FIRST,PRINT,BUG, MAT00050
C----- MAT02070 & MAT(2)=NE,P,PL,D,VL,V,LELE,LNAT, MAT00060
C----- MAT02070 & SHAT,ESE,EPSE,DUCT,EXCR,DAMAGE) MAT00070
C----- MAT02070 C----- IMPLICIT REAL(A-H,O-Z) MAT00090
C----- MAT02070 LOGICAL ERR,FIRST,PRINT,BUG MAT00100
C----- MAT02070 LOGICAL BTEST MAT00110
C----- MAT02070 DIMENSION SEC(100),SHAT(50),DUCT(5),EXCR(6) MAT00120
C----- MAT02070 CHARACTER*80 TYPE MAT00140
C----- MAT02070 C IF (IOPT.NE.1) LELE=5+3*SHAT(2)+2 MAT00160
C----- MAT02070 IF (IOPT.EQ.0) RETURN MAT00170
C----- MAT02070 C----- MAT00180
C----- MAT02070 C----- MAT00190
C----- MAT02070 C----- MAT00200
C----- MAT02070 C----- MAT00210
C----- MAT02070 C----- GLOBAL VARIABLES ----- MAT00220
C----- MAT02070 C IOPT = 1, INITIALIZE MATERIAL MAT00230
C----- MAT02070 C = 2, GET STIFFNESS MAT00240
C----- MAT02070 C SHAT = INTERNAL STORAGE MAT00250
C----- MAT02070 C SE = OUTPUT STIFFNESS MAT00260
C----- MAT02070 ----- BENDI DATA ----- MAT00270
C----- MAT02070 C----- MAT00280
C----- MAT02070 SHAT(1)=NSEGS, NUMBER OF BACKBONE SEGMENTS MAT00290
C----- MAT02070 SHAT(2)=NE, NUMBER OF SMALL AMPLITUDE LOOPS MAT00300
C----- MAT02070 SHAT(3)=CSE, CONSTANT STRAIN ENERGY MAT00310
C----- MAT02070 SHAT(4)=DVT, YIELD POINT FOR DUCTILITIES MAT00320
C----- MAT02070 SHAT(5) = BDAM BETA FOR DAMAGE INDEX MAT00330
C----- MAT02070 SHAT(5+I) = PP, BACKBONE MOMENT FOR POINT I MAT00340
C----- MAT02070 SHAT(5+I+NSEGS)= DP, BACKBONE ROTATION FOR POINT I MAT00350
C----- MAT02070 C----- MAT00360
C----- MAT02070 GO TO (100,200,300,400,500),IOPT MAT00370
C----- MAT02070 MAT00380
C----- MAT02070 100 CONTINUE ----- INPUT DATA FOR BENDI HYSTERESIS MODEL ----- MAT00400
C----- MAT02070 C NSEG = NUMBER OF BACKBONE SEGMENTS MAT00420
C----- MAT02070 C NI = NUMBER OF SMALL LOOP POINTS MAT00430

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C ET = ELASTIC STIFFNESS
C G = MOMENT GRADIENT
C PP = BACKBONE LOAD
C DP = BACKBONE DISPLACEMENT
C-----
C READ (5,*) TYPE ,NSEG,NI,DV,BOAM
READ(5,*) ( SMAT(S)=I ,I=1,NSEG)
READ(5,*) ( SMAT(S+I+NSEG),I=1,NSEG)
C
LELEN = 5+5*NI +2
LMAT = 5+2*NSEG
SMAT(1)=NSEG
SMAT(2)=NI
SMAT(3)=DV
SMAT(5)=BOAM
C----- CALC CONSTANT STRAIN ENERGV....
DL=0
PL=0
DO 10 I=1,NSEG
P=SMAT(S+I)
D=SMAT(S+I+NSEG)
IF (D.LE.DV) THEN
CSE=CSE + 0.5*(P+PL)*(D-DL)
PL=D
ELSE IF (D.EQ.DL) THEN
GO TO 20
ELSE
PV=PL+(DV-DL)*(P-PL)/(D-DL)
CSE=CSE + 0.5*(PV+PL)*(DV-DL)
GO TO 20
ENDIF
10 CONTINUE
20 SMAT(5)=CSE
C
IF (FIRST .OR. BUG) WRITE (6,55)
WRITE (6,57) MAT,NI,DV,BOAM,(SMAT(S)=K),SMAT(S+K+NSEG),K=1,NSEG
WRITE (6,*) ' '
C
55 FORMAT(' BEND1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER'
& ' BACKBONE CURVE POINTS - NATL NI ',5X,'DV',9X,
& ' BETA ',5X,' MOMENT',5X,' ROTATION')
57 FORMAT ( (28X,21F,2X,GL5=6,5GL15=6)/(68X,2GL15=6) )
C
RETURN
C----- GET STIFFNESS TERMS -----
200 CONTINUE
----- BEND1 MODEL DATA STORAGE FOR MEMBER -----
C
SEC 1)= K
C
SEC 2)= MULE
C
SEC 3)= DIR
C
SEC 4)= A
C
SEC 5)= PMQ
C
SEC 6)= PMH
C
SEC 7)= DMG
C
SEC 8)= DMH
C
SEC 9)= BAKCK
C
SEC 10)= ALPHAI
C
SEC 11)= ALPHAZ
C
SEC 12)= IR
C
SEC 13)= SRL
C
SEC 14)= SRE
C
SEC 15)= SRS
C
SEC 16)= SRM
C
SEC 17)= E EQ UNLOAD
C
SEC 18)= UPOSK(1)
C
SEC 19)= UPOSK(2)
C
SEC 20)= UPOSK(3)
C
SEC 21)= UNEGK(1)
C
SEC 22)= UNEGK(2)
C
SEC 23)= UNEGK(3)
C
SEC 24)= EMCRC(1)
C
SEC 25)= EMCRC(2)
C
SEC 26)= EMCRC(3)
C
SEC 27)= EMCRC(4)
C
SEC 28)= EMCRC(5)
C
SEC 29)= EMCRC(6)
C
SEC 30)= ESEK(1)
C
SEC 31)= ESEK(2)
C
SEC 32)= ESEK(3)
C
SEC 33)= EPSE
C
SEC 34)= PSE_OLD
C
SEC 34+1)= PRK(1)
C
SEC 34+2)= PRK(2)
C
SEC 34+3)= PRK(3)
C
SEC 34+4)= PRK(4)
C
SEC 34+5)= PRK(5)
C
SEC 34+6)= PRK(6)
C
SEC 34+7)= PRK(7)
C
SEC 34+8)= PRK(8)
C
SEC 34+9)= PRK(9)
C
SEC 34+10)= PRK(10)
C
SEC 34+11)= PRK(11)
C
SEC 34+12)= PRK(12)
C
SEC 34+13)= PRK(13)
C
SEC 34+14)= PRK(14)
C
SEC 34+15)= PRK(15)
C
SEC 34+16)= PRK(16)
C
SEC 34+17)= PRK(17)
C
SEC 34+18)= PRK(18)
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SEC 34+19)= PRK(19)
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SEC 34+20)= PRK(20)
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SEC 34+21)= PRK(21)
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SEC 34+22)= PRK(22)
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SEC 34+23)= PRK(23)
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SEC 34+24)= PRK(24)
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SEC 34+25)= PRK(25)
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SEC 34+26)= PRK(26)
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SEC 34+27)= PRK(27)
C
SEC 34+28)= PRK(28)
C
SEC 34+29)= PRK(29)
C
SEC 34+30)= PRK(30)
C
SEC 34+31)= PRK(31)
C
SEC 34+32)= PRK(32)
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SEC 34+33)= PRK(33)
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SEC 34+34)= PRK(34)
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SEC 34+35)= PRK(35)
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SEC 34+36)= PRK(36)
C
SEC 34+37)= PRK(37)
C
SEC 34+38)= PRK(38)
C
SEC 34+39)= PRK(39)
C
SEC 34+40)= PRK(40)
C
SEC 34+41)= PRK(41)
C
SEC 34+42)= PRK(42)
C
SEC 34+43)= PRK(43)
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SEC 34+44)= PRK(44)
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SEC 34+45)= PRK(45)
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SEC 34+46)= PRK(46)
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SEC 34+47)= PRK(47)
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SEC 34+48)= PRK(48)
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SEC 34+49)= PRK(49)
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SEC 34+50)= PRK(50)
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SEC 34+51)= PRK(51)
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SEC 34+52)= PRK(52)
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SEC 34+53)= PRK(53)
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SEC 34+54)= PRK(54)
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SEC 34+55)= PRK(55)
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SEC 34+56)= PRK(56)
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SEC 34+57)= PRK(57)
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SEC 34+58)= PRK(58)
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SEC 34+59)= PRK(59)
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SEC 34+60)= PRK(60)
C
SEC 34+61)= PRK(61)
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SEC 34+62)= PRK(62)
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SEC 34+63)= PRK(63)
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SEC 34+64)= PRK(64)
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SEC 34+65)= PRK(65)
C
SEC 34+66)= PRK(66)
C
SEC 34+67)= PRK(67)
C
SEC 34+68)= PRK(68)
C
SEC 34+69)= PRK(69)
C
SEC 34+70)= PRK(70)
C
SEC 34+71)= PRK(71)
C
SEC 34+72)= PRK(72)
C
SEC 34+73)= PRK(73)
C
SEC 34+74)= PRK(74)
C
SEC 34+75)= PRK(75)
C
SEC 34+76)= PRK(76)
C
SEC 34+77)= PRK(77)
C
SEC 34+78)= PRK(78)
C
SEC 34+79)= PRK(79)
C
SEC 34+80)= PRK(80)
C
SEC 34+81)= PRK(81)
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SEC 34+82)= PRK(82)
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SEC 34+83)= PRK(83)
C
SEC 34+84)= PRK(84)
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SEC 34+85)= PRK(85)
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SEC 34+86)= PRK(86)
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SEC 34+87)= PRK(87)
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SEC 34+88)= PRK(88)
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SEC 34+89)= PRK(89)
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SEC 34+90)= PRK(90)
C
SEC 34+91)= PRK(91)
C
SEC 34+92)= PRK(92)
C
SEC 34+93)= PRK(93)
C
SEC 34+94)= PRK(94)
C
SEC 34+95)= PRK(95)
C
SEC 34+96)= PRK(96)
C
SEC 34+97)= PRK(97)
C
SEC 34+98)= PRK(98)
C
SEC 34+99)= PRK(99)
C
SEC 34+100)= PRK(100)
C
NSEG=SMAT(1)
NI =SMAT(2)
J1= NSEG+6
J2= NI+55
J3=2*NI+55
J4=5*NI+55-1+2
SI=SMAT(6)/SMAT(6+NSEG)
210 DO 210 I=1,5
CALL HYSTOSK(P,D,PL,DL,V,NSEG,NI,
& SMAT(6),SMAT(1),SMAT(6),SMAT(1),SI,SMAT(5),
& SEC 1),SEC 2),SEC 3),SEC 4),SEC 5),SEC 6),SEC 7),SEC 8),SEC 9),
& SEC 10),SEC 11),SEC 12),SEC 13),SEC 14),SEC 15),SEC 16),SEC 17),SEC 18),SEC 19),SEC 20),SEC 21),SEC 22),SEC 23),SEC 24),SEC 25),SEC 26),SEC 27),SEC 28),SEC 29),SEC 30),SEC 31),SEC 32),SEC 33),SEC 34),SEC 35),SEC 36),SEC 37),SEC 38),SEC 39),SEC 40),SEC 41),SEC 42),SEC 43),SEC 44),SEC 45),SEC 46),SEC 47),SEC 48),SEC 49),SEC 50),SEC 51),SEC 52),SEC 53),SEC 54),SEC 55),SEC 56),SEC 57),SEC 58),SEC 59),SEC 60),SEC 61),SEC 62),SEC 63),SEC 64),SEC 65),SEC 66),SEC 67),SEC 68),SEC 69),SEC 70),SEC 71),SEC 72),SEC 73),SEC 74),SEC 75),SEC 76),SEC 77),SEC 78),SEC 79),SEC 80),SEC 81),SEC 82),SEC 83),SEC 84),SEC 85),SEC 86),SEC 87),SEC 88),SEC 89),SEC 90),SEC 91),SEC 92),SEC 93),SEC 94),SEC 95),SEC 96),SEC 97),SEC 98),SEC 99),SEC 100)
RETURN
C----- GET STIFFNESS TERMS -----
300 CONTINUE
SEC 4)= A
NSEG=SMAT(1)
NI =SMAT(2)
J1= NSEG+6
J2= NI+55
J3=2*NI+55
J4=5*NI+55-1+2
SI=SMAT(6)/SMAT(6+NSEG)
SET VELOCITY FLAG TO 1 TO REMOVE INFL OF HIGH FREQ VELOC
DVEL=V*VL
DVEL = 1
ICVC=0
IF (BUG) THEN
WRITE (6,*) '----- IN MATOS -----'
WRITE (6,*) 'P,D',P,D
WRITE (6,*) 'PL,DL',PL,DL
ENDIF
510 STIFF=SEC(1)
P=PL+(D-DL)*STIFF
A=SEC(4)
IF (A.EQ.0 .AND. SEC(2).EQ.0) THEN
A=SIGNXSMAT(6),P
IF (P.LT.PL .AND. PL.GT.0 .AND. P.GT.0) A=0
IF (P.GT.PL .AND. PL.LT.0 .AND. P.LT.0) A=0
ENDIF
ICVC=ICVC+1
IF (BUG) THEN
WRITE (6,*) 'STIFF=',STIFF,' A=',A
WRITE (6,*) ' P',P ' ICVC=',ICVC
ENDIF
C
IS P WITHIN LIMITS ?
IF (ICVC.GT.10) THEN
WRITE (6,*) 'MORE THAN 10 CYCLES IN MATOS, IELNO:',IELNO
ELSE IF ((PL.LE.P .AND. P.LT.A) .OR. (PL.GE.P .AND. P.GT.A) .OR.
& (DL.EQ.D)) THEN
IF (BUG) WRITE (6,*) 'C----- IS P WITHIN LIMITS ?'
CALL STRENG (SEC 50),SEC 53),SEC 54),P,PL,D,DL,SEC(1),SEC(17) )
CALL HYSTOSK(P,D,PL,DL,DVEL,NSEG,NI,
& SMAT(6),SMAT(1),SMAT(6),SMAT(1),SI,SMAT(5),
& SEC 1),SEC 2),SEC 3),SEC 4),SEC 5),SEC 6),
& SEC 7),SEC 8),SEC 9),
& SEC 10),SEC 11),SEC 12),SEC 13),SEC 14),SEC 15),
& SEC 16),SEC 17),SEC 18),SEC 19),SEC 20),SEC 21),SEC 22),SEC 23),SEC 24),SEC 25),SEC 26),SEC 27),SEC 28),SEC 29),SEC 30),SEC 31),SEC 32),SEC 33),SEC 34),SEC 35),SEC 36),SEC 37),SEC 38),SEC 39),SEC 40),SEC 41),SEC 42),SEC 43),SEC 44),SEC 45),SEC 46),SEC 47),SEC 48),SEC 49),SEC 50),SEC 51),SEC 52),SEC 53),SEC 54),SEC 55),SEC 56),SEC 57),SEC 58),SEC 59),SEC 60),SEC 61),SEC 62),SEC 63),SEC 64),SEC 65),SEC 66),SEC 67),SEC 68),SEC 69),SEC 70),SEC 71),SEC 72),SEC 73),SEC 74),SEC 75),SEC 76),SEC 77),SEC 78),SEC 79),SEC 80),SEC 81),SEC 82),SEC 83),SEC 84),SEC 85),SEC 86),SEC 87),SEC 88),SEC 89),SEC 90),SEC 91),SEC 92),SEC 93),SEC 94),SEC 95),SEC 96),SEC 97),SEC 98),SEC 99),SEC 100)
DVEL=1
C----- IS P GREATER THAN LIMITS ?
ELSE IF ((PL.LE.A .AND. A.LE.P) .OR. (PL.GE.A .AND. A.GE.P)) .AND.
& (STIFF.NE.0.00) THEN
DI=DL+(A-PL)/STIFF
PL=A
CALL STRENG (SEC 50),SEC 53),SEC 54),P,PL,D,DL,SEC(1),SEC(17) )
DVEL=1
ELSE
PI=P
DI=D
ENDIF
IF (BUG) THEN
WRITE (6,*) 'C----- IS P GREATER THAN LIMITS ?'
WRITE (6,*) 'PL,DL',PL,DL
WRITE (6,*) 'PI,DI',PI,DI
ENDIF
CALL HYSTOSK(P,D,PL,DL,1.00,NSEG,NI,
& SMAT(6),SMAT(1),SMAT(6),SMAT(1),SI,SMAT(5),
& SEC 1),SEC 2),SEC 3),SEC 4),SEC 5),SEC 6),
& SEC 7),SEC 8),SEC 9),
& SEC 10),SEC 11),SEC 12),SEC 13),SEC 14),SEC 15),
& SEC 16),SEC 17),SEC 18),SEC 19),SEC 20),SEC 21),SEC 22),SEC 23),SEC 24),SEC 25),SEC 26),SEC 27),SEC 28),SEC 29),SEC 30),SEC 31),SEC 32),SEC 33),SEC 34),SEC 35),SEC 36),SEC 37),SEC 38),SEC 39),SEC 40),SEC 41),SEC 42),SEC 43),SEC 44),SEC 45),SEC 46),SEC 47),SEC 48),SEC 49),SEC 50),SEC 51),SEC 52),SEC 53),SEC 54),SEC 55),SEC 56),SEC 57),SEC 58),SEC 59),SEC 60),SEC 61),SEC 62),SEC 63),SEC 64),SEC 65),SEC 66),SEC 67),SEC 68),SEC 69),SEC 70),SEC 71),SEC 72),SEC 73),SEC 74),SEC 75),SEC 76),SEC 77),SEC 78),SEC 79),SEC 80),SEC 81),SEC 82),SEC 83),SEC 84),SEC 85),SEC 86),SEC 87),SEC 88),SEC 89),SEC 90),SEC 91),SEC 92),SEC 93),SEC 94),SEC 95),SEC 96),SEC 97),SEC 98),SEC 99),SEC 100)
GO TO 510
C----- IS P LESS THAN LIMITS ?
ELSE IF ((P.LT.PL .AND. PL.LE.A) .OR. (P.GT.PL .AND. PL.GE.A)) .AND.
& (ABS(P-PL).GT. 0.0005*ABS(P+PL)) THEN
PI=PL+(P-PL)*.001
DI=DL+(D-DL)*.001
ELSE
PI=P
DI=D
ENDIF
IF (BUG) THEN
WRITE (6,*) 'C----- IS P LESS THAN LIMITS ?'
WRITE (6,*) 'PI,DI',PI,DI
ENDIF
CALL HYSTOSK(P,D,PL,DL,1.00,NSEG,NI,
& SMAT(6),SMAT(1),SMAT(6),SMAT(1),SI,SMAT(5),
& SEC 1),SEC 2),SEC 3),SEC 4),SEC 5),SEC 6),
& SEC 7),SEC 8),SEC 9),
& SEC 10),SEC 11),SEC 12),SEC 13),SEC 14),SEC 15),
& SEC 16),SEC 17),SEC 18),SEC 19),SEC 20),SEC 21),SEC 22),SEC 23),SEC 24),SEC 25),SEC 26),SEC 27),SEC 28),SEC 29),SEC 30),SEC 31),SEC 32),SEC 33),SEC 34),SEC 35),SEC 36),SEC 37),SEC 38),SEC 39),SEC 40),SEC 41),SEC 42),SEC 43),SEC 44),SEC 45),SEC 46),SEC 47),SEC 48),SEC 49),SEC 50),SEC 51),SEC 52),SEC 53),SEC 54),SEC 55),SEC 56),SEC 57),SEC 58),SEC 59),SEC 60),SEC 61),SEC 62),SEC 63),SEC 64),SEC 65),SEC 66),SEC 67),SEC 68),SEC 69),SEC 70),SEC 71),SEC 72),SEC 73),SEC 74),SEC 75),SEC 76),SEC 77),SEC 78),SEC 79),SEC 80),SEC 81),SEC 82),SEC 83),SEC 84),SEC 85),SEC 86),SEC 87),SEC 88),SEC 89),SEC 90),SEC 91),SEC 92),SEC 93),SEC 94),SEC 95),SEC 96),SEC 97),SEC 98),SEC 99),SEC 100)
GO TO 510
C
IF (BUG) WRITE (6,*) 'STIFF=',SEC(1), ' A=',SEC(4)
C----- TRANSFER ENERGIES FOR BOTH IOPT=5 AND 6.
400 ESE=SEC(30)
EPSE=SEC(55)
C----- TRANSFER DUCTILITIES AND EXCURSION RATIOS FOR BOTH IOPT=5 AND 6.
DO 410 I=1,5
DUCT(I)=MAX(SEC(17)+E,SEC(20)+I)
EMCR(I)=SEC(25)+I+5
410 EMCR(I)=SEC(25)+I
C
RETURN
C----- DAMAGE INDEX -----
500 ESE=SEC(30)
EPSE=SEC(55)
NSEGS=SMAT(1)
NI =SMAT(2)
DMAX =SMAT(5-2*NSEGS)
DV =SMAT(4)
BOAM =SMAT(5)
P =SEC(56+ 5*NI)
D =SEC(56+ 5*NI)
DI = SMAT(6+NSEGS)
IF (DV.LE.DI) THEN
PY=SMAT(6)*DV/DI
ELSE
DO 510 I=2,NSEGS
PI=SMAT(4+I)

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P2=SMAT(5+I)
D1=SMAT(4+I)*NSEG5
D2=SMAT(5+I)*NSEG5
IF (DV.GE.D1 .AND. DV.LE.D2) THEN
  PV=P1*(DV-D1)/(P2-P1)/(D2-D1)
GO TO 520
ENDIF
CONTINUE
510
ENDIF
520 DAMAGE=ABS(D)/DMAX + BDAM / (PV*DMAX) * EPSE
C
RETURN
END
-----
SUBROUTINE MAT04
& (IOPT ,IELNO ,ERR ,FIRST ,PRINT ,BUG,
& MAT ,SE ,P,PL,D,DL,V,VL,LELEM,LMAT,
& SMAT,EESE,EPSE,DUCT,EXCR,DAMAGE)
C
IMPLICIT REAL(A-H,O-Z)
LOGICAL ERR ,FIRST,PRINT,BUG
LOGICAL STRES
DIMENSION SEC(10),SMAT(20),DUCT(5),EXCR(6)
CHARACTER*80 TYPE
C
IF (IOPT.NE.1) IELEM=52+5*SMAT(2) +2
IF (IOPT.EQ.0) RETURN
C-----
C VARIABLES:
C-----
C GLOBAL VARIABLES
C IOPT = 1. INITIALIZE MATERIAL
C = 2. GET STIFFNESS
C RINPUT = INPUT DATA
C SMAT = INTERNAL STORAGE
C SE = OUTPUT STIFFNESS
C-----
C----- SHEAR1 DATA -----
C SMAT(1)=NSEG5, NUMBER OF BACKBONE SEGMENTS
C SMAT(2)=NI, NUMBER OF SMALL AMPLITUDE LOOPS
C SMAT(3)=CSE, CONSTRAINT STRAIN ENERGY...
C SMAT(4)=DV, YELD DISPLACEMENT
C SMAT(5)=DP, BACKBONE SHEAR FOR POINT I
C SMAT(6)=I+NSEG, BACKBONE DISPLACEMENT FOR POINT I
C SMAT(7)=BDAM, BETA FOR DAMAGE INDEX
C
GO TO (100,200,300,400,500),IOPT
C
100 CONTINUE
C----- INPUT DATA FOR SHEAR1 HYSTERESIS MODEL -----
C NSEG = NUMBER OF BACKBONE SEGMENTS
C NI = NUMBER OF SMALL LOOP POINTS
C DP = BACKBONE LOAD
C DL = BACKBONE DISPLACEMENT
C-----
READ (5,*) TYPE ,NSEG,NI,DV,BDAM
READ (5,*) ( SMAT(I) ,I=1,NSEG)
READ (5,*) ( SMAT(I+NSEG) ,I=1,NSEG)
LELEM = 52+5*NI +2
LMAT = 52+5*NI +2
SMAT(1)=NSEG
SMAT(2)=NI
SMAT(3)=CSE
SMAT(4)=DV
SMAT(5)=DP
SMAT(6)=I+NSEG
SMAT(7)=BDAM
C----- CALC CONSTANT STRAIN ENERGY ----
DL=0
PL=0
DO 10 I=1,NSEG
  P=SMAT(I)
  D=SMAT(I+NSEG)
  IF (D.LE.DV) THEN
    CSE=CSE + 0.5*(P+PL)*(D-DL)
    PL=D
  ELSE IF (D.EQ.DL) THEN
    GO TO 20
  ELSE
    PV=P1*(DV-DL)/(P-PL)/(D-DL)
    CSE=CSE + 0.5*(P+PV)*(D-DL)
    GO TO 20
  ENDIF
10 CONTINUE
20 SMAT(8)=CSE
C
IF (FIRST .OR. BUG) WRITE (6,65)
WRITE (6,67) MAT,NI,DV,BDAM,(SMAT(I+K),SMAT(I+K+NSEG),K=1,NSEG)
WRITE (6,*)
65 FORMAT('') SHEAR1 HYSTERESIS MODEL DATA - UNIT LENGTH MEMBER
& / / ' BACKBONE CURVE POINTS - MAT, NI DV '
& 5X,'BETA',6X, 5X,'STRESS',5X,'STRAIN'
67 FORMAT ('(2E11,2I4,2X,4G15.6)/(68N,2G15.6)')
C
RETURN
C----- GET STIFFNESS TERMS -----
200 CONTINUE
C----- SHEAR1 MODEL DATA STORAGE FOR MEMBER -----
C SEC 1)= K
C SEC 2)= RULE
C SEC 3)= DIR
C SEC 4)= A
C SEC 5)= PMG
C SEC 6)= PMH
C SEC 7)= DMG
C SEC 8)= DMH
C SEC 9)= BACKS
C SEC 10)= SR1
C SEC 11)= SR2
C SEC 12)= SR3
C SEC 13)= SRM
C SEC 14)= IR
C SEC 15)= S_EQ_UNLOAD
C SEC 16)= UPOS(1)
C SEC 17)= UPOS(2)
C SEC 18)= UPOS(3)
C SEC 19)= UNEG(1)
C SEC 20)= UNEG(2)
C SEC 21)= UNEG(3)
C SEC 22)= ENCR(1)
C SEC 23)= ENCR(2)
MAT05000 C SEC 24)= ENCR(3)
MAT05010 C SEC 25)= ENCR(4)
MAT05020 C SEC 26)= ENCR(5)
MAT05030 C SEC 27)= ENCR(6)
MAT05040 C SEC 28)= ESE
MAT05050 C SEC 29)= ESE
MAT05060 C SEC 30)= ESE
MAT05070 C SEC 31)= PSE
MAT05080 C SEC 32)= PSE_OLD
MAT05090 C SEC 32+1)=PRK 1)
MAT05100 C SEC 32+ )=PRK(NI)
MAT05110 C SEC 32+1+ )=ORC 1)
MAT05120 C SEC 32+ 2*NI)=ORC(NI)
MAT00090 C SEC 32+1+2*NI)=FRIC 1)
MAT00060 C SEC 32+ 5*NI)=FRIC(NI)
MAT00070 C SEC 33+ 5*NI)=P_MAX
MAT00080 C SEC 34+ 5*NI)=D_MAX
MAT00090 NSEG=SMAT(1)
MAT00100 NI =SMAT(2)
MAT00110 SI =SMAT(5)/SMAT(5+NSEG)
MAT00120 JI=NSEG+5
MAT00130 JS=NI+55
MAT00140 J=2*NI+55
MAT00150 J=5*NI+55-1 +2
DO 210 I=1,J
MAT00170 210 SEC(I)=0
MAT00180 CALL HVSTOK P, D,PL,DL, V ,NSEG,NI,BUG,
& SMAT( 5),SMAT(J1),SMAT( 5),SMAT(J1),SI,SMAT(5),SMAT(5),
& SEC 1) ,SEC 2) ,SEC 3) ,SEC 4) ,SEC 5) ,SEC 6) ,
& SEC 7) ,SEC 8) ,SEC 9) ,SEC 10) ,SEC 11) ,SEC 12) ,
& SEC 13) ,SEC 14) ,SEC 15) ,SEC 16) ,SEC 19) ,SEC 22) ,
& SEC 28) ,SEC 31) ,SEC 32) ,SEC 33) ,SEC 35) ,SEC 36) )
RETURN
C----- GET STIFFNESS TERMS -----
500 CONTINUE
NSEG=SMAT(1)
NI =SMAT(2)
SI = SMAT(5)/SMAT(5+NSEG)
JI=NSEG+5
JS=NI+55
J=2*NI+55
DVEL=V*VL
C SET VELOCITY FLAG TO 1 TO REMOVE INFL OF HIGH FREQ VELOC
DVEL = 1
ICVC=0
IF (BUG) THEN
  WRITE (6,*) ' IN MAT04 '
  WRITE (6,*) 'P,D',P,D
  WRITE (6,*) 'PL,DL',PL,DL
ENDIF
510 STIFF=SEC(1)
P=PL*(D-DL)*STIFF
A=SEC(4)
IF (A.EQ.0 .AND. SEC(2).EQ.0) THEN
  A=SIGN(SMAT(5),P)
  IF (P.LT.PL .AND. PL.GT.0 .AND. P.GT.0) A=0
  IF (P.GT.PL .AND. PL.LT.0 .AND. P.LT.0) A=0
ENDIF
ICVC=ICVC+1
IF (BUG) THEN
  WRITE (6,*) 'STIFF=',STIFF,' A=',A
  WRITE (6,*) 'P=',P,' ICVC=',ICVC
ENDIF
C----- IS P WITHIN LIMITS ? -----
IF (ICVC.GT.10) THEN
  WRITE (6,*) 'MORE THAN 10 CYCLES IN MAT04. IELNO',IELNO
ELSE IF ((P.LE.P .AND. P.LT.A) .OR. (P.LE.P .AND. P.GT.A) .OR.
(DL.EQ.D)) THEN
  IF (BUG) WRITE (6,*) 'C----- IS P WITH IN LIMITS ? '
  CALL STRENG (SEC(28),SEC(31),SEC(32),P,PL,D,DL,SEC(1),SEC(15) )
  CALL HVSTOK P, D,PL,DL,DVEL,NSEG,NI,BUG,
& SMAT( 5),SMAT(J1),SMAT( 5),SMAT(J1),SI,SMAT(5),SMAT(5),
& SEC 1) ,SEC 2) ,SEC 3) ,SEC 4) ,SEC 5) ,SEC 6) ,
& SEC 7) ,SEC 8) ,SEC 9) ,SEC 10) ,SEC 11) ,SEC 12) ,
& SEC 13) ,SEC 14) ,SEC 15) ,SEC 16) ,SEC 19) ,SEC 22) ,
& SEC 28) ,SEC 31) ,SEC 32) ,SEC 33) ,SEC 35) ,SEC 36) )
C----- IS P GREATER THAN LIMITS ? -----
ELSE IF ((P.LE.A .AND. A.LE.P) .OR. (P.LE.A .AND. A.GE.P)) .AND.
(STIFF.NE.0.00) THEN
  DL=DL+(A-PL)/STIFF
  PL=A
  CALL STRENG (SEC(28),SEC(31),SEC(32),P,PL,D,DL,SEC(1),SEC(15) )
  DL=D1
  PL=P1
  IF (ABS(P-PL).GT. 0.0005*ABS(P+PL)) THEN
    P1=P*(P-PL)*.001
    D1=DL*(D-DL)*.001
  ELSE
    P1=P
    D1=D
  ENDIF
IF (BUG) THEN
  WRITE (6,*) 'C----- IS P GREATER THAN LIMITS ? '
  WRITE (6,*) 'PL,DL',PL,DL
  WRITE (6,*) 'P1,D1',P1,D1
ENDIF
CALL HVSTOK P1,D1,PL,D1,1.00,NSEG,NI,BUG,
& SMAT( 5),SMAT(J1),SMAT( 5),SMAT(J1),SI,SMAT(5),SMAT(5),
& SEC 1) ,SEC 2) ,SEC 3) ,SEC 4) ,SEC 5) ,SEC 6) ,
& SEC 7) ,SEC 8) ,SEC 9) ,SEC 10) ,SEC 11) ,SEC 12) ,
& SEC 13) ,SEC 14) ,SEC 15) ,SEC 16) ,SEC 19) ,SEC 22) ,
& SEC 28) ,SEC 31) ,SEC 32) ,SEC 33) ,SEC 35) ,SEC 36) )
GO TO 510
C----- IS P LESS THAN LIMITS ? -----
ELSE IF ((P.LT.PL .AND. P.LE.A) .OR. (P.GT.PL .AND. P.LE.A)) .AND.
(ABS(P-PL).GT. 0.0005*ABS(P+PL)) THEN
  P1=P*(P-PL)*.001
  D1=DL*(D-DL)*.001
ELSE
  P1=P
  D1=D
ENDIF
IF (BUG) THEN
  WRITE (6,*) 'C----- IS P LESS THAN LIMITS ? '
  WRITE (6,*) 'P1,D1',P1,D1
ENDIF
CALL HVSTOK P1,D1,PL,D1,1.00,NSEG,NI,BUG,
& SMAT( 5),SMAT(J1),SMAT( 5),SMAT(J1),SI,SMAT(5),SMAT(5),
& SEC 1) ,SEC 2) ,SEC 3) ,SEC 4) ,SEC 5) ,SEC 6) ,
& SEC 7) ,SEC 8) ,SEC 9) ,SEC 10) ,SEC 11) ,SEC 12) ,
& SEC 13) ,SEC 14) ,SEC 15) ,SEC 16) ,SEC 19) ,SEC 22) ,
& SEC 28) ,SEC 31) ,SEC 32) ,SEC 33) ,SEC 35) ,SEC 36) )

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& SEC(28) ,SEC(31) ,SEC(32) ,SEC(33) ,SEC(35) ,SEC(36) )
GO TO 510
ENDIF
C
C IF (BUG) WRITE (6,*) 'STIFF',STIFF, A=,SEC(4)
C
C SAVE MAXIMUM DISPL AND LOAD
C IF (ABS(D).GT.ABS(SEC(5+5*NI))) THEN
SEC(33)= 5*NI:P
SEC(34)= 5*NI:D
ENDIF
C
C ----- TRANSFER ENERGIES FOR BOTH IOPT=3 AND 4.
400 ESE=SEC(28)
EPSE=SEC(31)
C
C ----- TRANSFER DUCTILITIES AND ENCRUSION RATIOS FOR BOTH IOPT=3 AND 4.
DO I=1,5
DUCT(I)=MAX(SEC(15+I),SEC(18+I))
ENCR(I)=SEC(21+I)
410 ENCR(I+3)=SEC(21+I+3)
RETURN
C
C ----- DAMAGE INDEX -----
500 ESE=SEC(28)
EPSE=SEC(31)
NSEG=SMAT(1)
NI=SMAT(2)
DMAX=SMAT(4+2*NSEG)
DY=SMAT(4)
BOAM=SMAT(5+2*NSEG)
P=SEC(35)-3*NI
D=SEC(34)-3*NI
IF (D.V.LE.SMAT(5+NSEG)) THEN
PV=SMAT(5)+DY/SMAT(5+NSEG)
ELSE
DO I=2,NSEG
P1=SMAT(5+I)
P2=SMAT(4+I)
D1=SMAT(5+I+NSEG)
D2=SMAT(4+I+NSEG)
IF (D.V.GE.D1 .AND. D.V.LE.D2) THEN
PV=P1+(D.V-D1)*(P2-P1)/(D2-D1)
GO TO 520
ENDIF
CONTINUE
510
ENDIF
520 DAMAGE=ABS(D)/DMAX + BOAM / (PV*DMAX) * EPSE
RETURN
END
C
SUBROUTINE MAT06
& (IOPT ,IELNO ,ERR ,FIRST ,PRDIT ,BUG,
& MAT ,SEC ,P,PL,D,DL,V,VL,LELEH,LNAT,
& SMAT ,ESEE ,EPSE ,DUCT ,ENCR ,DAMAGE)
C
C IMPLICIT REAL(A-H,O-Z)
C LOGICAL ERR,FIRST,PRDIT,BUG
C LOGICAL BTST
C DIMENSION SEC(100),SMAT(15),DUCT(5),ENCR(8)
C
C LELEH=7
C IF (IOPT.EQ.0) RETURN
C
C ----- VARIABLES -----
C ----- GLOBAL VARIABLES -----
C IOPT = 1. INITIALIZE MATERIAL
C IOPT = 2. GET STIFFNESS
C RNDPIT = INPUT DATA
C SMAT = INTERNAL STORAGE
C SE = OUTPUT STIFFNESS
C
C ----- TAKEDA DATA -----
SMAT(1)=EI, ELASTIC STIFFNESS
SMAT(2)=PC, CRACKING LOAD
SMAT(3)=DC, CRACKING DISPLACEMENT
SMAT(4)=PV, VEIL LOAD
SMAT(5)=DV, VEIL DISPLACEMENT
SMAT(6)=PU, ULTIMATE LOAD
SMAT(7)=DU, ULTIMATE DISPLACEMENT
SMAT(8)=OC, INITIAL STIFFNESS
SMAT(9)=CV, CRACKED STIFFNESS
SMAT(10)=YU, ULTIMATE STIFFNESS
SMAT(11)=OV, RELOADING STIFFNESS
SMAT(12)=CSE, CONSTANT STRAIN ENERGY AT VEIL
SMAT(13)=BDM, BETA FOR DAMAGE INDEX
C
C ----- INPUT DATA FOR TAKEDA HYSTERESIS MODEL -----
C THE FOLLOWING DATA IS INPUT ONCE FOR EACH MODEL
C
EI = MOMENT OF INERTIA
G = MOMENT GRADIENT
PC,DC = CRACKING LOAD AND DISPLACEMENT
PV,DV = VEIL LOAD AND DISPLACEMENT
PU,DU = ULTIMATE LOAD AND DISPLACEMENT
C
GO TO (100,200,500,100,500),IOPT
C
100 CONTINUE
READ (5,*) TYPE , (SMAT(I),I=2,7),BDM
C
LNAT = 15
SMAT(8) = SMAT(2) / SMAT(5)
SMAT(9) = (SMAT(4) - SMAT(2)) / (SMAT(5) - SMAT(3))
SMAT(10) = (SMAT(6) - SMAT(4)) / (SMAT(7) - SMAT(5))
SMAT(11) = (SMAT(2) - SMAT(4)) / (SMAT(5) - SMAT(3))
SMAT(12) = (SMAT(2) + SMAT(3)) / 2 + .5 * (SMAT(2) - SMAT(4)) * (SMAT(5) - SMAT(3))
SMAT(13) = BDM
C
IF (FIRST .OR. BUG) WRITE (6,5)
WRITE (6,6) MAT,BDM, SMAT(2),SMAT(6),SMAT(6),
SMAT(5),SMAT(5),SMAT(7)
5 FORMAT('/// TAKEDA HYSTERESIS MODEL- FOR UNIT LENGTH MEMBER')
6 FORMAT('//MAT0720
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ELSE IF ((P.LT.PL.AND. PL.LE.A) .OR. (P.GT.PL.AND. PL.GE.A)) THEN MAT02210 C SEC 9=EPSE MAT00750
IF (ABS(P-PL).GT. 0.0005*ABS(P+PL)) THEN MAT02220 C SEC 10=KEY MAT00740
PI=PL*(P+PL)*.001 MAT02230 C SEC 11=UP(SK 1) MAT00750
DI=DL*(D-DL)*.001 MAT02240 C SEC 12=UP(SK 2) MAT00760
ELSE MAT02250 C SEC 13=UP(SK 3) MAT00770
PI=P MAT02260 C SEC 14=ENCR(1) MAT00780
DI=D MAT02270 C SEC 15=ENCR(2) MAT00790
ENDIF MAT02280 C SEC 16=ENCR(3) MAT00800
IF (BUG) THEN MAT02410 C SEC 17=ENCR(1) MAT00810
WRITE (6,*) 'C----- IS P LESS THAN LIMITS ? ' MAT02420 C SEC 18=ENCR(2) MAT00820
WRITE (6,*) 'PI,DI=,PI,DI MAT02430 C SEC 19=ENCR(3) MAT00830
ENDIF MAT02440 C SEC 20=ENCR(4) MAT00840
CALL HYSTO6(PI,DI,PL,DL,1,1, MAT02450 C SEC 21=ENCR(5) MAT00850
& SEC 1),SEC 2),SEC 3),SEC 4),SEC 5),SEC 6), MAT02460 C SEC 22=ENCR(6) MAT00860
& SMAT( 2),SMAT( 3),SMAT( 4),SMAT( 5),SMAT( 6), MAT02470 C SEC 23=P_MAX MAT00870
& SMAT( 7),SMAT( 8),SMAT( 9),SMAT(10),SMAT(11),SMAT(12), MAT02480 C SEC 24=D_MAX MAT00880
& SEC 7),SEC 8),SEC 9),SEC 10),SEC 11),SEC 12),SEC 13), MAT02490 C MAT00890
& SEC 14),SEC 15),SEC 16),SEC 17),SEC 18),SEC 19),SEC 20), MAT02500 C INITIALIZE RULE #1 - ELASTIC BEHAVIOR MAT00900
& SEC 21),SEC 22),SEC 23),SEC 24),SEC 25),SEC 26),SEC 27),BUG, MAT02510 C MAT00910
& SEC 28),SEC 29),SEC 32),SEC 33),SEC 34),SEC 37),SEC 40)) MAT02520 C DO 210 I=1,22 MAT00920
GO TO 310 MAT02530 C 210 MAT00930
ENDIF MAT02540 C SEC 1)=0 MAT00940
C MAT02550 C CALL HYSTO7(0.,0.,0.,0.,SEC(1),SEC(2),SEC(3),SEC(4),SEC(5),V,VL, MAT00950
IF (BUG) WRITE (6,*) 'STIFF',STIFF', A,B=,SEC(3),SEC(4),SEC(27) & SMAT(1),SMAT(2),SMAT(3),SMAT(4),SMAT(5),BUG, MAT00960
MAT02570 & SEC(6),SEC(9),SEC(10),SEC(11),SEC(14),SEC(17)) MAT00970
C MAT02590 C RETURN MAT00980
MAT02600 C MAT00990
C----- GET STIFFNESS TERMS AND ACTUAL FORCE ----- MAT01010
500 CONTINUE MAT02610 C MAT01020
C----- CHECK TO SEE IF DO = 0 ? MAT01030
P=P MAT02620 C MAT01040
D=D MAT02630 C MAT01050
IF (D.EQ.DL) RETURN MAT02640 C MAT01060
C----- CALL HYSTO7 TO CALC NEW STIFFNESS AND GET LOAD P MAT01070
CALL HYSTO7(P,D,PL,DL,SEC(1),SEC(2),SEC(3),SEC(4),SEC(5),V,VL, MAT01080
& SMAT(1),SMAT(2),SMAT(3),SMAT(4),SMAT(5),BUG, MAT01090
& SEC(6),SEC(9),SEC(10),SEC(11),SEC(14),SEC(17)) MAT01100
C MAT01110
C----- SEL=SEC(1) MAT01120
MAT02750 C MAT01130
MAT02760 C----- TRANSFER ENERGIES FOR BOTH IOPT=5 AND 4. MAT01160
IF (ABS(D).GT.ABS(SEC(2))) THEN MAT02770 C MAT01170
SEC(2)=P MAT02780 C MAT01180
SEC(2)=D MAT02790 C MAT01190
ENDIF MAT02800 C MAT01200
MAT02810 C----- TRANSFER ENERGIES FOR BOTH IOPT=5 AND 4. MAT01220
400 EESE=SE(6) MAT02820 C MAT01230
EPESE=SE(9) MAT02830 C MAT01240
MAT02840 C----- TRANSFER DUCTILITIES AND ENCRUSION RATIOS FOR BOTH IOPT=5 AND 4. MAT01250
DO 410 I=1,3 MAT02850 C MAT01260
DUCT(I)=MAX(SEC(5)-I),SEC(5)+I) MAT02870 C MAT01270
ENCR(I)=SEC(9)+I) MAT02880 C MAT01280
410 ENCR(I)=SEC(16)+I) MAT02890 C MAT01290
RETURN MAT02900 C MAT01300
C----- DAMAGE INDEX ----- MAT01310
500 EESE=SE(29) MAT02950 C MAT01320
EPESE=SE(32) MAT02960 C MAT01330
PV= SMAT( 4) MAT02970 C MAT01340
PU= SMAT( 6) MAT02980 C MAT01350
DU= SMAT( 7) MAT02990 C MAT01360
P= SEC(46) MAT03000 C MAT01370
D= SEC(47) MAT03010 C MAT01380
BDAM=SMAT(13) MAT03020 C MAT01390
DAMAGE=ABS(D)/DU + BDAM/(PV*DU) * EPESE MAT03030 C MAT01400
C----- RETURN MAT01410
END MAT03040 C MAT01420
C----- SUBROUTINE MAT07 ----- MAT01430
& (IOPT ,IELNO ,ERR ,FIRST ,PRINT ,BUG, MAT00040 C MAT01440
& MAT ,SE ,P,PL,D,DL ,V,VL,LELE,LMAT, MAT00050 C MAT01450
& SMAT ,E,SE,EPSE,DUCT,EXCR,DAMAGE) MAT00060 C MAT01460
C----- IMPLICIT REAL(A-H,O-Z) MAT00070 C MAT01470
LOGICAL ERR,FIRST,PRINT,BUG MAT00080 C MAT01480
LOGICAL BTEST MAT00090 C MAT01490
DIMENSION SEC(100),SMAT(7),DUCT(5),ENCR(6) MAT00100 C MAT01500
CHARACTER*80 TYPE MAT00110 C MAT01510
C----- RESERVE STORAGE FOR ELEMENT MAT00120 C MAT01520
LELE=24 MAT00130 C MAT01530
IF (IOPT.EQ.0) RETURN MAT00140 C MAT01540
C----- C VARIABLES: ----- MAT00150 C MAT01550
C----- GLOBAL VARIABLES ----- MAT00160 C MAT01560
C IOPT = 1. INITIALIZE MATERIAL MAT00170 C MAT01570
C 2. GET STIFFNESS MAT00180 C MAT01580
C RINPUT = INPUT DATA MAT00190 C MAT01590
C SMAT = INTERNAL STORAGE MAT00200 C MAT01600
C SE = OUTPUT STIFFNESS MAT00210 C MAT01610
C----- GO TO (100,200,300,400,500),IOPT MAT00220 C MAT01620
C----- 100 CONTINUE ----- MAT00230 C MAT01630
C----- INTERPATE INPUT DATA ----- MAT00240 C MAT01640
KE = SMAT( 1) MAT00250 C MAT01650
PV = SMAT( 2) MAT00260 C MAT01660
KIE = SMAT( 3) MAT00270 C MAT01670
DV = SMAT( 4) MAT00280 C MAT01680
CSE = SMAT( 5) MAT00290 C MAT01690
DMAX = SMAT( 6) MAT00300 C MAT01700
BDAM = SMAT( 7) MAT00310 C MAT01710
C----- READ (5,*) TYPE ,(SMAT(I),I=1,3),DUCHAK,BDAM MAT00320 C MAT01720
C----- LMAT = 7 ----- MAT00330 C MAT01730
SMAT(4)=SMAT(2)/SMAT(1) MAT00340 C MAT01740
SMAT(5)=SMAT(4)*SMAT(2)/2 MAT00350 C MAT01750
SMAT(6)=SMAT(4)*DUCHAK MAT00360 C MAT01760
SMAT(7)=BDAM MAT00370 C MAT01770
C----- IF (FIRST .OR. BUG) WRITE (6,191) ----- MAT00380 C MAT01780
WRITE (6,192) MAT,(SMAT(K),K=1,3),DUCHAK,BDAM MAT00390 C MAT01790
C----- 191 FORMAT (/// BILINEAR HYSTERESIS MODEL PARAMETERS'// MAT00400 C MAT01800
& '-----'// MAT00410 C MAT01810
& ' MAT,'6X,' KE',10X,' PV',10X,' KIE', 7X,'MAX DUCT', MAT00420 C MAT01820
& ' 10X,' BET') MAT00430 C MAT01830
192 FORMAT (1X,15,7015.6/) MAT00440 C MAT01840
C----- RETURN ----- MAT00450 C MAT01850
C----- INITIALIZE STIFFNESS ----- MAT00460 C MAT01860
200 CONTINUE MAT00470 C MAT01870
C----- ELASTO-PLASTIC MODEL DATA STORAGE FOR MEMBER ----- MAT00480 C MAT01880
C SEC 1)=K MAT00490 C MAT01890
C SEC 2)=RULE MAT00500 C MAT01900
C SEC 3)=EPSE OLD MAT00510 C MAT01910
C SEC 4)=A, UPPER LIMIT BEFORE RULE CHANGE MAT00520 C MAT01920
C SEC 5)=B, LOWER LIMIT BEFORE RULE CHANGE MAT00530 C MAT01930
C SEC 6)=E=SEC(1) MAT00540 C MAT01940
C SEC 7)=E=SEC(2) MAT00550 C MAT01950
C SEC 8)=E=SEC(5) MAT00560 C MAT01960

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RX =DATA( 5,IMASS)
RV =DATA( 6,IMASS)
RZ =DATA( 7,IMASS)
RW =DATA( 8,IMASS)
RXZ =DATA( 9,IMASS)
RYZ =DATA(10,IMASS)
IGEN=DATA(11,IMASS)
INC =DATA(12,IMASS)
C
9 JOINT=IQUICK(NODE,JD,NODE)
C
IF (JOINT.LE.0) THEN
  WRITE (6,*) 'NODE #',NODE,
  & ' WAS NOT FOUND, CHECK INPUT. MASS IS OMITTED '
  GO TO 90
ENDIF
C
ICOS =JCOS(JOINT)
C
----- SET UP NODE MASS MATRIX IN XYZ COORDINATE SYSTEM
C----- SET UP TRANSFORMATION MATRIX, A = (CONST)
DO 10 I=1,6
  DO 10 J=1,6
    10 AC(I,J)=0
    20 AC(I,J)=1
    AC(4,2)=CONST(JOINT,1)
    AC(4,3)=CONST(JOINT,2)
    AC(5,1)=CONST(JOINT,3)
    AC(5,2)=CONST(JOINT,4)
    AC(6,1)=CONST(JOINT,5)
    AC(6,2)=CONST(JOINT,6)
C
----- SET UP NODE MASS MATRIX
DO 30 I=1,6
  DO 30 J=1,6
    30 SK(I,J)=0
C
SK(1,1)=PM
SK(2,2)=PV
SK(3,3)=PZ
SK(4,4)=RK
SK(5,5)=RV
SK(6,6)=RW
SK(4,5)=RVZ
SK(5,6)=RVZ
C
DO 40 I=1,6
  DO 40 J=1,6
    40 SK(J,I)=SK(I,J)
C
----- TRANSFORM MASS MATRIX TO ACCOUNT FOR CONSTRAINTS
DO 50 I=1,6
  DO 50 J=1,6
    50 SAT(I,J)=0
    50 SAT(I,J)=SAT(I,J) + SK(I,K)*AK(J,K)
C
DO 60 I=1,6
  DO 60 J=1,6
    60 SK(I,J)=SK(I,J) + AK(I,K)*SAT(K,J)
C
----- TRANSFER MASS MATRIX TO HALF STORAGE MODE
I=0
DO 70 I=1,6
  DO 70 J=1,6
    70 IMASS(I,J)=SK(I,J)
C
----- INITIALIZE THE DIAGONAL MASS MATRIX
DO 80 I=1,6
  80 LNK(I)=IDOF(JOINT,I)
C
IF (IOPT.EQ.1) THEN
C----- CALL SKYLINE TO RESERVE SPACE FOR THIS NODE'S MASS
IF (BUG) THEN
  WRITE (ELNO,915) NODE,(LNK(I),I=1,6)
  CALL LMATRK(SMASS,MD,6,21,ELNO)
  ENDF
  CALL SKYLNK2,NDOF,IRUG,TITLE,NHM,6,
  & LN,SMASS,MD,'GLOBAL MASS')
C
ELSE IF (IOPT.EQ.2) THEN
IF (BUG) THEN
  WRITE (ELNO,915) NODE,(LNK(I),I=1,6)
  915 FORMAT ('MASS AT NODE #',I6,' LN:',I6)
  CALL LMATRK(SMASS,MD,6,21,ELNO)
  ENDF
C
CALL FORML(MASS,MDM,NDOF,IND,SMASS,MD,6,21,LN,I,0)
C
ENDIF
90 CONTINUE
C
IF (IGEN.GT.0) THEN
  IGEN=IGEN-1
  NODE=NODE+INC
  GO TO 9
ENDIF
100 CONTINUE
C
RETURN
END
C=====
C MATRIX SOLUTION OF EQUATION AX=P, WHERE THE UPPER TRIANGULAR MATRIX
C OF THE SYMMETRIC MATRIX A IS STORED BY SKYLINES. P IS STORED AS
C A FULL MATRIX. THE MATRIX P IS REPLACED BY R AFTER BACK
C SUBSTITUTION IS COMPLETE. BOTH A AND P ARE ALTERED. ....
C GUYAN OPTION: IF GUYAN IS .TRUE, MASS MATRIX IS ALSO CONDENSED
C-----
SUBROUTINE MSOLL(IOPT,PRINT,N,IND,LROM,NLC,L1,L2,MD,A,P,FACTOR,
& GUYAN,MASS,MMASS,INDMAS,
& KCOND,KG,MDKG,IMDKG,ABORT)
DIMENSION A(IND),FACTOR(N),PC(LROM,NLC),MD(N+1)
DIMENSION MMASS(N+1),MDKG(N+1)
LOGICAL BTEST,ABORT
REAL MASS,INDMAS,KG,IMDKG
LOGICAL GUYAN,PRINT,KCOND

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MF000550 IJK(I,J)=MDK(J)-J-I MS000210
MF000560 LNK(I,J)=MDMASS(J)-J-I MS000220
MF000570 LNK(I,J)=MDK(GJ)-J-I MS000230
C-----
C MATRIX STORAGE SCHEME:
C THE MATRIX A IS Banded and SYMMETRIC. THUS ONLY THE SKYLINE ABOVE
C AND THE MAIN DIAGONAL NEEDS TO BE STORED. MS000240
C THE MATRIX A IS STORED IN A LINEAR ARRAY BY COLUMNS. THE VALUE ON
C THE MAIN DIAGONAL IS STORED IN THE LINEAR ARRAY FIRST. MS000260
C ADDRESSES OF THE LINEAR ARRAY ELEMENTS CONTAINING THE MAIN DIAGONAL
C TERMS ARE STORED IN MD. MS000280
C EXAMPLE: LET B BE THE SIX FULL SYMMETRIC MATRIX BELOW... MS000300
C
C | 1 | 5 | | 12 |
C | | 2 | 5 | | 11 | NOTE: BK(1,5),BK(1,4) AND BK(2,4) ARE ZERO. MS000340
C | | | 4 | 7 | 10 |
C | | | | 6 | 9 | MD= 1, 2, 4, 6, 8, 15 MS000350
C | | | | | 8 |
C-----
C THUS, BK(5,5)=AK(MDK5) = AK(4) MS000380
C BK(1,5)=AK(MDK5)-J-I IF J-I AND (MDKJ)-J-I>(MDKJ+1) MS000390
C =0 IF J-I AND (MDKJ)-J-I>(MDKJ+1) MS000400
C -MATRIX P IS NOT SYMMETRIC, AND IS STORED AS A FULL MATRIX MS000410
C-----
C VARIABLE TABLE:
C IOPT = OPTION NUMBER MS000440
C N = NUMBER OF DEGREES OF FREEDOM OF A MATRIX MS000450
C NLC = NUMBER OF LOAD CASES FOR THE P MATRIX MS000460
C L1 = FIRST ROW TO BE WORKED WITH MS000470
C L2 = LAST ROW TO BE WORKED WITH MS000480
C MD = ADDRESS OF THE MAIN DIAGONAL TERMS OF A MS000490
C P = LOAD MATRIX ON INPUT, SOLN (X) OF AX=P ON COMPLETION OF MS000500
C IOPT= MS000510
C FACTOR= TEMPORARY STORAGE MATRIX MS000520
C GUYAN = GUYAN REDUCTION FLAG FOR MASS MATRIX MS000530
C MASS= MASS MATRIX MS000540
C MDMASS= MASS MATRIX ADDRESSES OF MAIN DIAGONAL ELEMENTS MS000550
C KCOND= FLAG FOR CONDENSING OUT KG MS000560
C KG = GEOMETRIC STIFFNESS MATRIX MS000570
C MDKG = KG MATRIX ADDRESSES OF MAIN DIAGONAL ELEMENTS MS000580
C I = ROW NUMBER FOR ELIMINATION MS000590
C J = ROW NUMBER MS000600
C K = COLUMN NUMBER MS000610
C-----
L1=MAX(L1,I)
L2=MIN(L2,N)
C
GO TO (10,110,210,310),IOPT
10 CONTINUE
C-----
IOPT=1, REDUCE A AND P MS000700
C GAUSSIAN ELIMINATION IS USED TO REDUCE THE A AND P MATRICES MS000710
C FROM ROW L1 TO ROW L2. IF L1 IS NOT 1, IT IS ASSUMED THAT MS000720
C A AND P ARE ALREADY REDUCED FROM 1 TO L1... MS000730
C-----
IF (PRINT) THEN
  WRITE (6,500) 'IOPT=1, REDUCE STIFFNESS AND LOADS',L1,L2,N MS000750
  CALL LMATRK(L1,N,MD,'INPUT STIFFNESS') MS000760
  CALL LMATRK(P,N,NLC,'INPUT LOADS') MS000780
  IF (GUYAN) CALL LMATRK(MASS,MDMASS,N,INDMAS,'INPUT MASS') MS000790
  IF (KCOND) CALL LMATRK(KG,MDKG,N,INDKG,'INPUT KG ') MS000800
ENDIF
C
DO 100 L=L1,L2
  IF (L.EQ.N) GO TO 100
C-----
TEST FOR ZERO PIVOT..... MS000910
IF (AK(MDK(L),L.E.0) THEN MS000920
  WRITE (6,2000) L,MDK(L),AK(MDK(L)) MS000930
  ABORT=.TRUE. MS000940
  RETURN MS000950
ENDIF
C-----
CALCULATE THE FACTORS EACH ROW IS MULTIPLIED BY
DO 50 I=L+1,N
  LI=I,K=L,I
  IF (L1.LT.MDK(I+1)) THEN MS001040
    FACTOR(I)=AK(LI)/AK(MDK(I)) MS001050
  ELSE MS001060
    FACTOR(I)=0 MS001070
  50 CONTINUE MS001080
C-----
REDUCE A BY COLUMNS (J) EACH ROW (I)... MS001100
DO 40 I=L+1,N MS001110
  LI=I,K=L,I MS001120
  IF (LI.GE.MDK(J+1)) GO TO 40 MS001140
  DO 35 I=(L+1),J MS001150
    IJ=I,K(I,J)
    AK(IJ)=AK(IJ)-FACTOR(I)*AK(LJ) MS001160
  35 CONTINUE MS001180
  40 CONTINUE MS001190
C-----
REDUCE P BY COLUMNS (J) EACH ROW (I)... MS001210
DO 50 J=L,NLC MS001230
  IF (PC(L,J).EQ.0) GO TO 50 MS001240
  DO 45 I=(L+1),N MS001250
    PC(I,J)=PC(I,J)-FACTOR(I)*PC(L,J) MS001260
  50 CONTINUE MS001270
C-----
REDUCE MASS MATRIX BY GUYAN REDUCTION
IF (GUYAN) THEN
C-----
M22=M22 + K21/K11 * M11 * 1/K11 + K12
RM=MASS(MMASS(L))
IF (RM.NE.0) THEN
  DO 60 J=L+1,N
    IF (FACTOR(J).EQ.0) GO TO 60
    I1=MAX(L+1,(MDMASS(J+1)-MDMASS(J))
    DO 55 I=L1,J
      IJ=I,K(I,J)
      MASS(IJ)=FACTOR(I)*RM*FACTOR(J)
  60 CONTINUE
ENDIF
C-----
M22=M22 - K21/K11 * M12
DO 66 J=L+1,N
  LI=I,K(L,J)
  IF (LI.GE.MDMASS(J+1)) GO TO 66
  IF (MASS(LJ).EQ.0) GO TO 66
  DO 65 I=L+1,J
    IJ=I,K(I,J)
    MASS(IJ)=MASS(IJ)-FACTOR(I)*MASS(LJ)
  65 CONTINUE

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66 CONTINUE
C
C..... M22=M22 - K21 / K11 * K12
DO 70 J=L+1,N
  IF (FACTOR(J).EQ.0) GO TO 70
  DO 69 I=L+1,J
    L=I,K=L,I
    IF (LJ.GE.NOMASS(I+1)) GO TO 69
    I=I,K=L,I
    IF (I.J.LT.NOMASS(J+1))
      MASS(I)=MASS(I)-FACTOR(J)*MASS(L)
  &
  CONTINUE
70 CONTINUE
ENDIF
C
C----- REDUCE GEOMETRIC STIFFNESS MATRIX
IF (KGCMD) THEN
C
C..... KQ22=KQ22 + K21/K11 * KQ11 * 1/K11 * KQ12
RK6=KQ22/KQ12
IF (RK6.NE.0) THEN
  DO 80 J=L+1,N
    IF (FACTOR(J).EQ.0) GO TO 80
    I=MAX(L+1,J)-(MOK(J+1)-MOK(J))
    DO 75 I=I,J
      I=I,K=I,J
      KQ(I)=KQ(I)+FACTOR(I)*RK6*FACTOR(J)
    &
    CONTINUE
75 CONTINUE
80 CONTINUE
ENDIF
C
C..... KQ22=KQ22 - K21/K11 * KQ12
DO 86 J=L+1,N
  L=I,K=L,I
  IF (LJ.GE.MOK(J+1)) GO TO 86
  IF (KQ(L).EQ.0) GO TO 86
  DO 85 I=L+1,J
    I=I,K=L,I
    IF (I.J.LT.MOK(J+1))
      KQ(I)=KQ(I)-FACTOR(I)*KQ(L)
  &
  CONTINUE
85 CONTINUE
86 CONTINUE
C
C..... KQ22=KQ22 - KQ21 * 1/K11 * K12
DO 90 J=L+1,N
  IF (FACTOR(J).EQ.0) GO TO 90
  DO 89 I=L+1,J
    L=I,K=L,I
    IF (LJ.GE.MOK(I+1)) GO TO 89
    I=I,K=L,I
    IF (I.J.LT.MOK(J+1))
      KQ(I)=KQ(I)-FACTOR(J)*KQ(L)
  &
  CONTINUE
89 CONTINUE
90 CONTINUE
ENDIF
C
100 CONTINUE
IF (PRINT) THEN
  CALL LMATRX(A,N,D,'REDUCED STIFFNESS')
  CALL LMATRX(P,N,MLC,'REDUCED LOAD')
  IF (GUYAN) CALL LMATRX(MASS,NOMASS,N,DMAS,'REDUCED MASS')
  IF (KGCMD) CALL LMATRX(KG ,MOKG ,N,DMOKG , 'REDUCED KG')
ENDIF
RETURN
C
110 CONTINUE
C----- TOPT=2, REDUCE P ONLY
GAUSSIAN ELIMINATION IS USED TO REDUCE THE P MATRIX
FROM ROW 1 TO ROW L2. IF L1 IS NOT 1, IT IS ASSUMED THAT
A AND P ARE ALREADY REDUCED FROM 1 TO L1...
IF (PRINT) THEN
  WRITE (6,500) 'TOPT=2, REDUCE LOADS ONLY' ,L1,L2,N
  CALL LMATRX(A,N,D,MOKN+1,'REDUCED STIFFNESS')
  CALL LMATRX(P,N,MLC,'NEW LOAD MATRIX')
ENDIF
C
C----- LOOP FOR EACH ROW (L) TO REDUCE....
DO 160 J=L1,L2
  IF (ACMOK(J).LE.0) THEN
    WRITE (6,2000) L,MOK(L),ACMOK(J)
    ABORT=.TRUE.
    RETURN
  &
  CONTINUE
  LOOP FOR EACH COLUMN (J)
  DO 150 J=L1,MLC
    IF (P(L,J).EQ.0) GO TO 150
    DO 120 I=L+1,N
      I=I,K=L,I
      IF (I.J.LT.MOK(I+1)) P(I,J)=P(I,J)-AK(L)*P(L,J)/ACMOK(J)
    &
    CONTINUE
120 CONTINUE
150 CONTINUE
160 CONTINUE
RETURN
C
210 CONTINUE
C----- TOPT=5, BACK SUBSTITUTION
BACK SUBSTITUTION IS USED TO SOLVE FOR X IN SX=V, WHERE S IS
THE REDUCE UPPER TRIANGULAR FACTOR OF THE A MATRIX, AND V
IS THE REDUCED FORM OF THE P MATRIX. THE RESULTS (X) ARE
STORED IN P.
BACK SUBSTITUTION ONLY TAKES PLACE BETWEEN ROWS L1 AND L2.
IF (PRINT) THEN
  WRITE (6,500) 'TOPT=5, BACK SUBSTITUTION' ,L1,L2,N
  CALL LMATRX(A,N,D,MOKN+1,'REDUCED STIFFNESS')
  CALL LMATRX(P,N,MLC,'REDUCED LOAD')
ENDIF
C
C----- LOOP FOR EACH ROW L
DO 215 J=L1,MLC
  CALCULATE X FOR EACH LOAD CASE, STORE IN P
  DO 250 J=L2,L1,-1
    IF (ACMOK(J).LE.0) THEN
      WRITE (6,2000) J,MOK(J),ACMOK(J)
      CALL ERRTRA
      ABORT=.TRUE.
      RETURN
    &
    CONTINUE
    DO 215 LC=1,MLC
      P(J,LC)=P(J,LC)/ACMOK(J)
    &
    CONTINUE
215 CONTINUE

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SUBROUTINE MODOP(MODP,MODND,MPRE,MPRES,MAXMOD,MADE,MCOS,
&
  SLE,NSUP,ICMOP,
&
  ID,IDOF,INDEX,COORD,COSINE,CONST,
&
  JFLG,JTCOS,BUG,NSTRJT)
C
DIMENSION COORD(MAXMOD,5),IDX(MAXMOD),INDEX(MAXMOD),JFK(6),
&
  IDOF(MAXMOD,6),COSINE(5,5,MLCS),CONST(MAXMOD,6),
&
  JFLG(MAXMOD),JTCOS(MAXMOD),NSTRJT(MAXMOD,6)
C
DIMENSION VK(5),VK(5),VZ(5)
LOGICAL FLAG,PT,BUG,TEST,BTEST
CHARACTER*15 TYPE
CHARACTER*2 CX(6)
C
C VARIABLE TABLE...
C COORD = JOINT COORDINATES X,Y,Z
C ID = JOINT NUMBER
C IDOF = GLOBAL DEGREES OF FREEDOM ASSOC. WITH JOINT FX,FY,FZ,MX,MV,MZ
C JTCOS = ROW IN COSINE MATRIX ASSOC WITH JOINT
C COSINE = COSINE MATRIX
C CONST = GLOBAL CONSTRAINT MATRIX FOR EACH NODE
C JFLG = CONTAINS JOINT FLAG'S - MUST BE 2* BIT'S LONG.....
C BIT'S 0 TO 5 RESTRAIN DOF FX,FY,FZ,MX,MV,MZ
C BIT'S 6 TO 11 CONDENSE DOF FX,FY,FZ,MX,MV,MZ
C BIT'S 12 TO 17 CONSTRAINT DOF FX,FY,FZ,MX,MV,MZ
C BIT'S 18 TO 25 ELIMINATE DOF FX,FY,FZ,MX,MV,MZ
C NSTRJT = INTERNAL MASTER JT # OF CONSTRAINED JOINTS.....
C
C INPUT NODES
IF (BUG) WRITE (6,1000) 'INPUT NODES'
L=0
DO I=1
  READ (5,*) IDX(I),COORD(I,J),J=1,5),JTCOS(I),IGEN
  IF (IDX(I).LE.0) THEN
    NNODE=I-1
    GO TO 26
  &
  CONTINUE
  ENDOF
  IF (BUG) WRITE(6,50) I,IDX(I),COORD(I,J),J=1,5),JTCOS(I)
  IF (IGEN.GT.0) THEN
    READ (5,*) IDING,COORD1,COORD2,COORD3
    DO 25 K=1,IGEN
      I=I+1
      IDX(I)=IDX(I-1)+IDING
      IF (IDX(I).LE.0) THEN
        NNODE=I-1

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      GO TO 26
    ENDIF
    COORD(I,1)=COORD(I-1,1)+COORD1
    COORD(I,2)=COORD(I-1,2)+COORD2
    COORD(I,3)=COORD(I-1,3)+COORD3
    JTCOS(I)=JTCOS(I-1)
25  IF (BUG) WRITE(6,30) I,IDX(I),COORD(I,J),J=1,5,JTCOS(I)
    ENDIF
    IF (I.LT.NNODE) GO TO 20
26  CONTINUE
C----- SORT NODES
C----- CALL ISORT(ID,INDEX,NNODE)
C----- MOVE NODE INFO. TO TEMPORARY STORAGE
DO 40 I=1,NNODE
  J=INDEX(I)
  IDOF(I,1)=IDX(J)
  IDOF(I,2)=JTCOS(J)
  IDOF(I,3)=JTCOS(J)
  IDOF(I,4)=JTCOS(J)
  IDOF(I,5)=JTCOS(J)
  DO 40 K=1,5
    CONST(I,K)=COORD(J,K)*SCALE
40  CONTINUE
C----- MOVE NODES INFO BACK TO MAIN STORAGE, DELETE DUPLICATE INFO.
NNOLD=NNODE
I=0
J=0
45  I=I+1
  J=J+1
  IDX(I)=IDOF(J,1)
  IF (I.GE.2) THEN
    IF (IDX(I).EQ.IDX(I-1)) THEN
      I=I-1
      NNODE=NNODE-1
    ENDIF
  ENDIF
  JTCOS(I)=IDOF(J,2)
  DO ** K=1,5
    COORD(I,K)=CONST(J,K)
44  IF (I.LT.NNODE) GO TO 45
50  FORMAT(' NODE',I3,' I4,' X',F10.4,' Y',F10.4,' Z',F10.4,
  & ' ' COSR',I3)
C----- GLOBAL JOINT COSINE MATRIX
IF (BUG) WRITE(6,1000) 'DIRECTION COSINES ...'
DO 55 ICOS=1,NCOS
  READ(5,*) VX,VY
  CALL CROSS(VZ,VX,VY,0)
  CALL CROSS(VY,VZ,VX,1)
  DO 50 J=1,5
    COSINE(1,J,ICOS)=VX(J)
    COSINE(2,J,ICOS)=VY(J)
    COSINE(3,J,ICOS)=VZ(J)
50  IF (BUG) WRITE(6,56) ICOS,' VX',VX,' VY',VY,' VZ',VZ
55  FORMAT(' COS',I3,' '
  & ' SCA,SS,F9.5,' I',SP,F9.5,' J',F9.5,' K ',SS)
C----- INPUT RESTRAINTS
ZERO IDOF MATRIX WHICH WILL HOLD RESTRAINT, CONSTRAINT AND
ULTIMATELY DOF INFORMATION
DO 59 I=1,NNODE
59  JTLG(I)=0
  I=0
  FLAG=.TRUE.
60  I=I+1
  IF (I.LE.NISRT) THEN
    IF (FLAG.AND.BUG) WRITE(6,1000) ' NODE RESTRAINTS '
    FLAG=.FALSE.
    READ(5,*) NODE,IFN,IGEN,NOIDMC
65  IF (NODE.EQ.0) THEN
    DO 70 J=1,NNODE
      DO 68 II=1,6
        IF (IFPK(II).NE.0) JTLG(J)=IBSET(JTLG(J),II-1)
        IF (IFPK(II).EQ.2) JTLG(J)=IBSET(JTLG(J),II+1)
68  CONTINUE
        IF (BUG) WRITE(6,80) IDX(J),IFN
70  CONTINUE
      ELSE
        J=IQUICK(NODE,ID,NNODE)
        IF (J.EQ.0) THEN
          IF (BUG) WRITE(6,75) NODE
          ELSE
            DO 71 II=1,6
              IF (IFPK(II).NE.0) JTLG(J)=IBSET(JTLG(J),II-1)
              IF (IFPK(II).EQ.2) JTLG(J)=IBSET(JTLG(J),II+1)
71  CONTINUE
              IF (BUG) WRITE(6,80) IDX(J),IFN
            ENDIF
            IF (IGEN.GT.0) THEN
              NODE=NODE+NOIDMC
              IGEN=IGEN-1
              GO TO 65
            ENDIF
            GO TO 60
          ENDIF
        75  FORMAT(' NODE',I3,' NOT FOUND, RESTRAINT IGNORED...')
        80  FORMAT(' NODE',I4,' ' FX',I2,' FY',I2,' FZ',I2,
          & ' ' MZ',I2,' ' NV',I2,' ' NZ',I2)
      C----- INPUT NODE DOF'S TO BE CONDENSED OUT...
      I=0
      FLAG=.TRUE.
90  I=I+1
      IF (I.LE.NCOND) THEN
        IF (FLAG.AND.BUG)
          & WRITE(6,1000) ' NODE DOF'S TO BE CONDENSED OUT '
        FLAG=.FALSE.
        READ(5,*) NODE,IFN,IGEN,NOIDMC
95  IF (NODE.EQ.0) THEN
          DO 100 J=1,NNODE
            PT=.FALSE.
            DO 99 II=1,6
              IF (IFPK(II).NE.0.AND. .NOT.BTEST(JTLG(J),II-1)) THEN
                JTLG(J)=IBSET(JTLG(J),II+5)
                IFPK(II)=IFPK(II)
                PT=.TRUE.
            ELSE
              IFPK(II)=0
            ENDIF
          ENDIF
          CONTINUE
          99  IF (PT.AND.BUG) WRITE(6,80) IDX(J),IFN
        100

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ENDIF
510 CONTINUE
NFREE=NDOF-NCOND
C.....RESTRAINED DEGREES OF FREEDOM
DO 530 I=1,NDOF
DO 530 J=1,6
IF (BTEST(JTFLG(I),J-1) .AND. .NOT.BTEST(JTFLG(I),J+1))
& .AND. .NOT.BTEST(JTFLG(I),J+1)) THEN
NDOF=NDOF-1
IDOF(I,J)=NDOF
ENDIF
530 CONTINUE
C.....RESTRAINED DEGREES OF FREEDOM
DO 535 I=1,NDOF
DO 535 J=1,6
IF (BTEST(JTFLG(I),J+1) .AND. .NOT.BTEST(JTFLG(I),J+1)) THEN
NDOF=NDOF-1
IDOF(I,J)=NDOF
ENDIF
535 CONTINUE
NREST=NDOF-NFREE-NCOND
C.....CONSTRAINED DEGREES OF FREEDOM
I = NODE ID OF SLAVE NODE
II = NODE ID OF MASTER NODE
DO 520 I=1,NDOF
DO 520 J=1,6
... CHECK DOF FOR CONSTRAINT ...
IF (BTEST(JTFLG(I),J+1)) THEN
... DETERMINE MASTER NODE AND DOF ...
II=I
NODE=IDOF(I,J)
II=STRJ(II,J)
IF (II.EQ.0) THEN
WRITE (6,525) NODE,II,J
IDOF(I,J)=0
GO TO 520
ENDIF
IF (BTEST(JTFLG(II),J+1)) GO TO 515
IDOF(I,J)=IDOF(II,J)
... CHECK FOR DIFFERENT JOINT COORDINATE SYSTEMS ...
IF (JTCOS(I).NE.JTCOS(II)) THEN
WRITE (6,411) ID(I),ID(II)
FORMAT(' CONFLICTING COSINE ID NUMBERS, MASTER:',
& ' SLAVE:',I6,' CORRECT INPUT & RECAL...')
ENDIF
... CALCULATE THE CONSTRAINT MATRIX ...
IF (J.GE.4) THEN
NG=COORD(I,1)-COORD(II,1)
VG=COORD(I,2)-COORD(II,2)
ZG=COORD(I,3)-COORD(II,3)
W=COS(JTCOS(I))
VMS=COSINE(1,1,N)*NG+COSINE(1,2,N)*VG+COSINE(1,3,N)*ZG
VNS=COSINE(2,1,N)*NG+COSINE(2,2,N)*VG+COSINE(2,3,N)*ZG
ZMS=COSINE(3,1,N)*NG+COSINE(3,2,N)*VG+COSINE(3,3,N)*ZG
ENDIF
IF (J.EQ.4) THEN
CONST(I,1)=ZMS
CONST(I,2)=VMS
ELSE IF (J.EQ.5) THEN
CONST(I,3)=ZMS
CONST(I,4)=VMS
ELSE IF (J.EQ.6) THEN
CONST(I,5)=VMS
CONST(I,6)=ZMS
ENDIF
ENDIF
520 CONTINUE
525 FORMAT(' NODE#',I6,' NOT FOUND WHILE ASSIGNING CONSTRAINED',
& ' DOF TO NODE#',I6,' DOF#',I2,' --- DOF IS DELETED ')
C.....PRINT OUT ORDERED NODE INFO, AND DEGREES OF FREEDOM
WRITE (6,1000) 'NODE COORDINATES AND DEGREES OF FREEDOM'
WRITE (6,600) NDOF,NCOND,NFREE,NREST
600 FORMAT
& 4X,'TOTAL NUMBER OF DEGREES OF FREEDOM.....',I6,/,
& 4X,'NUMBER OF DEGREES OF FREEDOM CONDENSED OUT.....',I6,/,
& 4X,'NUMBER OF FREE DEGREES OF FREEDOM.....',I6,/,
& 4X,'NUMBER OF RESTRAINED DEGREES OF FREEDOM.....',I6,/,
& 4X,' NODE COS#',4X,'X-COORD',6X,'Y-COORD',6X,'Z-COORD',4X,
& 4X,'FX',6X,'FY',6X,'FZ',6X,'MX',6X,'MY',6X,'MZ')
DO 610 I=1,NDOF
DO 605 J=1,6
IF (BTEST(JTFLG(I),J-1)) THEN
CK(J)=R
ELSE IF (BTEST(JTFLG(I),J+1)) THEN
CK(J)=-C
ELSE
CK(J)=0
ENDIF
605 CONTINUE
610 WRITE(6,620) ID(I),JTCOS(I),(COORD(I,J),J=1,5),
& (IDOF(I,K),CK(K),K=1,6)
620 FORMAT(4X,I6,1P,15,3L5.5,0P,6(I6,A2))
WRITE(6,625)
625 FORMAT(10X,'NOTE: R = RESTRAINED DEGREE OF FREEDOM',/
& ' 10X' C = CONSTRAINED DEGREE OF FREEDOM')
C.....PRINT OUT CONSTRAINT MATRIX
IF (FLAG.TRUE) THEN
DO 540 I=1,NDOF
TEST=.FALSE.
DO 536 J=1,6
TEST = TEST .OR. BTEST(JTFLG(I),J+1)
IF (TEST) THEN
IF (FLAG) WRITE (6,1000) 'NODE CONSTRAINT MATRIX'
FLAG=.FALSE.
WRITE(6,550) ID(I),(CONST(I,J),J=1,6)
ENDIF
540 CONTINUE
550 FORMAT(4X,I6,1P,
& ' I12:',G12.5, ' I13:',G12.5,
& ' I21:',G12.5, ' I23:',G12.5,
& ' I31:',G12.5, ' I32:',G12.5)
ENDIF
C.....PRINT OUT DIRECTION COSINES

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WRITE (6,1000) 'DIRECTION COSINES ...'
DO 560 I=1,NDOF
WRITE (6,56) ICOS, ' VK:',(COSINE(1,J,ICOS),J=1,3),
& ' VV:',(COSINE(2,J,ICOS),J=1,3),
& ' VZ:',(COSINE(3,J,ICOS),J=1,3)
560 CONTINUE
RETURN
1000 FORMAT (//,5X,A//)
END
C.....SUBROUTINE PSIT(MODE,JTFLG,II)
SUBROUTINE PSIT(MODE,JTFLG,II)
DIMENSION JTFLG(NDOF),IX(NDOF)
LOGICAL FLAG(O:5)
LOGICAL BTEST
WRITE (6,40)
40 FORMAT (1X,' RESTRAINT', ' CONDENSE', ' CONSTR', ' ELIMINATE',/
& ' 14X,4X,' FFFMM',/14X,4X,' VVZVZ')
DO 20 I=1,NDOF
DO 10 J=0,25
10 FLAG(J)=BTEST(JTFLG(I),J)
20 WRITE (6,30) ID(I),(FLAG(K),K=0,25),JTFLG(I)
30 FORMAT (' NODE(',I4,')',4(4X,G11),110)
RETURN
END
C.....SUBROUTINE REACTK(IOPT,PRINT,NDOF,L1,L2,L3,L4,FORCE,DISPL,
& MD,A,KH,NDOF,NLOAD,FACTOR,
& MANNOD,IDOF,COORD,ID,TITLE,STEPID,HEAD,
& MCOS,COSINE,JTCOS,JTFLG,SUM)
SUBROUTINE REACTK(IOPT,PRINT,NDOF,L1,L2,L3,L4,FORCE,DISPL,
& MD,A,KH,NDOF,NLOAD,FACTOR,
& MANNOD,IDOF,COORD,ID,TITLE,STEPID,HEAD,
& MCOS,COSINE,JTCOS,JTFLG,SUM)
DIMENSION AK(N),MD(NDOF,1)
DIMENSION FORCE(NDOF,NLOAD),DISPL(NDOF,NLOAD)
DIMENSION IDOF(MANNOD,6)
DIMENSION IDX(MANNOD),COORD(MANNOD,5)
DIMENSION F(6),G(6),SUM(6),COSINE(5,5,NDOF),JTCOS(MANNOD)
DIMENSION JTFLG(MANNOD)
CHARACTER(*) TITLE(2),STEPID
CHARACTER*15 CK(6)
LOGICAL PRINT,HEAD,FLAG,BTEST
C.....IF (IOPT.EQ.1) THEN
C.....MODIFY LOADS FOR RESTRAINT DISPLACEMENTS
C.....CONSIDER THE PARTITIONED STIFFNESS WHERE X2 ARE THE RESTRAINT DISPL.
C.....
C I11 | K11 | K12 | K13
C I-1 | | | |
C I21 | K21 | K22 | K23
C.....THE MODIFIED FREE LOAD IS (P1-K12*X2) = K11*X1
C.....
C DO 10 I=L1,L2 C FULL STORAGE
C DO 10 J=L1,NLOAD C EQUIVALENT
C DO 10 K=L3,L4
C 10 FORCE(I,J)=FORCE(I,J)-(K1,K)*DISPL(K,J)
C.....
C DO 20 K=L3,L4
C MK=MK+K+1
C DO 10 I=L2,L1,-1
C IK=MK+K+1
C IF (IK.EQ.MK) GO TO 20
C FTJ=FORCE(I,J)
C AK=AK+IK
C DKJ=DISPL(K,J)
C 10 FORCE(I,J)=FORCE(I,J)+AK*DKJ
C 20 CONTINUE
C IF (PRINT)
C & CALL WMATRX(FORCE,NDOF,NLOAD,'MODIFIED LOADS')
C.....ELSE IF (IOPT.EQ.2) THEN
C.....
C.....SOLVE FOR REACTIONS
C.....CONSIDER THE PARTITIONED STIFFNESS WHERE X2 ARE THE RESTRAINT DISPL.
C.....
C I11 | K11 | K12 | K13
C I-1 | | | |
C I21 | K21 | K22 | K23
C.....THE REACTIONS ARE P2 = P2 + (K21*X1 + K22*X2) * FACTOR
C NOTE: BOTH P1 AND P2 CONTAIN FIXED END FORCES FROM MEMBER LOADS...
C THUS, K21*X1 + K22*X2 IS ADDED TO P2 TO GET THE REACTIONS.
C.....
C DO 120 I=L3,L4 C FULL STORAGE
C DO 120 J=L1,NLOAD C MODE EQUIVALENT
C FORCE(I,J)=0 * P2 CONTAINS FEF!!!
C DO 110 K=L1,L2
C 110 FORCE(I,J)=FORCE(I,J)+K(I,K)*DISPL(K,J)
C DO 120 K=L3,L4
C 120 FORCE(I,J)=FORCE(I,J)+K(I,K)*DISPL(K,J)
C.....
C DO 100 J=L1,NLOAD
C DO 100 I=L3,L4
C 100 FORCE(I,J)=0
C.....
C DO 120 I=L3,L4
C DO 120 J=L1,NLOAD
C DO 110 K=L2,L1,-1
C KI=MD(I)-I-K
C IF (KI.EQ.MDI+1) GO TO 120
C AK=AK+KI
C 110 FORCE(I,J)=FORCE(I,J)+AK*DISPL(K,J)*FACTOR
C 120 CONTINUE
C.....
C DO 140 I=L3,L4
C DO 140 K=L3,L4
C IF (I.LE.K) THEN
C IK=MK+K-I
C MK=MK+K+1
C ELSE
C IK=MK+I-K
C MK=MK+I+1
C ENDIF
C IF (IK.EQ.MK) GO TO 140
C AK=AK+IK
C DO 150 J=L1,NLOAD
C 150 FORCE(I,J)=FORCE(I,J)+AK*DISPL(K,J)*FACTOR
C 140 CONTINUE
C.....IF (PRINT)

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NDOF+230
NDOF+240
NDOF+250
NDOF+260
NDOF+270
NDOF+280
NDOF+290
NDOF+300
NDOF+310
NDOF+320
PBI00010
PBI00040
PBI00050
PBI00060
PBI00070
PBI00080
PBI00090
PBI00100
PBI00110
PBI00120
PBI00130
PBI00140
PBI00150
PBI00160
PBI00170
PBI00180
PBI00190
PBI00200
PBI00210
PBI00220
PBI00230
PBI00240
PBI00250
PBI00260
PBI00270
PBI00280
PBI00290
PBI00300
PBI00310
PBI00320
PBI00330
PBI00340
PBI00350
PBI00360
PBI00370
PBI00380
PBI00390
PBI00400
PBI00410
PBI00420
PBI00430
PBI00440
PBI00450
PBI00460
PBI00470
PBI00480
PBI00490
PBI00500
PBI00510
PBI00520
PBI00530
PBI00540
PBI00550
PBI00560
PBI00570
PBI00580
PBI00590
PBI00600
PBI00610
PBI00620
PBI00630
PBI00640
PBI00650
PBI00660
PBI00670
PBI00680
PBI00690
PBI00700
PBI00710
PBI00720
PBI00730
PBI00740
PBI00750
PBI00760
PBI00770
PBI00780
PBI00790
PBI00800
PBI00810
PBI00820
PBI00830
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PBI00860
PBI00870
PBI00880
PBI00890
PBI00900
PBI00910
PBI00920
PBI00930
PBI00940
PBI00950
PBI00960
PBI00970
PBI00980
PBI00990
PBI01000
PBI01010
PBI01020

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DO 25 K=1,3
  CTXVZ(I,J)=CTXVZ(I,J) + XVZ(I,K)*CT(K,J)
C
C ----- SKIP THE MEMBER END ECCENTRICITY MATRIX IF EX=EV=EZ=0
  IF (EX.EQ.0 .AND. EV.EQ.0 .AND. EZ.EQ.0) RETURN
C
C ----- CALC THE MEMBER END ECCENTRICITY MATRIX
  XVZ(1,1)=.0
  XVZ(1,2)=EZ
  XVZ(1,3)=EV
  XVZ(2,1)=EZ
  XVZ(2,2)=.0
  XVZ(2,3)=EK
  XVZ(3,1)=EV
  XVZ(3,2)=EK
  XVZ(3,3)=.0
C
C ----- CALC THE MEMBER END ECCENTRICITY MATRIX
  DO 50 I=1,3
    DO 50 J=1,3
      DO 50 K=1,3
        CTXVZ(I,J)=CTXVZ(I,J) + CT(K,I)*XVZ(K,J)
C
  RETURN
END
C
SUBROUTINE SKVLNK(IOPT,NDOF,IBUG,TITLE,MOIAG,IELDOF,LM,SE,NO,NAME)
  DIMENSION MOIAG(NDOF+1)
  DIMENSION IELDOF(1),LMK(IELDOP),SE,IELDOF*(IELDOF+1)/2)
  LOGICAL BTEST
  CHARACTER*(*) NAME,TITLE(2)
  CHARACTER*1 CK(100)
  LOGICAL PT,BUG
C
  IF (IOPT.EQ.1) THEN
    DO 10 I=1,NDOF+1
      MOIAG(I)=I
    IF (BTEST(BUG,12)) THEN
      WRITE(6,*) 'INITIAL VALUES'
      WRITE(6,220) (I,MOIAG(I),I=1,NDOF)
    ENDIF
  ELSE IF (IOPT.EQ.2) THEN
    DETERMINE THE SKYLINE OF THIS ELEMENT, AND MODIFY THE
    GLOBAL SKYLINE...
    C ..... I = THE ROW OF THE MEMBER STIFFNESS MATRIX
    C ..... J = THE COLUMN OF THE MEMBER STIFFNESS MATRIX
    C ..... IJ = THE ADDRESS OF THE MEMBER STIFFNESS TERM I,J
    C ..... LMI = THE ROW OF THE GLOBAL STIFFNESS MATRIX CORRESPONDING
    TO ROW I OF THE MEMBER STIFFNESS MATRIX
    C ..... LMJ = THE COLUMN OF THE GLOBAL STIFFNESS MATRIX CORRESPONDING
    TO COLUMN J OF THE MEMBER STIFFNESS MATRIX
    C ..... MOIAG(JJ) = THE JJ'TH ELEMENT OF THE GLOBAL SKYLINE MATRIX.
    AT THIS POINT THE GLOBAL SKYLINE MATRIX CONTAINS THE
    LOWEST ROW NUMBER THAT CONTAINS A NON-ZERO STIFFNESS
    TERM.
    DO 250 I=1,IELDOF
      LMI=LMK(I)
      IF (LMI.LE.0) GO TO 250
      DO 240 J=1,IELDOF
        LMJ=LMK(J)
        IF (LMJ.LE.0) GO TO 240
        IJ=NDK(J)+J-I
        IF (SE(IJ).EQ.0) GO TO 240
        IF (LMI.LE.LMJ) THEN
          MOIAG(LMJ)=MIN(MOIAG(LMJ),LMI)
        ELSE
          MOIAG(LMI)=MIN(MOIAG(LMI),LMJ)
        ENDIF
      CONTINUE
    CONTINUE
  ELSE IF (IOPT.EQ.3) THEN
    CALCULATE THE INDICES OF THE MAIN DIAGONAL TERMS...
    IF (BTEST(BUG,12)) THEN
      WRITE(6,*) 'AFTER COLUMN HEIGHTS'
      WRITE(6,220) (I,MOIAG(I),I=1,NDOF)
    ENDIF
    MOIAG(1)=1
    ICOLHT=1
    DO 310 IROW=2,(NDOF+1)
      ILOC=ICOLHT + MOIAG(IROW-1)
      ICOLHT(IROW)=MOIAG(IROW-1)
    310 MOIAG(IROW)=ILOC
    IF (BTEST(BUG,12)) THEN
      WRITE(6,*) 'ADDRESS OF MAIN DIAGONAL ELEMENTS'
      WRITE(6,220) (I,MOIAG(I),I=1,NDOF)
    520 FORMAT (' MOIAG',I5,' ',I5)
    ENDIF
    521 FORMAT (Z16)
  IF (.NOT.(BTEST(BUG,12) .OR. BTEST(BUG,9))) RETURN
  PRINT A MAP OF THE STIFFNESS ARRAY
  NL=MOIAG(NDOF+1)-MOIAG(1)+1
  NR=NDOF/100
  NP=NDOF/100
  NP=NDOF/100
  IF (NR.GT.0) NP=NP+1
  DO 270 IP=1,NP
    JCL=IP-1*100
    J2=MIN(IP*100,NDOF)
    J2=100
    IF (IP.EQ.NP) J2=NR
    WRITE(6,290) TITLE(1),TITLE(2),NAME,ML,(I,I=JCL,J2,10)
    DO 270 I=1,NDOF
      PT=FALSE
      DO 260 J=1,J2
        J=J+(IP-1)*100
        IJ=MOIAG(J)+J-I
        IF (I.J.LT.MOIAG(J+1) .AND. I.LT.J) THEN
          CK(JJ)=X
          PT=.TRUE.
        ELSE IF (I.EQ.J) THEN
          CK(JJ)=D
          PT=.TRUE.
        ELSE
          CK(JJ)=.
        ENDIF
      CONTINUE
    270 IF (PT) WRITE(6,295) I,(CK(J),J=1,J2)
  290 FORMAT ('1 STRUCTURE.....',A,/,
    & ' SOLUTION.....',A,/)

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ROTO1140 & ' SKYLINE OF THE 'A.' MATRIX ' /
ROTO1150 & ' THE MATRIX REQUIRES',16,' STORAGE LOCATIONS',
ROTO1160 & /ZK,12(I4,'!.....')
ROTO1170 295 FORMAT (16,15ZAL)
ROTO1180
ROTO1190 C
ROTO1200 ENDIF
ROTO1210 RETURN
ROTO1220 END
C
SUBROUTINE SKVLNK(NDOF,LS,14,NDK,NO,NDMASS,NDKG,KGFORM)
  DIMENSION NDMASS(NDOF+1),NDK(NDOF+1),NDKG(NDOF+1)
C
C ----- DEVELOP SKYLINE OF DYNAMIC STIFFNESS (S)
ROTO1280
ROTO1290 C ..... MDS(I) = ADDRESS OF DYNAMIC STIFF. MAIN DIAGONAL TERM ROW I
ROTO1300 C ..... MDS(J) = ADDRESS OF STIFFNESS MAIN DIAGONAL TERM ROW J
ROTO1310 C ..... NDMASS(I) = ADDRESS OF MASS MAIN DIAGONAL TERM ROW I
ROTO1320 C ..... MDSG(I) = ADDRESS OF GEOMETRIC STIFF. MAIN DIAGONAL TERM ROW I
ROTO1330 C
ROTO1340 C ..... LSTIFF = # OF STIFFNESS TERMS IN COLUMN J
ROTO1350 C ..... LMASS = # OF MASS TERMS IN COLUMN J
ROTO1360 C ..... LKG = # OF KG TERMS IN COLUMN J
ROTO1370 C ..... L = # OF S TERMS IN COLUMN J
ROTO1380 C
  NFREE=L-LS+1
  MDS(1)=1
  LK=0
  DO 110 JI=2,NFREE+1
    J=JI-LS-1
    LSTIFF=MDS(J)+MDS(J-1)
    LMASS=NDMASS(J)+NDMASS(J-1)
    IF (KGFORM.EQ.2) LKG=MDSG(J)+MDSG(J-1)
    LK=LK+1,MAX(LSTIFF,LMASS,LKG)
  110 MDS(JI)=MDS(JI-1)+L
C
  RETURN
  END
C
SUBROUTINE SMAK, FINDS THE MAXIMUM AND MINIMUM VALUES
  DIMENSION A(N,DT,A,VNK,VM,T1,T2,MLEN,AVE,STDEV,RMS)
  LOGICAL BTEST
  REAL*8 T,SUMK,SUMSQ,ADBL
  AVE=0
  J=JL-LS-1
  STDEV=0
  RMS=0
  VNK=AK(1)
  VM=AK(1)
  T=DT
  T1=DT
  T2=DT
  IF (N.LE.1) RETURN
  ADBL=AK(1)
  SUMSQ=ADBL**2
  DO 40 I=2,N
    ADBL=AK(I)
    SUMK = SUMK + ADBL
    SUMSQ = SUMSQ + ADBL**2
    IF (VM.LT.AK(I)) THEN
      VM=AK(I)
      T1=I
    ELSE IF (VNK.GT.AK(I)) THEN
      VNK=AK(I)
      T2=I
    ENDIF
  T=DT
  AVE=SUMK/N
  STDEV=SQRT((SUMSQ-SUMK**2)/(N*(N-1)))
  RMS=SQRT(SUMSQ/N)
  RETURN
  END
C
SUBROUTINE SOLN(OPTION)
  LOGICAL BTEST
  CHARACTER*80 NAME,OPTION
  INCLUDE (ZCOMM)
  STEPID=' '
C
C =====
C CHOOSE THE SOLUTION ==
C DETERMINE SOLUTION NO. ==
CALL GETINT(OPTION,'SOL',NSOLN,0.,TRUE.,FALSE.)
C
C =====
IF (NSOLN.EQ.1) THEN
  CALL SOL01
ELSE IF (NSOLN.EQ.2) THEN
  MLOAD=1
  NAME=D0
  CALL SOL02
ELSE IF (NSOLN.EQ.3) THEN
  MLOAD=1
  NAME=D0
  CALL SOL05
ELSE IF (NSOLN.EQ.4) THEN
  MLOAD=1
  CALL SOL04
ELSE
  WRITE(6,*) 'INVALID SOLN',NSOLN
  STOP 'INVALID SOLUTION NUMBER'
ENDIF
50 RETURN
END
C
SUBROUTINE SOL01
  LOGICAL PRINT,OSPLG,HEAD,AXIAL,BTEST
  CHARACTER*80 NAME
  DIMENSION RINPUT(100)
  INCLUDE (ZCOMM)
C
  READ(5,*) MLOAD,NAME
  WRITE(6,1) TITLE(1),TITLE(2),MLOAD
  1 FORMAT ('1 STRUCTURE.....',A,/,
    & ' SOLUTION.....',A,/)
  8 'X',SOLUTION #1, STATIC - ELASTIC ANALYSIS //
  8 'X',SOLUTION #2, STATIC - ELASTIC ANALYSIS //

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C      BLK, ' NUMBER OF LOAD CASES .....', IS)
C      IF (N2(ZKGT+5).EQ.2) WRITE (6,2)
C      2 FORMAT (1X, ' GEOMETRIC STIFFNESS IS NOT INCLUDED, '
C      & ' USE KGDATA3=1 TO INCLUDE GEOMETRIC STIFFNESS.')
C      ----- INITIALIZE STORAGE FOR STIFFNESS, LOAD AND DISPL. ....
C      ELSTIC=.TRUE.
C      ----- INITIALIZE STORAGE FOR STIFFNESS, LOAD AND DISPL. ....
C      Z(IZSTIF) = LOCATION OF THE STIFFNESS MATRIX
C      Z(IZLOAD) = LOCATION OF THE LOAD MATRIX
C      Z(IZLOAD) = LOCATION OF THE DISPLACEMENT MATRIX
C      IF (IZLOAD.EQ.0) THEN
C        IZ = IZ
C      ENDOF
C      IF (IZDISP.EQ.0) THEN
C        IZ = IZ+NDOF*NLOAD
C      ENDOF
C      IF (IZVEL.EQ.0) THEN
C        IZ = IZ+NDOF*NLOAD
C      ENDOF
C      IF (IZVEL.EQ.0) THEN
C        IZVEL = IZ
C      ENDOF
C      DO 3 I=1,NDOF
C        Z(I+IZVEL-1) = 0
C      IF (IZVEL.EQ.0) THEN
C        IZVEL = IZ
C      ENDOF
C      DO 4 I=1,NDOF
C        Z(I+IZVEL-1) = 0
C      IF (IZFUB.EQ.0) THEN
C        IZ = IZ+NDOF
C      ENDOF
C      DO 5 I=1,NDOF
C        Z(I+IZFUB-1) = 0
C      ENDOF
C      ----- SET UP CONSTANTS -----
C      L1=L2=NCOND+NFREE
C      L3=NCOND+NFREE+1
C      L4=NDOF
C      IF (MAKELD.GT.0) THEN
C        IZELD=IZ
C        IZ=IZ + MAKELD*5
C        IZELD=IZ
C        IZ=IZ + MAKELD*12
C      ENDOF
C      IM=IZ+1
C      IMD=N2(IZIM+L4)
C      CALL SOL01A
C      & (L1,L2,L3,L4,IMD,NLOAD,MAKELD,NELD,NMODE,NCOS,NELMT,ABORT,
C      & IZDISP,IZLOAD,HSTOR,IBUG,MANNO,ITITLE,STEPID,
C      & Z(IZSTIF), Z(IZLOAD), Z(IZDISP), Z(IZVEL), Z(IZVEL),
C      & Z(IZFUB),NZ(IZELD), Z(IZELD), Z(IM),NZ(IZMD),
C      & NZ(IZID),NZ(IZIDOF), Z(IZCONST),NZ(IZFLG), Z(IZCORD),
C      & Z(IZCOS),NZ(IZCOS),SUMRCT)
C      RETURN
C      END
C      SUBROUTINE SOL01A
C      & (L1,L2,L3,L4,IMD,NLOAD,MAKELD,NELD,NMODE,NCOS,NELMT,ABORT,
C      & IZDISP,IZLOAD,HSTOR,IBUG,MANNO,ITITLE,STEPID,
C      & STIF,LOAD,DISP,VEL,DVEL,
C      & FUB,IELD,ELD,WORK,MD,
C      & ID, IDOF,CONST,JFLG,COORD,
C      & COSINE,JTCOS,SUMRCT)
C      CHARACTER*(*) ITITLE(2),STEPID
C      LOGICAL PRINT,OSPLG,HEAD,AXIAL,BTEST,BUG,ABORT,BUGS
C      CHARACTER*80 NAME
C      DIMENSION RINPUT(100),SUMRCT(6)
C      REAL LOAD
C      DIMENSION STIF(IMD),LOAD(L4,NLOAD),DISP(L4,NLOAD),VEL(L4),DVEL(L4)
C      DIMENSION FURK(L4),IELD,MAKELD(5),ELD,MAKELD(12),HORK(1),MD(L4+1)
C      DIMENSION CORDX(MANNO(5)),IDY(MANNO(5)),
C      & IDOF(MANNO(6)),COSINE(5,5,NCOS),CONST(MANNO(6)),
C      & JFLG(MANNO(6)),JTCOS(MANNO(6))
C      BUG=BTEST(IBUG,5)
C      BUGS=BTEST(IBUG,5)
C      =====
C      C= INPUT LOADING DATA ==
C      =====
C      ----- ZERO LOAD AND DISPLACEMENT MATRIX -----
C      DO 6 I=1,L4
C      DO 6 J=1,NLOAD
C      LOAD(I,J)=0
C      DISP(I,J)=0
C      6 DISP(I,J)=0
C      ----- INPUT JOINT LOADS -----
C      JOINT LOADS AND SUPPORT DISPLACEMENTS ARE STORED IN THE
C      DISPLACEMENT MATRIX
C      CALL JOIL04(BUGS,MANNO,L4,NMODE,NLOAD,L2,
C      & ID, IDOF,CONST,DISP,
C      & OSPLG,JFLG,ITITLE,.FALSE.)
C      ----- INPUT ELEMENT LOADS -----
C      ELEMENT LOADS ARE STORED IN THE LOAD MATRIX
C      IF (MAKELD.GT.0) THEN
C        CALL ELELO4(BUGS,L5,NELMT,MAKELD,NELD,L4,NLOAD,
C      & LOAD,IELD,ELD,IZDISP,IZLOAD,NAME,ITITLE,.FALSE.)
C      ...ADD ELEMENT LOADS ON FREE JOINTS TO THE JOINT LOADS ON FREE
C      ...JOINTS. STORE IN THE DISPLACEMENT MATRIX
C      ...SAVE ELEMENT LOADS ON ALL JOINTS IN LOAD MATRIX, USED LATER
C      ...FOR CALCULATING THE REACTIONS.
C      DO 10 I=1,L2
C      DO 10 J=1,NLOAD
C      DISP(I,J)=DISP(I,J)+LOAD(I,J)
C      ...SHAP THE SIGN OF THE FEF AT REACTIONS
C      DO 15 I=1,L4
C      DO 15 J=1,NLOAD
C      LOAD(I,J)=-LOAD(I,J)
C      ENDOF
C      =====
C      C= FORMULATE STIFFNESS ==
C      =====

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C= GET AND PRINT MAXIMUM REACTIONS ===
C=====
C
WRITE (6,1000) TITLE(1),TITLE(2)
DO 1020 I=1,L4
  WORK(I) =LOAD(I,1)
  DO 1020 J=2,MLOAD
    IF (ABS(LOAD(I,J)),GT,ABS(WORK(I))) WORK(I)=LOAD(I,J)
1020 CONTINUE
DO 1050 I=1,6
1050 SURFCT(I)=0
CALL REACTN(4,TRUE,MMODE,L1,L2,L3,L4,WORK,DISP,
& MD,STIF,MD,L4,1,1,0,
& MAMNO,IZDF,COORD,JD,TITLE,STEPID,,FALSE,,
& NCOS,COSINE,JTCOS,JTFLG,SURFCT)
C
C=====
C= PRINT MAXIMUM ELEMENT FORCES ===
C=====
C
WRITE (6,1000) TITLE(1),TITLE(2)
LSTTVP=0
PRINT=.TRUE.
HEAD=.FALSE.
DO 1510 TELNO=L,NELMT
1510 CALL ELEMIB
& L2,LSTTVP,PRINT,IREL,HEAD,NAME,RESE,EPSE,DAMAGE,
& TELNO,I,ELDOF,KGDOF,PGEOM,RDMPUT,AXIAL,IZDISP,IZLOAD,MSTOR)
C
RETURN
C
220 FORMAT (5X,IS,IP,6G15.6)
200 FORMAT ('1 GLOBAL','A',LOADING #' ,IS//
& 4X,'NODE','X','DY','ISX','DZ','ISX','RY','ISX','RZ')/SOL02250
END
C=====
SUBROUTINE SOL02
LOGICAL PRINT,DISPFLG,HEAD,REPEAT,SLMASS,AXIAL,TEST,NEKOV,BTEST
LOGICAL UNBAL
DIMENSION RDMPUT(100)
CHARACTER*1 NAME
CHARACTER*20 INTEG
INCLUDE 'ZCOMMON'
C
C=====
C= PRINT HEADER ===
C=====
WRITE (6,10) TITLE(1),TITLE(2)
10 FORMAT ('1 STRUCTURE.....','A./
& ' SOLUTION.....','A./)
C
C=====
C= INPUT LOADING DATA ==
C=====
READ (5,*) INTEG,THETA,ELSTIC,UNBAL
READ (5,*) IPRINT,WRITE,MAXACC,SLMASS
READ (5,*) TO,DT,TF,GRAV
IPRINT=MAX(IPRINT,1)
C
IF (TEST<INTEG,'LINEAR' ,.FALSE.) THEN
INTEG=1
WRITE (6,11) 'LINEAR ACCELERATION METHOD'.
& '=====
ELSE IF (TEST<INTEG,'AVERAGE' ,.FALSE.) THEN
INTEG=2
WRITE (6,11) 'AVERAGE ACCELERATION METHOD'.
& '=====
ELSE IF (TEST<INTEG,'WILSON' ,.FALSE.) THEN
INTEG=5
WRITE (6,11) 'WILSON THETA METHOD'.
& '=====
WRITE (6,12) THETA
ELSE IF (TEST<INTEG,'WILSON' ,.FALSE.) THEN
WRITE (6,*) 'INVALID INTEGRATION METHOD'
WRITE (6,11) INTEG,'=====
RETURN
ENDIF
C
CHECK FOR INVALID INTEGRATION WITH PROPORTIONAL DAMPING
IF (INTEG.EQ.1 .OR. INTEG.EQ.2) .AND. FDAMP.NE.1) THEN
WRITE (6,19)
19 FORMAT (5X,'INTEGRATION METHOD IS ONLY VALID FOR ',
& 'PROPORTIONAL DAMPING'//,5X,'SOLN IS ABORTED')
RETURN
ENDIF
C
WRITE (6,13) TO,DT,TF,GRAV,IPRINT
IF (ELSTIC) WRITE (6,14)
C
11 FORMAT (
& 'X', SOLUTION #2, 'A', OF NUMERICAL INTEGRATION//
& 'X', '=====','A', '=====')
12 FORMAT (
& 'X', THETA ..... ,IP,615.6)
13 FORMAT (
& 'X', INITIAL TIME ..... ,IP,615.6/
& 'X', TIME STEP ..... ,IP,615.6/
& 'X', FINAL TIME ..... ,IP,615.6/
& 'X', ACCELERATION DUE TO GRAVITY ..... ,IP,615.6/
& 'X', STEP INTERVAL FOR PRINTING ..... ,OP,IS)
14 FORMAT (
& 'X', THE STRUCTURE IS ASSUMED TO BEHAVE ELASTICALLY')
C
C=====
C= SET GEOMETRIC STIFFNESS FLAGS ==
C=====
KGLDAD=NZ(IZKGD1+1)
KGTYP=NZ(IZKGD2+2)
KGFORM=NZ(IZKGD3+3)
NEKNG=.TRUE.
IF (KGLDAD.EQ.0 .OR. KGTYP.EQ.0 .OR. KGFORM.EQ.0) NEKNG=.FALSE.
C
C----- SET UP CONSTANTS -----
L1=L1
L2=NCOMD
L3=L2+1
L4=NCOMD +NFREE
L5=L4+1
L6=NDOF
C
C----- INITIALIZE STORAGE FOR LOAD, DISPL, VELOC, ACCEL
Z(IZLOAD) = LOCATION OF THE TOTAL LOAD MATRIX
Z(IZDISP) = LOCATION OF THE TOTAL DISPLACEMENT MATRIX
SOL01900 C Z(IZVEL) = LOCATION OF THE TOTAL VELOCITY MATRIX
SOL01910 C Z(IZACC) = LOCATION OF THE TOTAL ACCELERATION MATRIX
SOL01920 C Z(IZDLOA) = LOCATION OF THE INCREMENTAL LOAD MATRIX
SOL01930 C Z(IZDOSP) = LOCATION OF THE INCREMENTAL DISPLACEMENT MATRIX
SOL01940 C Z(IZDVEL) = LOCATION OF THE INCREMENTAL VELOCITY MATRIX
SOL01950 C Z(IZDACC) = LOCATION OF THE INCREMENTAL ACCELERATION MATRIX
SOL00980
SOL00990
SOL01000
SOL01010
SOL01020
SOL01030
SOL01040
SOL01050
SOL01060
SOL01070
SOL01080
SOL01090
SOL01100
SOL01110
SOL01120
SOL01130
SOL01140
SOL01150
SOL01160
SOL01170
SOL01180
SOL01190
SOL01200
SOL01210
SOL01220
SOL01230
SOL01240
SOL01250
SOL01260
SOL01270
SOL01280
SOL01290
SOL01300
SOL01310
SOL01320
SOL01330
SOL01340
SOL01350
SOL01360
SOL01370
SOL01380
SOL01390
SOL01400
SOL01410
SOL01420
SOL01430
SOL01440
SOL01450
SOL01460
SOL01470
SOL01480
SOL01490
SOL01500
SOL01510
SOL01520
SOL01530
SOL01540
SOL01550
SOL01560
SOL01570
SOL01580
SOL01590
SOL01600
SOL01610
SOL01620
SOL01630
SOL01640
SOL01650
SOL01660
SOL01670
SOL01680
SOL01690
SOL01700
SOL01710
SOL01720
SOL01730
SOL01740
SOL01750
SOL01760
SOL01770
SOL01780
SOL01790
SOL01800
SOL01810
SOL01820
SOL01830
SOL01840
SOL01850
SOL01860
SOL01870
SOL01880
SOL01890
SOL01900
SOL01910
SOL01920
SOL01930
SOL01940
SOL01950
SOL01960
SOL01970
SOL01980
SOL01990
SOL02000
SOL02010
SOL02020
SOL02030
SOL02040
SOL02050
SOL02060
SOL02070
SOL02080
SOL02090
SOL02100
SOL02110
SOL02120
SOL02130
SOL02140
SOL02150
IF (IZLOAD.EQ.0) THEN
IZLOAD = IZ
CALL CKSTOR(0,0)
DO 1 I=1,NDOF
Z(I+IZLOAD-1) = 0
ENDIF
C
IF (IZDISP.EQ.0) THEN
IZDISP = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 2 I=1,NDOF
Z(I+IZDISP-1) = 0
ENDIF
C
IF (IZVEL.EQ.0) THEN
IZVEL = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 3 I=1,NDOF
Z(I+IZVEL-1) = 0
ENDIF
C
IF (IZACC.EQ.0) THEN
IZACC = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 4 I=1,NDOF
Z(I+IZACC-1) = 0
ENDIF
C
IF (IZDLOA.EQ.0) THEN
IZDLOA = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 5 I=1,NDOF
Z(I+IZDLOA-1) = 0
ENDIF
C
IF (IZDOSP.EQ.0) THEN
IZDOSP = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 6 I=1,NDOF
Z(I+IZDOSP-1) = 0
ENDIF
C
IF (IZDVEL.EQ.0) THEN
IZDVEL = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 7 I=1,NDOF
Z(I+IZDVEL-1) = 0
ENDIF
C
IF (IZDACC.EQ.0) THEN
IZDACC = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 8 I=1,NDOF
Z(I+IZDACC-1) = 0
ENDIF
C
IF (IZFUB.EQ.0) THEN
IZFUB = IZ
IZ = IZ+NDOF
CALL CKSTOR(0,0)
DO 9 I=1,NDOF
Z(I+IZFUB-1) = 0
ENDIF
D=IZ+1
C
C----- FORM MASS MATRIX -----
IMDS =NZ(IZDMS+NDOF)
DO 400 I=1,IMDS
400 Z(I+IMDS-1)=0.
CALL NFORM2,IMASS,MMASS,Z(IZMASS),NZ(IZDMS),MD,NDOF,IMDS,
& TITLE,MMODE,MAMNO,NCOS,BTEST(1,BUG,5),IBUG,
& NZ(IZID),Z(IZCOS),NZ(IZIDOF),Z(IZCNS),NZ(IZJFLG),
& NZ(IZJGOS),Z(IZMBA1),Z(IM),NZ(IM+1),Z(IM+2),
& Z(D= 65),Z(D= 99))
C
C----- FORM SPECIAL MASS MATRIX -----
IF (SLMASS) THEN
READ (5,*) IMASS,IFMASS
IMASS=IMASS+1
CALL MASSIN,IMASS,IFMASS,.FALSE.,BUG,IBUG,TITLE,MMZ,MMZDZ,
& MAMNO,NCOS,MMODE,IZ,IM,IZID,Z,NZ,IZ,
& IZSLND,IZSLUS,IZLMI,IZKE,IZMOTZ,
& NDOF,MMASS,IZCOS,IZIDOF,IZCNS,IZJFLG,IZJGOS,'GLOBAL MASS',
& MCOMD,NFREE,IZMD)
ELSE
IZSLMS=0
IZSLMO=0
IMDMSL=1
ENDIF
IMDS =NZ(IZDMS+NDOF)
C
C----- SET UP STORAGE FOR MAIN DIAGONAL ADDRESS OF DYNAMIC STIFFNESS
IZDMS = IZ
IZ = IZ + NFREE +1
CALL CKSTOR(0,IM)
C
C----- DEVELOP SKV,LINE OF DYNAMIC STIFFNESS (S)
CALL SKVLNK,NDOF,L3,L4,
& NZ(IZDMS),NZ(IZD),NZ(IZDMS),NZ(IZDMKG),KGFORM)
C
C----- DETERMINE THE LENGTH OF THE DYNAMIC STIFFNESS MATRIX
IMDS=NZ(IZDMS+NFREE) - NZ(IZDMS) +1
C
C----- DETERMINE THE ADDRESS OF THE DYNAMIC STIFFNESS MATRIX
IZS = IZ
IZ = IZ+NZ(IZDMS+NFREE)
SOL00920 C

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C----- DEFINE STORAGE REQD FOR NUMERICAL INTEGRATION
AND INITIALIZE VALUES
C
IZAN = IZ
IZ = IZ+NFREE
IZBN = IZ
IZ = IZ+NFREE
IZPBAR = IZ
IZ = IZ+NFREE
C
C----- SAVE STORAGE FOR DYNAMIC GROUND ACCELERATIONS
IZAGT=IZ
IZ = IZ+MAXACC
IZAGTV=IZ
IZ = IZ+MAXACC
IZAGTZ=IZ
IZ = IZ+MAXACC
IZAINP=IZ
MAXDMP=MAX(NDOF,MAXACC)
IZ = IZ+MAXDMP
IZMCOSS=IZ
IZ = IZ+MDOF*5
C
C----- SAVE STORAGE FOR ENERGY CALCULATIONS
IZZERO=IZ
IZ = IZ+MDOF
IZDM = IZ
IZ = IZ+MDOF
IZVM = IZ
IZ = IZ+MDOF
IZDBAR=IZ
IZ = IZ+MDOF
IZDL02=IZ
IZ = IZ+MDOF
IZTFD = IZ
IZ = IZ+MDOF
IZDFD = IZ
IZ = IZ+MDOF
IZFG = IZ
IZ = IZ+MDOF
IZDFG = IZ
IZ = IZ+MDOF
DO 25 I=0,MDOF-1
  Z(IZFG+I)=0
  Z(IZDFG+I)=0
  Z(IZVM+I)=0
  Z(IZDBAR+I)=0
  Z(IZDL02+I)=0
  Z(IZTFD+I)=0
  Z(IZDFD+I)=0
C
25
C-----
IZDMAX=IZ
IZ = IZ+MDOF
IZVMAX=IZ
IZ = IZ+MDOF
IZANMAX=IZ
IZ = IZ+MDOF
IZDMAX=IZ
IZ = IZ+MDOF
DO 28 I=1,5
  Z(IZDMAX+I)=0
  Z(IZVMAX+I)=0
  Z(IZANMAX+I)=0
C
28
DO 29 I=1,6
  Z(IZDMAX-1+MDOF+I)=0
DO 50 I=1,6
  SUMRC(I)=0
C
C-----
C=INPUT FILE OUTPUT CONTROL DATA
C-----
IF (.INWRITE.GT.0) THEN
  IOPT=1
  CALL DMPACT(IOPT,INWRITE,IO,DT)
ENDIF
C
C----- SET UP WORK STORAGE AREA ...
IH = IZ + 1
C
C----- CHECK STORAGE REQUIREMENTS ...
CALL CKSTOR(NDOF,IH)
C
C----- DETERMINE THE LENGTH OF THE STIFFNESS MATRIX
IND=NZ(IZDM+MDOF) - NZ(IZDM) + 1
C----- DETERMINE THE LENGTH OF THE MASS MATRIX
INDM=NZ(IZDMNS+MDOF) - NZ(IZDMNS) + 1
C----- DETERMINE THE LENGTH OF THE GEOMETRIC STIFFNESS MATRIX
IF (NZ(IZKGD+5).EQ.2) THEN
  INDKG=NZ(IZDKG+MDOF) - NZ(IZDKG) + 1
ELSE
  INDKG=1
ENDIF
C
C----- CALL SOL2A TO CALC DATA ....
CALL SOL2A
& (L1,L2,L3,L4,L5,L6,IND,INDMS,INDKG,INDS,INDMSL,ABORT,ITLCPU,
& NLOAD, NAKELD, NMODE, NCOSS, NEMHT,
& IZDISP, IZLOAD, NSTOR, IBUG, MAXNOD,
& TITLE, STEPID, NAINP, NDOF, NFREE,
& KFORM, KLOAD, KGTYP, NCON, INTEG,
& NEKG, NEK, NCON, KCOND, UNBAL,
& INTEG, THETA, ELSTIC, IWRITE,
& MAXACC, SLMASS, TO, DT, TF,
& GRAV, FDAMP, FMASS, IZDOSP, IZDLOA,
& Z(IZDISP), Z(IZVEL), Z(IZACC), Z(IZLOAD), Z(IZAN),
& Z(IZDOSP), Z(IZVEL), Z(IZACC), Z(IZDLOA), Z(IZBN),
& Z(IZSTIF), Z(IZMASS), Z(IZSLMS), Z(IZKG), Z(IZS),
& NZ(IZDM), NZ(IZDMNS), NZ(IZSLMD), NZ(IZDMNS),
& Z(IZDAMP), Z(IZPBAR), Z(IZMCOSS), Z(IZAGT),
& Z(IZAGTV), Z(IZAGTZ), Z(IZAINP), Z(IZFLG), Z(IZCOORD),
& NZ(IZD), NZ(IZDOF), Z(IZCONST), NZ(IZFLG), Z(IZCOORD),
& EIE,ESE,PSE,EKE,EDD,
& Z(IZZERO), Z(IZFG), Z(IZDFG) )
C
RETURN
C
END
C----- SUBROUTINE SOL2A
SUBROUTINE SOL2A

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CALL DVLOAD1,BUGS,MAXACC,NOOF,NAIMP,T,TL,
& ACCELZ,TOACC,DTACC,GRAV,
& MAXNO,MMODE,COSINE,DOF,JTFLG,JTCOS,NCOS,
& AGTX,AGTY,AGTZ,MASS,MMOM,INDMS,
& AIMP,NCOS,LOAD,GA,GAT )
ELSE
CALL DVLOAD1,BUGS,MAXACC,NOOF,NAIMP,T,TL,
& ACCELZ,TOACC,DTACC,GRAV,
& MAXNO,MMODE,COSINE,DOF,JTFLG,JTCOS,NCOS,
& AGTX,AGTY,AGTZ,MASS,MMOM,INDMS,
& AIMP,NCOS,LOAD,GA,GAT )
ENDIF

C
C----- GET INITIAL DYNAMIC LOAD
IF (SMASS) THEN
CALL DVLOAD2,BUGS,MAXACC,NOOF,NAIMP,T,TL,
& ACCELZ,TOACC,DTACC,GRAV,
& MAXNO,MMODE,COSINE,DOF,JTFLG,JTCOS,NCOS,
& AGTX,AGTY,AGTZ,MASS,MMOM,INDMS,
& AIMP,NCOS,LOAD,GA,GAT )
ELSE
CALL DVLOAD2,BUGS,MAXACC,NOOF,NAIMP,T,TL,
& ACCELZ,TOACC,DTACC,GRAV,
& MAXNO,MMODE,COSINE,DOF,JTFLG,JTCOS,NCOS,
& AGTX,AGTY,AGTZ,MASS,MMOM,INDMS,
& AIMP,NCOS,LOAD,GA,GAT )
ENDIF

C
C----- INITIALIZE INTEGRATION ROUTINES
C
IF (INTEGO.EQ.1) THEN
CALL LDMACC1,BUGS,DT,TO,TF,T,1,00,NEWKDV,
& L1,L2,L3,L4,L5,L6,INDMS,IND,INDS,INDKG,NOOF,NFREE,
& KGLD,KGFORM,
& ACC,VEL,DISP,LOAD,
& DACC,DVEL,DOISP,OLA02,WORK,
& MASS,MMOM,DAMP,STIFF,MD,
& KG,MMKG,FZ,GRAV,
& SBAR,MOS,AN,BN,PBAR,
& FDAMP,FMASS,C1,C2,C3,C4,C5,C6,C7,ALPHA,BETA,C10,C11,ABORT)
ELSE IF (INTEGO.EQ.2) THEN
CALL AVEACC1,BUGS,DT,TO,TF,T,THETA,NEWKDV,
& L1,L2,L3,L4,L5,L6,INDMS,IND,INDS,INDKG,NOOF,NFREE,
& KGLD,KGFORM,
& ACC,VEL,DISP,LOAD,
& DACC,DVEL,DOISP,OLA02,WORK,
& MASS,MMOM,DAMP,STIFF,MD,
& KG,MMKG,FZ,GRAV,
& SBAR,MOS,AN,BN,PBAR,
& FDAMP,FMASS,C1,C2,C3,C4,C5,C6,C7,ALPHA,BETA,C10,C11,ABORT)
ENDIF
IF (ABORT) GO TO 5000

C
C=====
CWRITE INITIAL DATA TO OUTPUT FILE
C=====
IF (WRITE.GT.0) THEN
IOPT=2
CALL EMPQAT(IOPT,WRITE,TO,DT)
ENDIF

C
C=====
C LOOP FOR EACH TIME STEP, ISTEP=CURRENT STEP
C=====
C... NSTEP = NUMBER OF TIME STEPS
C... ISTEP = TIME STEP NUMBER
C... T = CURRENT TIME
C... TL = TIME AT PREVIOUS TIME STEP
C... TO = INITIAL TIME
C... DT = TIME INCREMENT
C... TL = FINAL TIME

MCON2 = MCON1
NSTEP = (TF-TO)/DT
T = TO
DO 500 ISTEP=1,NSTEP
T=I*DT
TL=T-DT
WRITE (STEPID,90) ISTEP,T
90 FORMAT ('STEP:',I6,', TIME:',I9.5)

C
C=====
C CALC INCREMENTAL LOADS
C=====
I2=2
CALL DVLOAD2,BUGS,MAXACC,NOOF,NAIMP,T,TL,
& ACCELZ,TOACC,DTACC,GRAV,
& MAXNO,MMODE,COSINE,DOF,JTFLG,JTCOS,NCOS,
& AGTX,AGTY,AGTZ,MASS,MMOM,INDMS,
& AIMP,NCOS,LOAD,GA,GAT )
FZ = ACCELZ

C
C----- ADD UNBALANCED LOADS TO THE LOAD VECTOR. ---- STORE AS DLOAD2
C STORE OLD UNBALANCED LOADS AT REACTIONS IN DLOAD
IF (UNBAL) THEN
DO 195 I=L1,L4
DLOAD2(I)=DLOAD(I)+FUB(I)
195 DO 196 I=L5,L6
DLOAD2(I)=-FUB(I)
C*** OMIT UNBALANCED LOAD FROM REACTIONS...
C*** UNBALANCED LOADS ADDED TO THE FRAME ARE REGISTERED BY
C*** 1) INERTIAL FORCES
C*** 2) DAMPING FORCES
C*** 3) MEMBER FORCES
C*** SUBTRACTING UNBALANCED FORCES FROM REACTIONS DUE TO MEMBER FORCES
C*** NEGLECTS THE REACTIONS DUE TO INERTIAL AND DAMPING FORCES.
DLOAD(I)=-FUB(I)
C***
196 FUB(I)=0.0
ELSE
DO 197 I=L1,L6
197 DLOAD2(I)=DLOAD(I)
ENDIF

C
C=====
C FORMULATE STIFFNESS
C=====
C FORMULATE THE STIFFNESS IF THE FLAG NEWK IS TRUE, THIS FLAG IS
C INITIALIZED ABOVE, AND SET WHEN THE ELEMENT FORCES ARE CALC.
C THE STIFFNESS IS ALSO FORMULATED IF KG IS TO BE CALCULATED
C AND CONDENSATION IS TO BE PREFORMED, (THE STIFFNESS IS NEEDED
C FOR THE CONDENSATION PROCEDURE...)

SOL01320 REPEAT=.TRUE.
SOL01330 KNAME=0
SOL01340 100 IF (NEWK) THEN
SOL01350 I1=1
SOL01360 CALL FORM(I1)
SOL01370 C----- CALL LMATRK(STIFF,MD,L4,IND,'GLOBAL STIFFNESS MATRIX')
SOL01380 IF (BUGS) THEN
SOL01390 CALL LMATRK(STIFF,MD,NOOF,IND,'GLOBAL STIFFNESS DUMP=?')
SOL01400 ENDF
SOL01410 ENDF
SOL01420 C
SOL01430 C=====
SOL01440 C= FORM GEOMETRIC STIFFNESS
SOL01450 C=====
SOL01460 C FORMULATE THE GEOMETRIC STIFFNESS IF THE FLAG NEWK IS TRUE, THIS
SOL01470 C FLAG INITIALIZED ABOVE.
SOL01480 C IF KDATA(1)=1, THE GEOMETRIC STIFFNESS IS FORMED ONCE, AND
SOL01490 C MULTIPLIED BY A SCALAR TO ACCOUNT FOR CHANGES
SOL01500 C IN THE TOTAL VERTICAL LOAD. THUS THE GEOMETRIC
SOL01510 C STIFFNESS ONLY NEEDS TO BE FORMED ONCE.
SOL01520 C IF KDATA(1)=2, THE GEOMETRIC STIFFNESS IS BASED ON THE AXIAL
SOL01530 C FORCE IN THE ELEMENTS, AND IS RECALCULATED EACH
SOL01540 C TIME THE AXIAL FORCE CHANGES.
SOL01550 C IF KDATA(3)=1, THE GEOMETRIC STIFFNESS IS FORMED WITH THE
SOL01560 C STIFFNESS, THUS A SEPERATE CALL TO FORM IS
SOL01570 C NOT NEEDED
SOL01580 C IF KDATA(3)=2, A SEPERATE GEOMETRIC STIFFNESS MATRIX IS FORMED
SOL01590 C IF (NEWKG) THEN
SOL01600 C
SOL01610 C FORMULATE SEPERATE GEOMETRIC STIFFNESS MATRIX
SOL01620 C IF (KGFORM.EQ.2) THEN
SOL01630 F2 = 0
SOL01640 I2=2
SOL01650 CALL FORM(I2)
SOL01660 KGM2=KGM1
SOL01670 IF (BUGS) THEN
SOL01680 CALL LMATRK(KG,MMKG,NOOF,INDKG,'KG MATRIX DUMP=?')
SOL01690 ENDF
SOL01700 ELSE
SOL01710 KGM2=.FALSE.
SOL01720 ENDF
SOL01730 C
SOL01740 ENDF
SOL01750 C
C=====
C CONDENSE OUT FREE DISPL
C=====
C... IF MCON2 IS TRUE THE MASS MATRIX IS ALSO REDUCED BY GUYAN REDUCTION
C... IF KGM2 IS TRUE THEN KG IS ALSO REDUCED
IF (MCON2.GT.0 .AND. NEWK) THEN
CALL MSOLL1,BUGS,L4,IND,NOOF,I1,I1,L2,
& MD,STIFF,DLOAD2,WORK,
& MCON2,MASS,MMOM,INDMS,
& KGM2,KG,MMKG,INDKG,ABORT)
IF (ABORT) GO TO 5000
MCON2 = .FALSE.
KGM2 = .FALSE.
ELSE IF (MCON2.GT.0) THEN
REDUCE THE DYNAMIC LOAD MATRIX IF OLD STIFFNESS IS USED...
CALL MSOLL2,BUGS,L4,IND,NOOF,I1,I1,L2,
& MD,STIFF,DLOAD2,WORK,
& MCON2,MASS,MMOM,INDMS,
& KGM2,KG,MMKG,INDKG,ABORT)
IF (ABORT) GO TO 5000
ENDIF

C
C=====
C DETERMINE IF A NEW DYNAMIC STIFFNESS NEEDS TO BE CALC
C=====
IF (NEWK .OR. NEWKG .OR. (KGLD.EQ.1 .AND. ACCELZ.EQ.ACCEL0)) THEN
NEWK=.TRUE.
ACCEL0=ACCELZ
ELSE
NEWK=.FALSE.
ENDIF

C
C=====
C SOLVE DYNAMIC EQUATION FOR INCREMENTAL DISPL
C=====
I2=2
IF (INTEGO.EQ.1) THEN
CALL LDMACC2,BUGS,DT,TO,TF,T,1,00,NEWKDV,
& L1,L2,L3,L4,L5,L6,INDMS,IND,INDS,INDKG,NOOF,NFREE,
& KGLD,KGFORM,
& ACC,VEL,DISP,LOAD,
& DACC,DVEL,DOISP,OLA02,WORK,
& MASS,MMOM,DAMP,STIFF,MD,
& KG,MMKG,FZ,GRAV,
& SBAR,MOS,AN,BN,PBAR,
& FDAMP,FMASS,C1,C2,C3,C4,C5,C6,C7,ALPHA,BETA,C10,C11,ABORT)
ELSE IF (INTEGO.EQ.2) THEN
CALL AVEACC2,BUGS,DT,TO,TF,T,THETA,NEWKDV,
& L1,L2,L3,L4,L5,L6,INDMS,IND,INDS,INDKG,NOOF,NFREE,
& KGLD,KGFORM,
& ACC,VEL,DISP,LOAD,
& DACC,DVEL,DOISP,OLA02,WORK,
& MASS,MMOM,DAMP,STIFF,MD,
& KG,MMKG,FZ,GRAV,
& SBAR,MOS,AN,BN,PBAR,
& FDAMP,FMASS,C1,C2,C3,C4,C5,C6,C7,ALPHA,BETA,C10,C11,ABORT)
ENDIF
IF (ABORT) GO TO 5000

C
C=====
C BACK SUBSTITUTION TO SOLVE FOR NON-DYNAMIC DOF
C=====
C DISP C = T * DISP F
C DISP C = INV(K,CC) * (-K,CF)*DISP(F)
C SUBRN REA_CTN (IOPT=1)
C PREFORMS THE MULTIPLICATION DISP C=(-K,CF)*DISP F
C SUBRN MSOLL (IOPT=5)
C PREFORMS THE BACK SUBSTITUTION TO EQUIVALENT TO
C DISP_C=INV(K,CC)*DISP_C
ONE=1.00
IF (MCON2.GT.0) THEN
I3=5
I4=1
C----- DISPLACEMENTS
IF (BUGS) WRITE(6,*) '----- CALC DISPL'
CALL REACTN11,BUGS,MMODE,L1,L2,L3,L4,DOISP,DOISP,
& MD,STIFF,MDKNOOF,NOOF,1,ONE,
& MAXNO,DOF,COORD,DT,ITLE,STEPID,.FALSE.,

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& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
CALL MSOLL(15,BUGS,L4,DND,NDOF,11,1,1,2,ND,STIFF,
DOISP,WORK,
.FALSE,MASS,MOMS,1,
.FALSE,KG,MOKG,1,ABORT)
IF (ABORT) GO TO 5000
-----
VELOCITIES
IF (BUGS) WRITE(6,*) '----- CALC VELOC'
CALL REACTN(1,BUGS,NMODE,1,1,2,1,5,L4,DVEL,DVEL,
ND,STIFF,NKNDOP,NDOF,1,ONE,
MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
CALL MSOLL(15,BUGS,L4,DND,NDOF,11,1,1,2,ND,STIFF,
DVEL,WORK,
.FALSE,MASS,MOMS,1,
.FALSE,KG,MOKG,1,ABORT)
IF (ABORT) GO TO 5000
-----
ACCELERATION
IF (BUGS) WRITE(6,*) '----- CALC ACCEL'
CALL REACTN(1,BUGS,NMODE,1,1,2,1,5,L4,DACC,DACC,
ND,STIFF,NKNDOP,NDOF,1,ONE,
MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
CALL MSOLL(15,BUGS,L4,DND,NDOF,11,1,1,2,ND,STIFF,
DACC,WORK,
.FALSE,MASS,MOMS,1,
.FALSE,KG,MOKG,1,ABORT)
IF (ABORT) GO TO 5000
ENDIF
C
C=====
C= CALCULATE INCREMENTAL MEMBER FORCES ==
C
C ELEID CALLS THE INDIVIDUAL ELEMENT LIBRARIES, EACH OF WHICH DETERMINES
C 1) DID THE STIFFNESS CHANGE? IF SO: MEME=.TRUE.
C 2) SHOULD THE INCREMENTAL DISPLACEMENT BE RECALCULATED?
C IF SO: KSAME=KSAME+ (A VALUE DEPENDING ON ELEMENT TYPE)
C
C
C IOPT=0
C LSTIYP=0
C PRINT=.FALSE.
C HEAD=.FALSE.
C MEME=.FALSE.
C HELMT=HELMT
C DO 150 IELN=1,NELMT
150 CALL ELEID
& (IOPT,LSTIYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,EDD,
& IELN,IELDOF,KDOF,PGEOM,RINPUT,AXIAL,IZZOSP,IZZOLA,MSTOR)
C
C=====
C= ZERO STIFFNESS CHANGE FLAGS IF ELASTIC ==
C=====
IF (ELSTIC) THEN
MEME=.FALSE.
KSAME=0
ENDIF
C
C=====
C= DETERMINE IF KG IS TO BE UPDATED BASED ON ==
C= CHANGING ELEMENT AXIAL FORCE ==
C=====
IF (KLOAD.EQ.2) THEN
MEME=.TRUE.
IF (NCOND.GT.0) MEME=.TRUE.
ELSE
MEME=.FALSE.
ENDIF
ENDIF
C
C=====
C= REPEAT STEP IF NECESSARY ==
C=====
C IF AN ELEMENT STIFFNESS CHANGE DECIDED THAT THE STEP BE REANALYZED,
C REFORMULATE THE STIFFNESS AND REANALYZE
C THE VARIABLE REPEAT IS SET UP TO SUPPRESS THE REANALYZING OF A STEP
C CURRENTLY, EACH STEP MAY ONLY BE REANALYZED ONCE, THIS PREVENTS
C AN ENDLESS LOOP.
C
IF (KSAFE.NE.0 .AND. REPEAT) THEN
REPEAT=.FALSE.
GO TO 100
ENDIF
C
C=====
C= SOLVE FOR REACTIONS ==
C=====
C REACTIONS ARE DUE TO INTERNAL MEMBER FORCES
C
IF (BUGS) WRITE(6,*) '----- CALC REACTN'
CALL REACTN(2,BUGS,NMODE,1,1,1,5,L6,DLOAD,DOISP,
ND,STIFF,NKNDOP,NDOF,1,1,0,
& MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
C
C----- GET SUMMATION OF REACTIONS
CALL REACTN(3,BUGS,NMODE,1,1,1,5,L6,DLOAD,DOISP,
ND,MOKG,KG,MOKG(NDOF),NDOF,1,1,0,
& MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
C
C----- GET SUMMATION OF REACTIONS DUE TO UNBALANCED LOAD
IF (.NOT.ELSTIC)
& CALL REACTN(5,BUGS,NMODE,1,1,1,5,L6,DLOAD,DOISP,
& MOKG,KG,MOKG(NDOF),NDOF,1,1,0,
& MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
C
C=====
C= SOLVE FOR INCREMENTAL GEOMETRIC STIFFNESS FORCE, DFG ==
C=====
C----- INCREMENTAL GEOMETRIC STIFFNESS FORCE
IF (KFORM.EQ.2) THEN
IF (BUGS) WRITE(6,*) '----- INCREMENTAL FORCE DUE TO KG'
CALL TPLY(BUGS,TRUE,IND,L4,L5,L4,
& MOKG,KG,DFG,DOISP)
C
SCALE FORCE TO INCLUDE GROUND ACCELERATION ...
DO 159 I=L5,L4
159 DFG(I)=(1+P2)*DFG(I)
ENDIF
C
C=====
C= SOLVE FOR INCREMENTAL DAMPING FORCE, DFDAMP ==
C=====
IF (BETA.NE.0) THEN
C----- INCREMENTAL DAMPING FORCE DUE TO STIFFNESS ...
IF (BUGS) WRITE(6,*)
'----- DAMPING FORCE/REACT DUE TO STIFFNESS'
CALL TPLY(BUGS,TRUE,IND,L6,L5,L4,L5,L4,
& ND,STIFF,DFDAMP,DVEL)
& CALL TPLY(BUGS,TRUE,IND,L6,L5,L4,L5,L4,
& ND,STIFF,DFDAMP,DVEL)
C----- INCREMENTAL DAMPING FORCE DUE TO KG ...
IF (KFORM.EQ.2) THEN
IF (BUGS) WRITE(6,*)
'----- DAMPING FORCE/REACT DUE TO KG'
CALL TPLY(BUGS,TRUE,IND,L6,L5,L4,L5,L4,
& MOKG,KG,WORK,DVEL)
& CALL TPLY(BUGS,TRUE,IND,L6,L5,L4,L5,L4,
& MOKG,KG,WORK,DVEL)
DO 158 I=L5,L4
158 DFDAMP(I)=DFDAMP(I)-MOKG(I)
ENDIF
C----- CALC SUM OF STIFFNESS PROPORTIONAL DAMPING REACTIONS
CALL REACTN(5,BUGS,NMODE,1,1,1,5,L6,DFDAMP,DVEL,
& MOMS,MASS,MOMS(NDOF),NDOF,1,1,0,
& MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
C----- MULTIPLY BY BETA
DO 160 I=L6
160 DSUMFDC(I)=DSUMFDC(I)*BETA
IF (BUGS) WRITE(6,*) 'I,DSUMFDC(I),BETA',I,DSUMFDC(I),BETA
DO 161 I=L5,L4
161 DFDAMP(I)=DFDAMP(I)*BETA
C
IF (ALPHA.NE.0) THEN
C----- INCREMENTAL DAMPING FORCE DUE TO MASS ...
IF (BUGS) WRITE(6,*) '----- DAMPING FORCE DUE TO MASS'
DO 162 I=L5,L4
162 MOKG(I)=0
& CALL TPLY(BUGS,TRUE,IND,L4,L3,L4,L3,L4,
& MOMS,MASS,WORK,DVEL)
C----- CALC SUM OF FD
CALL REACTN(5,BUGS,NMODE,1,1,2,1,5,L4,WORK,DVEL,
& MOMS,MASS,MOMS(NDOF),NDOF,1,1,0,
& MANNOD,DOF,COORD,ID,TITLE,STEPID,TRUE,
& NCOSS,COSINE,JTCOS,JIFLG,DSUMRC)
C----- MULTIPLY BY ALPHA ADD TO PREVIOUS SUM ...
IF (BETA.NE.0) THEN
DO 165 I=L5,L4
165 DFDAMP(I)=DFDAMP(I)+ALPHA*MOKG(I)
DO 167 I=L6
167 DSUMFDC(I)=DSUMFDC(I)+TSUM(I)*ALPHA
ELSE
DO 168 I=L5,L4
168 DFDAMP(I)=ALPHA*MOKG(I)
DO 166 I=L6
166 DSUMFDC(I)=TSUM(I)*ALPHA
ENDIF
IF (BUGS) WRITE(6,*) 'DSUMFDC(I),DSUMFDC(I)'
IF (BUGS) THEN
DO 169 I=L5,L4
169 WRITE(6,*) 'I,I,DFDAMP,DFDAMP(I),FDAMP,FDAMP(I)'
ENDIF
C
C=====
C= CALC AND ENERGIES AND QUANTITIES ==
C=====
WRITE(6,*) 'STEP,IPRNT',EQ,0
HEAD=WRITE
C
IF (HEAD) WRITE(6,250) TITLE(1),TITLE(2),',',ISTEP,STEPID
IF (SLMASH) THEN
C----- ENERGY FORMULATION WITH SPECIAL LOADING MASS ---
BASED ON APPLIED LOADING
CALL ENERGY
& (L1,L2,L3,L4,L5,L6,NDOF,MANNOD,NCOSS,BUG11,TRUE,
& IND,IMONS,INDKG,ND,MOMS,MOKG,TRUE,WRITE,ABORT,
& STIFF,KG,MASS,
& ETE,ESE,PSE,EKE,EDD,
& ALPHA,BETA,KFORM,HELMT,NMODE,DT,SUMRB,
& DSUMRC,DSUMRC,SLMFD,DSUMFD,TFDAMP,DFDAMP,FZ,
& ZERO,GV,GD,ZERO,GVT,GDT,WORK,MOKG(L6+1),FG,DFG,
& DACC,DVEL,DOISP,ACC,VEL,DISP,ZERO,ZERO,
& ID,DOF,CNST,JIFLG,COORD
& COSINE,JTCOS)
ELSE
C----- ENERGY FORMULATION WITH/O SPECIAL LOADING MASS ---
BASED ON GROUND MOTION
CALL ENERGY
& (L1,L2,L3,L4,L5,L6,NDOF,MANNOD,NCOSS,BUG11,TRUE,
& IND,IMONS,INDKG,ND,MOMS,MOKG,TRUE,WRITE,ABORT,
& STIFF,KG,MASS,
& ETE,ESE,PSE,EKE,EDD,
& ALPHA,BETA,KFORM,HELMT,NMODE,DT,SUMRB,
& DSUMRC,DSUMRC,SLMFD,DSUMFD,TFDAMP,DFDAMP,FZ,
& GA,GV,GD,GAT,GVT,GDT,WORK,MOKG(L6+1),FG,DFG,
& DACC,DVEL,DOISP,ACC,VEL,DISP,ZERO,ZERO,
& ID,DOF,CNST,JIFLG,COORD
& COSINE,JTCOS)
ENDIF
ELEM=AMAX1(SMGL(EIE),ELEM)
ESEM=AMAX1(SMGL(ESE),ESEM)
PSEM=AMAX1(SMGL(PSE),PSEM)
EKEN=AMAX1(SMGL(EKE),EKEN)
EDDM=AMAX1(SMGL(EDD),EDDM)
IF (ABORT) GO TO 5000
C
C=====
C= GET TOTAL GLOBAL LOAD, DISPL, VELOC AND ACCEL ==
C=====
IF (BUG6) WRITE(6,520)
DO 510 I=L1,NDOF
510 ACC(I)=DACC(I)+ACD(I)
VEL(I)=DVEL(I)+VEL(I)
DISP(I)=DDISP(I)+DISP(I)
LOAD(I)=DLOAD(I)+LOAD(I)
TFDAMP(I)=DFDAMP(I)+TFDAMP(I)
FG(I)=DFG(I)+FG(I)
IF (ABS(ACD(I)).GT.ABS(ACCMARK(I))) ACCMARK(I)=ACD(I)

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IF (ABS(VEL(I)).GT.ABS(VELMAX(I))) VELMAX(I)=VEL(I)
IF (ABS(DISP(I)).GT.ABS(DSPMAX(I))) DSPMAX(I)=DISP(I)
IF (ABS(LOAD(I)).GT.ABS(RCTMAX(I))) RCTMAX(I)=LOAD(I)
IF (BUG)
WRITE (6,550) I,DISP(I),DVEL(I),DACC(I),DLOAD(I),
DISP(I),VEL(I),ACC(I),LOAD(I)
DACC(I)=0.00
DVEL(I)=0.00
DDISP(I)=0.00
DFDAMP(I)=0.00
DLGAD(I)=0.00
510
C
DO 509 I=1,6
SUMRCC(I)=DSUMRCC(I)+SUMRCC(I)
SUMFDC(I)=DSUMFDC(I)+SUMFDC(I)
SUMF0=SQRT(SUMRCC(1)**2+SUMRCC(2)**2+SUMRCC(3)**2)
SUMM0=SQRT(SUMRCC(4)**2+SUMRCC(5)**2+SUMRCC(6)**2)
SUMF0=MAX(SUMF0,SUMFDC)
SUMM0=MAX(SUMM0,SUMM0)
C
320 FORMAT (' DOP',6X,'D0',12X,'DV',12X,'DA',12X,'DP',
12X,' D',12X,' V',12X,' A',12X,' P')
330 FORMAT (1X,I6,1P,9L4.6)
C
C= PRINT TOTAL GLOBAL DISPLACEMENTS, VELOCITIES, ACCELERATIONS ==
C
IF (WRITE) THEN
CALL JOIDSP(1,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,DISP,
TITLE,'DISPLACEMENTS',STEPID,.TRUE.,
NCO,S,COSINE,JTCOS,JTFLG)
CALL JOIDSP(1,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,VEL,
TITLE,'VELOCITIES',STEPID,.TRUE.,
NCO,S,COSINE,JTCOS,JTFLG)
CALL JOIDSP(1,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,ACC,
TITLE,'ACCELERATIONS',STEPID,.TRUE.,
NCO,S,COSINE,JTCOS,JTFLG)
ENDIF
C
C= PRINT TOTAL GLOBAL REACTIONS ==
C
IOPT=5
CALL REACTX IOPT,WRITE,NNODE,1,LS,14,LD,LOAD,ACC,
NMS,MASS,NMS,NDOF,NDOF,1,ONE,
MANNO,IDOF,COORD,LD,TITLE,STEPID,.TRUE.,
NCO,S,COSINE,JTCOS,JTFLG,SUMRCC)
IF (WRITE) WRITE (6,515) SUMRCC,SUMM0
515 FORMAT ('/4X,RESULTANT OF REACTIONS, FORCE=',IP,G12.4,
MOMENT=',G12.4')
DO 511 I=1,6
J=NDOF+I
IF (ABS(RCTMAX(I)).GT.ABS(RCTMAX(J))) RCTMAX(J)=SUMRCC(I)
511 CONTINUE
C
C= CALCULATE AND PRINT TOTAL MEMBER FORCES ==
C
IOPT=5
LSTTYP=0
IF (WRITE) THEN
PRINT=.TRUE.
HEAD=.TRUE.
ELSE
PRINT=.FALSE.
HEAD=.FALSE.
ENDIF
DO 500 IELNO=1,NELMT
CALL ELELIB
& (IOPT,LSTTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,DAMAGE,
IELNO,IELDOF,KGDOF,PGEOM,RINPUT,AXIAL,IZDOSP,IZDOLA,MSTOR)
C
C= CALCULATE AND PRINT DUCTILITY AND EXCURSION RATIOS ==
C
IOPT=11
LSTTYP=0
IF (WRITE) THEN
PRINT=.TRUE.
HEAD=.TRUE.
DO 512 IELNO=1,NELMT
CALL ELELIB
& (IOPT,LSTTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,DAMAGE,
IELNO,IELDOF,KGDOF,PGEOM,RINPUT,AXIAL,IZDOSP,IZDOLA,MSTOR)
ENDIF
C
C= WRITE DATA TO OUTPUT FILES ==
C
IF (WRITE,GT.0) THEN
IF (MOD(ISTEP,WRITE).EQ.0) THEN
IOPT=2
CALL DMPDAT(IOPT,WRITE,TO,DT)
ENDIF
ENDIF
C
C= CHECK ELAPSED CPU TIME ON THE UMRSX SYSTEM ==
CALL CPUTIM(CPUREN,CPUELA)
ITLCPU=CPUREN+CPUELA
IF (ITLCPU,GT.0) THEN
IF (CPUREN,LT,.05*ITLCPU OR CPUREN,LT.5) THEN
WRITE (6,4991) ITLCPU,CPUELA,CPUREN,ISTEP,I
ABORT=.TRUE.
GO TO 5000
4991 FORMAT (//
'======'//
' CPU TIME AT BEGINNING OR EXECUTION.....',I7,' (SEC) =='/
' ELAPSED CPU TIME.....',I7,' (SEC) =='/
' CPU TIME REMAINING.....',I7,' (SEC) =='/
' NUMBER OF STEPS COMPLETED.....',I7,' =='/
' SOLUTION STOP TIME.....',IP,G14.7,' =='/
'======'//)
ENDIF
ENDIF

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500 CONTINUE
C
C= CLOSE OUTPUT FILES ==
C
5000 IF (WRITE,GT.0) THEN
IOPT=5
CALL DMPDAT(IOPT,WRITE,TO,DT)
ENDIF
C
C= PRINT MAXIMUM GLOBAL DISPLACEMENTS ==
C
251 FORMAT ('1 STRUCTURE.....',A,/,
' SOLUTION.....',A,/,
' MAXIMUM VALUES FOR ALL STEPS //')
STEPID=' '
ISTEP=0
WRITE (6,251) TITLE(1),TITLE(2)
CALL JOIDSP(2,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,DSPMAX,
TITLE,'MAXIMUM DISPLACEMENTS',STEPID,.FALSE.,
NCO,S,COSINE,JTCOS,JTFLG)
WRITE (6,251) TITLE(1),TITLE(2)
CALL JOIDSP(2,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,VELMAX,
TITLE,'MAXIMUM VELOCITIES',STEPID,.FALSE.,
NCO,S,COSINE,JTCOS,JTFLG)
WRITE (6,251) TITLE(1),TITLE(2)
CALL JOIDSP(2,MANNO,NDOF,NNODE,1,LS,14,LD,
IDOF,CNST,ACCMAX,
TITLE,'MAXIMUM ACCELERATIONS',STEPID,.FALSE.,
NCO,S,COSINE,JTCOS,JTFLG)
C
C= PRINT MAXIMUM GLOBAL REACTIONS ==
C
WRITE (6,251) TITLE(1),TITLE(2)
DO 5100 I=1,6
SUMRCC(I)=RCTMAX(I)+NDOF)
5100 CONTINUE
CALL REACTX 4,.TRUE.,NNODE,1,LS,14,LD,RCTMAX,DSPMAX,
NMS,MASS,NMS,NDOF,NDOF,1,ONE,
MANNO,IDOF,COORD,LD,TITLE,STEPID,.FALSE.,
NCO,S,COSINE,JTCOS,JTFLG,SUMRCC)
WRITE (6,511) SUMRCC,SUMM0
511 FORMAT ('/4X,MAXIMUM RESULTANT OF REACTIONS, FORCE=',IP,G12.4,
MOMENT=',G12.4')
C
C= PRINT MAXIMUM MEMBER FORCES ==
C
LSTTYP=0
PRINT=.TRUE.
HEAD=.FALSE.
WRITE (6,251) TITLE(1),TITLE(2)
DO 5500 IELNO=1,NELMT
5500 CALL ELELIB
& (LSTTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,DAMAGE,
IELNO,IELDOF,KGDOF,PGEOM,RINPUT,AXIAL,IZDOSP,IZDOLA,MSTOR)
C
C= MEMBER DUCTILITY AND EXCURSION RATIOS ==
C
IF (.NOT.ELSTIC) THEN
PRINT=.TRUE.
HEAD=.FALSE.
WRITE (6,251) TITLE(1),TITLE(2)
DO 5510 IELNO=1,NELMT
5510 CALL ELELIB
& (LSTTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,DAMAGE,
IELNO,IELDOF,KGDOF,PGEOM,RINPUT,AXIAL,IZDOSP,IZDOLA,MSTOR)
ENDIF
C
C= PRINT DAMAGE INDICES ==
C
IF (.NOT.ELSTIC) THEN
LSTTYP=0
HEAD=.FALSE.
PRINT=.TRUE.
WRITE (6,251) TITLE(1),TITLE(2)
DAMAGE=0
DO 5520 IELNO=1,NELMT
CALL ELELIB
& (LSTTYP,PRINT,IREL,HEAD,NAME,ESE,EPSE,EDAM,
IELNO,IELDOF,KGDOF,PGEOM,RINPUT,AXIAL,IZDOSP,IZDOLA,MSTOR)
5520 DAMAGE=DAMAGE+(ESE+PSE)
WRITE (6,5530) DAMAGE
5530 FORMAT ('10X,STRUCTURE DAMAGE INDEX=',IP,G15.5)
ENDIF
C
C= PRINT PEAK ENERGY INFO ==
C
WRITE (6,251) TITLE(1),TITLE(2)
WRITE (6,5540) ELEM,ELEM,PGEOM,ELEM,EDDM
5540 FORMAT (' PEAK ENERGY VALUES // IP,
' MAX INPUT ENERGY.....',G12.5/,
' MAX ELASTIC STRAIN ENERGY.....',G12.5/,
' MAX PLASTIC STRAIN ENERGY.....',G12.5/,
' MAX KINETIC ENERGY.....',G12.5/,
' MAX DAMPING ENERGY.....',G12.5/)
C
RETURN
C
250 FORMAT ('1 STRUCTURE.....',A,/,
' SOLUTION.....',A,/,
' 2X,A,/, ' LOADING #',15,5X,A)
C
END
SUBROUTINE SOL05
LOGICAL TEST,QUIT,BTEST
INCLUDE (ZCOMM)
C
SET UP CONSTANTS
L1=1

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L2=NCOND
L3=L2+1
L4=NCOND+NFREE
L5=L4+1
L6=NDOF
ELSTIC=.TRUE.
C
C----- INITIALIZE STORAGE
Z(IZEVAL) = LOCATION OF THE EIGENVALUES
Z(IZEVEC) = LOCATION OF THE EIGENVECTORS
Z(IZA) = LOCATION OF THE SYMMETRIC STIFFNESS
Z(IZB) = LOCATION OF THE SYMMETRIC MASS OR KG
C
IZEVAL = IZ
IZ = IZ+NFREE
IZEVEC = IZ
IZ = IZ+NFREE*NFREE
IZA = IZ
IZB = IZ
IZ = IZ+NFREE*(NFREE+1)/2
IZTMP = IZ
IZ = IZ+NDOF
IMZIZ
C
CALL CKSTOR(NDOF,IM)
C
IMD = NZ(IZMD+NDOF)
IMDMS = NZ(IZDMS+NDOF)
IMDKG = NZ(IZDKG+NDOF)
IMDAB = NFREE*(NFREE+1)/2
C
C----- FORM MASS MATRIX -----
DO 400 I=1,IMDMS
Z(I+IZMASS-1)=0.
C
CALL MFORM(2,IMASS,MMASS,Z(IZMASS),NZ(IZDMS),NO,NDOF,IMDMS,
& TITLE,MODE,MANNO,NCOS,BTEST(I,IBUG,5),IBUG,
& NZ(IZID),Z(IZCOS),NZ(IZIDOF),Z(IZCNST),NZ(IZFLG),
& NZ(IZJCS),Z(IZJGOT),Z(IZJ),Z(IZJMP),Z(IZJ27),
& Z(IZ+65),Z(IZ+99))
C
CALL SOLOSA
& (L1,L2,L3,L4,L5,L6,IMD,IMDMS,IMDKG,IMDAB,KGCOND,MCOND,ABORT,
& Z(IZKGT),NZ(IZKGT+1),NZ(IZKGT+2),NZ(IZKGT+5),
& NDOF, NCOND, NFREE, TITLE, STEPID,
& Z(IZSTIF),Z(IZMASS),Z(IZKG),Z(IZA),Z(IZB),
& NZ(IZMD),NZ(IZDMS),NZ(IZDKG),Z(IZJ),Z(IZJMP),
& NMODE, NCOS, NELMT, MANNO, IBUG,
& NZ(IZID),NZ(IZIDOF),Z(IZCNST),NZ(IZFLG),Z(IZCORO),
& Z(IZCOS),NZ(IZJCS),Z(IZZEVAL),Z(IZZEVEC))
C
RETURN
END
C
SUBROUTINE SOLOSA
& (L1,L2,L3,L4,L5,L6,IMD,IMDMS,IMDKG,IMDAB,KGCOND,MCOND,ABORT,
& KGDATA,KGLOAD,KGTIPE,KGFORM,
& NDOF, NCOND, NFREE, TITLE, STEPID,
& STIFF, MASS, KG, A, B,
& MD, MMS, MOKG, WORK, TMP,
& NMODE, NCOS, NELMT, MANNO, IBUG,
& ID, IDOF, CNST, JFLG, COORD,
& COSINE, JTCOS, EVAL, EVEC,
LOGICAL TEST,QUIT,BTEST,MCOND,KGCOND,MCOND1,KCOND1,ABORT
REAL MASS,KG,KGDATA
DIMENSION STIFF(IMD),MASS(IMDMS),KG(IMDKG),A(IMDAB),B(IMDAB)
DIMENSION MD(L6+1),MMS(L6+1),MOKG(L6+1),WORK(L6),TMP(L6)
DIMENSION EVAL(NFREE),EVEC(NFREE),SUMRGT(6)
DIMENSION COORD(MANNO,5),JTCOS(MANNO)
& JDFLG(MANNO,6),COSINE(5,5),NCOS,CNST(MANNO,6),
& IDFLG(MANNO),JTCOS(MANNO))
C
CHARACTER*1 NAME
CHARACTER*40 OPTION
CHARACTER*(*) TITLE(2),STEPID
C
C=====
C= INPUT DATA =====
C-----
READ(5,*) OPTION,IPRT,IPRT2
C
IF (TEST(OPTION,'FREQ').FALSE.) THEN
IOPT=1
OPTION='NATURAL FREQUENCIES'
ELSE IF (TEST(OPTION,'BUCK').FALSE.) THEN
IOPT=2
OPTION='ELASTIC BUCKLING LOAD'
ELSE
WRITE(6,*) 'SOL-05 INVALID OPTION: ',OPTION
RETURN
ENDIF
C
IF (IPRT.LE.0) IPRT=NFREE
IPRT=MIN(NFREE,IPRT)
IPRT2=MIN(IPRT2,IPRT)
C
WRITE(6,10) TITLE(1),TITLE(2),OPTION,IPRT
10 FORMAT('1 STRUCTURE.....',A,/,
& ' SOLUTION.....',A,/)
&K,' SOLUTION #S, DETERMINE EIGENVALUES AND EIGENVECTORS '//
&K,' OPTION:.....',A,/,
&K,' NUMBER OF EIGENVALUES:.....',IS)
C
C=====
C= FORMULATE STIFFNESS =====
C-----
CALL FORM(I)
IF (BTEST(1,IBUG,5)) CALL LMATRIX(STIFF,NO,NDOF,IMD,
& 'GLOBAL STIFFNESS MATRIX')
C
C=====
C= FORM GEOMETRIC STIFFNESS =====
C-----
C FORMULATE THE GEOMETRIC STIFFNESS IF THE FLAG MENK IS TRUE, THIS
FLAG INITIALIZED ABOVE
C
IF (KGDATA(1)=1), THE GEOMETRIC STIFFNESS IS FORMED ONCE, AND
MULTIPLIED BY A SCALAR TO ACCOUNT FOR CHANGES
IN THE TOTAL VERTICAL LOAD. THUS THE GEOMETRIC

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STIFFNESS ONLY NEEDS TO BE FORMED ONCE.
IF (KGDATA(1)=2), THE GEOMETRIC STIFFNESS IS BASED ON THE AXIAL
FORCE IN THE ELEMENTS, AND IS RECALCULATED EACH
TIME THE AXIAL FORCE CHANGES.
IF (KGDATA(1)=1), THE GEOMETRIC STIFFNESS IS FORMED WITH THE
STIFFNESS, THUS A SEPERATE CALL TO FORM IS
NOT NEEDED.
IF (KGDATA(1)=2), A SEPERATE GEOMETRIC STIFFNESS MATRIX IS FORMED
FORMULATE SEPERATE GEOMETRIC STIFFNESS MATRIX
IF (IOPT.EQ.2) THEN
KGFORM=2
KGDATA=0
I2=2
CALL FORM(I2)
IF (BTEST(1,IBUG,5)) CALL LMATRIX(KG,MOKG,NDOF,IMDKG,
& 'GLOBAL GEOMETRIC STIFFNESS MATRIX')
ELSE
IF (BTEST(1,IBUG,5)) CALL LMATRIX(MASS,MMS,NDOF,IMDMS,
& 'GLOBAL MASS MATRIX')
ENDIF
C
C=====
C= CONDENSE OUT NON-FREE DOF =====
C-----
IF (MCOND IS TRUE THE MASS MATRIX IS ALSO REDUCED BY GUYAN REDUCTION)
IF (KCOND.GT.0) THEN
I1=1
IF (IOPT.EQ.2) THEN
MCOND1=.FALSE.
KCOND1=KCOND
ELSE IF (IOPT.EQ.1) THEN
KCOND1=.FALSE.
MCOND1=MCOND
ENDIF
SET UP COLUMN ZERO LOAD VECTOR
DO 28 I=1,NDOF
IMV(I)=0
CALL MSOLL(1,BTEST(1,IBUG,6),L6,IMD,NDOF,1,1,1,L2,
& MD,STIFF,TMP,WORK,
& MCOND1,MASS,MMS,IMDMS,
& KCOND1,KG,MOKG,IMDKG,ABORT)
IF (ABORT) RETURN
ENDIF
C
C=====
C= TRANSFER STIFFNESS INTO A MATRIX =====
C-----
NOTE: THIS ROUTINE USES A SYMMETRIC MATRIX DEFINED BELOW
C
1 2 3
2 5 6
3 9 10
11 12 13 14 15
16 17 18 19 20 21
22 23 24 25 26 27 28
C
NOTE: THE STORAGE METHOD USED
FOR STIFFNESS, MASS AND
GEOMETRIC STIFFNESS ARE
DIFFERENT.
C
QUIT=.FALSE.
L=0
DO 50 I=L5,L6
DO 50 J=L5,I
L=L+1
JI=MD(I)+I-J
J2=MD(I+1)
IF (JI.GE.J2) THEN
ACL=0.
ELSE
ACL=STIFF(JI)
ENDIF
IF (BTEST(1,IBUG,5)) WRITE(6,29) I,J,L,JI,J2,ACL
29 FORMAT('1',IS,' J',IS,' L',IS,' JI',IS,' J2',IS,' A',
& ' IP,615.5)
C
CHECK FOR ZERO'S ON MAIN DIAGONAL
IF (I.EQ.J .AND. ACL.LE.0) THEN
QUIT=.TRUE.
WRITE(6,52) I,ACL)
ENDIF
50 CONTINUE
52 FORMAT('5X,DOF #',IS,' IS .LE. 0 IN THE STIFFNESS MATRIX...',
& '5X,('I,I)=',IP,612.4,' SOLN IS ABORTED')
C
C=====
C= TRANSFER MASS OR GEOMETRIC STIFFNESS INTO B MATRIX =====
C-----
IF (IOPT.EQ.1) THEN
L=0
DO 40 I=L5,L6
DO 40 J=L5,I
L=L+1
JI=MDMS(I)+I-J
J2=MDMS(I+1)
IF (JI.GE.J2) THEN
BCL=0.
ELSE
BCL=MASS(JI)
ENDIF
IF (BTEST(1,IBUG,5)) WRITE(6,59) I,J,L,JI,J2,BCL)
59 FORMAT('1',IS,' J',IS,' L',IS,' JI',IS,' J2',IS,' B',
& ' IP,615.5)
C
CHECK FOR ZERO'S ON MAIN DIAGONAL
IF (I.EQ.J .AND. BCL.LE.0) THEN
QUIT=.TRUE.
WRITE(6,42) I,BCL)
ENDIF
40 CONTINUE
42 FORMAT('5X,DOF #',IS,' IS .LE. 0 IN THE MASS MATRIX...',
& '5X,('I,I)=',IP,612.4,' SOLN IS ABORTED')
ELSE
L=0
DO 50 I=L5,L6
DO 50 J=L5,I
L=L+1
JI=MDKG(I)+I-J
J2=MDKG(I+1)
IF (JI.GE.J2) THEN

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ELSE BCL=0.
      BCL)=KGCJ(I)
      ENDDIF
49 IF (BTEST(1BUG,5)) WRITE (6,49) I,J,L1,J1,L2,BCL)
      FORMAT (' I',15,' J',15,' L',15,' J1',15,' J2',15,' B',
      IP,15.5)
C----- CHECK FOR ZERO'S ON MAIN DIAGONAL
      IF (I.EQ.J .AND. BCL).LE.0) THEN
          QUIT=.TRUE.
          WRITE (6,52) I,BCL)
          ENDDIF
C
S0 CONTINUE
S2 FORMAT ('SK,DOF #',15,
      & ' IS .LE. 0 IN THE GEOMETRIC STIFFNESS MATRIX...',
      & ' SK,(X,I,1),IP,15.5, ' SOLN IS ABORTED')
C
      ENDDIF
C----- RETURN IF A MAIN DIAGONAL IS LE ZERO
      IF (QUIT) RETURN
C=====
C= SOLVE FOR EIGENVALUES AND EIGENVECTORS =====
C----- DMSL SU ROUTINE EI2ZS
C EIGENVALUES AND EIGENVECTORS OF A*X-LAMBDA*B*X=0
C A = STIFFNESS - REAL, SYMMETRIC MATRIX
C B = MASS OR GEOMETRIC STIFFNESS - REAL, SYMMETRIC MATRIX
C N = NUMBER OF DOF OF A AND B
C IJOB = 0 - CALC. EIGENVALUES ONLY
C       = 1 - CALC. EIGENVALUES AND EIGENVECTORS
C       = 2 - CALC. EIGENVALUES, EIGENVECTORS AND PERFORMANCE INDEX,
C       = 3 - CALC. PERFORMANCE INDEX, PI
C PISAK(1), PIS(1) - ROUTINE PERFORMED WELL
C 1<PI<100 - ROUTINE PERFORMED SATISFACTORILY
C 100<PI - ROUTINE PERFORMED POORLY
C O = EIGENVALUES (LAMBDA), N BV 1
C Z = EIGENVECTORS, N BV N
C IZ = ROW DIMENSION OF Z MATRIX
C WK = WORK AREA, N*(N+1)
C IER = ERROR PARAMETER
C 129 - A IS NOT POSITIVE DEFINITE
C 129+J - ROUTINE FAILED ON EIGENVALUE J, EIG'S 1 TO J-1 ARE OK
C-----
      IJOB=2
      IER=0
      CALL EI2ZS(A,B,NFREE,IJOB,EVAL,EVEC,NFREE,WORK,IER)
      IF (IER.NE.0) WRITE (6,*)
      & 'ER, 'ROR CODE',IER, ' IN DMSL ROUTINE EI2ZS'
      WRITE (6,*) ' PERFORMANCE INDEX:',WORK(1)
C-----
C= NORMALIZE MODE SHAPE TO MAX VALUE OF ONE =====
      DO 90 J=1,IPRT
          AMIN=0
          AMAX=0
          DO 80 I=1,NFREE
              AMIN=MIN(AMIN,EVECC(I,J))
              AMAX=MAX(AMAX,EVECC(I,J))
          IF (AMIN.GT.AMAX) AMAX=AMIN
          IF (AMAX.EQ.0) AMAX=1
      C
      90 I=1,NFREE
          EVECC(I,J)=EVECC(I,J)/AMAX
C-----
C= PRINT EIGENVALUES AND EIGENVECTORS =====
      IST=1
      IEND=MIN(IST+6,IPRT)
      WRITE (6,110) I
      IF (I.EQ.2) THEN
          WRITE (6,120) (EVAL(I),I,IST,IEND)
      ELSE IF (IOPT.EQ.1) THEN
          DO 125 I=IST,IEND
              EVAL(I)=EVECC(I,I)
              WRITE (6,126) (EVAL(I),I,IST,IEND)
          DO 127 I=IST,IEND
              EVAL(I)=EVAL(I) / 6.2851855
              WRITE (6,128) (EVAL(I),I,IST,IEND)
          DO 129 I=IST,IEND
              IF (EVAL(I).EQ.0) EVAL(I)=1.E-15
              EVAL(I)=1.00 / EVAL(I)
              WRITE (6,130) (EVAL(I),I,IST,IEND)
          ENDDIF
          WRITE (6,135)
          110 FORMAT('      MODE',7(I10,5X))
          120 FORMAT('      EIGENVALUE:',7(G14.5,1X))
          126 FORMAT('      FREQ (RAD/SEC):',7(G14.5,1X))
          128 FORMAT('      FREQUENCY (HZ):',7(G14.5,1X))
          130 FORMAT('      PERIOD (SEC):',7(G14.5,1X))
          135 FORMAT('      EIGENVECTORS:')
C-----
C= EIGENVECTORS
      DO 140 I=1,NFREE
          II=I+NCOOD
          140 WRITE (6,150) II,(EVECC(I,J),I,IST,IEND)
          150 FORMAT('      DOF',16,' ',IP,7(G14.5,1X))
C-----
      IF (IEND.LT.IPRT) THEN
          WRITE (6,10) TITLE(1),TITLE(2),OPTION,IPRT
          IST=IEND+1
          GO TO 100
      ENDDIF
C=====
C= CALC EIGEN VECTORS FOR NONDYNAMIC DOF =====
C-----
C----- TRANSFER EIGENVECTORS TO TEMP STORAGE
C
      DO 500 IFREQ=1,IPRTZ
C-----
C----- TRANSFER EIGENVECTORS TO TEMP STORAGE
      DO 200 J=L1,L2
          WORK(J)=0
      DO 210 J=L3,L4
          WORK(J)=EVECC(J-L2,IFREQ)
      DO 220 J=L5,L6

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      SOL01960 220 WORK(J)=0
      SOL01970
      SOL01980
      C----- CALC EIGENVECTORS FOR CONDENSED OUT DOF
      SOL01990 CALL REACT(I1,BTEST(1BUG,6),NMODE,L1,L2,L3,L4,THP,WORK,
      & MD,STIFF,IMD,NDOF,I,1,1,0,
      SOL02000 & NAKMO,IOF,COORD,ID,TITLE,STEPID,.FALSE.,
      SOL02010 & NCOO,COSINE,JTCOS,JFLG,SUBRECT)
      SOL02020 CALL HSCALE(5,BTEST(1BUG,6),L4,IMD,NDOF,I1,L1,L2,
      SOL02040 & MD,STIFF,THP,WORK,
      SOL02050 & .FALSE.,MASS,NEMS,1,
      SOL02060 & .FALSE.,KG ,MDKG,I,ABORT)
      SOL02070 IF (ABORT) RETURN
      SOL02080
      SOL02090
      C----- NORMALIZE MODE SHAPE TO MAX VALUE OF ONE
      SOL02100 AMIN=0
      SOL02110 AMAX=0
      SOL02120 DO 230 I=L1,L6
          AMIN=MIN(AMIN,WORK(I))
          AMAX=MAX(AMAX,WORK(I))
      SOL02150 230 IF (AMIN.GT.AMAX) AMAX=AMIN
      SOL02160
      SOL02170 DO 240 I=L1,L6
          WORK(I)=WORK(I)/AMAX
      SOL02180
      SOL02190
      SOL02200
      C----- PRINT EIGENVALUE AT EACH MODE
      SOL02210 IF (IOPT.EQ.2) WRITE (STEPID,250) IFREQ,EVAL(IFREQ)
      SOL02220 IF (EVAL(IFREQ).EQ.0) EVAL(IFREQ)=1.E-15
      SOL02230 FREQ=1.00/EVAL(IFREQ)
      SOL02240 IF (IOPT.EQ.1) WRITE (STEPID,260) IFREQ,FREQ
      SOL02250
      C-----
      SOL02260 CALL JOTDSP(L1,NAKMO,NDOF,NMODE,I,L3,L4,LD,
      SOL02270 & IOF,CNST,WORK,
      SOL02280 & TITLE,'EIGENVECTORS',STEPID,.TRUE.,
      SOL02290 & NEMS,COSINE,JTCOS,JFLG)
      SOL02500 250 FORMAT ('MODE #',15,' EIGENVALUE:',1P,15.6)
      SOL02510 260 FORMAT ('MODE #',15,' FREQUENCY:',1P,15.6)
      SOL02520 500 CONTINUE
      SOL02530
      SOL02540 RETURN
      SOL02550
      SOL02560 END
      SOL02570
      C-----
      SOL02580 SUBROUTINE SOLO
      SOL02590 LOGICAL BTEST,UNBAL
      SOL02600 INCLUDE (ZCOMM)
      SOL02610
      SOL02620
      C=====
      SOL02630 C= SET GEOMETRIC STIFFNESS FLAGS =====
      SOL02640
      SOL02650 Z(IZKGD)=0.00
      SOL02660 K(LOAD)=Z(IZKGD+1)
      SOL02670 K(VE)=Z(IZKGD+2)
      SOL02680 K(FORM)=Z(IZKGD+5)
      SOL02690
      C-----
      SOL02700 C= READ INFO AND SET OPTIONS =====
      SOL02710 READ (5,*) NAKELD,IPRINT,IWRITE,UNBAL
      SOL02720 IPRINT=NAKELD*IPRINT,1)
      SOL02730
      C-----
      SOL02740 C= PRINT HEADER =====
      SOL02750 WRITE (6,101) TITLE(1),TITLE(2),IPRINT,IWRITE
      SOL02760 101 FORMAT ('1 STRUCTURE.....',A, /
      SOL02770 & ' SOLUTION.....',A, /
      SOL02780 & ' SOLUTION #', ' STATIC NONLINEAR SOLUTION ' /
      SOL02790 & ' ', ' USE NEMAK(5)=1 TO INCLUDE GEOMETRIC STIFFNESS.' /
      SOL02800 & ' ', ' INTERVAL FOR PRINTING DATA.....',15, /
      SOL02810 & ' ', ' INTERVAL FOR WRITING DATA TO FILE.....',15, /
      SOL02820
      C-----
      SOL02830 IF (K(FORM.EQ.2) WRITE (6,11)
      SOL02840 11 FORMAT ('X', ' GEOMETRIC STIFFNESS IS NOT INCLUDED. '
      SOL02850 & ' IF ( UNBAL) WRITE (6,15) ' & ' NOT '
      SOL02860 15 FORMAT(' UNBALANCED JOINT FORCES',A,' ADDED TO THE NEXT CYCLE')
      SOL02870
      C=====
      SOL02880 C= INPUT FILE OUTPUT CONTROL DATA =====
      SOL02890
      SOL02900 IF (IWRITE.GT.0) THEN
          IOPT=1
          IO=0
          CALL DNDPAT(IOPT,IWRITE,TO,DT)
          ENDDIF
      C-----
      SOL02910 C= INITIALIZE STORAGE REQ'D FOR THIS SOLN =====
      SOL02920
      SOL02930 C Z(IZLOAD) = LOCATION OF THE TOTAL LOAD MATRIX
      SOL02940 C Z(IZDISP) = LOCATION OF THE TOTAL DISPLACEMENT MATRIX
      SOL02950 C Z(IZVEL) = LOCATION OF THE TOTAL VELOCITY MATRIX
      SOL02960 C Z(IZDLOA) = LOCATION OF THE INCREMENTAL LOAD MATRIX
      SOL02970 C Z(IZDISP) = LOCATION OF THE INCREMENTAL DISPLACEMENT MATRIX
      SOL02980 C Z(IZVEL) = LOCATION OF THE INCREMENTAL VELOCITY MATRIX
      SOL02990 C Z(IZIQ) = LOCATION OF THE JOINT LOADS
      SOL03000 C Z(IZR) = LOCATION OF THE ELEMENT LOADS
      SOL03010
      SOL03020 IF (IZLOAD.EQ.0) THEN
          IZLOAD = IZ
          IZ = IZ+NDOF
          DO 1 I=L1,NDOF
              Z(I+IZLOAD-1) = 0
          ENDDIF
      SOL03030
      SOL03040 IF (IZDISP.EQ.0) THEN
          IZDISP = IZ
          IZ = IZ+NDOF
          DO 2 I=L1,NDOF
              Z(I+IZDISP-1) = 0
          ENDDIF
      SOL03050
      SOL03060 IF (IZVEL.EQ.0) THEN
          IZVEL = IZ
          IZ = IZ+NDOF
          DO 5 I=L1,NDOF
              Z(I+IZVEL-1) = 0
          ENDDIF
      SOL03070
      SOL03080 IF (IZDLOA.EQ.0) THEN
          IZDLOA = IZ
          SOL03090
          SOL03100
          SOL03110
          SOL03120
          SOL03130
          SOL03140
          SOL03150
          SOL03160
          SOL03170
          SOL03180
          SOL03190

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      SOL03200
      SOL03210
      SOL03220
      SOL03230
      SOL03240
      SOL03250
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      SOL03270
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      SOL03790
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      SOL03820
      SOL03830
      SOL03840
      SOL03850
      SOL03860

```

```

      IZ = IZ+NDOF
      DO 5 I=1,NDOF
        Z(I+IZDLOA-1) = 0
      ENDDIF
    C
    IF (IZDOSP.EQ.0) THEN
      IZDOSP = IZ
      IZ = IZ+NDOF
      DO 6 I=1,NDOF
        Z(I+IZDOSP-1) = 0
      ENDDIF
    C
    IF (IZDVEL.EQ.0) THEN
      IZDVEL = IZ
      IZ = IZ+NDOF
      DO 7 I=1,NDOF
        Z(I+IZDVEL-1) = 0
      ENDDIF
    C
    IZQ = IZ
    IZ = IZ+NDOF
    DO 8 I=1,NDOF
      Z(I+IZQ-1) = 0
    C
    IZR = IZ
    IZ = IZ+NDOF
    DO 9 I=1,NDOF
      Z(I+IZR-1) = 0
    C
    IF (IZFUB.EQ.0) THEN
      IZFUB = IZ
      IZ = IZ+NDOF
      ENDDIF
      DO 10 I=1,NDOF
        Z(I+IZFUB-1) = 0
    C
    IZUBLD = IZ
    IZ = IZ+NDOF
    IZUBDP = IZ
    DO 12 I=1,NDOF
      Z(I+IZUBLD-1) = 0
      Z(I+IZUBDP-1) = 0
    C
    IZ = IZ+1
    C----- DETERMINE THE LENGTH OF THE STIFFNESS MATRIX
      MD=NZ(IZND+NDOF) - NZ(IZND) + 1
    C
    C----- SET UP CONSTANTS -----
      L1=L
      L2=NCONO
      L3=L2+1
      L4=NCONO+NFREE
      L5=L4+1
      L6=NDOF
    C
      NLQAD=1
    C
      ELSTIC=.FALSE.
    C
    IF (MARELD.GT.0) THEN
      IZELD=IZ
      IZ = IZ + MARELD*5
      IZELD=IZ
      IZ = IZ + MARELD*12
    ENDDIF
    C-----
      IZFG = IZ
      IZ = IZ+NDOF
      IZDFG = IZ
      IZ = IZ+NDOF
      IZDMAX = IZ
      IZ = IZ+NDOF
      IZRMAX = IZ
      IZ = IZ+NDOF
      IZDRL0 = IZ
      IZ = IZ+NDOF
      IZDRL0A = IZ
      IZ = IZ+NDOF
      DO 27 I=0,NDOF-1
        Z(IZFG+I) = 0
        Z(IZDFG+I) = 0
        Z(IZDMAX+I) = 0
        Z(IZRMAX+I) = 0
        Z(IZDRL0A+I) = 0
      ENDDIF
    C
    C----- CHECK MEMORY -----
      CALL CKSTOR(NDOF,IM)
    C
    C----- SET UP CONSTANTS -----
      IMD = NZ(IZND + NDOF)
      IMONS = NZ(IZDONS + NDOF)
      IMOKG = NZ(IZDKG + NDOF)
      IMONSL = 1
      IMOS = 1
    C
    C-----
    C= ZERO GROUND MOTION ==
    C-----
      DO 18 I=1,6
        SUMRC(I) = 0.
    C
    C= ZERO GROUND MOTION ==
    C-----
      DO 19 I=1,9
        GROUND(I) = 0.
    C
    C-----
    C= CALC PRINTING INFO ==
    C-----
      IPDISP = 6+MNODE
      IPRCTN = 7
      DO 20 I=1,MNODE
        DO 15 J=0,5
          IF (BITEST(NZ(IZJFLG-1+I),J)) THEN
            IPRCTN=IPRCTN+1
            GO TO 20
          ENDDIF

```

```

      SOL00870 15 CONTINUE
      SOL00880 20 CONTINUE
      SOL00890 IPELEM=NEUMT
      SOL00900 LSTTYP=0
      SOL00910 * DO 26 I=1,MELMT
      SOL00920 * J=NZ(IZJFLG-1)
      SOL00930 IF (NZC(I).NE.LSTTYP) IPELEM=IPELEM+4
      SOL00940 26 LSTTYP=NZC(I)
      SOL00950 111 FORMAT (OP,' ZMATRCK',I6,' ',I15,IP,C20,10)
    C
    CALL SOL004
      & CL1,L2,L5,L4,L5,L6,IMD,IMONS,IMDKG,IMOS,IMONSL,ABORT,
      & MARELD,IPRNT,IMRITE,UMBAL,
      & NLOAD,MNODE,MOS,MELMT,
      & IZDOSP,IZDLOA,IZUG,MARELD,
      & TITLE,STEPID,NDOF,NFREE,Z(IZDRL0A),
      & KFORM,KLOAD,KGTYPE,MCONO,Z(IZDRLD),
      & NEWKG,NEWK,MCONO,KCONO,SUMRC,
      & Z(IZDOSP),Z(IZVEL),Z(IZLOAD),Z(IZR),Z(IZFUB),
      & Z(IZDOSP),Z(IZVEL),Z(IZDLOA),Z(IZR),Z(IZH),
      & Z(IZSTIF),Z(IZMASS),Z(IZKG),Z(IZELD),Z(IZUBLD),
      & NZ(IZND),NZ(IZDONS),NZ(IZDKG),NZ(IZTEL),Z(IZUBDP),
      & NZ(IZQ),NZ(IZDFG),Z(IZONST),NZ(IZJFLG),Z(IZCOORD),
      & Z(IZCOS),NZ(IZCOS),EIE,ESE,PSE,EKE,EDO,
      & Z(IZFG),NZ(IZDFG)
      RETURN
    C
    END
    C-----
    SUBROUTINE SOL004
      & CL1,L2,L5,L4,L5,L6,IMD,IMONS,IMDKG,IMOS,IMONSL,ABORT,
      & MARELD,IPRNT,IMRITE,UMBAL,
      & NLOAD,MNODE,MOS,MELMT,
      & IZDOSP,IZDLOA,IZUG,MARELD,
      & TITLE,STEPID,NDOF,NFREE,RLOAD,
      & KFORM,KLOAD,KGTYPE,MCONO,DRLOA,
      & NEWKG,NEWK,MCONO,KCONO,SUMRC,
      & IPDISP,IPRCTN,IPELEM,DSPMAX,ACTMAX,
      & ODISP,DVEL,OLQAD,Q,FUB,
      & STIFF,MASS,KG,ELD,UBLQAD,
      & MD,MOS,MKG,ELD,UBLDISP,
      & ID,IDOF,CNST,JFLG,COORD,
      & COSINE,JTCOS, EIE,ESE,PSE,EKE,EDO,
      & FG,DFG
    C
    DOUBLE PRECISION EIE,ESE,PSE,EDO,EKE
    C
    CHARACTER*(*) TITLE(2),STEPID
    LOGICAL IPRINT,DSPLG,HEAD,REPEAT,AXIAL,TEST,NEWKY,BTEST,ABORT
    LOGICAL NEWKG,NEWK,MCONO,KCONO,UMBAL,MCONO2,KCONO2,WRITE
    LOGICAL BUGS,BUGS,BUG6,BUG11
    CHARACTER*80 NAME
    CHARACTER*20 INTEG
    REAL LOAD,MASS,MASSSL,KG,MOS
    INTEGER FOMF,MASS
    DIMENSION SUMRC(6),DSUMRC(6),SUMFX(6),DSUMFX(6),SUMRC(6),SUMRC(6)
    DIMENSION DSUMRC(6),ACTMAX(6),DRLOA(6),RLOAD(6)
    DIMENSION DIMINP(100)
    DIMENSION STIFF(DM),MASS(DONS),KG(DMKG)
    DIMENSION MD(L6+1),MOS(L6+1),MKG(L6+1)
    DIMENSION LOAD(L6),DISP(L6),VEL(L6),R(L6),FGL(L6),DFGL(L6)
    DIMENSION DLOAD(L6),DISP(L6),DVEL(L6),R(L6)
    DIMENSION FUB(L6),UBLQAD(L6),UBLDISP(L6)
    DIMENSION MORK(2*L6)
    DIMENSION COOR(MARELD*3),ID(MARELD)
    DIMENSION IDOF(MARELD),COSINE(5),MOS,CONST(MARELD*6),
      & JFLG(MARELD),JTCOS(MARELD)
    DIMENSION IELDX(1),ELDX(1)
    DIMENSION GAK(5),GV(5),GD(5)
    DIMENSION GAT(5),GVT(5),GDT(5)
    LOGICAL NEWKAC
    CHARACTER*10 STEP,STEP2
    C
    SUMRC(1)=0
    SUMRC(2)=0
    SUMRC(3)=0
    SUMRC(4)=0
    SUMRC(5)=0
    SUMRC(6)=0
    SUMF0=0
    SUMF0=0
    SUMF0=0
    SUMF0=0
    C-----
    BUGS = BITEST(BUG, 5)
    BUGS = BITEST(BUG, 5)
    BUG6 = BITEST(BUG, 6)
    BUG11 = BITEST(BUG, 11)
    C-----
    C
    C----- INITIALIZE ENERGY CONSTANTS -----
    C-----
    EIE=0
    ESE=0
    PSE=0
    EKE=0
    EDO=0
    C
    C-----
    C= SET GEOMETRIC STIFFNESS FLAGS ==
    C-----
    IF (KLOAD.EQ.0 .OR. KGTYPE.EQ.0 .OR. KFORM.EQ.0) NEWKG=.FALSE.
    C
    C= SET STIFFNESS FLAGS ==
    C-----
    NEWK = .TRUE.
    KSAME = 0
    C
    C-----
    C= INPUT LOADING DATA ==
    C-----
    C----- MATRICES Q AND R ARE ZEROED IN THE CALLING PGM. -----
    C
    C----- INPUT JOINT LOADS -----
    C
    C= JOINT LOADS AND SUPPORT DISPLACEMENTS ARE STORED IN Q
    CALL J01LQ(BUGS,MARELD,NDOF,MNODE,NLOAD,
      & ID,IDOF,CNST,Q,DSPLG,JFLG,TITLE,.FALSE.)
    C

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      SOL02110
      SOL02120
      SOL02130
      SOL02140
      SOL02150
      SOL02160
      SOL02170
      SOL02180
      SOL02190
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      SOL02270
      SOL02280
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      SOL02370
      SOL02380
      SOL02390
      SOL00090
      SOL00090
      SOL00060
      SOL00070
      SOL00080
      SOL00090
      SOL00100
      SOL00110
      SOL00120
      SOL00130
      SOL00140
      SOL00150
      SOL00160
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      SOL00880
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      SOL00900
      SOL00910
      SOL00920
      SOL00930
      SOL00940
      SOL00950
      SOL00960
      SOL00970
      SOL00980
      SOL00990
      SOL01000
      SOL01010
      SOL01020

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C ----- INPUT ELEMENT LOADS -----
C ELEMENT LOADS ARE STORED IN R
C IF (MAKELD.GT.0)
  & CALL ELEMLOC(BUGS,LS,NELMT,MAKELD,MELD,NDOF,MLOAD,
  & R,ZELO,ELD,IZDISP,IZLOAD, NAME,TITLE,.FALSE.)
C
C
C=====
C=WRITE INITIAL DATA TO OUTPUT FILE =====
C IF (DIRITE.GT.0) THEN
  IOPT=2
  CALL DMPDAT(IOPT,DIRITE,TO,DT)
ENDIF
C
C
C=====
C= LOOP FOR EACH TIME STEP ISTEP=CURRENT STEP # =====
C... ISTEP = STEP NUMBER
C FACTOR= CURRENT TARGET LOAD = FACTOR*(INPUT LOAD)
C FACTL = PREVIOUS TARGET LOAD
C FACT2 = NEXT TARGET LOAD
C DF = LOAD STEP
C DFL = PREVIOUS LOAD STEP
C DFN = NEXT LOAD STEP
C FMAX = MAXIMUM ALLOWABLE INCREMENTAL LOAD / STEP
C DMAX = MAXIMUM ALLOWABLE INCREMENTAL DISPLACEMENT / STEP
C
  ISTEP=0
  FACTL=0
  DF=0
  READK5,* STEP2,FACT2,PHAX2,DMAX2,NUMB2
1000 STEP =STEP?
  IF (TEST(STEP,'END',.FALSE.)) GO TO 5000
  FACTOR=FACT2
  PHAX =PHAX2
  DMAX =DMAX2
  NUMB =NUMB2
  NUMDOP=NUMB2
  READK5,* END=1010) STEP2,FACT2,PHAX2,DMAX2,NUMB2
  GO TO 1020
1010 STEP2='END'
  FACT2=FACTOR
1020 IF (TEST(STEP,'END',.FALSE.)) GO TO 5000
  IF (FACTOR.EQ.0) GO TO 1000
C
1100 ISTEP=ISTEP+1
  WRITE (STEPID,90) STEP,ISTEP,FACTOR
  IF (BUGS.OR.BUGS.OR.BUG6.OR.BUG11) THEN
    WRITE (6,91) STEP,ISTEP,FACTOR
    WRITE (6,*) 'MEMB:',MEMBK,' MEMBK:',MEMBK
  ENDIF
  90 FORMAT ('A',STEP',IS',FACTOR',JP,G11,4)
  91 FORMAT ('1',A,STEP',IS',FACTOR',JP,G11,4)
C
C=====
C= CALC INCREMENTAL LOADS ==
C=====
C 1) ADD ELEMENT LOADS, AND JOINT LOADS ON FREE JOINTS
C 2) SAVE IN DLOA FOR CALCULATING UNBALANCED FORCES FOR THE NEXT STEP.
C 3) PUT JOINT DISPLACEMENTS IN DOISP FOR RESTRAINED JOINTS.
C 4) PUT THE NEGATIVE ELEMENT LOAD IN DLOA FOR RESTRAINED JOINTS, THIS
C IS USED TO CALCULATE REACTIONS.
C 5) ZERO THE UNBALANCED LOAD VECTOR
C 6) IS USED TO CALCULATE REACTIONS.
  DFL=DF
  DFN=FACTOR-FACTL
  DFN=FACT2-FACTOR
  IF (PHAX.EQ.0 .AND. DMAX.EQ.0 .AND. NUMB.GT.0) DF=DF/NUMB
  IF (DF.EQ.0) GO TO 1000
C
  DO 106 I=1,L6
    DLOAD(I)=(Q(I)-R(I))*DF
C
  ...CHANG THE SIGN OF THE FEET AT REACTIONS
  DO 110 I=1,L6
    DDISP(I)=-Q(I)*DF
C
110 DOISP(I)=Q(I)*DF
C
C=====
C= FORMULATE STIFFNESS =====
C=====
C FORMULATE THE STIFFNESS IF THE FLAG MEMB IS TRUE. THIS FLAG IS
C INITIALIZED ABOVE, AND SET WHEN THE ELEMENT FORCES ARE CALC.
C THE STIFFNESS IS ALSO FORMULATED IF KG IS TO BE FORMED
  REPEAT=.TRUE.
  KSAME=0
100 IF (MEMB.OR.MEMB) THEN
  I11=
  CALL FORMK11
  IF (KLOAD.EQ.1) MEMB=.FALSE.
  ENDIF
C
C=====
C= MODIFY LOADS FOR RESTRAINT DISPLACEMENTS =====
C=====
C IF (OSPLG) THEN
  ... ZERO INCREMENTAL REACTION LOAD VECTOR ----
  DO 113 I=1,L6
    DLOAD(I)=0
  113 CALL REACTK1,BUGS,NMODE,L1,L4,L5,L6,DRLOA,DOISP,
  & MD,STIFF,IND,NDOF,L1,L4,
  & MAXNOO,IDO,COORD,ITITLE,STEPID,.FALSE.,
  & NDCS,COSINE,JTCOS,JIFLG,SUMRC)
C
  ... ADD INCREMENTAL REACTION LOADS TO OTHER LOADS
  DO 114 I=1,L6
    DLOAD(I) = DLOAD(I) + DRLOA(I)
  114 ENDIF
C
C SAVE IN LOADS IN DOISP FOR CALCULATING FREE DISPL FOR THIS STEP.
  DO 115 I=1,L6
    DOISP(I) = DLOAD(I)
  115
C
C=====
C= SOLVE FOR FREE DISPL. =====
C=====
  IF (BUGS) THEN
    IF (MEMB .OR. MEMB)
      & CALL LMATKX(STIFF,MD,NDOF,IND,'GLOBAL STIFFNESS DUMP=?')
      & CALL MMATKX(CLOAD,NDOF,MLOAD,'LOAD MATRIX DUMP=?')
  ENDIF
C
SOL01050 IF (MEMB .OR. MEMB) THEN
SOL01060 CALL MSOLL(1,.FALSE.,L4,IND,NDOF,MLOAD,L1,L4,
SOL01070 MD,STIFF,DOISP,MORX,.FALSE.,MASS,MOMS,1,.FALSE.,KG,MOKG,1,
SOL01080 & ABORT)
SOL01090 IF (ABORT) GO TO 5000
SOL01100 ELSE
SOL01110 CALL MSOLL(2,.FALSE.,L4,IND,NDOF,MLOAD,L1,L4,
SOL01120 MD,STIFF,DOISP,MORX,.FALSE.,MASS,MOMS,1,.FALSE.,KG,MOKG,1,
SOL01130 & ABORT)
SOL01140 IF (ABORT) GO TO 5000
SOL01150 ENDF
SOL01160 CALL MSOLL(3,.FALSE.,L4,IND,NDOF,MLOAD,L1,L4,
SOL01170 MD,STIFF,DOISP,MORX,.FALSE.,MASS,MOMS,1,.FALSE.,KG,MOKG,1,
SOL01180 & ABORT)
SOL01190 IF (ABORT) GO TO 5000
SOL01200 C
SOL01210 IF (BUGS)
SOL01220 & CALL MMATKX(DOISP,NDOF,MLOAD,'DISPLACEMENT DUMP=?')
C
C=====
C= SCALE SOLN SUCH THAT PM LE PMAX, DM LE DMAX ==
C=====
  DM=0
  PM=0
  DO 150 I=1,L4
    PM=MAX(DLOAD(I),-DLOAD(I),PM)
    DM=MAX(DOISP(I),-DOISP(I),DM)
  150 IF ((DM.GT.DMAX .AND. DMAX.NE.0) .OR.
  & ((PM.GT.PMAX .AND. PMAX.NE.0) .AND.
  & (DM.NE.0))) THEN
    F1=DM
    F2=0
    IF (DMAX.NE.0) F1=DM/DMAX
    IF (PMAX.NE.0) F2=PM/PMAX
    F=MAX(F1,F2)
    DF=DF/F
    MEMBAC=.FALSE.
    DO 140 I=1,L6
      DRLOA(I)=DRLOA(I)/F
      DLOAD(I)=DLOAD(I)/F
      DOISP(I)=DOISP(I)/F
      DDISP(I)=DDISP(I)/F
    140 ELSE IF (PMAX.EQ.0 .AND. DMAX.EQ.0 .AND. NUMB.GT.1) THEN
      MEMBAC=.FALSE.
      NUMB=NUMB-1
    ELSE
      MEMBAC=.TRUE.
      DF=DF*DF/DFN
    ENDF
C
  AFAC=FACTL*DF
C
C=====
C= SOLVE FOR DISPL DUE TO UNBALANCED FORCES ==
C=====
C..... USE FIRST STIFFNESS TO CALCULATE UNBALANCED FORCES.
C IF THE STEP IS REPEATED, DO NOT USE THE NEW STIFFNESS.
C IF (UNBAL.AND.REPEAT) THEN
  DO 104 I=1,L4
    ULOAD(I) = -FUBK(I)
  104 DO 105 I=1,L6
    UDISP(I) = -FUBK(I)
  105 UDISP(I) = 0.00
  IF (BUGS)
    & CALL MMATKX(ULOAD,NDOF,MLOAD,'UNBALANCED LOAD MATRIX?')
    & CALL MSOLL(2,.FALSE.,L4,IND,NDOF,MLOAD,L1,L4,
    & MD,STIFF,UBDISP,MORX,.FALSE.,MASS,MOMS,1,.FALSE.,KG,MOKG,1,
    & ABORT)
    IF (ABORT) GO TO 5000
    CALL MSOLL(3,.FALSE.,L4,IND,NDOF,MLOAD,L1,L4,
    & MD,STIFF,UBDISP,MORX,.FALSE.,MASS,MOMS,1,.FALSE.,KG,MOKG,1,
    & ABORT)
    IF (ABORT) GO TO 5000
    & CALL MMATKX(UBDISP,NDOF,MLOAD,'UNBALANCED DISPLACEMENT?')
  ENDF
C
C..... ADD UNBALANCED FORCES AND DISPL TO STRUCTURAL LOAD AND DISPL.
C IF (UNBAL) THEN
  DO 107 I=1,L4
    DOISP(I)=DOISP(I)+UBDISP(I)
  107 CONTINUE
  DO 109 I=1,L6
    DLOAD(I)=DLOAD(I)+ULOAD(I)
  109 CONTINUE
  ENDF
C
C..... CALCULATE THE NORM OF THE UNBALANCED FORCES
  SUM=0
  DO 108 I=1,L6
    SUM=SUM+FUBK(I)**2
  108 FUBK(I)=0.00
  FNORM = SQRT(SUM/L6)
C
C=====
C= CALC PSLD-VELOCITY =====
C=====
  IF (ISTEP.EQ.1) THEN
    DO 120 I=1,L6
      VEL(I)=R(I)-R(I)
  120 DWEL(I)=Q(I)-R(I)
  PSVEL=2
  DWEL =1
  ELSE IF (FACTOR.EQ.AFAC .AND.
  & NOT((FACTL.LT.FACTOR .AND. FACTOR.LT.FACT2) .OR.
  & (FACTL.GT.FACTOR .AND. FACTOR.GT.FACT2))) THEN
    PSVEL=PSVEL
  DO 121 I=1,L6
    DWEL(I)= PSVEL * (Q(I)-R(I))
  121 DWEL =1
  ELSE IF (DWEL.NE.0) THEN
    DO 122 I=1,L6
      DWEL(I)=0
  122 DWEL =0
  ENDF
C
C=====
C= CALCULATE INCREMENTAL MEMBER FORCES ==
C=====
C ELE_L1B CALLS THE INDIVIDUAL ELEMENT LIBRARIES, EACH OF WHICH DETERMINES
C 1) DID THE STIFFNESS CHANGE? IF SO; MEMB=.TRUE.
C 2) SHOULD THE INCREMENTAL DISPLACEMENT BE RECALCULATED?
C IF SO; KSAME=KSAME+ (A VALUE DEPENDING ON ELEMENT TYPE)

```

```

C 3) THE INCREMENTAL ELEMENT FORCES
C 4) THE TOTAL ELEMENT FORCES- STORED IN FUB.
C
LSTTYP=0
PRINT=.FALSE.
HEAD=.FALSE.
NEHKS=.FALSE.
DO 150 IELNO=1,NELNT
  IOPT=4
  CALL ELEM1B
  & (IOPT,LSTTYP,PRINT,IREL,HEAD,NAME,EISE,EPSE,DAMAGE,
  & IELNO,IJDOF,KGDOF,PGEOM,RINPUT,AXIAL,IJZDOSP,IJZLOA,HSTOR)
  IOPT=IOPT
150 CONTINUE
C
C=====
C= REPEAT STEP IF NECESSARY ==
C=====
C 3 IF AN ELEMENT STIFFNESS CHANGE DICTATED THAT THE STEP BE REANALIZED,
C REFORMULATE THE STIFFNESS AND REANALIZE
C THE VARIABLE REPEAT IS SET UP TO SUPPRESS THE REANALIZING OF A STEP
CURRENTLY, EACH STEP MAY ONLY BE REANALIZED ONCE, THIS PREVENTS
C AN ENDLESS LOOP.
C
IF (KSAME,NE.D.AND. REPEAT) THEN
  REPEAT=.FALSE.
  GO TO 100
ENDIF
C
C=====
C= SOLVE FOR REACTIONS ==
C=====
IOPT=2
CALL REACTN2,BUGS,MODE,L1,L4,L5,L6,DLOAD,DISP,
  & MD,STIFF,IND,NOOF,L1,L0,
  & MAXMOD,IJDOF,COORD.ID,TITLE,STEPID,.FALSE.,
  & NCOSS,COSINE,JTCOS,JTFLG,SUMRC)
C
C=====
C= SOLVE FOR INCREMENTAL GEOMETRIC STIFFNESS FORCE, DFG ==
C=====
C----- INCREMENTAL GEOMETRIC STIFFNESS FORCE
IF (KFORM.EQ.2) THEN
  IF (BUGS) WRITE(6,*) '----- INCREMENTAL FORCE DUE TO KG '
  CALL TMRV,BUGS,.TRUE.,IND,L4,L5,L6,L4,L5,L4,
  & MKG,KG,DFG,DISP)
CC SCALE FORCE TO INCLUDE GROUND ACCELERATION ...
ENDIF
C
C=====
C= PRINT STEP SIZE ==
C=====
ISTEP=ISTEP
IPRNT=IPRNT
WRITE(=MOK,ISTEP,IPRNT).EQ.0)
IF (WRITE) THEN
  WRITE (6,245) TITLE(1),TITLE(2),STEPID,FACTOR,AFAC,DF,FACTL,
  & PHAK,DMAX,FNOBR
245 FORMAT ('1 STRUCTURE.....',A,/,
  & ' SOLUTION.....',A,/,ZK,A/,
  & ' TARGET FACTOR.....',IP,G12,*,
  & ' FACTOR.....',IP,G12,*, ' INC. FACTOR.....',G12,*,
  & ' PREV. FACTOR.....',G12,*,
  & ' PHAK.....',G12,*,
  & ' DMAX.....',G12,*,
  & ' NORM OF UNBALANCED FORCE:',G12,*)
  LINE=6
ENDIF
C
C=====
C= CALC AND ENERGIES AND DUCTILITIES ==
C=====
IF (WRITE) LINE=LINE+9
C----- PULL JOINT DISPL FORCES OUT OF LOAD MATRIX ...
IF (DSPLG) THEN
  DO 157 I=1,L4
    LOAD(I) = LOAD(I) - DRLOAD(I)
    DLOAD(I) = DLOAD(I) - DRLOAD(I)
  ENDOF
  CALL ENERGY
  & (L1,L2,L3,L4,L5,L6,NOOF,MAXMOD,NCOSS,BUG11,.FALSE.,
  & IJDOF,IND,NOOF,MD,MONS,MOK,.FALSE.,WRITE,ABORT,
  & STIFF,KG,MASS,
  & EIE,ESE,PSE,EKE,EDD,
  & ALPHA,BETA,CEFORM,NELNT,MODE,DT,SUMRC,
  & SUMRC,DSUMRC, SUNFD,DSUNFD,FOAMP,OFAMP, FZ,
  & GA,GV,GO,GAT,GVT,GDT, MORK,MORK(L6+1),ZERO,ZERO,
  & DACC,DVEL,DDISP,ACC,VEL,DISP,LOAD,DLOAD,
  & ID, IJDOF, CNST, JTFLG, COORD
  & COSINE, JTCOS )
  IF (ABORT) RETURN
C
C=====
C= GET TOTAL GLOBAL LOADS AND DISPL ==
C=====
DO 239 I=1,L4,L6
  LOAD(I)=LOAD(I)+DLOAD(I)+RLOAD(I)
  RLOAD(I) = RLOAD(I) + DRLOAD(I)
  DISP(I)=DISP(I)+DDISP(I)
  FGI(I) =FGI(I) +DFGI(I)
239 CONTINUE
DO 240 I=L5,L6
  LOAD(I)=LOAD(I)+DLOAD(I)
  DISP(I)=DISP(I)+DDISP(I)
  FGI(I) =FGI(I) +DFGI(I)
240 CONTINUE
C
C----- GET MAXIMUM LOADS AND DISPL
DO 1007 I=L1,L6
  IF (ABS(DISP(I)).GT.ABS(OSPMAX(I))) OSPMAX(I)=DISP(I)
  IF (ABS(LOAD(I)).GT.ABS(RCTMAX(I))) RCTMAX(I)=LOAD(I)
1007 CONTINUE
C
C=====
C= PRINT TOTAL GLOBAL DISPLACEMENTS ==
C=====
IF (WRITE) THEN
  IF (IPDISP=LINE.LE.60) THEN
    LINE=IPDISP+LINE
  ELSE
    LINE=IPDISP+4
    WRITE (6,250) TITLE(1),TITLE(2), ISTEP,STEPID
    ENDOF
250 FORMAT ('1 STRUCTURE.....',A,/,
  & ' SOLUTION.....',A,/,
  & ' ZK, ',LOADING',IS,SK,A)
  CALL JOIDSP1,MAXMOD,NOOF,MODE,L1,L5,L6,ID,
  & IJDOF,CNST,DISP,
  & TITLE,'DISPLACEMENTS',STEPID,.FALSE.,
  & NCOSS,COSINE,JTCOS,JTFLG)
  ENDOF
C
C=====
C= PRINT TOTAL GLOBAL REACTIONS ==
C=====
IF (WRITE) THEN
  IF (IPRCTN=LINE.LE.60) THEN
    LINE=IPRCTN+LINE+4
  ELSE
    LINE=IPRCTN+8
    WRITE (6,250) TITLE(1),TITLE(2), ISTEP,STEPID
    ENDOF
  ENDOF
  CALL REACTN5,WRITE,MODE,L1,L4,L5,L6,LOAD,DISP,
  & MD,STIFF,IND,NOOF,L1,L0,
  & MAXMOD,IJDOF,COORD.ID,TITLE,STEPID,.FALSE.,
  & NCOSS,COSINE,JTCOS,JTFLG,SUMRC)
  SUMFO=SUM(SUMRC(1)**2+SUMRC(2)**2+SUMRC(5)**2)
  SUMMO=SUM(SUMRC(4)**2+SUMRC(5)**2+SUMRC(6)**2)
  SUMFO=MAX(SUMFO,SUMMO)
  IF (WRITE) WRITE (6,315) SUMFO,SUMMO
  S15 FORMAT ('/X, RESULTANT OF REACTIONS, FORCE=',IP,G12,*,
  & ' MOMENT=',G12,*)
C
DO 1008 I=L1,L6
  IF (ABS(SUMRC(I)).GT.ABS(SUMRC(I))) SUMRC(I)=SUMRC(I)
1008 CONTINUE
C
C=====
C= CALCULATE AND PRINT TOTAL MEMBER FORCES ==
C=====
IOPT=5
LSTTYP=0
HEAD=.FALSE.
IF (WRITE) THEN
  PRINT=.TRUE.
  IF (IPELEM=LINE.LE.60) THEN
    LINE=IPELEM+LINE
  ELSE
    LINE=IPELEM+4
    WRITE (6,250) TITLE(1),TITLE(2), ISTEP,STEPID
  ELSE
    PRINT=.FALSE.
  ENDOF
  DO 500 IELNO=1,NELNT
    IOPT=5
    CALL ELEM1B
    & (IOPT,LSTTYP,PRINT,IREL,HEAD,NAME,EISE,EPSE,DAMAGE,
    & IELNO,IJDOF,KGDOF,PGEOM,RINPUT,AXIAL,IJZDOSP,IJZLOA,HSTOR)
  C
  C=====
  C= PRINT MEMBER DUCTILITY AND EXCURSION RATIOS ==
  C=====
  IOPT=11
  LSTTYP=0
  HEAD=.FALSE.
  IF (WRITE) THEN
    PRINT=.TRUE.
    IF (IPELEM=LINE.LE.60) THEN
      LINE=IPELEM+LINE
    ELSE
      LINE=IPELEM+4
      WRITE (6,250) TITLE(1),TITLE(2), ISTEP,STEPID
    ELSE
      PRINT=.FALSE.
    ENDOF
    DO 510 IELNO=1,NELNT
      IOPT=5
      CALL ELEM1B
      & (IOPT,LSTTYP,PRINT,IREL,HEAD,NAME,EISE,EPSE,DAMAGE,
      & IELNO,IJDOF,KGDOF,PGEOM,RINPUT,AXIAL,IJZDOSP,IJZLOA,HSTOR)
  C
  C=====
  C= WRITE DATA TO OUTPUT FILES ==
  C=====
  IF (WRITE.GT.0) THEN
    IF (MOK,ISTEP,IPRNT).EQ.0) THEN
      IOPT=2
      CALL DMPDAT(IOPT,WRITE,TO,DT)
    ENDOF
  C
  C=====
  C= EITHER GET A NEW FACTOR, OR KEEP WORKING ON THE CURRENT ONE ==
  C=====
  FACTL=FACTL*HF
  GO TO 1100
C
C=====
C= CLOSE OUTPUT FILES ==
C=====
5000 IF (WRITE.GT.0) THEN
  IOPT=5
  CALL DMPDAT(IOPT,WRITE,TO,DT)
  ENDOF
C
C=====
C= PRINT MAXIMUM DISPLACEMENTS ==
C=====
LINE=IPDISP+4
WRITE (6,250) TITLE(1),TITLE(2),O,'MAXIMUM DISPLACEMENTS'
CALL JOIDSP2,MAXMOD,NOOF,MODE,L1,L5,L6,ID,
  & IJDOF,CNST,OSPMAX,
  & TITLE,'DISPLACEMENTS','MAXIMUM VALUES',.FALSE.,
  & NCOSS,COSINE,JTCOS,JTFLG)
C
C=====

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ENDIF
C.....RESERVE STORAGE
NZ(IZMAT+MAT)=IZ
IZNK=IZ+200
C.....CALL MATERIAL LIBRARY TO INITIALIZE MATERIAL DATA
CALL MATLIB
& (IOPT ,LSTTYP ,PT ,IREL,HEAD,NAME,EESSE,EPSE,DUCT,EXCR,
& P ,PL ,D ,DL ,V ,VL ,LELEN ,LMAI ,
& MAT ,MATTYP,SE,-1,DAMAGE)
C.....RESERVE STORAGE
IZ=IZ+MAT+1
C
IF /MAT .LT.MMAT GO TO 110
120 CONTINUE
C=====
C2 INPUT GEOMETRIC STIFFNESS DATA ==
C=====
C Z(IZKGD+0) = VERTICAL GROUND ACCELERATION
C NZ(IZKGD+1) = 0, GEOMETRIC STIFFNESS IS NOT CONSIDERED
& = 1, LOAD= F(INPUT)*(1.0+ACCEL)
& = 2, PREVIOUS LOAD STEP'S AXIAL LOAD IS USED
C NZ(IZKGD+2) = TYPE OF ELEMENT GEOMETRIC STIFFNESS TO BE USED
& = 0, GEOMETRIC STIFFNESS IS NOT CONSIDERED
& = 1, LUMPED FORMULATION
& = 2, CONSISTENT FORMULATION
C NZ(IZKGD+3) = FORM OF SOLUTION
& = 0, GEOMETRIC STIFFNESS IS NOT CONSIDERED
& = 1, KG IS SUBTRACTED FROM ELEMENT STIFFNESS
& = 2, SEPARATE GLOBAL KG IS FORMED
C KGCCOND = LOGICAL FLAG, TRUE IF KG IS TO BE CONDENSED

IZKGD=IZ
IZ =IZ+4
READ (5,*) (NZ(IZKGD+I),I=1,5),KGCCOND
I=IZKGD
IF (NZ(I+1).EQ.0 .OR. NZ(I+2).EQ.0 .OR. NZ(I+3).EQ.0) THEN
NZ(I+1)=0
NZ(I+2)=0
NZ(I+3)=0
ELSE
WRITE (6,150) TITLE(1),TITLE(2)
IF (NZ(I+1).EQ.1) WRITE (6,160)
& 'KLOAD = 1, LOAD= F(INPUT)*(1.00+ACCEL)',
& ' F(INPUT) IS POSITIVE IN COMPRESSION',
& ' ACCEL IS POSITIVE GLOBAL Z-AXIS ACCELERATION'
& IF (NZ(I+1).EQ.2) WRITE (6,160)
& 'KLOAD = 2, PREVIOUS LOAD STEP'S AXIAL LOAD IS USED'
& IF (NZ(I+2).EQ.1) WRITE (6,160)
& 'KGTYP = 1, LUMPED FORMULATION'
& IF (NZ(I+2).EQ.2) WRITE (6,160)
& 'KGTYP = 2, CONSISTENT FORMULATION'
& IF (NZ(I+3).EQ.1) WRITE (6,160)
& 'KGFORN = 1, KG IS SUBTRACTED FROM ELEMENT STIFFNESS'
& IF (NZ(I+3).EQ.2) WRITE (6,160)
& 'KGFORN = 2, SEPARATE GLOBAL KG IS FORMED'
WRITE (6,160)
IF (KGCCOND) WRITE (6,160)
& '- THE GEOMETRIC STIFFNESS MATRIX IS CONDENSED'
& 'WITH THE STRUCTURAL STIFFNESS MATRIX.'
IF (.NOT.KGCCOND) WRITE (6,160)
& '- THE GEOMETRIC STIFFNESS MATRIX IS NOT CONDENSED'
& 'WITH THE STRUCTURAL STIFFNESS MATRIX.'
ENDIF
150 FORMAT ('1 STRUCTURE.....',A,
& ' SOLUTION.....',A,
& ' SK, GEOMETRIC STIFFNESS DATA ',
& 'SK,=====')
160 FORMAT('SK,A)
C=====
C2 SET UP STORAGE FOR GEOMETRIC STIFFNESS DATA ==
C=====
GLOBAL STIFFNESS STORAGE
C NZ(IZKMG) = INDICES OF THE MAIN DIAGONAL TERMS
C Z(IZKMG) = GLOBAL GEOMETRIC STIFFNESS MATRIX
IF (NZ(IZKGD+3).EQ.2) THEN
IZKMG=IZ
IZ =IZ+NDOF+1
CALL SKV.LNK(1,NDOF,IBUG,TITLE,NZ(IZKMG),
& KDOOF,NZ(IZKMG),Z(IZKMG),ND,'GLOBAL GEOMETRIC STIFFNESS')
ELSE
DUMMY LOCATION FOR KG TO AVOID ADDRESSING EXCEPTIONS
KG DATA IS NOT STORED IN THESE LOCATIONS...
IZKMG=IZKGD
IZKMG=IZKGD
IZKMG=IZKGD
ENDIF
C=====
C INPUT ELEMENT DATA ==
C=====
READ (5,*) NEMT
----- ELEMENT STORAGE -----
NZ(IZELE) = # OF MATERIAL PROPERTIES (NEMT)
NZ(IZELE+1) = ABSOLUTE ADDRESS OF ELEMENT #1
NZ(IZELE+2) = ABSOLUTE ADDRESS OF ELEMENT #2
NZ(IZELE+3) = ABSOLUTE ADDRESS OF ELEMENT #3
.
.
.
NZ(IZMAT+NEMT) = ABSOLUTE ADDRESS FOR ELEM # NEMT
Z(NZ(IZELE+1)) = MATERIAL DATA FOR ELEMENT #1
.
.
.
Z(NZ(IZELE+2)) = MATERIAL DATA FOR ELEMENT #1
.
.
.
IOPT=1
IZELE=IZ
IZ =IZ+NEMT+1
NZ(IZELE)=NEMT

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STRO1520 FIRST=.TRUE.
STRO1530 HEAD=.TRUE.
STRO1540 IGEN=0
STRO1550 IELNO=0
STRO1560 LSTTYP=0
C----- LOOP FOR EACH ELEMENT -----
210 IELNO=IELNO+1
IF (IGEN.LE.0) THEN
READ (5,*) TYPE
C
IF (TEST(TYPE,'3D-BEAM',.FALSE.)) THEN
NINPUT= 10
NINZ = 505
NELTYP= 1
C
ELSE IF (TEST(TYPE,'SPRING',.FALSE.)) THEN
NINPUT= 10
NINZ = 153
NELTYP= 2
C
ELSE IF (TEST(TYPE,'SHEAR WALL',.FALSE.)) THEN
NINPUT= 9
NINZ = 769
NELTYP= 3
C..... TO ADD ADDITIONAL ELEMENTS, COPY THE NEXT FOUR LINES
ELSE IF (TEST(TYPE,'1',.FALSE.)) THEN
NINPUT= (2)
NINZ = (3)
NELTYP= (4)
C... CHANGE THE FOLLOWING VALUES
C... (1) YOUR ELEMENT NAME
C... (2) # OF VALUES TO BE INPUT
C... (3) # OF STORAGE LOCATIONS REQD FOR ELEMENT
C... (4) ELEMENT ID NUMBER = XX
C... ADD CALL ELEM TO SUBPROGRAM ELEM_LIB
C... ADD SUBPROGRAM ELEM
C.....
ELSE IF (TEST(TYPE,'END',.FALSE.)) THEN
NEMT=IELNO-1
NZ(IZELE)=NEMT
GO TO 500
ELSE
WRITE (6,*) 'INVALID ELEMENT TYPE: ',HEAD
GO TO 210
ENDIF
BACKSPACE (5)
READ (5,*) TYPE,NAME, (RINPUT(I),I=1,NINPUT),IGEN
IF (IGEN.GT.0) READ (5,*) (GINPUT(I),I=1,NINPUT)
ELSE
IGEN=IGEN-1
NAME='GENERATED'
DO 220 I=1,NINPUT
220 RINPUT(I)=RINPUT(I)+GINPUT(I)
ENDIF
111 FORMAT ('OP: ZNATRK',I6,' ',I15,JP,G20,10)
C.....RESERVE STORAGE
NZ(IZELE+IELNO)=IZ
IC=IZ
IZNK=IZ
C.....STORE ELEMENT TYPE
NZ(IC) =NELTYP
C.....CALL ELEMENT LIBRARY TO DETERMINE THE STORAGE FOR MATL DATA
IOPT=9
HEAD=.FALSE.
LSTTYP=0
CALL ELEM LIB
& (IOPT ,LSTTYP ,TRUE,IREL,HEAD,NAME ,EESSE,EPSE,DAMAGE,
& IELNO ,IELDOF,KDOOF,PGEON,RINPUT,AXIAL ,IZDISP,IZLOAD,MSTOR)
C.....RESERVE STORAGE
IZ=IZ+MINZ+MSTOR
IZNK=IZ
C.....CALL ELEMENT LIBRARY TO INITIALIZE ELEMENT DATA AND RETURN
C.....INFO ON ELEMENT DOF...
IOPT=1
CALL ELEM LIB
& (IOPT ,LSTTYP ,TRUE,IREL,HEAD,NAME ,EESSE,EPSE,DAMAGE,
& IELNO ,IELDOF,KDOOF,PGEON,RINPUT,AXIAL ,IZDISP,IZLOAD,MSTOR)
C.....RELEASE UNUSED STORAGE .....
IZ=IZ-IREL
C.....DO UP ELEMENT DATA IF DEBUGGING
IF (TEST(DBG,8)) THEN
WRITE (6,*) 'IZLN=',IZLN,' IZKE=',IZKE
J=1
DO 7000 I=IC,(IZNK-1)-IREL
J=J+1
7000 IF (NZ(I).NE.0) WRITE (6,7010) IELNO,J,I,NZ(I),Z(I)
7010 FORMAT (' IELNO:',I3, ' ',I6, ' Z:',I6, ' ',I10,JP,Q18,8)
ENDIF
C.....RESERVE SPACE IN THE SKVLINE FOR THE STIFFNESS
CALL SKV.LNK(2,NDOF,IBUG,TITLE,NZ(IZMD),
& IELDOF,NZ(IZLN),Z(IZKE),ND,'GLOBAL STIFFNESS')
C.....RESERVE SPACE IN THE SKVLINE FOR THE GEOMETRIC STIFFNESS
IF (NZ(IZKGD+3).EQ.1 .AND. AXIAL) THEN
CALL SKV.LNK(2,NDOF,IBUG,TITLE,NZ(IZMD),
& KDOOF,NZ(IZLNG),Z(IZKEG),ND,'GLOBAL GEOMETRIC STIFFNESS')
ELSE IF (NZ(IZKGD+3).EQ.2 .AND. AXIAL) THEN
CALL SKV.LNK(2,NDOF,IBUG,TITLE,NZ(IZMD),
& KDOOF,NZ(IZLNG),Z(IZKEG),ND,'GLOBAL GEOMETRIC STIFFNESS')
ENDIF
C
IF (IELNO.LT.NEMT) GO TO 210
500 CONTINUE
C=====
C2 MODIFY GEOMETRIC STIFFNESS MATRIX FOR CONDENSATION ==
C=====
C THE CONDENSATION PROCESS MAY EXPAND THE GEOMETRIC STIFFNESS MATRIX'S
C SKVLINE. THE MAXIMUM SKVLINE OF BOTH THE GEOMETRIC STIFFNESS AND
C THE STIFFNESS MATRIX IS USED.
IF (NZ(IZKGD+3).EQ.2 .AND. KGCCOND .AND. NCOND.GT.0) THEN
DO 510 I=0,NDOF
I=I+1
NMG(I)=NZ(IZKMG+I)
NZ(IZKMG+I)=MIN(NZ(IZKMG+I),NZ(IZMD+I))

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STRO2570  
STRO2580  
STRO2590  
STRO2600  
STRO2610  
STRO2620  
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STRO2670  
STRO2680  
STRO2690  
STRO2700  
STRO2710  
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STRO2770  
STRO2780  
STRO2790  
STRO2800  
STRO2810  
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STRO2990  
STRO3000  
STRO3010  
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STRO3090  
STRO3100  
STRO3110  
STRO3120  
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STRO3160  
STRO3170  
STRO3180  
STRO3190  
STRO3200  
STRO3210  
STRO3220  
STRO3230  
STRO3240  
STRO3250  
STRO3260  
STRO3270  
STRO3280  
STRO3290  
STRO3300  
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STRO3660  
STRO3670  
STRO3680  
STRO3690  
STRO3700  
STRO3710  
STRO3720  
STRO3730  
STRO3740  
STRO3750  
STRO3760  
STRO3770  
STRO3780  
STRO3790  
STRO3800  
STRO3810  
STRO3820  
STRO3830  
STRO3840  
STRO3850

```

310 CONTINUE
ENDIF
C
C
C=====
Ca SET UP GLOBAL STIFFNESS STORAGE ==
C
C      NZ(IZND) = INDICES OF THE MAIN DIAGONAL TERMS
C      Z(IZSTIF) = GLOBAL STIFFNESS MATRIX
C
CALL SKV(LINKS,NDOF,ISUG,TITLE,NZ(IZND))
& IELDOF,NZ(IZLM),Z(IZKE),MO,'GLOBAL STIFFNESS'
C
IZSTIF=IZ
IZ = IZ+(IZND+DOF) * I
C
C=====
Ca SET UP STORAGE FOR GEOMETRIC STIFFNESS DATA ==
C
C      NZ(IZDKG) = INDICES OF THE MAIN DIAGONAL TERMS
C      Z(IZDKG) = GLOBAL GEOMETRIC STIFFNESS MATRIX
C
IF (NZ(IZDKG).EQ.2) THEN
CALL SKV(LINKS,NDOF,ISUG,TITLE,NZ(IZDKG))
& KDOF,NZ(IZLM),Z(IZKE),MO,'GLOBAL GEOMETRIC STIFFNESS'
C
IZKG = IZ
IZ = IZ + NZ(IZDKG+DOF)
ENDIF
C
C=====
Ca INPUT MASS MATRIX ==
C
C      NMASS = NUMBER OF NODAL MASSES TO BE INPUT
C      FMASS = 0, NO MASS MATRIX
C      1, MASS MATRIX DUE TO NODAL MASSES ONLY
C      MCOND = LOGICAL FLAG, TRUE IF MASS IS TO BE CONDENSED...
C
READ (5,*) NMASS,FMASS,MCOND
C
CALL MASSK(NMASS,FMASS,MCOND,ISUG,TITLE,NMAZ,MANDZ,
& MAND,NDOS,NDODE,IZ,IZD,Z,NZ,DZ,
& IZNDMS,IZMSS,IZLM,IZKE,IZHAT,
& NDOF,NMASS,IZDOS,IZDOF,IZNSZ,IZJLG,IZJCS,'GLOBAL MASS')
C
& MCOND,IFRE,IZND)
IF (MCOND.GT.0) THEN
WRITE (6,160) ' '
IF (MCOND) THEN
WRITE (6,160) ' - THE MASS MATRIX IS ' '
CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.'
&
ELSE
WRITE (6,160) ' - THE MASS MATRIX IS NOT ' '
CONDENSED WITH THE STRUCTURAL STIFFNESS MATRIX.'
&
ENDIF
ELSE
WRITE (6,499)
499 FORMAT('//5X,' ZERO MASS MATRIX '//
& 5X,'=====')
ENDIF
C
C=====
Ca INPUT DAMPING DATA ==
C
C      NDAMP = NUMBER OF NODAL DAMPING COEF TO BE INPUT = 0
C      FDAMP = 0, NO DAMPING MATRIX
C      1, ALPHA AND BETA INPUT
C
NDAMP=0
FDAMP=1
READ (5,*) NDAMP,FDAMP
IF (FDAMP.EQ.1) THEN
IZDAMP=IZ
IZZ=IZ + 2
READ (5,*) ALPHA,BETA
Z(IZDAMP) = ALPHA
Z(IZDAMP+1) = BETA
WRITE(6,500) ALPHA,BETA
ENDIF
500 FORMAT('//5X,' PROPORTIONAL DAMPING COEFFICIENTS '//
& 5X,'=====')
& 5X,'ALPHA',IP,G15.5,' BETA',G15.5)
C
C=====
Ca ZERO LOAD AND DISPL INDICES ==
C
IZLOAD=0
IZDISP=0
IZVEL=0
IZACC=0
IZDLOAD=0
IZDDISP=0
IZDVEL=0
IZDACC=0
C
RETURN
END
C=====
LOGICAL FUNCTION TEST(OPTION,TARGET,DEFLT)
CHARACTER*(*) OPTION,TARGET
LOGICAL DEFLT,BTEST
JS INDEXT(OPTION,TARGET)
IF (DEFLT) THEN
IF (J.LT.2) THEN
TEST=.TRUE.
ELSE IF (OPTION(J-2):(J-1)).NE.'NO') THEN
TEST=.TRUE.
ELSE
TEST=.FALSE.
ENDIF
ELSE
IF (J.EQ.0) THEN
TEST=.FALSE.
ELSE IF (J.LT.2) THEN
TEST=.TRUE.
ELSE IF (OPTION(J-2):(J-1)).EQ.'NO') THEN
TEST=.FALSE.
ELSE
TEST=.TRUE.
ENDIF
ENDIF
RETURN
END
C=====
C TRIANGULAR MATRIX MULTIPLICATION ...
C MATRIX A IS AN UPPER TRIANGULAR MATRIX, WITH MAIN DIAGONAL ADDRESS
C MATRIX MD, X IS A VECTOR. P=AX

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STRO5870 C THE MULTIPLICATION IS CARRIED OUT FROM ROW I1 TO I2 AND FROM
STRO5880 C COLUMN J1 TO J2.
STRO5890 C=====
STRO5900 SUBROUTINE TMPLVCP(PRINT,ZERO,IND,N,IR1,IR2,J1,J2,MD,A,P,X)
STRO5910 DIMENSION A(IND),X(N),P(N),MD(N+1)
STRO5920 LOGICAL BTEST,PRINT,ZERO
C
I1(I1,J)=MD(J)+J-I
IF (PRINT) THEN
WRITE (6,500) 'TRIANGULAR MULTIPLICATION',
& IR1,IR2,J1,J2,N
& CALL LMATRX(A,MD,N,MD(N+1),'MATRIX A ')
ENDIF
C
--- ZERO P ---
IF (ZERO) THEN
DO 520 J=IR1,IR2
520 P(J)=0
ENDIF
C
--- MULTIPLY TERMS ABOVE AND INCLUDING THE MAIN DIAGONAL
DO 20 J=J1,J2
IRC=J-MD(J)+1+MD(J)+1
MD=MD(J)+J
I1=MAX(IRC,IR1)
I2=MIN(J,IR2)
IF (I2.GE.I1) THEN
DO 10 I=I1,I2
10 P(I)=P(I)+A(MD(I)-J)*X(J)
20 CONTINUE
C
--- MULTIPLY TERMS BELOW THE MAIN DIAGONAL
DO 50 I=IR1,IR2
IRC=I-MD(I)+1+MD(I)+1
MD=MD(I)+I
I1=MAX(IRC,J1)
I2=MIN(I-1,I2)
IF (I2.GE.I1) THEN
DO 40 J=I1,I2
40 P(I)=P(I)+A(MD(I)-J)*X(J)
50 CONTINUE
ENDIF
500 FORMAT ('//2X,A/,2X,' IR1:',IS,' IR2:',IS,
& ' J1:',IS,' J2:',IS,' N:',IS)
IF (PRINT) THEN
DO 515 I=IR1,IR2
515 WRITE(6,520) I,X(I),P(I)
WRITE (6,*) ' '
520 FORMAT (2X,'DOF:',I6,' XDOF',IP,G15.5,' A*X=PCDOF:',G15.5)
ENDIF
RETURN
END
C=====
C UPPER TRIANGULAR MATRIX MULTIPLICATION ...
C MATRIX A IS AN UPPER TRIANGULAR MATRIX, WITH MAIN DIAGONAL ADDRESS
C MATRIX MD, X IS A VECTOR. P=AX
C THE MULTIPLICATION IS CARRIED OUT FROM ROW I1 TO I2 AND FROM
C COLUMN J1 TO N.
C=====
SUBROUTINE UTMPLVCP(PRINT,ZERO,IND,N,IR1,IR2,J1,J2,MD,A,P,X)
DIMENSION A(IND),X(N),P(N),MD(N+1)
LOGICAL BTEST,PRINT,ZERO
C
I1(I1,J)=MD(J)+J-I
IF (PRINT) THEN
WRITE (6,500) 'UPPER TRIANGULAR MULTIPLICATION',
& IR1,IR2,J1,J2,N
& CALL LMATRX(A,MD,N,MD(N+1),'MATRIX A ')
ENDIF
C
--- ZERO P ---
IF (ZERO) THEN
DO 520 J=J1,I2
520 P(J)=0
ENDIF
C
--- MULTIPLY TERMS ABOVE AND INCLUDING THE MAIN DIAGONAL
DO 20 J=J1,J2
IRC=J-MD(J)+1+MD(J)+1
MD=MD(J)+J
I1=MAX(IRC,IR1)
I2=MIN(J,IR2)
IF (I2.GE.I1) THEN
DO 10 I=I1,I2
10 P(I)=P(I)+A(MD(I)-J)*X(J)
20 CONTINUE
C
--- MULTIPLY TERMS BELOW THE MAIN DIAGONAL
DO 50 I=IR1,IR2
IRC=I-MD(I)+1+MD(I)+1
MD=MD(I)+I
I1=MAX(IRC,J1)
I2=MIN(I-1,I2)
IF (I2.GE.I1) THEN
DO 40 J=I1,I2
40 P(I)=P(I)+A(MD(I)-J)*X(J)
50 CONTINUE
ENDIF
500 FORMAT ('//2X,A/,2X,' IR1:',IS,' IR2:',IS,
& ' J1:',IS,' J2:',IS,' N:',IS)
IF (PRINT) THEN
DO 515 I=IR1,IR2
515 WRITE(6,520) I,X(I),P(I)
WRITE (6,*) ' '
520 FORMAT (2X,'DOF:',I6,' XDOF',IP,G15.5,' A*X=PCDOF:',G15.5)
ENDIF
RETURN
END
C=====
REAL FUNCTION VCOS(V1,V2)
DIMENSION V(5),V2(5)
VALUE (A1,A2,A5)=SQRT(A1**2+A2**2+A5**2)
DOT (A1,A1,G1,A2,G2)=A1*A2+G1*G2
C
AV1=VALUE(V(1),V(2),V(5))
AV2=VALUE(V2(1),V2(2),V2(5))
VDT=DOT(V(1),V(2),V(5),V2(1),V2(2),V2(5))
VCOS=VDT/(AV1*AV2)
RETURN
END
C=====
C VS = V1 X V2, VECTOR CROSS PRODUCT ...
C=====
SUBROUTINE VCROSS(V3,R1,R2)
DIMENSION V(5),V2(5),V3(5)
DIMENSION R1(5),R2(5)
DO 10 I=1,5
V3(I)=R1(I)
V3(I)=R2(I)

```



```

10 VZ(I)=RZ(I)
C
VX(I) = V1(I)*VX(S) - V1(S)*VX(2)
VY(I) = V1(I)*VY(S) - V1(S)*VY(2)
VZ(I) = V1(I)*VZ(S) - V1(S)*VZ(2)
C
RETURN
END
C-----
SUBROUTINE MATRKA(A,IR,IC,NAME)
DIMENSION A(IR,IC)
CHARACTER*(*) NAME
LOGICAL DMP,BTEST
C
CALL GETINT(NAME,'DUMP',IDUMP,0.,TRUE.,FALSE.)
IF (IDUMP.NE.0) THEN
DMP=.TRUE.
ELSE
DMP=.FALSE.
ENDIF
C
WRITE (6,*) ' '
WRITE (6,*) 'PRINTING MATRIX: ',NAME
DO 50 ICG=1,IC,6
IF (ICG.GT.1) WRITE (6,*) ' '
K=MIN(ICG+5,IC)
WRITE (6,10) (J,=ICG,K)
DO 20 I=1,IR
IF (DMP) THEN
DO 15 J=ICG,K
IF (A(I,J).NE.0) WRITE (IDUMP,*) I,J,A(I,J),NAME
15 ENDF
WRITE (6,50) I,(A(I,J),J=ICG,K)
20 CONTINUE
RETURN
10 FORMAT(' COLUMN',I7,IS,5(15M,IS))
50 FORMAT(' ROW',I4,6F20.6)
END
C-----
SUBROUTINE MTRKKA(A,IR,IC,NAME,IR0M)
DIMENSION A(IR0M,IC)
CHARACTER*(*) NAME
LOGICAL DMP,BTEST
C
CALL GETINT(NAME,'DUMP',IDUMP,0.,TRUE.,FALSE.)
IF (IDUMP.NE.0) THEN
DMP=.TRUE.
ELSE
DMP=.FALSE.
ENDIF
C
WRITE (6,*) ' '
WRITE (6,*) 'PRINTING MATRIX: ',NAME
DO 50 ICG=1,IC,6
IF (ICG.GT.1) WRITE (6,*) ' '
K=MIN(ICG+5,IC)
WRITE (6,10) (J,=ICG,K)
DO 20 I=1,IR
IF (DMP) THEN
DO 15 J=ICG,K
IF (A(I,J).NE.0) WRITE (IDUMP,*) I,J,A(I,J),NAME
15 ENDF
WRITE (6,50) I,(A(I,J),J=ICG,K)
20 CONTINUE
RETURN
10 FORMAT(' COLUMN',I7,IS,5(15M,IS))
50 FORMAT(' ROW',I4,6F20.6)
END

```

```

VCR00100 DX=VALUE(VX(I),VX(2),VX(S))
VCR00110 DY=VALUE(VY(I),VY(2),VY(S))
VCR00120 DZ=VALUE(VZ(I),VZ(2),VZ(S))
VCR00130 DO 50 I=1,5
VCR00140 VX(I)=VX(I)/DX
VCR00150 VY(I)=VY(I)/DY
VCR00160 VZ(I)=VZ(I)/DZ
VCR00170
C-----
PRINT DIRECTION COSINES
WRITE (6,*) ' VIEW NUMBER.....',IVIEW
WRITE (6,*) ' TITLE.....',TITLE
WRITE (6,*) ' X-LENGTH.....',VLEN
WRITE (6,*) ' Y-LENGTH.....',VLEN
WRITE (6,*) ' VX.....',VX
WRITE (6,*) ' VY.....',VY
WRITE (6,*) ' VZ.....',VZ
C-----
CALCULATE & PRINT ROTATED COORDINATES
DO 100 I=1,NUMB
DO 40 I=1,5
SR(I,J)=0
ER(I,J)=0
DO 50 I=1,5
SR(I,J)=SR(I,J) + VK(I)*SC(I,J)
SR(2,J)=SR(2,J) + VK(I)*SC(I,J)
SR(5,J)=SR(5,J) + VZ(I)*SC(I,J)
ER(1,J)=ER(1,J) + VK(I)*EC(I,J)
ER(2,J)=ER(2,J) + VK(I)*EC(I,J)
ER(5,J)=ER(5,J) + VZ(I)*EC(I,J)
50 ER(5,J)=ER(5,J) + VZ(I)*EC(I,J)
IF (J.EQ.1) THEN
DO 60 I=1,5
RMAX(I)=MAX(SR(I,J),ER(I,J))
RMIN(I)=MIN(SR(I,J),ER(I,J))
60 ELSE
DO 70 I=1,5
RMAX(I)=MAX(SR(I,J),ER(I,J),RMAX(I))
RMIN(I)=MIN(SR(I,J),ER(I,J),RMIN(I))
70 ENDF
100 WRITE (6,20) KEV(I),(SR(I,J),I=1,5),(ER(I,J),I=1,5),
& 'ROTATED POINT'
C-----
PLOT POINTS, USING CALCOMP LOSL PLOTTER COMMANDS...
C-----
LOOP FOR DIFFERENT VIEWS
DO 500 I=1,5
IF (I.EQ.1) THEN
DX=1
IY=2
ELSE IF (I.EQ.2) THEN
DX=2
IY=5
ELSE
DX=5
IY=1
ENDF
C-----
DRAW TRIM LINE
CALL PLOT(0.,11.,2)
CALL PLOT(0.,0.,2)
C-----
MOVE ORIGIN TO 0.5,0.5
CALL PLOT(.75, .5, -5)
C-----
GET SCALE FACTORS FOR X-Y PLOT
X(1)=RMIN(DX)
X(2)=RMAX(DX)
Y(1)=RMIN(IY)
Y(2)=RMAX(IY)
CALL SCALE(X,VLEN,2,1)
CALL SCALE(Y,VLEN,2,1)
X5=X(5)
X4=X(4)
Y5=Y(5)
Y4=Y(4)
C-----
PLOT AXIS
IF (PAKIS) THEN
CALL AKIS(0.00,-.05,LABEL(DX),-20,VLEN,0.,X(5),X(4))
CALL AKIS(-.05,0.00,LABEL(IY),20,VLEN,90.,Y(5),Y(4))
ENDF
C-----
PLOT MEMBERS
DO 200 J=1,NUMB
K(1)=SR(DX,J)
K(2)=ER(DX,J)
V(1)=SR(IY,J)
V(2)=ER(IY,J)
200 CALL LINE(X,Y,2,1,0,0)
C-----
PLOT TITLE
CALL SYMBOL(0,1,(VLEN+15),.16,TITLE,0.,80)
TEMP=LABEL(DX)/'---'/LABEL(IY)
CALL SYMBOL(0,1,(VLEN+61),.05,TEMP,0.,42)
C-----
MOVE ORIGIN BACK TO 0,0 AND ADVANCE PAGE
CALL PLOT(VLEN+.25,-.5,-5)
C-----
500 CONTINUE
1000 CONTINUE
2000 CONTINUE
C-----
DRAW TRIM LINE
CALL PLOT(0.,11.,2)
CALL PLOT(0.,0.,2)
C-----
CLOSE THE PLOTTING DEVICE
CALL PLOT(0.,0.,999)
C
STOP
END

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SEE00460
SEE00470
SEE00480
SEE00490
SEE00500
SEE00510
SEE00520
SEE00530
SEE00540
SEE00550
SEE00560
SEE00570
SEE00580
SEE00590
SEE00600
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SEE01570
SEE01580
SEE01590

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**C. PROGRAM SEE**  
**FILE: SEE FORTRAN**

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C-----
DEBUG UNIT(6),TRACE,SUBCHK,ZNIT,SUBTRACE
END DEBUG
PARAMETER (MMAX=1500)
LOGICAL PAKIS
CHARACTER*20 LABEL(5)
CHARACTER*80 TITLE
CHARACTER*42 TEMP
DIMENSION VX(5),VY(5),VZ(5),X(4),Y(4)
DIMENSION SC(5,MMAX),SRC(5,MMAX),KEV(MMAX),RMAX(5),RMIN(5)
DIMENSION EC(5,MMAX),ERC(5,MMAX)
CROSSX(A1,B1,C1,A2,B2,C2)=A1*B2-C1*B2+C1*A2-C2*A1
CROSSY(A1,B1,C1,A2,B2,C2)=A1*B2-A2*B1
VALUE(A1,A2,A5)=SORT(A1**2+A2**2+A5**2)
DOT(A1,B1,C1,A2,B2,C2)=A1*A2+B1*B2+C1*C2
LABEL(1)='ROTATED X AXIS'
LABEL(2)='ROTATED Y AXIS'
LABEL(3)='ROTATED Z AXIS'
C-----
INITIALIZE THE PLOTTING DEVICE
CALL PLOT(0,0,7)
C-----
INPUT & PRINT POINTS
DO 10 I=1,MMAX
READ (10,*)END=15 KEV(I),(SC(J,I),J=1,5),(EC(J,I),J=1,5)
10 WRITE (6,20) KEV(I),(SC(J,I),J=1,5),(EC(J,I),J=1,5),'INPUT POINT'
15 NUMB=I
IF (I.LE.MMAX) NUMB=I-1
20 FORMAT (I4,IS,1P,6G12.4,*,A3)
C-----
LOOP FOR EACH VIEW
READ(5,*) NVIEW
DO 2000 IVIEW=1,NVIEW
C-----
INPUT VIEWING DATA
READ (5,*) TITLE,VLEN,VLEN,PAKIS,VN,VV
C-----
CALCULATE DIRECTION COSINES
VZ(1)=VX(2)*VY(5)-VX(5)*VY(2)
VZ(2)=VX(1)*VY(5)+VX(5)*VY(1)
VZ(3)=VX(1)*VY(2)-VX(2)*VY(1)
VY(1)=VZ(2)*VX(5)-VZ(5)*VX(2)
VY(2)=VZ(1)*VX(5)+VZ(5)*VX(1)
VX(5)=VZ(1)*VX(2)-VZ(2)*VX(1)

```

